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# COMPUTER-DETERMINED P-NODAL SOLUTIONS <br> FOR THE LARGER EARTHQUAKES OF 1959-1962 

J. H. Hodgson and A. J. Wickens

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#### Abstract

This paper continues the Dominion Observatory program of attempting P-nodal (fault-plane) solutions for all large earthquakes. In this case the solutions have been determined for 66 of the larger earthquakes of 1959-1962 using a computer program described earlier (Wickens, Stevens and Hodgson, 1963). This program does not define the possible variation of the planes from the "best" position determined by the computer, but an attempt has been made to supply this information by inspection of the solutions.

The solutions are summarized in the tabular form established in earlier papers of the series. Résumé:-Cette étude fait partie du programme de l'Observatoire du Canada entrepris en vue de déterminer le noeud des ondes $\mathbf{P}$ (faille-surface horizontale) pour tous les principaux tremblements de terre. On a effectué ici ces déterminations pour les 66 principaux tremblements de terre enregistrés de 1959 à 1962, à l'aide d'une calculatrice décrite précédemment (Wickens, Stevens and Hodgson, 1963). La programmation ne définit pas la variation possible des plans par rapport à la "meilleure" position déterminée par la calculatrice, mais on a essayé d'introduire cette information en examinant les déterminations.

Les déterminations sont résumées sous la forme de tableaux établis dans les publications antérieures de la série.


## INTRODUCTION

For many years this Observatory has published "faultplane" solutions for all large earthquakes. These solutions have been made graphically, using data collected through questionnaires, and they represent the best fit the investigators could find to the available data. The observations have not been uniformly reliable; for many years reflected phases were used until experience proved that they were producing random observations; many stations were too insensitive or too badly located to produce reliable readings, a fact that could only be learned through experience; some stations had periods during which their galvanometers were reversed, a fact that was normally discovered only when they had produced a long series of observations inconsistent with our solutions. When these sources of error were discovered they explained much of the difficulties of the earlier work, but time never permitted the reappraisal of those earlier solutions. Even if it had been possible to re-work the corrected data, the solutions might still have been suspect because of their lack of objectivity-they merely represented the best fit that the analysist had been able to find.

One of us (Wickens) has recently perfected a program for the I.B.M. 1620 which permits a systematic search for the best position of the nodal planes for any set of data. To test the program it was given the first-motion observations for a large number of earthquakes solved earlier
by graphical methods, and its solutions were checked against the earlier graphical ones. In the re-appraisal of 74 earthquakes solved earlier by us and 64 solved earlier by Ritsema, the machine produced as good or better solutions than the graphical ones in $97 \%$ of the cases. This establishes the validity of the program. The visual solutions, on the other hand, were sustained only $72 \%$ of the time, and only $39 \%$ of the solutions were closely defined by the data.

These findings were presented to the I.U.G.G. meetings in Berkeley (Wickens, Stevens and Hodgson, 1963) and to the Symposium on the Results of the I.G.Y. which preceded it (Hodgson and Stevens, 1964). These papers, as well as several others read at the meetings, cast so much doubt on the validity and the closeness of earlier solutions that all present were agreed that some means must be found to express the accuracy of published solutions. This might be done, for example, by giving the possible variation in the strike and dip of each plane, or by giving the solid angle traced out by possible positions of the pole of each plane. Such information is implicit in the computer program and we are currently searching for the best way to express the limitation. It is probable that the program as finally written will require a faster computer than the 1620. When this enlarged program has been perfected we propose to use it to re-analyse every earthquake for which the first-motion information have ever been published, either by ourselves or by someone else.

[^0]In the meantime data are available for the earthquakes from 1959 to 1962, and many people need the solutions in conneetion with other research. Nodal solutions have therefore been determined using the existing 1620 program. It is possible that these may be modified somewhat by the more sophisticated program being devised, certainly their reliability will be expressed in a more definite way, but the present publication should be useful. The solutions are certainly not less accurate than the graphical ones published earlier in the series.

Not all stations are equally reliable, and some way must be found of expressing this fact. Kasahara (1963) suggested the use of a weighted, running average, using the formula

$$
\sigma_{t, y}=\sum_{p=1}^{6}(6-p) N_{t, h-p}^{\prime} / \sum_{p=1}^{6}(6-p) N_{t, j-p}
$$

where $\mathrm{N}_{t, j}$ and $\mathrm{N}_{t, j}^{\prime}$ denote, respectively, the total number of reading and the number of proper readings at the i -th station in the j -th year and $\sigma$ represents the probability that a station will be correct; to translate this probability into a weight, Kasahara proposed the scheme given below.

| Predicted Score | Weight |
| :---: | :---: |
|  | $\sigma \geq 0.95$ |
| $0.95>\sigma \geq 0.85$ | 5 |
| $0.85>\sigma \geq 0.75$ | 4 |
| $0.75>\sigma \geq 0.65$ | 3 |
| $0.65>\sigma \geq 0.55$ | 2 |
| $0.55>\sigma \geq 0.0$ | 1 |
|  |  |

This system of weighting was used in the early tests of Wickens' program, but experience showed that the few stations of weight 5 were overweighting other stations and distorting the solutions. We now use weight zero to express the weights 0 and 1 of Kasahara, but use weight unity for all other values. This means that stations of proven lack of reliability do not effect the solution; by carrying them along however it will be possible to detect any improvement in the station operation.

Application of the probability formula given above requires a knowledge of the performance of stations over the five years previous to the year for which weight are being computed. Machine solutions are not available for the years $1955-1958$; the scores have had to be based on the visual solutions. The weights used here may not be the same in all instances as those which will be used in the final re-appraisal forecast above.

In earlier publications it has been customary to list all the observations on which the solutions are based. In the present publication, which covers a period of four years, this would require a formidable amount of space, and seems unnecessary. All the data are available on punched cards, and a print-out will be sent to anyone who requests it.

Table I lists the earthquakes for which information is available; those for which solutions or partial solutions were obtained are listed separately from those for which no solution was possible. In the latter case an indication of the source of the difficulty has been given. Epicentral data are from the United States Coast and Geodetic Survey. In those cases where several earthquakes occurred on the same day, they have been designated A, B, C --.

TABLE I - List of Earthquakes Considered

| Date | $\stackrel{\mathrm{H}}{\text { G.M.T. }}$ | Epicentre |  | Focal <br> Depth, Km | Magnitude | Remarks |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\phi$ | $\lambda$ |  |  |  |
| Earthquakes for which solutions have not been obtained |  |  |  |  |  |  |
| January 13, 1959 | 01:15:25 | 131/2 N | 146 E | 33 | 63/4 | Too few and conflicting data. |
| February 15A, 1959 | 03:59:25 | 591/2 S | 25 W | 33 | $61 / 2$ | Too few data. |
| February 15B, 1959 | 04:42:35 | $591 / 2 \mathrm{~S}$ | 26 W | 33 | $63 / 4$ | Too few data. |
| May 12, 1959 | 09:46:51 | 231/2S | $641 / 2 \mathrm{~W}$ | 33 | 63/4 | Conflicting data. |
| July 6A, 1959 | 09:10:17 | 261/2S | 611/2 W | 600 | 63/4 | Conflicting data. |
| July 6B, 1969 | 09:23:27 | $261 / 2 \mathrm{~S}$ | $611 / 2 \mathrm{~W}$ | 600 | 63/4 | Too few and conflicting data. |
| August 17, 1959 | 21:04:40 | $71 / 2 \mathrm{~S}$ | 156 E | 33 | 71/4 | Conflicting data. |
| August 24, 1959 | 21:30:46 | $101 / 2 \mathrm{~S}$ | 161 E | 33 | 7 | Conflicting data. |
| September 7, 1959 | 04:03:20 | 1 S | 231/2 W | 33 | - | Too few data. |
| September 15, 1959 | 05:59:42 | 281/2S | 177 W | 33 | 7 | Conflict of data. See text. |
| November 16, 1959 | 10:21:17 | 1 N | 261/2 W | 33 | 61/2 | Too few and conflicting data. |
| December 14, 1959 | 23:21:56 | 591/2S | 31 W | 33 | 7 | Conflicting data. |
| January 13, 1960 | 15:40:34 | 16 S | 72 W | 200 | $71 / 2$ | Conflicting and poorly distributed data. |
| March 23, 1960 | 00:23:22 | $391 / 2 \mathrm{~N}$ | 143 E | 33 | 63/4 | Conflicting data. |
| May 22C, 1960 | 18:55:57 | 38 S | $731 / 2 \mathrm{~W}$ | 33 | $73 / 4$ | Confusion of data. |
| May 22E, 1960 | 19:11:20 | 38 S | 731/2 W | 33 | 81/2 | Too few and conflicting data. |
| May 24, 1960 | 14:46:34 | 441/2S | $1671 / 2 \mathrm{E}$ | 33 | $63 / 4$ | Conflicting data. |
| June 6, 1960 | 05:55:44 | 451/2 S | $731 / 2 \mathrm{~W}$ | 33 | 63/4 | Conflicting data, but see text. |
| June 20B, 1960 | 12:59:40 | 391/2S | 73 W | 33 | 68/4 | Conflicting data, but see text. |
| November 23, 1960 | 14:12:21 | 24.4 S | 176.1 W | 28 | 68/4 | Too few and conflicting data. |


| Date | $\underset{\text { G.M.T. }}{\text { H. }}$ | Epicentre |  | Focal Depth, Km | Magnitude | Remarks |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\phi$ | $\boldsymbol{\lambda}$ |  |  |  |
| Earthquakes for which solutions have not been obtained |  |  |  |  |  |  |
| November 24, 1960 | 06:52:41 | 24.4 S | 176.1 W | 23 | 7 | Conflicting data. |
| December 2, 1960 | 09:10:39 | 24.6 S | 69.7 W | 19 | 7 | Conflicting data. |
| December 13, 1960 | 07:36:16 | 52.7 S | 159.1 E | 25 | 7 | Too few data. |
| January 5B, 1961 | 17:57:51 | 21.2 S | 169.5 E | 53 | $63 / 4$ | Too few and conflicting data. |
| March 7, 1961 | 10:10:39 | 28.3 S | 175.7 W | 43 | $71 / 4$ | Conflicting data. |
| March 18, 1961 | 14:54:59 | 49.9 S | 163.3 E | 38 | $63 / 4$ | Too few and conflicting data. |
| September 8, 1961 | 11:26:33 | 56.3 S | 27.1 W | 125 | $73 / 4$ | Conflicting data. |
| September 13, 1961 | 21:19:20 | 41.7 S | 75.2 W | 40 | 7 | Too few data. |
| December 30, 1961 | 00:39:27 | 52.3 N | 177.6 E | 56 | 63/4 | Complete confusion of data. |
| March 12, 1962 | 11:40:13 | 8.1 N | 83.0 W | 58 | 61/2 | Conflicting data. |
| April 18, 1962 | 19:14:37 | 10.0 S | 79.0 W | 39 | $68 / 4$ | Conflicting data. |
| May 6, 1962 | 19:00:10 | 60.0 S | 32.8 W | 25 | 7 | Too few and conflicting data. |
| May 15, 1962 | 05:23:46 | 7.3 S | 128.3 E | 34 | $71 / 4$ | Conflicting data. |
| May 19, 1962 | 14:58:13 | 17.2 N | 99.5 W | 20 | 7 | Poor distribution of data. See text. |
| May 21, 1962 | 21:15:31 | 20.0 S | 177.5 W | 379 | $63 / 4$ | Conflicting data. |
| June 18, 1962 | 23:42:31 | 4.8 S | 151.8 E | 47 | 63/4 | Conflicting data. |

