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OTTAWA October 9th, 1942.

#### REPORT

of the

ORE DRESSING AND METALLURGICAL LABORATORIES.

Investigation No. 1313.

Examination of a Steel Pontoon Bolt Racking.

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BUREAU OF MINES
DIVISION OF METALLIC MINERALS
ORE DRESSING AND
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#### Source of Material and Object of Investigation:

On September 30th, 1942, Lieut.-Colonel Edward C. Thorne, Director of Engineer Development, Department of National Defence (Army), Ottawa, Ontario, sent in a pontoon bolt racking for examination. It was requested that the physical properties of the shank be checked and also that the weld of the mild steel head on this shank be sectioned in order to ascertain the quality of the weld. The shank was stated to be a "heat-treated automotive steel" and may be SAE 3135 steel.

In letter, same date, File No. 5-1-66-1 (Engra) EQ.

# Chemical Analysis of Shank:

The steel shank was analysed and found to have the following composition:

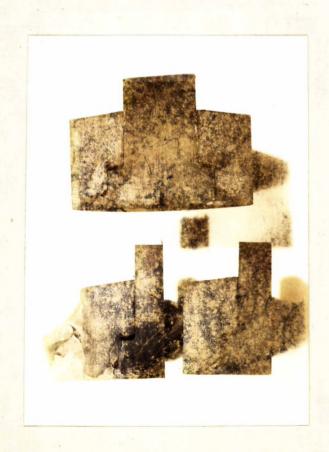
	Per cent			
Carbon (C)	179	0.31		
Manganese (Mn)	439	0.43		
Silicon (Si)	500	0.16		
Phosphorus (P)	613	0.016		
Sulphur (S)	63	0.032		
Chromium (Gr)	dio .	0.95		
Nickel (Ni)	63	3,18		
Molybdenum (Mo)	6320	None detected.		
Vanadium (V)	9	10 00		
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## Physical Properties:

(SARC)	ത് ത് മീട്ടി പ്രേയം അവരെ പ്രത്യാത്ത് കാര്യായത്ത് അവരെ പ്രത്യാത്ത് വരുന്നു. ഇത് വരുന്നു പ്രത്യായത്ത് വരുന്നു വരുന്ന		Specified	Found
	Ultimate strength, p.s.i.	<b>c</b> 3	107,000	174,800
	Yield strength, p.s.i.	000	78,000	162,000
	Elongation, per cent in 2 inches	-	22.0	16.0
	Reduction in area, per cent	co	50.0	49.5
	Izod impact, foot pounds	(2)	60.0	32.0
	Brinell hardness	120		352

<sup>0.2</sup> per cent proof stress.

# Macro-Examination of Welded Head: Figure 1.



(Macro-Examination of Welded Head, cont'd) -

A cross-sectional view of the weld is shown in Figure 1 after etching in 50 per cent hydrochloric acid for 30 minutes at 175° F. In the above photograph it will be observed that the head of the shank was not fully countersunk and also that the weld metal was porous. The fillet weld is about 1/8 inch wide, instead of \( \frac{1}{4} \) inch as specified.

## Hardness Tests:

A survey was carried out of the hardness of the weld metal, the racking bolt, and also the racking bolt head. The results obtained are given in Figure 2.

Figure 2.

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123 4 5678	No. V. H. N.
	1 187
9 10 11	2 194
	3 178
	5 354
	6 215
	7 264
	P 201
	9 167
	10 363
10.4	11 192
	No. V. H.N.
	2 270
17 1	2 270
	3 158
	4 156
	207
	7 380 1 197 9 163
	9 163
	/ / / / / /
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	No V. H. N.
6 6 7	1 354
	2 . 322
	3 274
	2 322 3 274 4 180 5 202
	7 193

VICKERS HARDNESS NUMBERS.

#### Discussion of Results:

The steel racking bolt, pontoon, was found to have the composition of an SAE 3435 steel, while the welded head consisted of a piece of cold rolled steel of SAE 1020 composition.

According to the International Nickel Company's heat-treating chart for SAE 3435 steel, one could expect to obtain the following physical properties after an oil quench from 1425° to 1475° F. at the indicated draw temperatures:

Nickel-Chromium Steel SAE 3435, Oil Quenched, (In small sizes  $\frac{1}{2}$ " to  $1\frac{1}{2}$ " diameter or thickness).

Physical Proporties		DIAW 850° F	II OOO F.
Ultimate stress, p.s.i.	æ	180,000	132,000
Yield stress, p.s.i.	43	142,000	115,000
Elongation in 2 inches, per cent	673	16.0	o, is
Reduction in area, per cent	ep	57.0	65.0
Brinell hardness	C1P	· 340	255
Izod impact, foot pounds	æ	32	65

The results obtained on the physical tests of the racking bolt indicate that the steel was drawn around 850° F. The properties of the steel are regarded as satisfactory. However, if greater impact properties are required it will be necessary to draw the steel at a higher temperature.

The fillet weld metal and the weld metal of the handle are quite porous. The amount of metal in the fillet weld is less than that specified. No brittle zones were observed in the hardness surveys of the weld and parent metals.

#### CONCLUSIONS:

The physical properties of the racking pin, although under the specified izod and elongation limits, were considered satisfactory.

The fillet weld could be improved considerably by making a 90° Vee weld instead of the 45° Vee annular weld used.

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