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OTTAWA

December 2, 1946.

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REPORT

of the

ORE DRESSING AND METALLURGICAL LABORATORIES.

Investigation No. 2146.

(Subsequent to Investigation Reports)
(Nos. 1991, 2002, 2014, 2015, 2105)
(and 2035, January-October, 1946.)

Research on Optimum Thread Form for Proposed Anglo-American-Canadian Screw Thread.

PART VII. - Investigation of Heat Treatment to be Used for Threaded Studs.

(This research is performed in collaboration with the National Bureau of Standards, Washington, U. S. A., the National Physical Laboratory, Teddington, England, and the National Research Council, Ottawa, Canada.

Abstract

In order to determine the minimum hardness variation attainable in the quenching treatment for steel to be used in the screw-thread research program, a hardness analysis has been carried out on a number of quenched bars of Atlas steel S.P.S. 245. This steel is comparable, as regards hardenability, to steel S.A.E. 6150, the type which is to be used in the screw-thread research.

Two quenching methods have been compared: in the first, bars of 1-inch diam. x 26 inches length were quenched in a vertical position without a shield; in the second, bars of identical size were quenched with a thin cylindrical shield in order to obtain uniform cooling effect in transferring specimens from the furnace to quenching tank.

CANADA

Bureau of Mines

Mineral Dressing and Metallurgy Division

Research Laboratories

DEPARTMENT MINES AND RESOURCES

Physical Metallurgy Mines and Geology Branch

OTTAWA December 2, 1946.

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PART VII. - Investigation of Heat Treatment to be Used for Threaded Studs.

Origin and Purpose of Investigation:

At a Screw Thread Research Committee Conference held in the Physical Metallurgy Research Laboratories, Ottawa, on August 22-23, 1946, it was agreed that for comparison tests of different thread forms in fatigue a homogeneous steel is required in order to eliminate the effect of undesirable variables. In order to obtain the requisite heat-treated homogeneous steel, it was decided that a series of experiments would be performed at the P.M.R.L. to establish (Origin and Purpose of Investigation, cent'd) -

the conditions of satisfactory laboratory heat treatment.

Due to the fact that a supply of the high-tensile material (steel S.A.E. 6150) which is to be used for Canadian stude was not readily available at the time these experiments were initiated, it was decided to proceed with this work, using an alternate material. A steel favourably comparable with steel S.A.E. 6150 as regards hardenability, Atlas steel S.P.S. 245, was selected for this purpose. Bar stock of this Atlas steel was received in the annealed condition.

PROCEDURE:

3. Preparation of Bars.

The 1-inch-diameter bar stock was cut into 26-inch lengths, so as to allow adequate material for the fixing of bars in the quenching fixture and for the cutting of 24-inch test specimens from the heat-treated bar. To facilitate the fastening of bars in the quenching fixture, two \frac{1}{2}-inch-diameter holes were drilled approximately 3/8 inch from either end of each bar. Prior to heat treatment, the bars were cleaned by means of sand blasting, also checked for alignment. A total of thirty-two bars were prepared in this manner and numbered.

2. Heat Treating Experiments.

(a) Quenching Treatments -

Using these bars, two quenching methods were compared: in the first, twenty-two of the bars were held
securely in a vertical position by means of a fixture during
the heat treating operation (Figure 1); in the second,
fourteen of the bars were held in a similar manner during
the heat treating operation, in addition to which specimens

(Heat Treating Experiments, cont'd) -

were enclosed in a thin cylindrical shield (Figure 2) in order to obtain a uniform cooling effect in transferring specimens from the heating furnace to the quenching oil. In both experiments, the bars were arranged in the fixture as illustrated in Figure 1, with a space of approximately 2 inches between each bar. In the second experiment, a space of about 2 inches was also left between the bars and the cylindrical shield.





35 K.W. VAPOCARB-HUMP FURNACE, SHOWING FIXTURE USED TO HOLD SPECIMENS IN POSITION DURING HEAT TREATMENT OPERATION.

(Figure 2 follows,) (on Page 4.

(Heat Treating Experiments, cont'd) -

Figure 2.

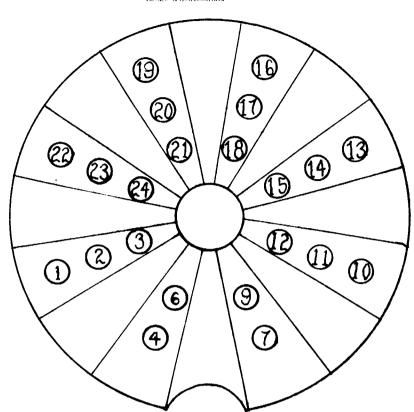


SHIELD USED TO ENCLOSE VERTICALLY HELD BAR SPECIMENSDURING HEAT TREATING OPERATION.

In Figure 3 is illustrated the positioning of the bars quenched without a shield, while Figure 4 illustrates the positions occupied by the bars quenched with the protective shield.

