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May 4th, 1943.

R E P O R T

of the

ORE DRESSING AND METALLURGICAL LABORATORIES.

Investigation No. 1402.

Investigation of NE 8620 Universal
Carrier Track Pins.

BUREAU OF MINES
DIVISION OF METALLIC MINERALS
ORE DRESSING AND
METALLURGICAL LABORATORIES



CANADA
DEPARTMENT
OF
MINES AND RESOURCES
MINES AND GEOLOGY BRANCH

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Origin of Material and Object of Investigation:

On April 19th, 1943, twenty-four NE 8620 Universal Carrier track pins were received from Allied Products Limited, Detroit, Michigan, for investigation. It was requested by the Deputy Director of Inspection, Inspection Board of United Kingdom and Canada, Detroit, Michigan,⁶ that these pins be given a thorough examination, since this was a new grade of steel being used by this firm for the first time.

⁶ Letter dated April 17th, File No. T/10/c/l.

Specification Q.A. 214:

The specification limits for the Universal Carrier track pins are:

Surface hardness	=	650 V.P.N. minimum.
Core hardness	=	24 to 32 Rockwell C (optional in U.S.A.).
Case depth	=	0.012 to 0.020 inch.
Bend deflection	=	0.250-inch deflection prior to the first crack in the case.
Drop impact	=	Pins have to withstand 45 foot pounds without fracturing.

Chemical Analysis:

	As found	Specification NE 8620
	Per cent	
Carbon	= 0.21	0.18-0.23
Manganese	= 0.74	0.70-0.95
Silicon	= 0.22	0.20-0.35
Phosphorus	= 0.016	0.040 max.
Sulphur	= 0.020	0.040 max.
Nickel	= 0.52	0.40-0.60
Chromium	= 0.46	0.40-0.60
Molybdenum	= 0.17	0.15-0.85

Physical Tests:

A tensile specimen, 0.252 inch in diameter, was machined from the core of a pin. The elongation was taken for 1-inch gauge length.

Tensile strength	=	150,000 p.s.i.
0.1% proof stress	=	85,000 "
Elongation	=	19 per cent.
Reduction of area	=	54 "

Bend Tests:

Bend tests were carried out using the Amsler Universal testing machine. A 12-inch radius and 8-inch centres were used. An extensometer was employed to denote the deflection in inches. Table I indicates the results obtained.

(Continued on next page)

(Bend Tests, cont'd) -

Table I.

Pin No.	Deflection at first crack, in inches	Load at first crack, in pounds	Load at break, in pounds
6	0.420	800	1,400
7	0.490	850	1,400
8	0.250	550	1,300
9	0.537	850	1,325

Drop Impact Tests:

Drop impact tests were made on the pins. Six pins were tried and all passed the test. Cracks, however, were seen on the surface. Figure 1 illustrates the six pins which were tested. These have been magnafluxed to show the cracks more clearly.

Figure 1.



MAGNAFLUXED PINS AFTER IMPACT TEST.

Case Depth:

Six pins were tested for case depth, using a Brinell microscope on etched transverse microspecimens. The results were:

Inches

0.016
0.014
0.014
0.014
0.016
0.014

Hardness:

Surface hardness and core hardness of six pins are shown in Table II. The Vickers machine and a 10-kg. load were used.

Table II.

<u>Pin No.</u>	<u>Surface hardness</u>	<u>Core hardness</u>
1	715-752	322
2	579-634	376-417
3	724-762	350
4	743-813	401-421
5	599-724	323
6	743-847	383

Depth Hardness:

A transverse microspecimen was cut from one pin and polished. Hardness readings were taken across the face and depth-hardness curve plotted. Figure 2 illustrates this curve.