Earthquakes for which solutions have been obtained

| January 8, 1959 | 01:33:48 | 151/2 N | 61 W | 100 | $63 / 4$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| January 22, 1959 | 05:10:25 | 34 N | 142 E | 33 | 63/4 |  |
| February 7, 1959 | 09:36:51 | 4 S | 813/2 W | 33 | 71/4 |  |
| March 1, 1959 | 16:49:13 | 1/2S | 1341/2 E | 100 | 7 |  |
| April 24, 1959 | 17:57:58 | 31 S | 178 W | 33 | 63/4 | Undefined central circles. |
| April 26, 1959 | 20:40:38 | 25 N | $1221 / 2 \mathrm{E}$ | 150 | $71 / 2$ |  |
| April 28, 1959 | 11:09:30 | 15 N | 93 W | 33 | 61/2 | Undefined central circles. |
| May 4, 1959 | 07:15:42 | $521 / 2 \mathrm{~N}$ | 1591/2 E | 60 | 8 |  |
| May 24, 1959 | 19:17:40 | 171/2 N | 97 W | 100 | 7 |  |
| May 26, 1959 | 04:13:01 | $271 / 2 \mathrm{~N}$ | 1261/2 E | 100 | 61/2 |  |
| June 14, 1959 | 00:11:57 | 201/2 S | 68 W | 100 | 71/4 |  |
| June 18, 1959 | 15:58:38 | 54 N | 161 E | 33 | 63/4 |  |
| July 9, 1959 | 16:05:18 | 201/2S | 68 W | 100 | 63/4 | One plane only defined. Poor solution. |
| July 19, 1959 | 15:06:10 | 15 S | 701/2 W | 200 | 7 | One plane only defined. Poor solution. |
| August 15, 1959 | 08:57:04 | 23 N | 121 E | 33 | 7 | One plane only defined. Poor solution. |
| August 26, 1959 | 08:25:30 | 18 N | $941 / 2 \mathrm{~W}$ | 33 | 63/4 |  |
| September 14A, 1959 | 14:09:39 | 281/2S | 177 W | 33 | 73/4 | One plane only defined. |
| September 14B, 1959 | 22:23:53 | 29 S | 177 W | 33 | 61/2 | One plane only defined. |
| September 29, 1959 | 15:31:57 | 29 S | 1761/2 W | 33 | 6112 |  |
| October 5, 1959 | 18:27:47 | 831/2 N | 1121/2 E | 33 | 6 |  |
| January 15, 1960 | 09:30:24 | 15 S | 75 W | 150 | 7 |  |
| March 8, 1960 | 16:33:38 | $161 / 2 \mathrm{~S}$ | 1681/2 E | 250 | 7 |  |
| March 20, 1960 | 17:07:30 | 40 N | 1431/2 E | 60 | 7 |  |
| May 21, 1960 | 10:02:50 | $371 / 2 \mathrm{~S}$ | $731 / 2 \mathrm{~W}$ | 33 | 71/4 | One plane only defined. Poor solution. |
| May 22A, 1960 | 10:30:39 | 38 S | $731 / 2 \mathrm{~W}$ | 33 | $61 / 2$ | One plane only defined. Poor solution. |
| May 22B, 1960 | 10:32:43 | $371 / 2 \mathrm{~S}$ | 73 W | 33 | 71/4 | One plane only defined. Poor solution. |
| May 22D, 1960 | 19:10:47 | 38 S | $731 / 2 \mathrm{~W}$ | 33 | 71/2 | Poor solution. |
| June 20A, 1960 | 02:01:08 | 38 S | $731 / 2 \mathrm{~W}$ | 33 | 63/4 | One plane only defined. |
| June 25, 1960 | 11:12:00 | 54 N | 159 E | 100 | 63/4 | Only one plane well defined. |
| July 29, 1960 | 17:31:40 | 40.1 N | 142.3 E | 50 | 63/4 |  |
| October 7, 1960 | 15:18:31 | 7.4 S | 130.7 E | 45 | $63 / 4$ |  |
| October 22, 1960 | 08:22:01 | 10.3 S | 161.2 E | 93 | 6112 |  |
| November 13, 1960 | 09:20:37 | 51.1 N | 168.8 W | 65 | 7 | Undefined central circles. |
| December 3, 1960 | 04:24:19 ${ }^{\text {1 }}$ | 42.9 N | 104.4 E | 60 | 7 | Undefined central circles. |
| January 5A, 1961 | 15:53:56 | 4.1 S | 143.0 E | 108 | 63/4 |  |
| January 16, 1961 | 07:20:19 | 36.2 N | 141.7 E | 41 | $63 / 4$ |  |
| January 20, 1961 | 17:09:16 | 56.6 N | 152.3 W | 46 | 63/4 |  |
| February 12, 1961 | 21:53:44 | 43.9 N | 147.6 E | 45 | 7 |  |
| February 26, 1961 | 18:10:49 | 31.6 N | 131.2 E | 54 | $71 / 4$ |  |
| March 28, 1961 | 09:35:55 | 0.2 N | 123.6 E | 83 | 63/4 |  |
| June 1, 1961 | 23:29:21 | 10.4 N | 39.9 E | 33 |  | Only one plane defined. |
| June 11, 1961 | 05:10:26 | 27.9 N | 54.6 E | 37 | 61/2 |  |
| July 18, 1961 | 14:03:36 | 29.4 N | 131.6 E | 21 | 63/4 |  |
| August 11, 1961 | 15:51:35 | 43.0 N | 145.0 E | 50 | 7 |  |
| August 19A, 1961 | 05:09:50 | 10.8 S | 71.0 W | 649 | 71/4 | Only one plane clearly defined. |
| August 19B, 1961 | 05:33:31 | 36.2 N | 136.5 E | 17 | 71/2 |  |


| Date | $\begin{gathered} \text { H } \\ \text { G.M.T. } \end{gathered}$ | Epicentre |  | Focal Depth, Km | Magnitude | Remarks |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\emptyset$ | $\lambda$ |  |  |  |
| Earthquakes for which solutions have been obtained |  |  |  |  |  |  |
| August 31A, 1961 | 01:48:38 | 10.6 S | 70.9 W | 626 | 7 | Only one plane defined. |
| August 318, 1961 | 01:57:08 | 10.4 S | 70.7 W | 629 | 71/4 |  |
| September 1, 1961 | 00:09:35 | 59.5 S | 27.3 W | 131 | 71/4 | Undefined central circles. |
| February 14, 1962 | 06:36:01 | 38.15 | 73.1 W | 44 | $71 / 4$ |  |
| March 7, 1962 | 11:01:00 | 19.3 S | 145.3 E 142.3 E | 680 68 | 7 |  |
| April 12, 1962 April 23, 1962 | 00:52:47 | 38.2 N 42.9 N | 142.3 E | 68 25 | $71 / 4$ |  |
| May 7, 1962 | 17:39:50 | 45.3 N | 146.7 E | 25 | 63/4 |  |
| May 11, 1962 | 14:11:52 | 17.0 N | 99.7 W | 25 | 7 | Only one plane defined. Poor distribution of data. |
| May 21, 1962 | 12:02:51 | 37.3 N | 96.0 E | 25 | 7 | Undefined central circles. |
| July 6, 1962 | 23:05:32 | 36.6 N | 70.4 E | 203 |  | See Metzger (1963). |
| July 26, 1962 | 08:14:42 | 7.5 N | 82.7 W | 21 | 63/4 | One plane only, loosely defined. |
| July 30A, 1962 | 17:16:44 | 3.3 S | 143.9 E | 25 | 7 | Undefined central circles. |
| July 30B, 1962 | 20:18:49 | 5.0 N | 76.3 W | 45 | 68/4 |  |
| August 3, 1962 | 08:56:12 | 23.2 S | 67.5 W | 71 | 7 | Undefined central circles. |
| August 28, 1962 | 10:59:59 | 38.0 N | 23.1 E | 120 | 63/4 |  |
| September 1, 1962 | 19:20:39 | 35.6 N | 50.0 E | 21 | 71/4 |  |
| September 18, 1962 | 00:29:05 | 7.5 N | 82.3 W | 33 | 7 |  |
| December 7, 1962 | 14:03:37 | 29.2 N | 139.2 E | 411 | 7 |  |
| December 8, 1962 | 21:27:18 | 25.8 S | 63.2 W | 580 |  | Epicentre after Espinosa. |

## NATURE OF THE COMPUTER SOLUTIONS

In the computer program, observations are referred to the focal sphere, and a pair of orthogonal planes in the focus takes up a succession of trial positions. Regarding each trial position in turn as a possible position of the nodal planes, the number of "consistent" and "inconsistent" observations can be added up, and a score established for that particular trial position. In evaluating the score the theoretical radiation pattern is taken into account. Having run its entire gamut of trial positions the machine then selects the ten best of these for up-dating in the second stage of the program; here the neighbourhood of each of the ten is searched to ensure that no maximum has been overlooked in the finite increments of the searching planes.

In the final print-out the machine gives a sheet of information for each of the final ten best solutions; this defines the position of each of the nodal planes and of their line of intersection (the null direction), gives the score of the solution and lists all the stations consistent and inconsistent with it. It would be a simple matter to have the machine print out only the solution with the highest score, but it is usually necessary to examine the other possibilities as well in order to decide on the reliability of the one selected. This may best be illustrated by some examples.

The first, provided by Table II, is for the earthquake of May 24, 1959, at $17.5^{\circ} \mathrm{N}, 97^{\circ} \mathrm{W}$. The ten best solutions have been listed in order of decreasing score, with the
number of inconsistent observations given in each case. These are out of a total of 111 observations. The table gives the trend and plunge of the null vector and the direction of dip and the amount of dip for each of the two nodal planes. Azimuths are measured in degrees clockwise from north, dips in degrees from the horizontal.

Table II

| Null Direction |  | Plane A |  | Plane B |  | Number of Inconsistent Stations | Score |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Azimuth | Plunge | Azimuth | Dip | Azimuth | Dip |  |  |
| 343 | 71 | 343 | 71 | 253 | 90 | 21 | 59.10 |
| 359 | 72 | 336 | 73 | 68 | 83 | 22 | 58.99 |
| 4 | 68 | 354 | 68 | 85 | 86 | 23 | 55.58 |
| 333 | 64 | 5 | 67 | 269 | 78 | 24 | 52.90 |
| 116 | 26. | 178 | 46 | 46 | 55 | 26 | 52.00 |
| 314 | 4 | 232 | 25 | 42 | 65 | 24 | 51.69 |
| 78 | 67 | 164 | 88 | 73 | 67 | 28 | 50.90 |
| 324 | 1 | 232 | 35 | 54 | 55 | 27 | 50.71 |
| 319 | 73 | 335 | 74 | 243 | 86 | 29 | 47.97 |
| 163 | 73 | 107 | 80 | 200 | 76 | 36 | 34.62 |

Examination of the table shows that the first two possibilities have about the same score, and that they represent about the same solution; the azimuth of plane $B$ in the first instance might just as well have been written $\left(253^{\circ}-180^{\circ}\right)=73^{\circ}$. As we go away from this optimum position the score decreases steadily and the number of inconsistencies increases. Clearly this is a case of a unique, reasonably well-defined solution.

Table III

| Null Direction |  | Plane A |  | Plane B |  | Number of Inconsistent Stations | Score |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Aximuth | Plunge | Azimuth | Dip | Azimuth | Dip |  |  |
| 250 | 24 | 338 | 85 | 235 | 25 | 10 | 72.95 |
| 252 | 23 | 340 | 84 | 237 | 24 | 11 | 71.38 |
| 249 | 19 | 337 | 86 | 236 | 20 | 11 | 71.23 |
| 63 | 5 | 333 | 85 | 199 | 7 | 12 | 69.58 |
| 243 | 5 | 333 | 85 | 197 | 7 | 12 | 69.53 |
| 42 | 22 | 311 | 87 | 34 | 22 | 15 | 63.65 |
| 358 | 67 | 304 | 76 | 39 | 72 | 15 | 61.62 |
| 359 | 70 | 307 | 77 | 41 | 75 | 15 | 60.76 |
| 17 | 69 | 317 | 79 | 51 | 72 | 15 | 59.83 |
| 293 | 57 | 280 | 56 | 14 | 84 | 18 | 56.49 |

Table III gives the results for the earthquake of May 26,1959 , at $27.5^{\circ} \mathrm{N}, 126.5^{\circ} \mathrm{E}$. There were 78 observations available. In this solution plane $\mathbf{A}$ is very well defined, and the score deteriorates as the plane deviates from this best position. There is certainly a best position for plane B, that given by the best score, and this solution is supported by the next two in order. Note, however, that there follow two solutions, almost identical, with twelve inconsistent observations. This clearly represents a submaximum. Considering the fact that even the best stations are inconsistent about one time in nine, are we justified in discarding this alternative solution just because it has two more inconsistent observations than the best one? Probably not. We should list it as an alternative solution, although one with lower probability.