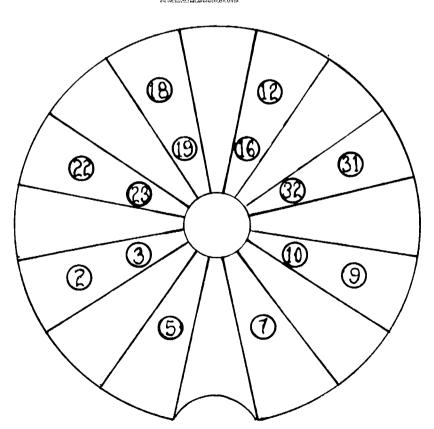
(Figures 3 and 4 follow,)
(on Page 5.

Figure 3.



Position of Bars Quenched Without Shield

Figure 4.



Position of Bars Quenched With Shield

(Heat Treating Experiments, cont'd) -

In both experiments, the bars were austenitized at 1.550° F. for $1\frac{1}{8}$ hours in a Vapocarb furnace, then quenched in oil at approximately 1.20° F.

as well as to check the relative uniformity of these two quenching treatments and to ascertain whether or not the quenching treatments had afforded sufficiently rapid cooling rates to result in the production of completely martensitic structures, a number of quenched bars were subjected to hardness analysis. Procedures followed in and results of hardness testing are dealt with below.

(b) Tempering -

After all necessary hardness tests had been made on test specimens cut from the quenched bars, the entire lot was drawn in a Leeds & Northrup Homo furnace at 1200° F. for a period of two hours, then cooled in still air.

Hardness tests were then carried out on specimens cut from the drawn bars. Procedures followed in hardness testing, as well as the results obtained, are presented below.

3. Hardness Tests.

(a) Bars Quenched Without Shield -

Three of the bars which had been quenched without the shield, Bars Nos. 13, 14 and 15, were selected for hardness testing. As seen from Figure 3, these three bars, because of the relative positions which they occupied during heat treatment, are representative of the quenched lot. Hardness tests were made on each bar at both ends, that is at both top and bottom, using both the Rockwell and Brinell instruments. It should be noted that, prior to hardness

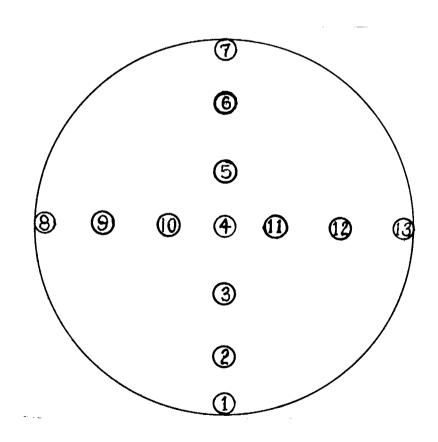
(Hardmens Tests, contid) -

tosting, about I inch of material was cut off each end of of each bar, thus removing the drilled portions which of course cooled differently than the central portions of the bars. Results of these hardness tests are recorded in Table I.

Discs, \$\frac{1}{2}\$ inch in thickness, were then cut from the centres of each of these three bars for transverse hardness tests. The hardness of these discs was checked by means of Rockwell "G" and Vickers measurements taken in two directions across the face of the disc, as indicated in Figure 5.

Results are tabulated in Table II.

Figure 5.



(Hardness Tests, cont'd) -

(b) Bars Quenched Without Shield and Tempered Using the same three bars, hardness tests were
carried out on each after tempering, a procedure somewhat
similar to that employed on the quenched bars being followed.
That is, hardness tests were performed on the outside surfaces of the bars as well as on 1-inch discs cut from the
top, centre and bottom of each bar. The results of these
tests are recorded in Tables III and IV.

(c) Bars Quenched With Shield -

Eight of the bars which had been quenched with the shield, Bars Nos. 2, 5, 9, 10, 22, 25, 31 and 32, were selected for hardness testing. As illustrated in Figure 4, these eight bars, because of the relative positions occupied by them during the heat treating operation, constitute a representative cross-section of the quenched lot. Three inch discs, similar to those previously described, were cut from each bar, one from each of the top, bottom and centre positions, then subjected to hardness tests. Results are given in Table V.

(d) Bars Quenched With Shield and Tempered -

The 1-inch discs referred to above were tested for hardness after tempering, readings being taken by means of both Vickers and Rockwell instruments. Hardness test results are tabulated in Table VI.

CONCLUSIONS:

In quenching without a shield, the maximum overall variation in surface hardness of the bars after quenching was determined to be Rockwell C-15 (Brinell 87), while the maximum overall variation in hardness of discs cut from the centres of these bars was found to be Rockwell C-3 (Vickers 41).

(Hardness Tests, contid) -

The same bars, after tempering, exhibited an overall maximum surface hardness variation of Rockwell C-7.5 (Brinell 40), and an overall maximum hardness variation between centres and both ends of Rockwell C-3.5 (Vickers 11).

