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OTTAWA April 11th, 1944.

REPORT

of the

ORE DRESSING AND METALLURGICAL LABORATORIES.

Investigation No. 1624.

Examination of Welded Bogie Suspension Bracket from Snowmobile.

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Division of Metallic Minerals.

Ore Dressing and Metallurgical Laboratories DEPARTMENT OF MINES AND RESOURCES

Mines and Geology Branch

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Origin of Material:

On February 7th, 1944, Mr. H. Stevenson, Assistant Director General, Army Engineering Design Branch, Department of Munitions and Supply, Ottawa, Ontario, submitted a snow-mobile begin suspension bracket for examination. This bracket was made by Messrs. Farand and Delorme, Montreal, Quebec, and is stated to be representative of production of that time.

The plant of Forend and Delorme, 433 St. Martin
Street, Montreal, Quebec, was visited on February 16th, 1944,
to obtain information and observe welding procedures. It was
learned that the assembly was tacked with Wilson No. 98 electrode and finished with Hollup-type N electrode. The welding
sequence and jigging were well planned and should be productive
of good weldments. The welding supervision was better than is

(Origin of Material, cont'd) -

ordinarily encountered but the one supervisor is unable to completely supervise the work of all of the welders employed on this job.

It was noticed that the welders tended to use too high welding currents for the size of electrodes employed.

It was also noted that in welding materials of unequal thicknesses the welders were directing the arc improperly. Fillet
welding technique was also faulty in that improper inclination
of electrode was employed, resulting in improper location of
weld metal. All of the above were brought to the attention of
the welder and welding supervisor, with the result that
corrections were made.

Object of Investigation:

- 1. To examine the welding of the bracket with a view to evaluating the suitability of the welding technique.
- 2. To make recommendations to improve the welding technique should this prove to be necessary.

Procedure:

- 1. The suspension bracket was subjected to a thorough visual examination. Figure 1 shows the bracket "as received".
- 2. The shaft rings were subjected to an x-ray examination by the National Research Council, Ottawa. Figures 2 to.

 ll are reproductions of the exographs of the welds of the shaft rings. In examining these reproductions it should be borne in mind that there is an inevitable loss of sensitivity in the reproduction process and that the colours of the reproduction are the reverse of the exograph itself.
- 3. Macro sections were machined from the welds of the shaft rings in those areas in which the exographs indicated the presence of welding defects. Figures 1, 12, 13 and 14 show the

(Procedure, cont'd) -

areas from which the samples were removed. Figures 15 to 17 show the macro samples after polishing and etching.

Discussion:

A visual examination of the bracket reveals considerable undercutting, irregular welds, and improperly located weld metal. The x-ray examination reveals porosity, undercutting, slag inclusions, and lack of fusion. All of the above are confirmed by macro examination and, in addition, there is some ovidence of poor fit-up.

Porosity, undercutting and slag inclusions are probably the result of using too high a welding current. This leads to a pronounced boiling action of the molten metal which is then difficult to control and direct. In the fillet welds around the strap joining the shaft ring to the main body, lack of fusion at the root of the weld is probably the result of improperly cleaned surfaces. All scale, dirt and grease should be removed before welding.

There is room for improvement in the fit-up of parts
to be welded. It cannot be reasonably expected that the welding
technique can in any way compensate for poor alignment of parts
to be welded. The electrode used should be quite suitable for
this part.

It will be noted from the above that the majority of the above defects arise from the errors in technique of the individual welders. Such defects are not unusual and may be readily eliminated by instructing welders on proper welding currents, electrode inclination and are direction on parts of unequal thicknesses. To ensure that these instructions are followed constant supervision and correction are required.

CONCLUSIONS:

1. The welding technique used is open to criticism. The following defects were found: porosity, undercutting, slag alaw the macro semples after inclusions, and lack of fusion.

(Procedure, control :

- 2. The electrodes and jigging method are good and should permit production of satisfactory parts.
- 3. Poor fit-up and lack of fusion are easily remedied by close attention to matching of parts and cleaning before welding. sent to IIA morett to hoat bue sentladfoot sale
 - 4. The welding defects found should be easy to eliminate. Instruction and supervision of welders as outlined above should have the desired effect.

Recommendations: on medical and an action and the head of the

1. Every effort should be made to improve fit-up of parts to be welded. The ent of only whole on amintol marte

the result of using too bigh a welding corrects this leads

- 2. Surfaces to be welded should be cleaned of all scale and dirt. som the dire a see alla . secatore become
- 3. Welding supervision should instruct welders on the effects of too high welding currents, improper electrode inclination, etc., and attempt to ensure that instructions are carried out our and the root had expensed over you at any explanant

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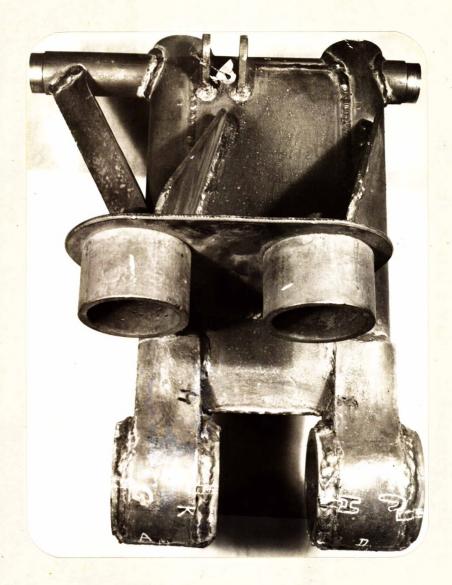
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Figure 1.