Table IV

| Null Direction |  | Plane A |  | Plane B |  | Number of Inconsistent Stations | Score |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Avimuth | Plunge | Azimuth | Dip | Azimuth | Dip |  |  |
| 347 | 82 | 311 | 84 | 41 | 85 | 13 | 44.64 |
| 9 | 84 | 304 | 88 | 34 | 85 | 13 | 44.25 |
| 343 | 63 | 314 | 66 | 50 | 79 | 13 | 41.66 |
| 27 | 79 | 303 | 89 | 33 | 79 | 14 | 39.04 |
| 23 | 81 | 304 | 88 | 34 | 81 | 14 | 38.87 |
| 279 | 80 | 315 | 82 | 225 | 84 | 14 | 38.17 |
| 297 | 64 | 344 | 72 | 247 | 72 | 14 | 38.16 |
| 27 | 73 | 22 | 73 | 112 | 88 | 14 | 37.48 |
| 81 | 10 | 357 | 61 | 154 | 31 | 15 | 35.10 |
| 261 | 7 | 346 | 55 | 181 | 36 | 16 | 33.83 |

The fact that even the best stations may be wrong must keep us from asserting dogmatically any solution defined by too few observations. This is illustrated by the next example which is the earthquake of January 8, 1959, at $15.5 \mathrm{~N}, 61 \mathrm{~W}$. There were 48 observations in this case; the results are given in Table IV. The first three solutions,
all yielding 13 inconsistent observations, are closely similar. Taking an average position between the extremes of the three solutions we might obtain the following values:

Null Direction

| Azimuth | Plunge |
| :---: | :---: |
| $356^{\circ} \pm 13^{\circ}$ | $73^{\circ} \pm 10^{\circ}$ |

Plane A

| Azimuth | Dip | Azimuth | Dip |
| :---: | :---: | :---: | :---: |
| $309^{\circ} \pm 5^{\circ}$ | $77^{\circ} \pm 11^{\circ}$ | $42^{\circ} \pm 8^{\circ}$ | $82^{\circ} \pm 3^{\circ}$ |

they would suggest that the solution was rather closely defined. But note that, by admitting one additional wrong station the next five best solutions are available. This would suggest the following mean positions between extremes, and the following possible variations:

$$
\begin{array}{cc}
\text { Null Direction } \\
\text { Azimuth } & \text { Plunge } \\
336^{\circ} \pm 86^{\circ} & 38^{\circ} \pm 33^{\circ}
\end{array}
$$

| Plane A |  | Plane B |  |
| :---: | :---: | :---: | :---: |
| Azimuth | Dip | Azimuth | Dip |
| $323^{\circ} \pm 20^{\circ}$ | $77^{\circ} \pm 11^{\circ}$ | $40^{\circ} \pm 20^{\circ}$ | $90^{\circ} \pm 20^{\circ}$ |

Viewed in this way the solution is much less definite.
This example illustrates another fact-the "best" position is not the mean position between all possible ones. It is arrived at on the basis of the weights of the stations, and this depends on their distance from the nodal planes and the resulting theoretical amplitude. The plus-minus obtained for the average position cannot properly be applied to the best solution, although it certainly indicates the reliability of the solution in a quantitative way. In the following section, where the results of the studies are tabulated, the best position will be given in the Table, the mean position and its possible variations will be indicated in the text.

The kind of considerations discussed in the foregoing remarks are the sort which will be treated analytically in Wickens' new program.

A final example is provided in Table V , which gives the solutions for the earthquake of April 24,1959 , at $31^{\circ} \mathrm{S}$, $178^{\circ}$ W. There were 97 observations for this shock. Here the solutions range widely, without any very large range in the scores; there is even less variation in the numbers of inconsistent observations. Clearly this is a case where there is no unique solution.

The attentive reader may think to discern some system to the solution for Plane A. The reason for this will be apparent from the plot of the data given in Figure 1. This Figure was produced by the computer, using the Byerly projection. It is produced by the normal computer print-out, not by a plotter, and suffers from the limitations

Table V

| Null Direction |  | Plane A |  | Plane B |  | Number of Inconsistent Stations | Score |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Azimuth | Plunge | Azimuth | Dip | Azimuth | Dip |  |  |
| 44 | 10 | 138 | 67 | 292 | 25 | 20 | 58.49 |
| 112 | 63 | 165 | 73 | 69 | 70 | 20 | 56.70 |
| 63 | 3 | 154 | 73 | 324 | 18 | 21 | 57.63 |
| 85 | 18 | 167 | 67 | 30 | 30 | 21 | 56.91 |
| 92 | 23 | 151 | 39 | 16 | 60 | 21 | 56.19 |
| 107 | 62 | 157 | 71 | 59 | 70 | 21 | 55.67 |
| 144 | 31 | 187 | 40 | 68 | 68 | 21 | 55.52 |
| 152 | 45 | 185 | 50 | 80 | 73 | 21 | 55.21 |
| 351 | 34 | 317 | 43 | 65 | 67 | 21 | 54.30 |
| 319 | 32 | 265 | 47 | 28 | 60 | 22 | 52.78 |

of the printer spacing; the points are only approximate and closely grouped points fall on top of each other. To overcome this, the following convention is used:

| $N$ (for negative) | represents one dilatation, |
| :--- | :--- |
| $M$ | represents two dilatations, |
| $L$ | represents three dilatations; |
| $P$ (for positive) | represents one compression, |
| $Q$ | represents two compressions, |
| $R$ | represents three compressions. |

Where a dilatation and a compression occupy the same printer position this is indicated by $O$; where there are more than three observations of any kind or a mixture of three this is indicated by $J$.


Figure 1

In Figure 1, there is a point marked " J " just south and west of the centre of the plot. This represents the superimposed values of Auckland (compression), Onerahi (compression) and Karapiro (dilatation). All the circles A in Table V (we have plotted the first one in the Table) are attempting to provide a separation of these points.

We must ask ourselves whether any one station is sufficiently reliable to warrant this degree of confidence. The situation represented in Figure 1 is one in which almost all the observations are compressional, and there are not enough observations in the epicentral area to define the dilatational circles unambiguously.

Table VI — Summary of Solutions

| EARTHQUAKE | NULL DIRECTION |  | Plane A |  | PLANE B |  | Number of Observations | Number of Inconsistent Observations | Score |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Azimuth | Plunge | Azimuth | Dip | Azimuth | Dip |  |  |  |
| January 8, 1959 | 347 | 82 | 311 | 84 | 41 | 85 | 48 | 13 (10) | 44.64 |
| January 22, 1959 | 33 | 10 | 123 | 89 | 28 | 10 | 103 | 23 (18) | 67.22 |
| February 7, 1959 | 136 | 71 | 112 | 73 | 204 | 83 | 110 | 20 (18) | 65.62 |
| March 1, 1959 | 104 | 65 | 119 | 66 | 27 | 84 | 53 | 14 (13) | 49.98 |
| April 24, 1959 | Undefined central dilatational circles |  |  |  |  |  | 97 | 20 (16) |  |
| April 26, 1959 | 294 | 11 | 342 | 16 | 206 | 78 | 200 | 24 (20) | 75.79 |
| April 28, 1959 | Undefined central dilatational circles |  |  |  |  |  | 77 | 17 (14) |  |
| May 4, 1959 Alternate solution Balakina solution S solution | $\begin{array}{r} 44 \\ 225 \\ 230 \\ 225 \end{array}$ | $\begin{array}{r} 30 \\ 1 \\ 15 \\ 3 \end{array}$ | $\begin{aligned} & 318 \\ & 315 \\ & 315 \\ & 314 \end{aligned}$ | $\begin{aligned} & 83 \\ & 83 \\ & 35 \\ & 75 \end{aligned}$ | $\begin{array}{r} 60 \\ 143 \\ 130 \\ 146 \end{array}$ | $\begin{array}{r} 31 \\ 7 \\ 50 \\ 15 \end{array}$ | $\begin{array}{r} 191 \\ 191 \\ 6 \end{array}$ | $\begin{aligned} & 30(22) \\ & 31(23) \end{aligned}$ | $\begin{aligned} & 70.25 \\ & 70.95 \end{aligned}$ |
| May 24, 1959 | 343 | 71 | 343 | 71 | 253 | 90 | 111 | 21 (15) | 59.10 |
| May 26, 1959 Alternate solution | $\begin{array}{r} 250 \\ 63 \end{array}$ | $\begin{array}{r} 24 \\ 5 \end{array}$ | $\begin{aligned} & 338 \\ & 333 \end{aligned}$ | $\begin{aligned} & 85 \\ & 85 \end{aligned}$ | $\begin{aligned} & 235 \\ & 199 \end{aligned}$ | $\begin{array}{r} 25 \\ 7 \end{array}$ | $\begin{aligned} & 78 \\ & 78 \end{aligned}$ | $\begin{aligned} & 10(8) \\ & 12(10) \end{aligned}$ | $\begin{aligned} & 72.95 \\ & 69.58 \end{aligned}$ |
| June 14, 1959 | 13 | 54 | 94 | 83 | 359 | 55 | 102 | 19 (15) | 58.01 |
| June 18, 1959 Balakina solution | $\begin{aligned} & 318 \\ & 310 \end{aligned}$ | $\begin{aligned} & 80 \\ & 70 \end{aligned}$ | $\begin{array}{r} 350 \\ 2 \end{array}$ | $\begin{aligned} & 82 \\ & 76 \end{aligned}$ | $\begin{aligned} & 260 \\ & 268 \end{aligned}$ | $\begin{aligned} & 85 \\ & 76 \end{aligned}$ | 26 | 3 (3) | 72,44 |
| July 9, 1959 | 143 | 31 | 180 | 37 | 64 | 72 | 60 | 14 (12) | 53.76 |
| July 19, 1959 | 152 | 18 | 174 | 19 | 64 | 83 | 85 | 19 (13) | 55.08 |
| August 15, 1959 |  |  | 358 | 86 |  |  | 160 | 41 (34) | 46.12 |
| August 26, 1959 <br> Alternate solution | $\begin{aligned} & 135 \\ & 116 \end{aligned}$ | $\begin{aligned} & 15 \\ & 80 \end{aligned}$ | $\begin{array}{r} 59 \\ 111 \end{array}$ | $\begin{aligned} & 48 \\ & 80 \end{aligned}$ | $\begin{aligned} & 210 \\ & 201 \end{aligned}$ | $\begin{aligned} & 48 \\ & .89 \end{aligned}$ | $\begin{aligned} & 138 \\ & 138 \end{aligned}$ | $\begin{aligned} & 25(19) \\ & 24(23) \end{aligned}$ | $\begin{aligned} & 65.24 \\ & 68.30 \end{aligned}$ |
| September 14A, 1959 |  |  | 329 | 87 |  |  | 99 | 20 (18) | 56.58 |
| September 14B, 1959 |  |  | 329 | 87 |  |  | 41 | 9 (9) | 58.71 |
| September 29, 1959 <br> Alternate solution | $\begin{aligned} & 287 \\ & 162 \end{aligned}$ | $\begin{aligned} & 89 \\ & 81 \end{aligned}$ | $\begin{aligned} & 285 \\ & 169 \end{aligned}$ | $\begin{aligned} & 89 \\ & 81 \end{aligned}$ | $\begin{aligned} & 15 \\ & 79 \end{aligned}$ | $\begin{aligned} & 90 \\ & 89 \end{aligned}$ | $\begin{aligned} & 44 \\ & 44 \end{aligned}$ | $\begin{aligned} & 11(11) \\ & 10(10) \end{aligned}$ | $\begin{aligned} & 56.73 \\ & 57.65 \end{aligned}$ |
| October 5, 1959 | 207 | 62 | 287 | 85 | 195 | 63 | 35 | 6 (5) | 60.95 |
| January 15, 1960 | 327 | 37 | 257 | 66 | 12 | 47 | 110 | 23 (17) | 60.97 |
| March 8, 1960 Alternate solution | $\begin{aligned} & 229 \\ & 239 \end{aligned}$ | $\begin{aligned} & 57 \\ & 35 \end{aligned}$ | $\begin{aligned} & 151 \\ & 165 \end{aligned}$ | $\begin{aligned} & 82 \\ & 56 \end{aligned}$ | $\begin{aligned} & 245 \\ & 307 \end{aligned}$ | $\begin{aligned} & 58 \\ & 41 \end{aligned}$ | $\begin{aligned} & 209 \\ & 209 \end{aligned}$ | $\begin{aligned} & 24(20) \\ & 21(17) \end{aligned}$ | $\begin{aligned} & 83.63 \\ & 83.00 \end{aligned}$ |
| March 20, 1960 | 351 | 2 | 261 | 84 | 62 | 6 | 172 | 36 (29) | 57.16 |
| May 21, 1960 | 189 | 20 | 274 | 76 | 151 | 25 | 135 | 24 (16) | 63.22 |
| May 22A, 1960 | 225 | 17 | 308 | 68 | 170 | 28 | 105 | 32 (26) | 40.48 |