- 2. In quenching with a shield, the maximum overall hardness variation between the centres and ends of quenched bars was found to be Rockwell C-8 (Vickers 115). After drawing, the maximum overall hardness variation between the centre, top and bottom portions was determined to be Rockwell C-2 (Vickers 10). From results obtained in hardness testing the quenched specimens, it is apparent that the cooling rate in quenching by this method was sufficiently rapid to result in a satisfactory martenaitic structure.
- ment in which the shield is employed, the minimum hardness variation consistently attainable with 1-inch-diameter bars of Atlas steel S.P.S. 245 is Rockwell C-2. The smuch as steel S.A.E. 6150 is favourably comparable as regards hardenability to Atlas steel S.P.S. 245, it should be possible to obtain a similarly small hardness deviation with the former steel using the heat treating equipment and technique described in the foregoing.

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T.W. Wlodek,

Head, Mechanical Section, P.M.R.L.

Ottawa, Canada, December 2, 1946. TWW: CHB: LB.

(Tables I to VI follow,) (on Pages 10 to 31.

TABLE I. - Surface Hardness of Quenched Bars (Without Shield).

		BAR NO.	13	ر الدور ا الدور الدور ال		BAR NO.	SANTANA SELEPTISTO PARTIES	T SACK TO THE SECOND SE		BAR NO.		
		a H D N I	E S S	ann saol gar lann sail airs a lann an an an Saon an Aireann an Saon an Aireann an Aireann an Aireann an Airean	ž	RDN			4	A R D N		energispersionere de de energis de service de la companie de la companie de la companie de la companie de la c La companie de la co
		o p Brinell		t o m Brinell	R. "G"	p Brinell		t c m Brinell	R. "G"	o p Brinell	R, TON	t o m Brinel
on the state of th	# 50	eø514	ee45	6534	ø57.5	00 555	48	త్త్రి601	59,5	534	49,5	95 55
	51	⊕⊕ 555	45.5	ø514	59	555	48	0 555	58.5	ტ 555	0 50,5	* 6578
	50	534	48	,	57.5	0 578	e+46,5		ee59.5	00 534	49	555
	51.5		46		9960		49		54,5		49.5	
	50.5		48		58,5	٠.	50		56	ere per Carolina	49	
	55		47		60		47		\$53.5		9948	٠
	58.5		46.5		60		 \$50,5		57	·	*	
	57.5		49		or the section of the				Additional designation of the control of the contro	v a a m	100 min 100 mi	
	9 659,5		9 50		Approximately and the state of				1	Some Stranger		
	56,5		46.5		Terr extension to the			The second se	Address Copyage			والمستران والمناولة والمستران ومترون والمستران والمستران
[©] Maximum Hardness Variation	9,5	41	5	20	2,5	23	4	46	6	21	2,5	25
⁹⁸ Overall Maximum Hardness Variation	No. of the last	Brinell Rockwel		5		Brinell Rockwell				rinell 4 ockwell		ningagyang mgagang dirindising at sa

*** Selection of the se

TABLE II. - Hardness of E" Discs from Quenched Bars (Without Shield).

· ·	BAR	N O. 13	BAR	N O. 14	BARI	N O. 15
Position on	HARDI		HARDN		HARDNI	ESS
Disc	Vickers 10-kg.load	Rockwell "C" 150-kg. load	Vickers 10-kg. load	Rockwell "C" 150-kg. load	Vickers 10-kg. load	Rockwell "C" 150-kg. load
1	5 99	55,5	606	# 56	579	0054
2	592	55.5	606	56	572	54.5
3	592	55.5	606	57	585	56.5
4	585	55	585	56	00572	55
5	585	55	585	9 57	606	56.5
6	585	55	606	56	592	55,5
77	592	\$ 54	585	56	606	56
8 -	e599	55	585	56	592	56
9	592	÷55,5	592	56	585	56
10	÷579	55	ø572	56,5	599	e#57
11	585	55.5	592	57	00613	56
18	585	55.5	599	56	613	56
13	590	54 .	ø 606	56	606	55
Maximum Hardness Variation	20	1.5	34	The state of the s	41	3
Overall Maximum Hardness Variat	3	kwell C-3 kers 41		auto-para la santa	e a gran e e e e e e e e e e e e e e e e e e e	

TABLE III. - Surface Hardness of Quenched and Drawn Bars (Without Shield).