BRACKET IN 'AS RECEIVED' CONDITION.

White rectangles indicate areas from which macro samples were received.

Figure 2.

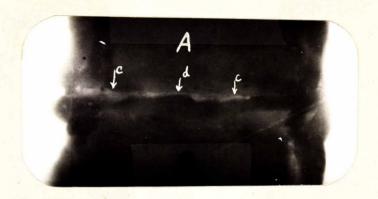
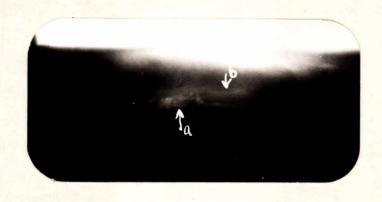


Figure 3.



Figure 4.



a = porosity or gas inclusions.
b = undercutting.
c = slag inclusions.
d = lack of fusion. Legend:

Figure 5.



Figure 6.

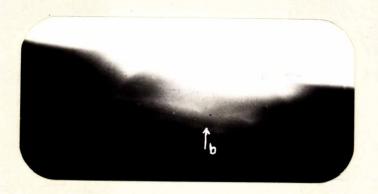


Figure 7.



Legend:

a - porosity or gas inclusions.
b - undercutting.
c - slag inclusions.
d - lack of fusion.

Figure 8.

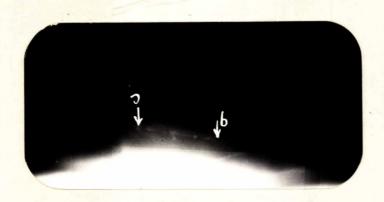


Figure 9.



Figure 10.



Legend:

a - porceity or gas inclusions.
b - undercutting.
c - slag inclusions.
d - lack of fusion.

Figure 11.

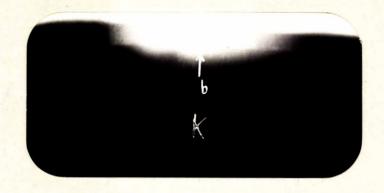


Figure 12.



CLOSE-UP OF ONE SHAFT RING.

White rectangles indicate areas from which macro samples were machined.

Note irregularity of welds.



CLOSE-UP OF WELD JOINING ENDS OF STRAP.

Note irregular width of weld.
White rectangles indicate areas from which macro samples were machined.

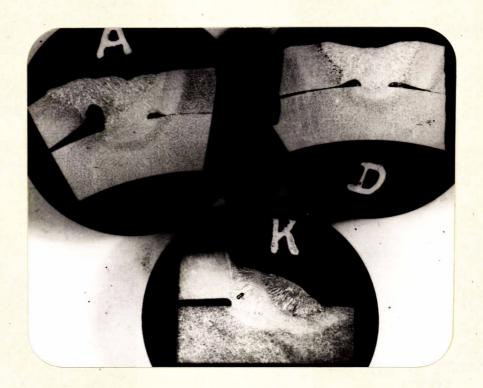




CLOSE-UP OF WEID JOINING ENDS OF STRAP.

Note irregularity of welds. White rectangles indicate areas from which macro samples were machined.

Figure 15.



MACRO SAMPLES OF WELDS OF SHAFT RINGS.

Letters same as in exographs and macrophotographs.

Sample		Comment
A	500	Gas inclusion at root of weld. Iow penetration. Poor fit-up on right side.
D	-	Penetration Low.
K	en	Good weld with small gas inclusion.

Figure 16.

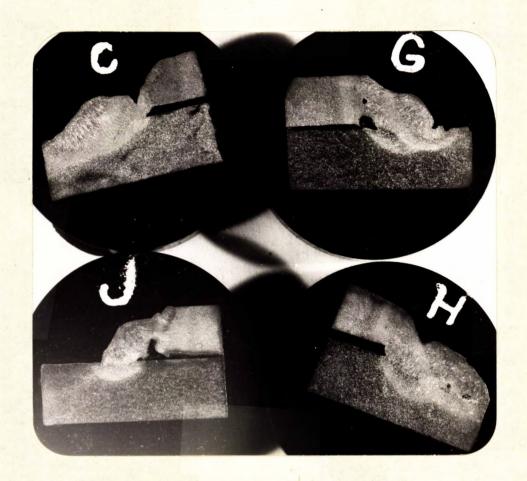


MACRO SAMPLES OF WELDS OF SHAFT RINGS.

Letters same as in exographs and macrophotographs.

Sample		Comment
В		Large gas inclusion at root of weld. Good penetration.
B2		Undercutting on vertical edge. Poor location of weld metal. Poor fit-up.
E	æ	Good penetration; slight under- cutting. Poor fit-up.
F		Poor penetration at root of weld. Very irregular and gassy weld.

Figure 17.



MACRO SAMPLES OF WEIDS OF SHAFT RINGS.

Letters same as in exographs and macrophotographs.

Sample		Comment
C	ergs	Poor fit-up; severe undercutting. Penetration good,
G	da	Gas inclusions at root of weld. Penetration good.
J	578	Lack of fusion at root of weld.
Н		Poor fit-up; some undercutting and gas inclusions.

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