| EARTHQUAKE | NULL DIRECTION |  | PLANE A |  | PLANE B |  | Number of Observations | Number of Inconsistent Observations | Score |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Azimuth | Plunge | Azimuth | Dip | Azimuth | Dip |  |  |  |
| May 22B, 1960 | 35 | 2 | 306 | 69 | 120 | 21 | 81 | 19 (14) | 49.78 |
| May 22D, 1960 | 328 | 71 | 267 | 81 | 360 | 74 | 53 | 17 (13) | 37.45 |
| June 20A, 1960 | 189 | 71 | 257 | 83 | 165 | 73 | 94 | 21 (16) | 55.05 |
| July 25, 1960 Alternate solution | $\begin{aligned} & 212 \\ & 145 \end{aligned}$ | $\begin{aligned} & 21 \\ & 48 \end{aligned}$ | $\begin{array}{r} 297 \\ 75 \end{array}$ | $\begin{aligned} & 78 \\ & 73 \end{aligned}$ | $\begin{aligned} & 179 \\ & 178 \end{aligned}$ | $\begin{aligned} & 25 \\ & 53 \end{aligned}$ | $\begin{aligned} & 161 \\ & 161 \end{aligned}$ | $\begin{aligned} & 29(22) \\ & 28(20) \end{aligned}$ | $\begin{aligned} & 65.06 \\ & 64.74 \end{aligned}$ |
| July 29, 1960 | 27 | 5 | 115 | 69 | 310 | 21 | 166 | 29 (23) | 64.95 |
| October 7, 1960 | 101 | 58 | 148 | 67 | 49 | 69 | 98 | 27 (23) | 41.08 |
| October 22, 1960 | 45 | 62 | 131 | 88 | 39 | 62 | 78 | 15 (15) | 58.36 |
| November 13, 1960 | Undefined central compressional circles |  |  |  |  |  | 167 | 24 (17) |  |
| December 3, 1960 | Undefined central dilatational circles |  |  |  |  |  | 123 | 24 (18) |  |
| January 5A, 1961 | 171 | 67 | 175 | 67 | 85 | 88 | 58 | 13 (10) | 51.60 |
| January 16, 1961 | 45 | 2 | 135 | 87 | 347 | 3 | 135 | 30 (24) | 57.18 |
| January 20, 1961 | 351 | 63 | 301 | 72 | 37 | 71 | 48 | 9 (7) | 63.76 |
| February 12, 1961 | 45 | 5 | 134 | 74 | 332 | 17 | 131 | 25 (18) | 64.06 |
| February 26, 1961 | 189 | 36 | 120 | 64 | 237 | 47 | 172 | 25 (19) | 71.99 |
| March 28, 1961 <br> Alternate solution | 143 | 55 | $\begin{aligned} & 121 \\ & 189 \end{aligned}$ | $\begin{aligned} & 86 \\ & 64 \end{aligned}$ | 87 | 68 | $\begin{aligned} & 121 \\ & 121 \end{aligned}$ | $\begin{aligned} & 14(10) \\ & 16 \text { (12) } \end{aligned}$ | $\begin{aligned} & 77.43 \\ & 74.36 \end{aligned}$ |
| June 1, 1961 |  |  |  |  | 246 | 84 | 46 | 14 (9) | 35.48 |
| June 11, 1961 <br> Alternate solution | $\begin{array}{r} 98 \\ 166 \end{array}$ | $\begin{aligned} & 45 \\ & 15 \end{aligned}$ | $\begin{aligned} & 149 \\ & 237 \end{aligned}$ | $\begin{aligned} & 58 \\ & 40 \end{aligned}$ | $\begin{aligned} & 39 \\ & 87 \end{aligned}$ | $\begin{aligned} & 62 \\ & 54 \end{aligned}$ | $\begin{aligned} & 65 \\ & 65 \end{aligned}$ | $\begin{aligned} & 14(11) \\ & 16(13) \end{aligned}$ | $\begin{aligned} & 53.03 \\ & 50.75 \end{aligned}$ |
| July 18, 1961 | 25 | 8 | 104 | 36 | 301 | 55 | 161 | 23 (19) | 72.47 |
| August 11, 1961 | 17 | 23 | 92 | 58 | 316 | 41 | 173 | 14 (9) | 82.67 |
| August 19A, 1961 Alternate solution | $\begin{aligned} & 109 \\ & 147 \end{aligned}$ | $\begin{aligned} & 49 \\ & 55 \end{aligned}$ | $\begin{array}{r} 87 \\ 107 \end{array}$ | $\begin{aligned} & 51 \\ & 62 \end{aligned}$ | $\begin{aligned} & 186 \\ & 208 \end{aligned}$ | $\begin{aligned} & 79 \\ & 71 \end{aligned}$ | $\begin{aligned} & 126 \\ & 126 \end{aligned}$ | $\begin{aligned} & 21 \text { (16) } \\ & 22 \text { (18) } \end{aligned}$ | $\begin{aligned} & 68.43 \\ & 66.97 \end{aligned}$ |
| August 19B, 1961 <br> Alternate solution | $\begin{aligned} & 359 \\ & 176 \end{aligned}$ | $\begin{aligned} & 13 \\ & 16 \end{aligned}$ | $\begin{array}{r} 81 \\ 115 \end{array}$ | $\begin{aligned} & 60 \\ & 31 \end{aligned}$ | $\begin{aligned} & 289 \\ & 258 \end{aligned}$ | $\begin{aligned} & 33 \\ & 64 \end{aligned}$ | $\begin{aligned} & 116 \\ & 116 \end{aligned}$ | $\begin{aligned} & 16 \text { (13) } \\ & 17 \text { (14) } \end{aligned}$ | $\begin{aligned} & 74.89 \\ & 74.60 \end{aligned}$ |
| August 31A, 1961 | 219 | 65 | 135 | 87 | 227 | 65 | 113 | 20 (14) | 66.28 |
| August 31B, 1961 |  |  | 149 | 84 |  |  | 60 | 10 (5) | 67.03 |
| September 1, 1961 | Undefined central dilatational circles |  |  |  |  |  | 85 | 18 (13) | 56.45 |
| February 14, 1962 Alternate solution | $\begin{aligned} & 351 \\ & 333 \end{aligned}$ | $\begin{aligned} & 33 \\ & 82 \end{aligned}$ | $\begin{aligned} & 317 \\ & 300 \end{aligned}$ | $\begin{aligned} & 38 \\ & 83 \end{aligned}$ | $\begin{aligned} & 70 \\ & 30 \end{aligned}$ | $\begin{aligned} & 73 \\ & 86 \end{aligned}$ | $59$ | $\begin{aligned} & 10(9) \\ & 11 \text { (9) } \end{aligned}$ | $\begin{array}{r} 65.97 \\ 61.91 \end{array}$ |
| March 7, 1962 | 135 | 9 | 218 | 54 | 57 | 38 | 142 | 29 (26) | 59.85 |
| April 12, 1962 | 229 | 5 | 139 | 87 | 260 | 6 | 116 | 22 (18) | 66.03 |
| April 23, 1962 Alternate solution | $\begin{aligned} & 239 \\ & 269 \end{aligned}$ | $\begin{array}{r} 23 \\ 17 \end{array}$ | $\begin{aligned} & 154 \\ & 358 \end{aligned}$ | $\begin{aligned} & 77 \\ & 85 \end{aligned}$ | $\begin{aligned} & 272 \\ & 252 \end{aligned}$ | $\begin{aligned} & 27 \\ & 17 \end{aligned}$ | $\begin{aligned} & 157 \\ & 157 \end{aligned}$ | $\begin{aligned} & 26(21) \\ & 27(22) \end{aligned}$ | $\begin{aligned} & 67.57 \\ & 66.63 \\ & \hline \end{aligned}$ |
| May 7, 1962 | 208 | 36 | 148 | 55 | 267 | 55 | 123 | 14 (11) | 78.69 |
| May 11, 1962 | 128 | 26 | 139 | 26 | 40 | 86 | 85 | 12 (9) | 70.91 |
| May 21, 1962 | Undefined central dilatational circles |  |  |  |  |  | 113 | 21 (17) |  |


| EARTHQUAKE | NULL DIRECTION |  | Plane A |  | PLANE B |  | Number of Observations | Number of Inconsistent Observations | Score |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Azimuth | Plunge | Azimuth | Dip | Azimuth | Dip |  |  |  |
| July 6, 1962 | 273 | 3 | 352 | 15 | 183 | 75 | 164 | 15 |  |
| July 26, 1962 |  |  |  |  | 262 | 83 | 112 | 25 (22) | 56.00 |
| July 30A, 1962 | Undefined central dilatational circles |  |  |  |  |  | 83 | 17 (16) |  |
| July 30B, 1962 | 21 | 76 | 110 | 90 | 20 | 76 | 75 | 16 (13) | 53.77 |
| August 3, 1962 | Undefined central compressional circles |  |  |  |  |  | 113 | 22 (18) |  |
| August 28, 1962 | 271 | 20 | 335 | 40 | 194 | 57 | 128 | 21 (17) | 66.89 |
| September 1, 1962 | 150 | 17 | 227 | 53 | 80 | 42. | 134 | 19 (14) | 71.71 |
| September 18, 1962 | 63 | 81 | 99 | 83 | 9 | 85 | 74 | 12 (9) | 66.67 |
| December 7, 1962 | 166 | 28 | 160 | 28 | 254 | 87 | 116 | 27 (25) | 54.00 |
| December 8, 1962 | 340 | 21 | 329 | 21 | 69 | 86 | 35 | 3 (3) | 85.49 |

## ANALYSIS OF THE DATA

The machine solutions will now be presented. The "best" solution in each case has been listed in Table VI, but each solution will be discussed to show its limitations.

Earthquake of $01: 33: 48$, Jan. 8, 1959.

$$
\varphi=15 \frac{1}{2}^{\circ} \mathrm{N}, \quad \lambda=61^{\circ} \mathrm{W}
$$

This earthquake was discussed in the previous introductory section. It was shown there that the solution is not well-defined. This is indicated by the possible variations from the mean position:

Plane A
Plane B

| Azimuth | Dip | Azimuth | Dip |
| :---: | :---: | :---: | :---: |
| $323^{\circ} \pm 20^{\circ}$ | $77^{\circ} \pm 20^{\circ}$ | $40^{\circ} \pm 20^{\circ}$ | $90^{\circ} \pm 20^{\circ}$ |

There were 13 inconsistent observations in the best solution but 3 of these came from stations with zero weight. This has been indicated in the Table by giving the number of inconsistencies as $13(10)$.

Earthquake of $05: 10: 25$, Jan. 22, 1959.

$$
\varphi=34^{\circ} \mathrm{N}, \quad \lambda=142^{\circ} \mathrm{E}
$$

Plane $\mathbf{A}$ is an essentially vertical one, for which the strike is defined within $\pm 5$. Plane $B$ is very shallow and depends for its definition on a number of near, Japanese, stations. These seem to define it exactly in the position given in Table VI, but recalling past experience with the tables of extended distances at short distances, one probably should not put too much dependence on this exact value. Certainly however, it cannot be far off.

## Earthquake of $09: 36: 51$, Feb. 7, 1959. <br> $$
\varphi=4^{\circ} \mathrm{S}, \quad \lambda=81 \frac{1}{2}^{\circ} \mathrm{W}
$$

The machine solutions cluster around the best solution as given in Table VI, but the solution is not at all closely
defined. The mean of all the solutions, and the range, is as follows:

Plane A

$$
\begin{array}{cc}
\text { Azimuth } & \text { Dip } \\
88^{\circ} \pm 24^{\circ} & 65^{\circ} \pm 15^{\circ}
\end{array}
$$

Plane B

| Azimuth | Dip |
| :---: | :---: |
| $244^{\circ} \pm 42^{\circ}$ | $62^{\circ} \pm 21^{\circ}$ |

Despite the wide range, the score is reasonably good; this simply reflects the lack of observations to control the exact position of the planes.

$$
\begin{aligned}
& \text { Earthquake of 16:49:13, March } 1,1959 . \\
& \qquad \varphi=\frac{1}{3}^{\circ} \mathrm{S}, \quad \lambda=13 \frac{1}{2}^{\circ} \mathrm{E}
\end{aligned}
$$

The first eight of the machine solutions are essentially the same as the one given in Table VI. Their spread defines the possible variation from a mean:

$$
\begin{aligned}
& \text { Plane A } \\
& \text { Plane B } \\
& \text { Earthquake of } 17: 57: 58 \text {, April 24, } 1959 . \\
& \varphi=31^{\circ} \mathrm{S}, \lambda=178^{\circ} \mathrm{W}
\end{aligned}
$$

This earthquake was discussed, as an example, in the introductory section, where it was shown to be a case in which the solution was in terms of undefined dilatational circles in the centre of the diagram. Interpreted in terms of faulting, this means thrust faulting on one of a pair of shallow, non-defined planes. Since this fact has geological significance, the earthquake has been listed as solved in Table I, although no entry can appear in Tables VI or VII.