r valus (sporter e franche south (s) Princepulme (s) prince (s) estis (s) estis (s) estis (s) estis (e frança e		BAR NO.	13			BAR NO.	14	-		BAR NO.	15	programme to the week the wife and
			NES	S		HARD				HARD	CAMPANY TO SERVICE WHEN THE PROPERTY OF	・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・
	R."C"	p Brinell		t o m Brinell		o p Brinell		tom Brinell	R. "C"	p Brinell		t o m
	24	% 269	19	2 269	25	9 8 2 6 9	21	•248	00 20	00 269	p 21.	6 262
	\$ 21.5	00 248	21.5	0 248	25.5	* 241	20.5	% 229	21	0 269	22.5	0 0241
	22		19		25		22.5		24		22.5	
	22		9 018.5		25		60 20		0 23.5		66 25	
	21.5		18.5	~	Ф22		22.5		20.5	_	21.5	
	26		22.5		23		21		21.5		22	
	23.5		18.5		ФФ26		22.5		22.5	,	21	
	9 026		. 22				\$23		23.5		21.5	
	23		© 23						21			
	23		20									
Maximum Hardness Variation	4.5	21	4.5	21	4	28	3	19	3.5	C	4	21
Overall Maximum Hardness Variation	n	Brinell Rockwel	21 0-7.5			Erinell Rockwell	40 C→6		,	Brinell Rockwel	28 1 C-5	

ooMaximum overall hardness variation for all bars) Brinell 40.
) Rockwell C-7.5.

TABLE IV. - Hardness of 2 Discs from Quenched and Drawn Bars (Without Shield)

	BARNO). 13 TOP	BAR NO. 1	3 CENTRE	BAR NO. 1	3 BOTTOM
Position on	HARDN	IESS	HARDI	IESS	HARDN	ESS
Disc	Vickers 10 kg. load	Rockwell "C"	Vickers 10 kg. load	Rockwell "C"	Vickers 10-kg. load	Rockwell "C"
1	272	26	274	25.5	274	624
2	272	26.5	274	25	274	24.5
3	270	26	270	25	274	26
4.	272	26	⊕ 270	25	274	25.5
5	270	- 26	272	25,5	●270	26
., 6	272	27	\$276	26	\$274	626 ,5
7	272	26.5	272	26	274	25,5
8	♦ ●270	0 25	270	0024	274	25
9)	♦♦279	9927	272	6 26	274	26.5
10	272	26.5	272	26	274	26
11	274	26	272	25	274	26
12	274	26.5	270	25	274	25.5
13	274	27	274	24	274	25
Maximum Hardness Variation	9	2	6	2	4	2,5
Overall Maximum Hardness Varia	ž.	kwell C-3				

TABLE IV (cont'd) - Hardness of 2" Discs from Quenched and Drawn Bars (Without Shield).

	BARNO	Company to the state of the sta	description in the control of the co	4 CENTRE	· ·	4 BOTTOM
Position on	3	NESS	HARDI	IESS		RDNESS
Disc	Vickers 10 kg. load	Rockwell "C"	Vickers 10 kg. load	Rockwell "C"	Vickers 10-kg. load	Rockwell "C"
1	272	26	274	25.5	274	25.5
2	272	26.5	274	25	274	25.5
3	274	27	0 270	25	274	26
4	6272	26	270	25	274	26
5	274	0027.5	272	25.5	\$ 276	25.5
6	276	27	±276	26	270	e 24,5
7	274	26.5	272	26	270	25
8	272	624	270	90 24	270	26,5
9	⊕ ⊕279	26.5	272	Ф26	99268	26
10	276	. 27	272	26	274	26
11	272	25	272	25	274	*26.5
12	272	25	270	25	274	25.5
13	279	24.5	274	24	274	24.5
Maximum Hardness Variation	7	3.5	6	2	8	2
Overall Maximum Hardness Variation	Rockwell C- Vickers ll	3.5				

TABLE IV (cont'd) - Hardness of 2" Discs from Quenched and Drawn Bars (Without Shield).

		BAR NO.	15 T O P	BARNO.	L5 CENTRE	BAR NO.	5 BOTTOM
Position	on	9	NESS	HARDI	NESS	НАІ	RDNESS
Disc		Vickers 10 kg. load	Rockwell "C"	Vickers 10 kg. load	Rockwell "C"	Vickers 10-kg. load	Rockwell "G"
1		274	0024	++268.	0 24	274	25,5
2	****	274	26.5	270	25,5	274	25.5
3	***	274	26.5	272	25	274	e 26.5
4	- 100 100	274	25	272	25	272	25.5
5	· E	272	26.5	272	25	274	26
6	ager.	272	26	⊕ 274	e25.5	274	26
7	ANT A	00 276	25.5	270	24	\$272	+25
8	egity	6 270	26	272	25	272	25
9	*	272	25	. 274	24	272	25
10	Ĵ.	276	26	274	25	274	25
11	-	276	26.5	272	24,5	• 276	26
12	, Park	276	26.5	272	25	274	25,5
13		270	6627	274	25	276	26
Maximum Varla		6	3	6	1.5	4	1.5
00verall Hardnes	Maximum s Variation	Rockwell C-3	and the second s				3

TABLE V. - Hardness of 2" Discs from Quenched Bars (With Shield).