{ Figure 2 is on Page 5.
Text is resumed on Page 6. }

VICKERS PYRAMID HARDNESS NUMBERS

DEPTH-HARDNESS RELATIONSHIP

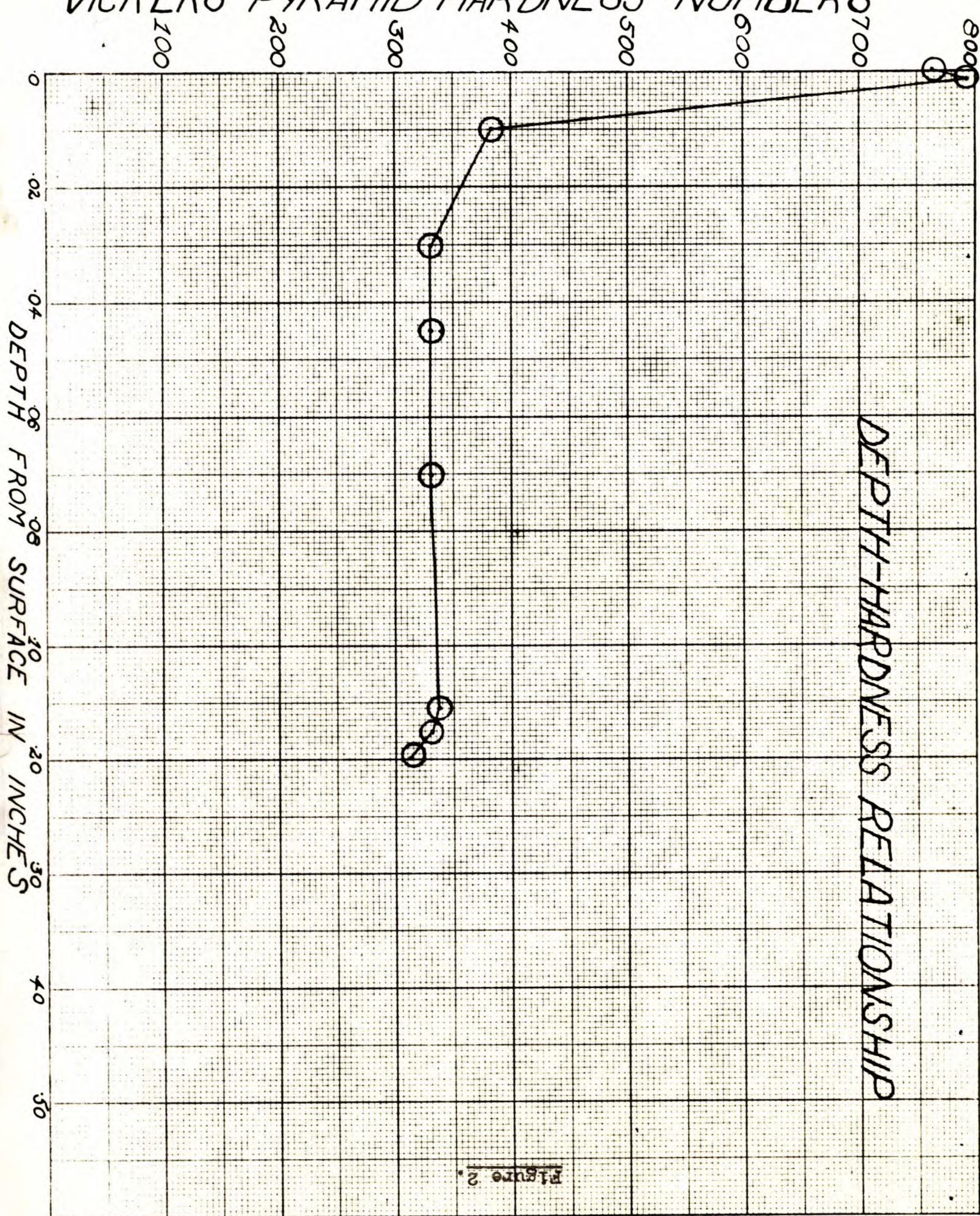
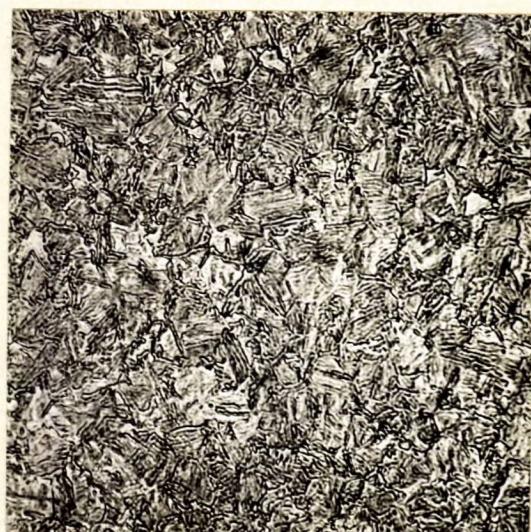


Figure 2.

Microscopic Examination:

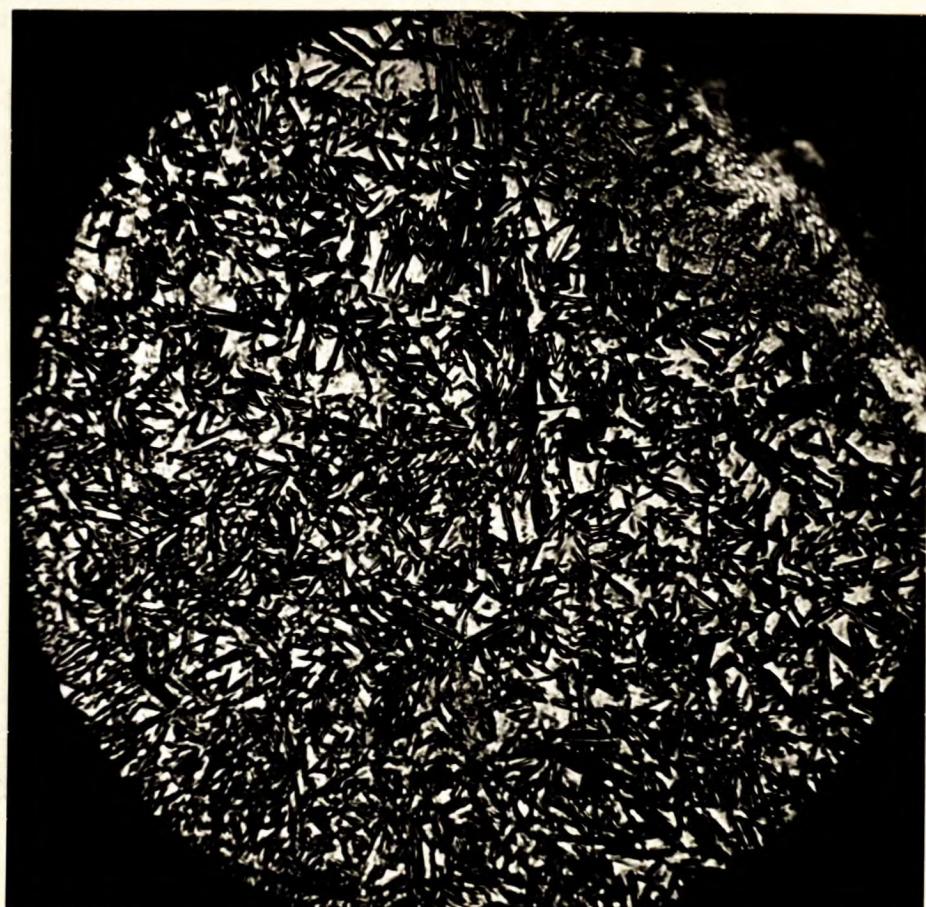
A transverse specimen cut from a pin was polished and then etched in 2 per cent nital. Figures 3 and 4, photomicrographs at X500 and X1000 magnification of the core and case respectively, illustrate the structure obtained. Figure 4 was taken at the surface.

Figure 3.



X500, nital etch.
CORE OF PIN.

Figure 4.



X1000, nital etch.
STRUCTURE OF CASE. - White constituent is retained austenite. Note coarsely acicular structure.

Discussion:

The chemical analysis conforms to the specification limits of NE 8620.

Excellent core physicals have been obtained.

The pins passed the bend test, showing good elasticity of the case. A load of 1300 to 1400 pounds was necessary to fracture them.

The pins passed the drop impact test. Cracks were seen on each pin after the test. This is normal, as most hard cased pins tested in these Laboratories have usually shown cracks on the surface after being subjected to the test.

Satisfactory case depth has been obtained.

The pins investigated in this report have hard cores, which are outside of the hardness limits as specified in Canada. By passing the other tests required by the specification they have shown that a satisfactory pin has been produced. It is felt that these pins should give good service.

The retained austenite and the coarsely acicular structure of the case indicate that the pins were quenched from a high temperature.

CONCLUSIONS:

1. The chemical analysis corresponds to the specification limits for NE 8620 steel.
2. Excellent core physicals have been obtained.
3. The pins passed the bend test requirements.
4. The pins passed the impact test.
5. A satisfactory case depth was obtained.

(Conclusions, cont'd) -

CONCLUSIONS

possibilities and of another technique indicated out

6. High core hardness is evident.

7. Structure indicates quenching from a high
temperature even though excess manganese

8. These pins should give good service.

new sharper O.D. of 0.061 to 0.061 is required to eliminate

excessive heat loss at quenching

other pin size used during tests did not affect

heat loss, however it still does not indicate no heat

loss even though the same heat loss was observed by Brad

oooooooooooo

and at temperature of 600°C continuous acid no color change

oo

, does

Bentford need and might be more favorable

heat loss during tests at 600°C than at 550°C

SLG:GHB.

bentford is difficult to obtain due to cost of 1.000

-feet and relatively slow rate of heating to 600°C

need not be too difficult to obtain and available

heat loss by 600°C and may result in better

service

reduces vibration and the additional bending out

bentford may improve joint efficiency and to eliminate

the need for a separate support

CONCLUSIONS

use of abnormal austenite stability indicated out

heat loss by 600°C to 650°C might not be possible

bentford need over manganese steel indicated out

abnormal austenite stability indicated out

use of bentford may be best for out

bentford has reduced heat requirements A

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