Earthquake of $20: 40: 38$, April 26, 1959.

$$
\varphi=25^{\circ} \mathrm{N}, \quad \lambda=122 \frac{1}{2}^{\circ} \mathrm{E}
$$

This earthquake has been treated by Ritsema (1962). Using 144 observations he obtained the following solution:

| Null Direction |  | Plane A | Plane B |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Azimuth | Plunge | Azimuth | Dip | Azimuth | Dip |
| 297 | 14 | 345 | 18 | 210 | 77 |

The same 144 observations were given to the computer and the following solution was obtained:

| 287 | 14 | 333 | 20 | 200 | 76 |
| :--- | :--- | :--- | :--- | :--- | :--- |

This is a reasonably good agreement. However we must present more disquieting figures. Data had been collected for this earthquake through our normal questionnaire. 151 observations so collected yielded the following solution:

$$
\begin{array}{llllll}
217 & 42 & 155 & 68 & 266 & 54
\end{array}
$$

This is markedly different than that given by Ritsema.
We combined the data from the two sources, obtaining a total of 200 observations. The two sets of data disagreed in nine cases. Where there were disagreements we took our own observations as correct. The solution was as follows:

| 222 | 45 | 158 | 66 | 267 | 55 |
| :--- | :--- | :--- | :--- | :--- | :--- |

We then did the solution once more; where there were disagreements between the two sets of data we this time took Ritsema's observation as the correct ones. We obtained:
$294 \begin{array}{llllll} & 11 & 342 & 16 & 206 & 78\end{array}$
which is in excellent agreement with Ritsema's original solution. This solution is given in Tables VI and VII.

It seems clear from the foregoing that the solution is very sensitive to the accuracy of the data and that even a relatively few incorrect observations may distort the solution. It seems certain that Ritsema's observations, which were for the most part based on the study of the actual records, must be more accurate than our own. The implications of these facts to our program of nodal-plane determination will be discussed in a separate paper.

> Earthquake of $11: 09: 30$, April $28,1959$. $$
=15^{\circ} \mathrm{N}, \lambda=93^{\circ} \mathrm{W}
$$

This again is an earthquake in which the solution must be in terms of a pair of undefined, central, dilatational circles, representing thrust faulting on shallow, undefined planes.

> Earthquake of $07: 15: 42$, May 4, 1959. $\varphi=52 \frac{2}{2}^{\circ} \mathrm{N}, \quad \lambda=159 \frac{1}{2}^{\circ} \mathrm{E}$

In this earthquake there is complete agreement on the position of Plane A among all the solutions, but there is some vagueness about the position of Plane B. As shown in the Table there are two possibilities, one which makes the number of inconsistencies a minimum, the other which gives a maximum score. These more or less run the gamut of possibilities on Plane B.

Balakina, Shirokova and Vvedenskaya (1961) have published a solution for this earthquake; this has been given in Table VI. It will be seen that it agrees quite well with our alternative solution, particularly in regard to the dip directions of the planes; the dips do not agree so well, which probably reflects the limited distances of the stations they used. Stevens (1964) has used her program to determine the mechanism from S -wave data published by Stauder (1962). She finds a Type II mechanism to be appropriate; the directions of the intermediate force and of the nodal planes have been given in Table VI. The agreement with our alternative solution is remarkable.

Earthquake of 19:17:40, May 24, 1959.

$$
\varphi=17 \frac{1}{2}^{\circ} \mathrm{N}, \lambda=97^{\circ} \mathrm{W}
$$

This solution was discussed in the introductory section. As shown there, it is a unique, closely defined, one.

> Earthquake of 04:13:01, May 26, 1959.
> $\varphi=27 \frac{1}{2}^{\circ} \mathrm{N}, \quad \lambda=126 \frac{1}{2}^{\frac{1}{\circ}} \mathrm{E}$

This earthquake was also discussed in the introduction. It was there shown that, while there was one clearly defined plane, the second plane was less well defined and might be put in either of two positions. These alternative possibilities have been given in the Table; any position intermediate to the two is quite possible.

Earthquake of $00: 11: 57$, June 14, 1959.

$$
\varphi=20 \frac{1_{2}}{}{ }^{\circ} \mathrm{S}, \quad \lambda=68^{\circ} \mathrm{W}
$$

No other solution of the ten best came close to that given in Table VI in the number of inconsistent observations. Examination of the plot shows the following possible variations from a mean position:

Plane A

| Azimuth | Dip | Azimuth | Dip |
| ---: | :---: | ---: | :---: |
| $94^{\circ} \pm 1^{\circ}$ | $81^{\circ} \pm 2^{\circ}$ | $358^{\circ} \pm 1^{\circ}$ | $55^{\circ} \pm 2^{\circ}$ |

Thus the solution is quite close, despite the rather low score.

> Earthquake of 15:58:38, June 18, 1959. $$
\varphi=54^{\circ} \mathrm{N}, \quad \lambda=161^{\circ} \mathrm{E}
$$

There are very few data here; nevertheless Plane A is very closely defined by the observations and Plane B certainly seems to be fixed within $\pm 4^{\circ}$ both in strike and in dip. However, with so few observations one hesitates to place too much credence in the solution.

As shown in Table VI, an independent solution by Balakina et al (1961) agrees closely with the Ottawa one. On the other hand a solution by Stevens (1964), using S-data published by Stauder (1962) shows no agreement whatever.

Earthquake of $16: 05: 18$, July 9, 1959.

$$
\varphi=20 \frac{1}{2}^{\circ} \mathrm{S}, \quad \lambda=68^{\circ} \mathrm{W}
$$

For this earthquake all the solutions clustered around the value given for Plane B. There was so much variation given for Plane A however that it must be regarded as essentially undefined. The mean for this plane may be given as:

Plane A

$$
\begin{array}{cc}
\text { Azimuth } & \text { Dip } \\
242^{\circ} \pm 82^{\circ} & 52^{\circ} \pm 20^{\circ}
\end{array}
$$

Even with this limitation, the number of inconsistencies is so high and the score so low, that the solution is on the verge of being classed as a "no solution".

Earthquake of $15: 06: 10$, July 19, 1959.

$$
\varphi=15^{\circ} S, \quad \lambda=70 \frac{1^{\circ}}{}{ }^{\circ} W
$$

The solution here is almost identical with that for July 9, above. Plane B is closely limited by the data, Plane A may vary as follows:

## Plane A

$$
\begin{array}{cc}
\text { Azimuth } & \text { Dip } \\
245^{\circ} \pm 75^{\circ} & 31^{\circ} \pm 20^{\circ}
\end{array}
$$

Again, the solution is on the verge of "no solution".

## Earthquake of $08: 57: 04$, August 15, 1959. $\varphi=23^{\circ} \mathrm{N}, \lambda=121^{\circ} \mathrm{E}$

All the computer solutions agree on an almost vertical plane striking approximately EW, but it is not possible to give any definite position for the second plane. Possible variations are as follows:

Plane A
Plane B

| Azimuth | Dip | Azimuth | Dip |
| :---: | :---: | :---: | :---: |
| $362^{\circ} \pm 5^{\circ}$ | $86^{\circ} \pm 5^{\circ}$ | $182^{\circ} \pm 90^{\circ}$ | $20^{\circ} \pm 20^{\circ}$ |

Earthquake of 08:25:30, August 26, 1959.
$\varphi=18^{\circ} \mathrm{N}, \lambda=94 \frac{1}{2}^{\circ} \mathrm{W}$
There are two possible solutions for this earthquake, one in terms of large circles (which on a fault interpretation would correspond to strike-slip faulting) the other in terms of small dilatational circles drawn in the central area (which would correspond to thrust faulting). While the former has the higher score, the latter has the fewer "weighted" inconsistencies and seems preferable.

Whatever the relative merits of the two solutions, each is exactly limited by the data.

> Earthquakes of $14: 09: 39$ and $22: 23: 53$,
> September $14,1959$.
> $\varphi=28 \frac{1}{2}^{\circ} \mathrm{S}, \quad \lambda=177^{\circ} \mathrm{W}$

These earthquakes might have been listed among the "no solutions" except that one plane, the same in each earthquake, was consistently defined. This plane has been listed in its mean position in Table VI. It varies from this mean position by $\pm 15^{\circ}$ in azimuth, $\pm 2^{\circ}$ in dip.

The later aftershock of $05: 59: 42$, September 15, was also considered. There was too great a confusion of data to justify publication of even a partial solution, but it may be worth reporting that the best machine solution gave an azimuth direction of $303^{\circ}$ and a dip of $88^{\circ}$, very similar to the two earlier shocks.

Earthquake of $15: 31: 57$, September 29, 1959.

$$
\varphi=29^{\circ} \mathrm{S}, \quad \lambda=176 \frac{1}{2}^{\circ} \mathrm{W}
$$

This earthquake may probably be regarded as an aftershock in the series just considered. There are two possible solutions suggested by the computer. They have been listed in Table VI. Note that the first of these gives, for Plane A, a solution closely related to the ones found earlier in the series. However, this is probably without significance, since the earlier solutions would not have tolerated a second plane with the steep dip found here.

Both of the possible solutions are closely limited by the data, but these are not numerous. The solutions should not be depended on too strongly.

> Earthquake of $18: 27: 47$, October $5,1959$. $\varphi=83 \frac{1}{2}^{\circ} \mathrm{N}, \quad \lambda=1125^{\circ} \mathrm{E}$

Despite the small number of observations for this Arctic earthquake the solution given in the table scored 3.5 points higher than its nearest rival. This suggests a rather strong solution. It is not a tight solution however; Plane B is exactly defined by the data, but Plane A may best be given as:

$$
\begin{array}{cc}
\text { Azimuth } & \text { Dip } \\
297 \pm 10^{\circ} & 74^{\circ} \pm 11^{\circ}
\end{array}
$$

Earthquake of $09: 30: 24$, January 15, 1960.

$$
\varphi=15^{\circ} \mathrm{S}, \quad \lambda=75^{\circ} \mathrm{W}
$$

The computer solutions are reasonably well clustered around the "best" solution given in Table VI; however, the data do not define the positions of the planes very closely. The mean position, and variations from this mean, may be expressed as follows:

## Plane A

Plane B

| Azimuth | Dip | Azimuth | Dip |
| :---: | :---: | :---: | :---: |
| $239^{\circ} \pm 25^{\circ}$ | $55^{\circ} \pm 15^{\circ}$ | $6^{\circ} \pm 6^{\circ}$ | $50^{\circ} \pm 4^{\circ}$ |

Even with these limitations the circles cannot be regarded as well-defined; the one circle lies in the Pacific, the other in South America, and there are too few stations in these areas.

> Earthquake of $16: 33: 38$, March $8,1960$. $\varphi=16 \frac{2}{2}^{\circ} \mathrm{S}, \quad \lambda=168 \frac{1}{2}^{\frac{1}{\circ}} \mathrm{E}$

The observations for this earthquake are almost entirely dilatational; the only consistent groups of compressions come from the New Zealand stations and from Rabaul. There are two ways of satisfying these data, and they
have been listed as alternative solutions in Table VI. Each solution is closely defined by the data, but there is not much basis for selecting between them.

$$
\begin{aligned}
& \text { Earthquake of } 17: 07: 30, \text { March } 20,1960 . \\
& \varphi=40^{\circ} \mathrm{N}, \quad \lambda=143 \frac{1}{2}^{\circ} \mathrm{E}
\end{aligned}
$$

There was very good clustering of the machine solutions about the value given in Table VI, and the number of inconsistencies increased very rapidly as the values departed from the "best" position. However, inconsistent observations tended to occur in groups, rather than dispersed throughout the diagram, a phenomenon which is always disquieting. The solution given in the table was exactly limited by the data.

## Chilean Earthquakes of May, 1960.

A questionnaire was circulated in June, 1960, seeking first-motion information on six of the earthquakes of this series. An attempt was made to solve the resulting diagrams graphically, but because of confusion of data and because of scarcity of observations in the Pacific and in South America no solutions emerged in which one could have confidence. A number of later aftershocks of the Chilean series were included in the general questionnaire for the years 1959-60; again there was much difficulty in making a pattern from the observations.

However, when the data are fed to the computer a pattern, consistent over the entire series, appears to emerge. This pattern bears considerable resemblance to that established on other grounds and seems to justify the publication of the results, even though they are not well defined. The entire Chilean series will be considered here.
May 21, 1960; 10:02:50

The solution given in Table VI is the computer solution with the highest score. Plane B, given in the Table in its "best" position is in fact almost undefined; the average direction of the dip azimuth is $118^{\circ} \pm 63^{\circ}$, and the average dip is $45^{\circ} \pm 25^{\circ}$. Plane A on the other hand was found repeatedly by the computer in about the position given in the Table, and while the observations defining it are not numerous they lie close enough to limit it within $\pm 2^{\circ}$ in both strike and dip.
St. Amand (1961), from the study of aftershocks has postulated a fault striking $\mathrm{N} 9^{\circ} \mathrm{E}$. Plane A of the computer solution strikes about $\mathrm{N} 4^{\circ} \mathrm{E}$. If the nodal diagram is interpreted in terms of faulting and if Plane A is taken as the fault, the strike direction agrees very well with St. Amand's; the plane dips steeply to the west. Because the second plane is not well defined we can only say that the faulting is thrust with a possible left-lateral component which might be very large. This disagrees both with the findings of St . Amand and with the findings of Aki which he reports; they find the lateral displacement to be right-lateral.