	BARNO	2 TOP	BAR NO.	2 CENTRE		BOTTOM
Position on	•	NESS		ONESS		DNESS
Disc	Vickers 10-kg. load	Rockwell "C"	Vickers 10 kg. load	Rockwell "G"	Vickers 10-kg. load	Rockwell "C"
graphic strategic control for a description from the strategic control of the strategic control	592	55	585	54	560	55
2	585	55	585	55	592	55
3	592	56	579	0 53	572	54
4	572	55,5	566	55	554	53
5	579	56	554	54.5	585	54
6	⇒ 592	55.5	566	53	572	54
7	579	55	\$ 530	-53	572	54
8	572	55	\$ 606	54	e¢613	55
9	554	54.5	599	55.5	599	♦56
10	585	56	599	* 56	548	55.5
11	554	ø b 56,5	572	55	542	52
12	554	56	572	55.5	542	52
13	♦ 542	♦54	592	54	\$\$ 530	99 51
⊕Maximum Hardness Variation	50	2.5	76	3	83	5
Overall Maximum Hardness Variation	Rockwell C-5. Vickers 83	,5				ann o pargen ar ye sonach ilipaanik ook kansish brake oo dayk an asar bangon saagan saar

TABLE V (Cont'd) - Hardness of " Discs from Quenched bars (With Shield).

	BAR NO.		BAR NO.	3 CENTRE	BAR NO. 3	BOTTOM
Position on	7	NESS	The second secon	NESS		NESS
Disc	Vickers : 10-kg, load:	Rockwell "C"	Vickers 10-kg. load	Rockwell "C"	Vickers 10-kg. load	Rockwell "C"
1	572	÷53	99498 9	0 53	585	53
2	579	53	572	55	579	54.5
3	592	53	e 579	54	566	52
4	\$ 566	53.5	528	54	560	52.5
. 5	579	55	572	55	0 548	00 52
6	572	55.5	572	@ 56	579	52
7	00 606	56	572	56	585	52
8	579	56	572	53	6 606	48
9	592	55	572	53	572	49
10	572	ø ø 59	579	53	579	49
11	579	53	579	56	566	54
12	579	53	572	56	585	55
13	566	53,5	566	56	585	\$ 56
Maximum Hardness Variation SOverall Maximum	40 Rockwell C-7	6	81	3	58	4
Hardness Variation	Vickers 108			Orași antica con contra supri a cipro antica cana con contra suprimenta de la contra contra contra contra contr		

TABLE V (Contid) - Hardness of 2" Discs from Quenched Bars (With Shield).

). 9 T O P		9 CENTRE		BOTTOM
Position on	1	RDNESS		RDNESS	.1	NESS
Disc	Vickers 10-kg. load	Rockwell "C"	Vickers 10-kg. load	Rockwell "C"	Vickers 10-kg. load	Rockwell "C"
1	585	ø53.5	ф 6 13	56	572	55
2	ø572	54	606	56	579	55
3	599	55	585	⊕⊕56	585	54.3
4	585	54	. 572	55	\$606	54
5	ø606	55	579	54	572	55
6	572	ø56	585	54	585	56
7	592	54	⊕ ⊕536	54	606	55
8	606	54	572	54	Soft	e 53
9	572	54	572	@ \$53	spot.	53
10	585	54.5	579	54	\$562	53
11	606	55	585	55.5	572	54
12	599	56	579	55.5	579	●56
13	579	55,5	585	54	599	56
oMaximum Hardness Variation	34	2.5	77	3	44	3
Overall Maximum Hardness Variation	Rockwell C-3 Vickers 77		and the same of th			

TABLE V (CONT'd) - Hardness of B" Discs from Quenched Bars (With Shield).

	BAR NO.	10 T 0 P	BAR NO.	10 CENTRE	BAR NO.	10 BOTTON
Position on		NESS		DNESS	HAR	DNESS
Disc	Vickers 10-kg. load	Rockwell "C"	Vickers 10-kg. load	Rockwell "C"	Vickers 10-kg, load	Rockwell "C"
1	585	54	e 548	53	554	55
2	**************************************	54	585	53.5	572	54
3	548	54.5	572	ee52.5	579	55
4	572	54.5	579	55,5	579	54.5
5	579	55.5	585	54.5	566	54.5
6	585	÷55.5	6 606	55	585	53.5
7	572	55	606	55,5	548	⊕53
8	548	ø53 _° 5	606	ee56	ø548 -	53.5
9	566	55.5	579	55	572	55
10	599	54,5	572	56	566	e 55.5
11	⊕⊕ 606	55.5	548	53	579	54.5
12	599	54	585	53	585	53
13	572	54	585	54	\$606	53
Maximum Hardness Variation Overall Maximum	70 Rockwell C-3	2 .5	58	3.5	58	2,5

TABLE V (Cont'd) - Hardness of 2" Discs from Quenched Bars (With Shield).

Position on	1	NESS TOP	HARL	22 CENTRE	HAR	22 BOTTOM PONESS
Disc	Vickers 10-kg. load:	Rockwell "C"	Vickers 10-kg. load	Rockwell "C"	Vickers 10-kg. load	Rockwell "C"
1	585	54.5	579	e 56	585	55
2	579	55,5	585	56	⊕ 606	55,5
3	00 566	55.5	599	55.5	579	55.5
4	599	54.5	606	\$55	6 572	6 54
5	585	55	585	56	606	56
6	579	55	\$ 572	56	599	⊕⊕ 56.5
7	572	55	579	55.5	599	56
8	. ••606	00 53	579	56	592	56
9	592	54	ø 606	56	592	56.5
10	572	54,5	585	56	572	55
11	585	55	572	55	579	54
12	579	0 55.5	579	56	585	54
13	599	54.5	579	55,5	579	54
Maximum Hardness Variation	40	2.5	34	1	34	2,5
Overall Maximum Hardness Variation	Rockwell C-3	.5	The second secon			

TABLE V (Contid) - Hardness of 2" Discs from Quenched Bars (With Shield).

Position on	BAR NO.	23 TOP	WHITE THE PARTY AND ADDRESS OF THE PARTY AND A	23 CENTRE	ă	23 BOTTOM DNESS
Disc	Vickers 10-kg. load		Vickers	Rockwell "C".	VICKERS 10-kg. load	Rockwell "C"
1	572	⊕⊕52	579	54	599	55
2	579	53	⊕ 536	53	599	55.5
3	₩9536	53	542	952.5	585	55.5
4	566	54.5	599	54,5	572	55
5	542	\$ 55	585	53,5	ø536	56
6	585	54.5	ø606	54	548	54
7	579	54	536	54.5	542	54
8	566	53	579	54	572	54
9	. 585	52	572	53.5	579	⊕ 53 ₃ 5
10	599	55	579	54.5	ø606	00 56
11 12 13	00606 572 579	55 55 55	606 585 5,99	a55 .5 55.5 55	58 5 606 599	54.5 54 54
♦Maximum Hardness Variation	70	3	70	3	70	2.5
Overall Maximum Hardness Variation	Rockwell C-4		ng garangan at taon ayan ayan mangapan ayan ayan ayan ayan ayan ayan ayan			

TABLE V (Cont'd) - Hardness of 2" Discs from Quenched Bars (With Shield).

Position on	1	31 TOP	HAF	DNESS	BAR NO. 31 BOTTOI	
Disc	Vickers 10-kg. load:	Rockwell "C"	Vickers 10-kg. load	Rockwell "C"	Vickers 10-kg. load	Rockwell "C"
1	572	90 52	÷572	⊕ 53	572	0 53
2	585	52	585	53,5	585	53,5
3	579	53.5	599	53,5	579	54
4	585	53,5	585	54	566	53,5
5	572	55	572	55	572	⊕ 56
6	ø606	♦ 55°5	* 606	⊕⊕56	00 606	56
7	579	55	585	55	592	55
8	572	55.5	579	55,5	96 566	53
9	606	53	572	55.5	579	54
10	585	55	606	56	585	55
11	572	54	572	55	572	54.5
12	579	54	579	55	579	55
13	9 566	53	572	54	599.	56
Maximum Hardness Variation Overall Maximum Hardness Variation	Rockwell C-4 Vickers 40	3.5	34	3	40	3

TABLE V (Cont'd) - Hardness of 2" Discs from Quenched Bars (With Shield).

	HARDNESS		BAR NO. 3	S CENTRE	BAR NO. 32 BOTTON	
Position on			HARDNESS		1	DNESS
Disc	Vickers 10-kg. load	Rockwell "C"	Vickers 10-kg. load	Rockwell "C"	Vickers 10-kg, load	Rockwell "C"
1	585	0054	585	654	599	55.5
2	♦ 572	54.5	579	56	572	56
3	579	56	ø572	e 57	566	57
4	599	56	% 606	55.5	** 606	55
5	572	55	599	56	572	\$57
6	⊕ 606	54	599	56	579.	56.5
7	599	54	. 592	54	585	\$ 54
8	579	55,5	585	56	572	56
9	576	56	572	56.5	599	56
10	606	99 57	579	57	572	57
11	585	55	599	56.5	00 566	55.5
12	599	54	606	56.5	572	54.5
13	572	54	572	56	579.	54
♦Maximum Hardness Variation	34	3	34	3	40	3
ooverall Maximum Hardness Variation	Rockwell C-3 Vickers 40			A service of the serv	and the first of the second	

oolwaximum overall hardness variation for all bars) Vickers 115.
Rockwell C-8.

TABLE VI - Hardness of $\frac{1}{2}$ Discs from Quenched and Drawn Bars (With Shield).