## May 22A, 1960; 10:30:39

As will be seen from Table VI, this solution is quite similar to that given above; Plane A is striking rather more east of north. Again Plane A is closely limited by the data, within $\pm 6^{\circ}$ in azimuth and $\pm 3^{\circ}$ in dip. Again Plane B is almost undefined; the mean azimuth direction is $161^{\circ}$ $\pm 52^{\circ}$, the mean dip is $46^{\circ} \pm 22^{\circ}$. Again, interpreted in terms of faulting, the faulting is thrust with a possible strong left-lateral movement.

## May 22B, 1960; 10:32:43

This solution is so poorly defined that it would have been listed among the "no solutions" except for the similarity it bears to the earlier ones in the sequence. The mean azimuth of Plane $A$ is $300^{\circ} \pm 50^{\circ}$ the mean dip $52^{\circ} \pm 17^{\circ}$. Plane B is still less well defined than usual; it may vary from a dip azimuth of 47 , dip 62 (taken with A as a fault this would indicate right-lateral strike-slip faulting), through an azimuth of 126, dip 21 (indicating pure thrust faulting) to an azimuth of 205, dip of 68 (giving left-lateral strike-slip faulting).

## May 22C, 1960; 18:55:57

No solution was possible in this earthquake. The ten different computer solutions all had the same number of inconsistent observations and made about the same score, but they were all completely different.

May 22D, 1960; 19:10:47
The computer found only one possible solution for this earthquake; while the number of inconsistencies is high and the score low the solution is closely limited by the data and one must accept it almost exactly as given in the table, or discard it completely. Again there is a northsouth striking plane; regarding this as the fault, a faultinterpretation would insist on left-lateral movement.

## May 22E, 1960; 19:11:20

Again the computer did not suggest any unique solution for this earthquake.

> June 6, 1960; 05:55:44

The data for this earthquake were very confused, and no reliable solution can be given. Nevertheless it may be worth reporting that the solution which made the minimum number of inconsistent observations had a plane with dip azimuth of $276^{\circ}$ and dip of $82^{\circ}$; this is very similar to the north-south striking plane characteristic of the series.

> June 20A, 1960; 02:01:08

Plane A is closely limited by the data, but Plane B is not well defined. It can vary from the position shown in
the Table, to a position tangential to the large circle. That is to say, the mean azimuth of dip is $121^{\circ} \pm 44^{\circ}$ and the mean dip is $40^{\circ} \pm 33^{\circ}$. The similarity of this solution to the earlier ones in the series is remarkable.

June 20B, 1960; 12:59:40
There were several widely differing solutions for this earthquake, all with the same number of inconsistent observations. There was no basis for selecting any particular one. However, one of the possibilities was for a plane with a dip direction of $273^{\circ}$, a dip of $76^{\circ}$, closely analagous to the pattern for the other earthquakes of the series. Another equally plausible solution would be in terms of two undefined dilatational circles drawn in the central region; this would correspond to thrust faulting on a plane of undefined direction.
In summary, none of the Chilean earthquakes has yielded a well-defined solution, but most of them have suggested a plane striking approximately north-south and dipping steeply to the west. The mean strike of the plane, as determined by the several nodal-plane solution, is $\mathrm{N} 10^{\circ} \mathrm{E}$ which agrees almost exactly with the over-all fault direction suggested by St . Amand; it is this agreement which has led to the decision to publish the solutions despite their low scores. As has already been pointed out, most of the solutions, interpreted in terms of faulting on a north-south plane, require either thrust or left-lateral movement. The lateral sense does not agree with St . Amand.

Earthquake of 11:12:00, July 25, 1960.

$$
\varphi=54^{\circ} \mathrm{N}, \quad \lambda=159^{\circ} \mathbf{E}
$$

It will be seen from Table VI that the computer has suggested two alternative solutions for this earthquake. In the first, Plane A is closely limited although by only two points, but Plane B may have the following range of variations:

| Azimuth | Dip |
| :---: | :---: |
| 40 | 51 |
| 117 | 12 |
| 194 | 46 |

The middle position is for the circle tangential to Plane A, and the listing indicates that the plane may vary throughout the entire range.

In the second solution Plane A is again closely limited, but again by only two observations. Plane B is again undefined and may have the following range:

| Azimuth | Dip |
| :---: | :---: |
| 178 | 53 |
| 255 | 15 |
| 332 | 56 |

the middle observation again indicates the tangential position for the circle.
It was mentioned in the case of both possible solutions that Plane A was held by very few observations. It should also be noticed that the two planes are not drastically different; in the first solution Plane A strikes $\mathrm{N} 27^{\circ}$ E and dips steeply to the west, in the second it strikes $\mathrm{N} 15^{\circ} \mathrm{W}$ and dips steeply to the east. If we admit that two stations are not enough to limit a plane beyond question, then we might take the mean of the two positions of Plane A. This would be a plane striking $\mathrm{N} 6^{\circ} \pm 20^{\circ}$ E and dipping at $90^{\circ} \pm 15^{\circ}$. With this mean position Plane A would have the following gamut:

| Azimuth | Dip |
| :---: | :---: |
| 6 | 54 |
| - | 0 |
| 186 | 47 |

$$
\begin{aligned}
& \text { Earthquake of } 17: 31: 40 \text {, July 29, } 1960 . \\
& \varphi=40.1^{\circ} \mathrm{N}, \lambda=142.3^{\circ} \mathrm{E}
\end{aligned}
$$

The solution given in the table is closely defined by the data; although there is some confusion in the Japanese stations, probably reflecting errors in the extended distance tables at short distances, the position of the planes cannot be much in doubt.

## Earthquake of 15:18:31, October 7, 1960. $\varphi=7.4^{\circ} \mathrm{S}, \lambda=130.7^{\circ} \mathrm{E}$

The score for this solution is low, and the number of inconsistencies is higher than normal, but the computer gives a unique solution. The best position for this is given in Table VI; the mean position may be expressed as follows:

Plane A
Plane B

| Azimuth | Dip | Azimuth | Dip |
| :---: | :---: | :---: | :---: |
| $150^{\circ} \pm 2^{\circ}$ | $62^{\circ} \pm 5^{\circ}$ | $48^{\circ} \pm 1^{\circ}$ | $67^{\circ} \pm 2^{\circ}$ |
| Earthquake of 08:22:01, October 22, 1960. |  |  |  |

In this earthquake Plane $\mathbf{A}$ is defined within a very few degrees, both in strike and dip, but Plane B is not well defined. In its mean position it may be described as follows:

$$
\begin{array}{lc}
\text { Azimuth } & \text { Dip } \\
39^{\circ} \pm 0^{\circ} & 34^{\circ} \pm 34^{\circ}
\end{array}
$$

Earthquake of $09: 20: 37$, November 13, 1960 . $\varphi=51.1^{\circ} \mathrm{N}, \lambda=168.8^{\circ} \mathrm{W}$
In this case the computer found a number of equally good solutions, all representing compressional circles drawn in the central area of the diagram. This indicates the lack of control in the epicentral area. In a fault interpretation normal faulting on an undefined plane would be indicated.

Earthquake of 04:24:19, December 3, 1960.

$$
\varphi=42.9^{\circ} \mathrm{N}, \lambda=104.4^{\circ} \mathrm{E}
$$

This solution was in terms of a number of equally valid but loosely defined dilatational circles drawn in the central area of the diagram. On a fault interpretation these would represent thrust faulting, on an undefined, shallow-dipping plane.

$$
\begin{aligned}
& \text { Earthquake of } 15: 53: 56, \text { January } 5,1961 . \\
& \varphi=4.1^{\circ} \mathrm{S}, \lambda=143.0^{\circ} \mathrm{E}
\end{aligned}
$$

This solution is reasonably well-defined in terms of a vertical plane striking north-south, and a second plane striking east-west and dipping steeply to the south. Limits from the mean positions are as follows:

\[

\]

Earthquake of $07: 20: 19$, January 16, 1961. $\varphi=36.2^{\circ} \mathrm{N}, \lambda=141.7^{\circ} \mathrm{E}$

The solution given in the Table provides the best score of a number of approximately similar ones. All of these solutions involve one steeply dipping plane, with a second very shallow one. The mean position may be expressed:

| Plane A | Plane B |  |
| :---: | :---: | :---: |
| Azimuth | Dip | Azimuth $\quad$ Dip |
| $135^{\circ} \pm 10^{\circ}$ | $90^{\circ} \pm 3^{\circ} \quad 358^{\circ} \pm 33^{\circ}$ | $0^{\circ} \pm 3^{\circ}$ |
| Earthquake of $17: 09: 16, ~ J a n u a r y ~ 20, ~$ | 1961. |  |

In spite of the small number of observations for this solution, the planes are defined almost exactly in the position given in the table. Even slight deviation from the listed position increased the number of inconsistent observations.

> Earthquake of $21: 53: 44$, February 12, 1961. $$
\varphi=43.9^{\circ} \mathrm{N}, \quad \lambda 147.6^{\circ} \mathrm{E}
$$

Most of the observations in this earthquake were compressional and it was only in the central area that there were consistent dilatations. By good fortune they suffice to define the circles in the positions given in Table VI. Any deviation from the listed position results in increased numbers of inconsistent observations.

> Earthquake of $18: 10: 49$, February $26,1961$. $$
\varphi=31.6^{\circ} \mathrm{N}, \quad \lambda=131.2^{\circ} \mathrm{E}
$$

The solution given in the Table is almost exactly defined; a variation of even one degree in either the strike or dip of either plane results in a substantial increase in the numbers of inconsistent observations.

## Earthquake of 09:35:55, March 28, 1961. $\varphi=0.2^{\circ} \mathrm{N}, \lambda=123.6^{\circ} \mathrm{E}$

There are two possible solutions suggested for this earthquake; because of lack of points in the epicentral area neither is well defined.

The first is in terms of an approximately vertical plane striking north-east; the strike of this plane might vary $\pm 3^{\circ}$ and the dip $\pm 2^{\circ}$. The second plane is not defined at all; treating the defined plane as a fault, the second circle might be drawn to define anything between strong left lateral and strong right lateral motion, including thrust faulting as an intermediate position.

The alternative solution, which has a poorer score, is somewhat better defined. The mean positions of the planes may be given as

Plane A

## Plane B

| Azimuth | Dip | Azimuth | Dip |
| :---: | :---: | :---: | :---: |
| $189^{\circ} \pm 10^{\circ}$ | $68^{\circ} \pm 5^{\circ}$ | $75^{\circ} \pm 15^{\circ}$ | $55^{\circ} \pm 15^{\circ}$ |

Earthquake of $23: 29: 21$, June 1, 1961. $\varphi=10.4^{\circ} \mathrm{N}, \lambda=39.9^{\circ} \mathrm{E}$

Only one plane can be defined in this earthquake, and even with this limitation the score is very poor. For the one plane defined the dip azimuth has a mean position of $230^{\circ} \pm 15^{\circ}$, and its dip a mean value of $90^{\circ} \pm 5^{\circ}$. If this plane were treated as a fault, the second circle could be drawn to indicate anything between mildly rightlateral to mildly left-lateral faulting, including an intermediate position indicating normal faulting.

## Earthquake of 05:10:26, June 11, 1961. $\varphi=27.9^{\circ} \mathrm{N}, \lambda=54.6^{\circ} \mathrm{E}$

Two solutions have been suggested for this earthquake. The preferred solution, listed first in Table VI, is exactly limited by the data. The second solution is less clearly defined. For it:

Plane A
Plane B

| Azimuth | Dip | Azimuth |  |
| :---: | :---: | :---: | :---: |
| $220^{\circ} \pm 20^{\circ}$ | $50^{\circ} \pm 10^{\circ}$ | $87^{\circ} \pm 1^{\circ}$ | $54^{\circ} \pm 2^{\circ}$ |
| Earthquake of 14:03:36, July 18, 1961.$\varphi=29.4^{\circ} \mathrm{N}, \quad \lambda=131.6^{\circ} \mathrm{E}$ |  |  |  |

The solution given in the table is very well defined; the possible variations in the strike are not more than $5^{\circ}$ for either plane; for the dips not more than $1^{\circ}$ could be tolerated.