Position on	BAR NO. 2 TOP HARDNESS		HARDNESS		BAR NO. 2 BOTTOM	
						NESS
Disc	Vickers 10-kg. load:	Rowckell "C"	Vickers 10-kg, load	Rockwell "C"	Vickers 10-kg. load	Rockwell "C"
1.	262	27	\$266	26.5	264	26.5
2	262	26.5	264	26.5	262	• 27
3	260	27	264	627	260	27
4	264	26.5	264	26	\$ 266	\$ 26
5	262	27.5	262	26.5	264	27
6	260	27.5	\$258	27	264	27.5
7	66 258	***************************************	260	26.5	262	27.5
8	262	27	264	26	264	26.5
9	** 266	27	262	27	@ 258	27,5
10	262	27.5	262	27	262	27.5
11	266	00 28	264	27	262	27
12	262	27.,5	266	27	266	27.5
13	262	26.5	258	26	264	27,5
oMaximum Hardness Variation	8	2	8	I.	8	1
Overall Maximum Hardness Variation	Rockwell C- Vickers 8	Z				

TABLE VI (Cont'd) - Hardness of 2" Discs from Quenched and Drawn Bars (With Shield).

Position on Discs	BAR NO. 3 TOP HARDNESS		BAR NO.	3 CENTRE	BAR NO. 3 BOTTOM		
			HARI	ONESS	HARDNESS		
	Vickers 10-kg. load	Rockwell "C"	Vickers 10-kg. load	Rockwell "C"	Vickers 10-kg. load	Rockwell "C"	
1	264	⊕27 .5	262	6 27	262	27	
2	264	27.5	260	27.5	\$268	27	
3	266	6 26.5	⊕ ⊕ 268	27.5	262	27	
4	• 268	26.5	264	00 28	264	6926	
5	262	27.5	00 258	28	⊕260	26.5	
6	\$260	27.5	260	27.5	264	27	
7	264	26.5	262	27	262	27	
8	260	27.5	262	27	262	27	
9	262	27.5	264	28	264	27 ,5	
10	262	27	268	28	260	27.5	
11	266	27	262	28	264	27	
12	264	27.5	260	27.5	262	27	
13	262	27	264	27,5	262	27	
oMaximum Hardness Variation	8	1	10	I management and the second se	8	1.5	
60verall Maximum Hardness Variation	Rockwell C- Vickers 10	Commence of the second					

TABLE VI (Cont'd) - Hardness of 2" Discs from Quenched and Drawn Bars (With Shield).

	BAR NO.	Company of the Compan	Vignative commence and consist the advisory to be a thirty factory	9 CENTRE	The state of the s	prompted procedure to the contract of the cont
Position on	-	HARDNESS		DNESS	1	ONESS
Disc	Vickers 10-kg. load	Rockwell "C"	Vickers 10-kg. load	Rockwell "C"	Vickers 10-kg. load	Rockwell "C"
1	264	** 26	264	627	262	*26
2	262	27	262	27	262	27
3	262	26.5	264	ø27.5	** 264	27.5
4	⊕ 260	26.5	262	27	♦♦ 258	27
5	262	27	262	27.5	262	*28
6	260	27.5	ø260	27	262	27.5
7	⊕⊕ 268	27	262	27	262	27.5
8	260	26.5	260	27	260	26,5
9	262	00 28	264	27.5	264	27.5
10	262	27.5	** ** 268	27.5	262	27.5
11	264	27	264	27.5	262	28
12	264	27.5	264	27	260	27.5
13	268	26	264	27	262	27
Maximum Hardness Variation	4000 Section (1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2	8	0.5	6 -	2 name a compression de consiste de consis
bOyerall Maximum Hardness Variation	Rockwell C-2 Vickers 10				NA COLUMN TO THE	

TABLE VI (Cont'd) - Hardness of 2" Discs from Quenched and Drawn Bars (With Shield).

Position on	BAR NO.	10 T O P		10 CENTRE	HARD	10 BOTTOM
Disc	Vickers 10-kg, load:	Rockwell "C"	Vickers 10-kg. load:	Rockwell "C"	Vickers 10-kg. load:	Rockwell "C"
1	260	26.5	e262	e26,5	6 262	0 26
2	262	27	264	27	264	26.5
3	99 268	27	262	27	266	27
4	⊕ ⊕258	26.5	262	26.5	2 268	26.5
5	264	27	6 268	27	266	26.5
/ 6	268	÷27.5	262	27	268	27,5
7	262	27	262	27	260	26,5
8	260	26.5	264	26,5	262	26.5
9	264	27	262	27	262	27.5
10	266	27.5	262	\$27.5	262	00 28
11	264	27	264	27	264	27
12	262	27	264	27.5	264	27
13	264	- 6 026	264	27	266	27
oMaximum Hardness Variation	10	1.5	6	. 1	6	2
oOverall Maximum Hardness Variation	Rockwell C-2 Vickers 10					

TABLE VI (Cont'd) - Hardness of 2" Discs from Quenched and Drawn Bars (With Shield).

Position on	BAR NO. 22 TOP HARDNESS		Antiniotheriny in autymorphism contribute in the charge of	22 CENTRE	BAR NO.	22 BOTTOM
			HARDNESS		HARDNESS	
Disc	Vickers 10-kg. load	Rockwell "C"	Vickers 10-kg. load	Rockwell "C"	Vickers 10-kg. load	Rockwell "C"
1	266	27	264	27	e 268	€ 27
2	264	��26,5	264	27	264	2 27.5
3	266	27,5	262	27	÷262	27.5
4	262	27	262	e 26,5	262	27.5
5	264	00 28	264	27	262	27,5
6	⊕260	28	262	0 27,5	264	27.5
7	264	27,5	6 266	26.5	262	27.5
8	264	27.5	264	27	262	27
9	262	27.5	264	27.5	264	27
10	262	28	264	27.5	264	27.5
11	266	28	266	27	262	27.5
12	● ●268	27.5	266	27.5	262	27.5
13	262	27	***	27	262	27
eMaximum Hardness Variation	8	1.5	8	1	6	0,5
Overall Maximum Hardness Variation	Rockwell C-l Vickers 10	o D				and colding to compressing the majority to the constitution and the coldinary of the coldinary of the coldinary and the

TABLE VI(Cont'd) - Hardness of $\frac{1}{2}$ Discs from Quenched and Drawn Bars (With Shield).

Adhan	I was to the same of the same	Supplementarion appropriate transport and provide the providence of the providence o		23 CENTRE	enditorismonromanerominamento anticomo	23 BOTTOM
Position on	9	RDNESS		NDNESS		NESS
Disc	Vickers 10-kg. load	Rockwell "C"	Vickers 10-kg. load	Rockwell "C"	Vickers 10-kg. load	Rockwell "G"
1	b 266	00 26	262	÷26,5	⊕ 268	6 26
2	262	27	262	27	264	27.5
3	262	27	⊕ 260	27	264	e 28
4	264	27	266	26.5	266	27
5	266	27	264	27	262	28
6	260	27	00 268	27.5	0 262	27.5
7	⊕	27	260	27	262	27
8	260	27	262	27	262	27
9	266	27	262	27	264	27
10	264	0 27.5	264	27	266	27.5
11	264	27.5	264	. 27	262	27.5
12	264	27.5	266	⊕ 0 28	264	27
1.3	262	26	268	27	264	26.5
oMaximum Hardness Variation	8	1.5	8	1.5	6	. 2
Overall Maximum Hardness Variation	Rockwell C-2 Vickers 10		· ·			

TABLE VI (Cont'd) - Hardness of 2" Discs from Quenched and Drawn Bars (With Shield).

Position on Disc		31 TOP	AND DESCRIPTION OF THE PARTY OF	31 CENTRE	AND THE RESIDENCE AND ADDRESS OF THE PARTY O	31 BOTTOM
	HARDNESS			DNESS		NESS
	Vickers 10-kg. load	Rockwell "C"	Vickers 10-kg. load	Rockwell "C"	Vickers 10-kg. load	Rockwell "C"
1	262	27	264	. 27	•260	±27
2	••266	⊕ 26.5	® 266	27	ø266	27
3	264	27	0 260	27	266	6028
4	266	27	266	27	260	27.5
5	264	∌ 27.5	264	27	262	27.5
6	266	27.5	262	0 27.5	262	28
7	00 260	27	262	26.5	260	27
8	262	27	262	26.5	262	26.5
9	264	27.5	260	27.5	262	27.5
10 ^	266	27.5	264	27.5	266	27.5
11	260	27.5	264	⊕ ⊕ 26	260	27
12	262	27.5	264	27.5	264	27.5
13	262	27.5	262	26.5	264	27
Maximum Hardness Variation	6	1	6	1.5	6	I.
Overall Maximum Hardness Variation	Rockwell C-2 Vickers 6	the state of the s				es accumentation pour la general tight internet construct TAP MARIA, air stability de la const

TABLE VI (Cont'd) - Hardness of 2" Discs from Quenched and Drawn Bars (With Shield).

	BAR NO.		SANGERY CONTROLLED TO THE CONTROL OF T	32 CENTRE	www.com.ungroup.monedoument.moningle/france/videushepur_commando	32 BOTTOM	
Position on Disc	HARDNESS			NESS	HARDNESS		
	Vickers 10-kg, load	Rockwell "C"	Vickers 10-kg. load	Rockwell "C"	Vickers 10-kg. load	Rockwell "C"	
1	264	90 26.5	264	27.5	264	⊕27	
2	90 266	27	6 262	27.5	* 266	27	
3	266	27.5	264	0 28	• •262	+28	
4	264	27	262	627	266	27	
5	60 262	27.5	262	27.5	262	28	
6	262	0 028	262	27.5	262	28	
7	262	27.5	264	27	264	27	
8	262	27.5	262	27.5	262	27	
9	262	27	0 266	27.5	262	27.5	
10	262	27	266	28	262	28	
11	264	27	264	28	264	28	
12	262	27.5	264	27.5	264	27.5	
1.3	262	27	266	27.5	264	27	
eMaximum Hardness Variation	4	1.5	4	1	4	1	
Overall Maximum Hardness Variation	Rockwell C-	. 5		and joint constants.		augi sadasan egahin yarra sasan eresi gasta da en	