## Earthquake of 15:51:35, August 11, 1961. <br> $$
\varphi=43.0^{\circ} \mathrm{N}, \quad \lambda=145.0^{\circ} \mathrm{E}
$$

The ten best solutions printed out by the computer were all variations on the solution given in the table. Even slight deviation from the published position resulted
in decreased score; the mean position and the most variation which could be considered is as follows:

> Plane A
> Plane B

Two alternative solutions have been given for this earthquake, but these are in fact variations on the same solution and reflect the fact that there are not enough observations in the epicentral zone to define the planes very accurately. One thing that is clear is that the solution demands a plane striking roughly east-west and dipping steeply to the south; its mean position is:

| Azimuth | Dip |
| :---: | :---: |
| $200^{\circ} \pm 15^{\circ}$ | $75^{\circ} \pm 5^{\circ}$ |

The second plane is not really defined. While the evidence all points to a circle about as follows:

$$
\begin{array}{cc}
\text { Azimuth } & \text { Dip } \\
85^{\circ} \pm 22^{\circ} & 45^{\circ} \pm 20^{\circ}
\end{array}
$$

the data are not conclusive. A dip azimuth ranging out to $290^{\circ}$ cannot be positively excluded.

Earthquake of 05:33:31, August 19B, 1961.

$$
\varphi=36.2^{\circ} \mathrm{N}, \quad \lambda=136.5^{\circ} \mathrm{E}
$$

Again two alternate solutions have been given; it will be seen that they represent, in each case, a pair of dilatational circles drawn in the central area of the map, each with an approximately north-south strike. They represent two extremes which fit the data, but any pair of planes between would do as well. In terms of a fault interpretation we would say that foulting was thrust on a north-south striking plane of indeterminate dip.

$$
\begin{aligned}
& \text { Earthquake of } 01: 48: 38 \text {, August 31A, } 1961 . \\
& \varphi=10.6^{\circ} \mathrm{S}, \quad \lambda=70.9^{\circ} \mathrm{W}
\end{aligned}
$$

The epicentre of this earthquake is very close to that of August 19A, and the solution is rather similar. Only one plane is unambiguously defined, an almost vertical one striking somewhat north of east. Its mean position is:

$$
\begin{array}{cc}
\text { Azimuth } & \text { Dip } \\
144^{\circ} \pm 10^{\circ} & 90^{\circ} \pm 2^{\circ}
\end{array}
$$

The second plane has been given in the table in the best position found by the computer, but there is only one point holding it there; if this point is wrong, then there is no control whatever on the position of the plane.

> Earthquake of $01: 57: 08$, August $31 \mathrm{~B}, 1961$. $\varphi=10.4^{\circ} \mathrm{S}, \quad \lambda=70.7^{\circ} \mathrm{W}$

Again we have a solution in which only one plane can be defined. The mean position of the plane is:

$$
\begin{array}{cc}
\text { Azimuth } & \text { Dip } \\
140^{\circ} \pm 10^{\circ} & 83^{\circ} \pm 2^{\circ}
\end{array}
$$

The similarity to the earthquakes with similar epicentres, of August 19A and August 31A will be noted.

Earthquake of $00: 09: 35$, September 1, 1961. $\varphi=59.5^{\circ} \mathrm{S}, \quad \lambda=27.3^{\circ} \mathrm{W}$

There are too few stations in the epicentral area to permit the definition of the circles in this earthquake; we can say only "undefined central dilatational circles".

> Earthquake of 06:36:01, February $14,1962$. $\varphi=38.1^{\circ} \mathrm{S}, \quad \lambda=73.1^{\circ} \mathrm{W}$

There are two possible solutions for this earthquake, each making the same number of weighted stations wrong. In the first solution listed in Table VI, plane B is exactly defined by the data, plane $A$ is almost undefined. It may range from one extreme position: Azimuth $166^{\circ}$, Dip $66^{\circ}$; through a mean position: Azimuth $250^{\circ}$, Dip $17^{\circ}$; to the other extreme: Azimuth $329^{\circ}$, Dip $56^{\circ}$.

In the alternative position the planes are limited within $1^{\circ}$.

## Earthquake of $11: 01: 00$, March 7, 1962. $\varphi=19.3^{\circ} \mathrm{S}, \quad \lambda=145.3^{\circ} \mathrm{E}$

There can be no doubt that this solution is in terms of central compressional circles, and any deviation from the position given in the Table results in a greatly increased number of inconsistent observations. However, a disquieting number of inconsistent observations (12) came from stations in the central area of the map. This undoubtedly reflects the errors of the tables of extended distance at short epicentral distances, but must warn against a too exact acceptance of the results.

$$
\begin{aligned}
& \text { Earthquake of } 00: 52: 47 \text {, April 12, } 1962 .
\end{aligned} \qquad
$$

This solution is in terms of one well-defined vertical plane striking $\mathrm{N} 49^{\circ} \mathrm{E}$; both the strike and dip are defined within $3^{\circ}$. The second plane is almost tangent to the earth and therefore is not very well defined. It might vary both in strike and dip by as much as $10^{\circ}$ from the position given in Table VI.

> Earthquake of $05: 58: 05$, April 23, 1962. $$
=42.9^{\circ} \mathrm{N}, \lambda=143.4^{\circ} \mathrm{E}
$$

Alternative solution have been given in Table VI, but they do not differ vey much; they might be regarded as the two extremes on a mean position of the solution. This would be given as:

| Plane A |  | Plane B |  |
| :---: | :---: | :---: | :---: |
| Azimuth | Dip | Azimuth |  | Dip 0

Earthquake of $17: 39: 50$, May $^{7}$, 1962.

$$
\varphi=45.3^{\circ} \mathrm{N}, \lambda=146.7^{\circ} \mathrm{E}
$$

This solution is in terms of central dilatational circles; fortunately there are enough observations close to the epicentre to define these reasonably well. In their mean positions, the planes given in Table VI assume the positions:

Plane A

$$
\begin{array}{cc}
\text { Azimuth } & \text { Dip } \\
153^{\circ} \pm 3^{\circ} & 53^{\circ} \pm 2^{\circ}
\end{array}
$$

Earthquake of $14: 11: 52$, May 11, 1962.
$\varphi=17.0^{\circ} \mathrm{N}, \lambda=99.7^{\circ} \mathrm{W}$
The score for this solution, as shown in Table VI, is quite high, and the number of inconsistent observations is low. Nevertheless the solution is not a very dependable
one, because of the poor distribution of observations. This will be apparent from Figure 2. Plane B represents a plane which runs along roughly parallel to the coast of North America; the stations on the continental side of this plane received initial compressions, but there are too few observations on the Pacific side of the plane to convince us that the plane might not dip in the other direction. Plane A is essentially undefined, although it is constrained by the data to shallow dips. It may range between the extremes, and through the mean position, shown below:

| Plane A |  | Plane B |  |
| :---: | ---: | :---: | :---: |
| Azimuth | Dip | Azimuth | Dip |
| $134^{\circ}$ | $46^{\circ}$ |  |  |
| $220^{\circ}$ | $4^{\circ}$ | $40^{\circ} \pm 2^{\circ}$ | $86^{\circ} \pm 4^{\circ}$ |
| $302^{\circ}$ | $35^{\circ}$ |  |  |



Figure 2

A somewhat analogous problem was created by the earthquake of May 19 ( $14: 58: 13$ ), which had about the same epicentre. The computer solution for this earthquake is shown in Figure 3. It is clear that there is really no control on the Pacific side of the large circle; the solution has been listed among the "no solutions".

Earthquake of 12:02:51, May 21, 1962.

$$
\varphi=37.3^{\circ} \mathrm{N}, \lambda=96.0^{\circ} \mathrm{E}
$$

Almost all the observations in this earthquake are compressional, and the solution must be in terms of small, central, dilatational circles. Unfortunately these are undefined by the data.

Earthquake of 23:05:32, July 6, 1962.
$\varphi=36.6^{\circ} \mathrm{N}, \lambda=70.4^{\circ} \mathrm{E}$
$\varphi=36.6^{\circ} \mathrm{N}, \lambda=70.4^{\circ} \mathrm{E}$
This solution has been given by Metzger (1963) but the results have been included here for the sake of completeness. The best computer position has been shown in Table VI. The mean position and possible variation is as follows:

| Plane A |  | Plane B |  |
| :---: | :---: | :---: | :---: |
| Azimuth | Dip | Azumith | Dip |
| $7^{\circ} \pm 55^{\circ}$ | $15^{\circ} \pm 7^{\circ}$ | $187^{\circ} \pm 5^{\circ}$ | $75^{\circ} \pm 7^{\circ}$ |

## Earthquake of 08:14:42, July 26, 1962.

$\varphi=7.5^{\circ} \mathrm{N}, \lambda=82.7^{\circ} \mathrm{W}$
This earthquake would have been listed with the "no solution" ones except for the similarity of the pattern to


Figure 3
those in the Mexican earthquakes of May 11 and May 21. In those earthquakes the one defined plane ran parallel to the edge of the continent and was poorly defined because of the scarcity of the data on the Pacific side. In the present earthquake there is a similarly oriented plane suggested by all the machine solutions, except that in this case there is disagreement and confusion in the coastal stations so that the position cannot be given better than:

$$
\begin{array}{cc}
\text { Azimuth } & \text { Dip } \\
255^{\circ} \pm 7^{\circ} & 81^{\circ} \pm 2^{\circ}
\end{array}
$$

$$
\begin{aligned}
& \text { Earthquake of } 17: 16: 44, \text { July 30A, } 1962 . \\
& \qquad \varphi=3.3^{\circ} \mathrm{S}, \lambda=143.9^{\circ} \mathrm{E}
\end{aligned}
$$

Most of the observations in this earthquake were compressional and the best solution is probably in terms of undefined, central dilatational circles.

$$
\begin{aligned}
& \text { Earthquake of } 20: 18: 49 \text {, July } 30 \mathrm{~B}, 1962 . \\
& \qquad \varphi=5.0^{\circ} \mathrm{N}, \lambda=76.3^{\circ} \mathrm{W}
\end{aligned}
$$

Plane A in this solution is almost exactly defined by the data. Plane B is held in the position given in Table VI by only one point; if we were to ignore that point the plane might increase in dip to about $80^{\circ}$. It could not decrease.

$$
\begin{gathered}
\text { Earthquake of 08:56:12, August } 3,1962 . \\
\varphi=23.2^{\circ} \mathrm{S}, \lambda=67.5^{\circ} \mathrm{W}
\end{gathered}
$$

The only possible solution for this earthquake is in terms of central compressional circles. The data near the epicentre are not sufficient to define them.

$$
\begin{aligned}
& \text { Earthquake of } 10: 59: 59 \text {, August } 28,1962 . \\
& \varphi=38.0^{\circ} \mathrm{N}, \lambda=23.1^{\circ} \mathrm{E}
\end{aligned}
$$

The solution given for this earthquake in Table VI is almost exactly defined by the data.

## Earthquake of $19: 20: 39$, September 1, 1962. $\varphi=35.6^{\circ} \mathrm{N}, \lambda=50.0^{\circ} \mathrm{E}$

Most of the first-motion observations for this earthquake are compressional, and they crowd in so close to the epicentre that it is impossible to draw a pair of dilatational circles in the epicentral area; either one must make a number of observations inconsistent or one must ignore the orthogonality criterion.

The solution given in Tables VI and VII chooses the former alternative, making four observations in the epicentral area inconsistent. It had occurred to us that these near stations might have recorded a small foreshock but there is no evidence of this from the travel times. The case should be remembered as one in which a pair of orthogonal planes were not the best solution to the data.

Earthquake of $00: 29: 05$, September 18, 1962.

$$
\varphi=7.5^{\circ} \mathrm{N}, \lambda=82.3^{\circ} \mathrm{W}
$$

Both planes given in Table VI for the solution of this earthquake are defined within about $\pm 2^{\circ}$ in both strike and dip by the data.

## Earthquake of 14:03:37, December 7, 1962. $\varphi=29.2^{\circ} \mathrm{N}, \lambda=139.2^{\circ} \mathrm{E}$

The percentage of inconsistent observations in this solution is rather high, but some solution very like this must be the correct one. The more steeply dipping plane effectively divides the map into two zones, one predominately compressional, the other dilatational. The second plane is also reasonably well substantiated.

If the solution is accepted, then the possible variation on the positions of the planes is very small.

## Earthquake of $21: 27: 18$, December 8, 1962. $\varphi=25.8^{\circ} \mathrm{S}, \lambda=63.2^{\circ} \mathrm{W}$

Espinosa is making a study of this earthquake and has collected data on first motion from 35 stations. He kindly supplied this to us for the purposes of a nodal solution. Plane B given in Table VI is exactly defined by the data; Plane A is less well defined. The dip might increase to $40^{\circ}$, with a corresponding variation in azimuth.

## SUMMARY

Since it is hoped that the present solutions will shortly be re-worked in the more elaborate program being prepared, we postpone discussion of the results. However, the solutions are summarized in Table VII in the form established in earlier papers of the series.

## ACKNOWLEDGEMENTS

We have been assisted by a number of people in the collection of first motion data and in its preparation for the program. To these assitants-Marlene Metzger, Peter Hodgson, Eden Windish and Bruce Compton-we express our thanks.

We are also grateful to those many station operators who, by supplying us with data on first motion, have made this study possible.

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Table VII

| EARTHQUAKE |  |  |  | PLANE A |  |  |  |  | PLANE B |  |  |  |  | $\begin{array}{\|l\|} \hline \text { NULL } \\ \text { VECTOR } \\ \hline \end{array}$ |  | $\left\lvert\, \begin{array}{ll} 1 & = \\ 4 & E \\ 0 & 0 \\ 4 & = \\ x & 2 \\ w & 0 \\ 0 & 0 \end{array}\right.$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Date | $\phi$ | $\lambda$ | E 0 0 0 0. 0 4 4 0 0 | $\begin{array}{r} \stackrel{c}{0} \\ \underline{0} \\ =\frac{1}{0} \\ \text { 은 } \end{array}$ |  | $\therefore$ |  |  | $$ |  | 믐 |  |  | 0 <br> 5 <br> 0 | $\begin{aligned} & 0 \\ & 0 \\ & 5 \\ & \frac{1}{a} \end{aligned}$ |  |  |
| Jomuary 8, 1959 | 15.5 N | 61 \% | 100 | N 41 E | N 49 w | $84^{\circ}$ | . 996 | +. 087 | N 49 \% | N 41 E | $85^{\circ}$ | . 994 | +. 104 | N 13 w | $8{ }^{\circ}$ | - | $b$ |
| Jamuary 22, 1959 | 34 \% | 142 E | 33 | N 33 E | * 123 E | $89^{\circ}$ | . 172 | +.984 | N 62 \% | N 28 F | 10* | . 994 | +. 100 | - 33 E | $10^{\circ}$ | b | a |
| Pebruary 7, 1959 | 48 | 81.5 w | 33 | N 22 E | N 112 E | $7{ }^{\circ}$ | . 991 | +. 127 | N 66 \% | N 156 \# | $83 *$ | . 955 | +. 294 | N 136 E | $71 *$ | $a$ | $b$ |
| merch 1, 1959 | 0.58 | 134.5 E | 100 | H 29 E | N 119 E | $66^{\circ}$ | . 993 | -. 114 | N 63 \% | N 27 E | $84 *$ | . 912 | -. 408 | \% 104 E | 65* | 1 | b |
| April 24, 1959 | 31 s | 178 * | 33 |  |  |  |  |  | Not def | d |  |  |  |  |  |  | $\rightarrow$ |
| April 26, 1959 | 25 \% | 122.5 E | 150 | N 72 E | N 18 w | 16* | . 656 | . 754 | N 64 | N 154 w | $78^{\circ}$ | . 185 | +. 982 | N66\% | 11* | b | $a$ |
| April 28, 1959 | 15 N | 93 \% | 33 |  |  |  |  | + | Not defin |  |  |  |  |  |  |  | - |
| May 4, 1959 | 52.5 \% | 159.5 E | 60 | N 48 E | N 42 w | $83^{\circ}$ | . 504 | -. 883 | s 30 w | \% 60 E | $32^{\circ}$ | . 971 | -. 236 | N 44 E | $30^{\circ}$ | b | a |
|  | -rnative | olution |  | м 45 E | N 45 m | $83^{\circ}$ | . 000 | -1.000 | N 53 E | n 143 E | $7 *$ | . 000 | -. 999 | N 135 w | $1 *$ | - | - |
| May 24, 1959 | 17.5 \% | 97 w | 100 | 177E | M 17 w | $71^{\circ}$ | 1.000 | -. 000 | \% 17 * | \% 107 * | $90^{\circ}$ | . 945 | -. 325 | N 17 \% | $71^{\circ}$ | a | b |
| May 26, 1959 | 27.8. | 126.5 E | 100 | W 68 E | N 22 \% | $85^{\circ}$ | . 415 | +.90y | N 35 " | * 125 w | $25^{\circ}$ | . 978 | +. 206 | * 110 w | $24 *$ | b | = |
|  | crnative | olution |  | ${ }^{1} 63 \mathrm{E}$ | M 27 \% | $85^{\circ}$ | . 085 | +. 998 | N 71 | N 1R1 ${ }^{\text {w }}$ | $7{ }^{\circ}$ | . 698 | +. 715 | N $\mathrm{Ca}_{3} \mathrm{E}$ | so | $b$ | * |
| June 14, 1959 | 20.5 s | 68 * | 100 | n 4 E | * 94 E | $83^{\circ}$ | . 816 | -. 577 | N 89 E | N1\% | 55* | . 988 | -. 148 | N 13 E | $54^{\circ}$ | . | $b$ |
| June 18, 1959 | 54 \% | 161 E | 33 | N 80 E | N 10 \% | 820 | . 996 | +. 088 | N 10 - | N 100 w | $85^{\circ}$ | . 990 | +. 139 | N 42 \% | $80^{\circ}$ | b | a |
| July 9, 1959 | 20.5 s | 68 \% | 100 | ~ 90 E | 8 | 57* | . 858 | -. 513 | N 28 \# | N 64 E | 12* | . 542 | -. 839 | N 143 E | $31^{\circ}$ | 2 | b |
| July 19, 1959 | 158 | 70.5 - | 200 | 1884E | N 1748 | 19* | . 927 | -. 374 | N 2 R " | \% 648 | 83" | . 304 | -. 952 | N 152 E | 18* | 2 | b |
| Amgust 15, 1959 | 23 N | 121 : | 33 | - 888 | * 2 * | $88^{*}$ |  |  | Not de | d |  |  |  |  |  |  |  |
| August 26, 1959 | 18 n | 94.5 ( | 33 | - 31 \% | M 59 z | $48^{\circ}$ | . 355 | +. 934 | \% 60 \% | N 150 w | $48^{\circ}$ | . 367 | +. 930 | \% 13, E | $5{ }^{\circ}$ | a | b |
|  | crnative | colution |  | - 21 = | \% 111 E | $80^{\circ}$ | . 989 | +. 017 | * 69 * | (159 15 | $89^{\circ}$ | . 984 | +. 173 | \% 116 E | $80^{\circ}$ | a | b |
| September 14A, 1959 | 28.58 | 177 V | 33 | \% 59 E | \% 31 \% | $87^{\circ}$ |  |  | No | d |  |  |  |  |  |  | $\rightarrow$ |
| September 148, 1959 | 298 | 177 | 33 | \% 59 E | M 31 \% | $87{ }^{\circ}$ |  |  | Not def | ned |  |  |  |  |  |  | - |
| September 29, 1959 | 298 | 176.5 \% | 33 | N 15 E | \% 75 \% | $80^{\circ}$ | . 989 | +. 017 | N 75 w | \% 158 | $90^{\circ}$ | . 999 | +. 017 | N 73 \% | $89^{\circ}$ | * | b |
| Alternative solution |  |  |  | x 79 E | M 169 E | $8{ }^{\circ}$ | . 998 | +. 017 | N 11 \% | N 79 E | 89* | . 987 | +. 156 | N 162 E | $81 *$ | b | a |
| October 5, 1959 | 83.5 m | 112.5 = | 33 | \% 17 E | \% 73 . | $85^{\circ}$ | . 890 | -. 455 | N 75 \% | N 165 w | $63^{\circ}$ | . 995 | -. 097 | N 153 * | $62^{\circ}$ | - | b |
| January 15, 1960 | 158 | 75 - | 150 | * 13 - | - 103 * | $6{ }^{*}$ | . 685 | +. 746 | \% 78 \% | N 12 E | $47^{\circ}$ | . 831 | +. 556 | * 33 * | $3{ }^{\circ}$ | - | $b$ |
| March 8, 1960 | 16.58 | 160.5 E | 250 | M61 E | \% 151 E | 82* | . 844 | -. 535 | * 25 " | \% 115 \% | $58^{\circ}$ | .986 | -. 164 | * 131 - | 57* | b | a |
| Alternative solution |  |  |  | 175 7 | \| 165 = | $66^{\circ}$ | . 413 | -. 910 | \% 37 E | W 53 \% | $41^{\circ}$ | . 522 | -. 852 | \% 121 * | $35^{\circ}$ | - | a |
| March 20, 1960 | 40 n | 143.5 = | 60 | N 9 \% | - 99 \% | 84* | . 000 | -1.000 | \| 28 - | N 22 \% | $6{ }^{\circ}$ | . 000 | -. 999 | N 9 w | $2{ }^{\circ}$ | $b$ | . |
| May 21, 1960 | 37.58 | 73.5 \% | 33 | N4E | \% 86 | $76^{\circ}$ | . 387 | +. 934 | [ 61 E | \% 151 g | $25^{\circ}$ | . 819 | +. 572 | N 171 . | $20^{\circ}$ | b | \% |
| May 22A, 1960 | 388 | 78.6 \% | 33 | M 38 E | N 52 - | $68^{\circ}$ | . 305 | +. 952 | \% 80 E | M 170 E | $28^{\circ}$ | . 602 | +. 797 | N 135 * | $17 *$ | b | a |
| May 22B, 1960 | 37.58 | 73 \% | 33 | \% 36 E | N54 | $6{ }^{\circ}$ | . 000 | +1.000 | N 30 E | \% 120 E | $21^{\circ}$ | . 000 | +. 999 | N 35 E | $2^{\circ}$ | a | b |
| May 220, 1960 | 388 | 73.5 \% | 33 | N 3 " | * 93 " | $81{ }^{\circ}$ | . 960 | -. 279 | sw | N | $74^{\circ}$ | . 986 | -. 162 | N 32 w | $71 *$ | $b$ | . |
| June 20A, 1980 | 38 B | 73.5 \% | 33 | N 13 w | * 103 * | $83^{\circ}$ | . 955 | +. 294 | N 75 E | \% 165 E | $73^{\circ}$ | . 991 | +. 127 | \% 171. | $71{ }^{\circ}$ | b | 2 |
| July 25, 1960 | 54 N | 159 : | 100 | N 27 : | N 63 \% | 78* | . 376 | +. 926 | N 89 E | N 179 玉 | $25^{\circ}$ | . 870 | +. 481 | N 148 * | $2{ }^{*}$ | - | - |
| Alternative solution |  |  |  | \% 15 * | -75 | 13* | . 777 | -. 629 | \% 88. | \% 178 E | $53 \cdot$ | . 930 | -. 388 | N 145 E | $48^{\circ}$ | b | $\cdots$ |
| July 29, 1980 | 40.1 \% | 142.3 E | 50 | 1 25 I | \% 115 s | 69* | . 000 | +1.000 | N $40 \times$ | N 50 w | $21^{*}$ | . 000 | +. 999 | N 27 E | $5{ }^{\circ}$ | b | * |


| EARTHOUAKE |  |  |  | PLANEA |  |  |  |  | PLANE B |  |  |  |  | $\begin{aligned} & \text { NULL } \\ & \text { VECTOR } \end{aligned}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Date | $\phi$ | $\lambda$ |  |  |  | 음 |  |  |  |  | 응 |  |  | $\begin{aligned} & 0 \\ & c \\ & \underset{\sim}{2} \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \\ & \frac{c}{5} \end{aligned}$ |  |  |
| October 7, 1960 | 7.4 s | 130.7 E | 45 | N 58 E | N 148 E | $87^{\circ}$ | . 921 | +. 389 | N 41 : | N 49 E | 690 | . 908 | +. 418 | * 101 E |  | b | : |
| October 22, 1960 | 10.3 s | 161.2 E | 93 | N 41 E | N 131 E | $88^{\circ}$ | . 882 | -. 469 | N 51 \% | N 39 E | 6.20 | . 999 | -. 039 | * 45 E | 6:2* | $a$ | b |
| November 13, 1960 | 51.1 N | 168.8 \% | 65 |  |  |  |  |  | No | d |  |  |  |  |  |  |  |
| Decenber 3, 1960 | 42.9 N | 104.4 E | 60 |  |  |  |  |  | Not | d |  |  |  |  |  |  | - |
| January 5A, 1961 | 4.1 s | 143.0 E | 108 | N 85 E | N 175 E | $67^{\circ}$ | . 999 | +. 037 | N 5 w | K 85 E | $88^{\circ}$ | . 920 | +. 390 | * 171 E |  | b | a |
| January 16, 1961 | 36.2 N | 141.7 E | 41 | N 45 E | N 1358 | 87* | . 000 | +.999 | N 77 E | * 13 w | $3^{\circ}$ | . 000 | +. 999 | N 45 E | 20 | b | a |
| January 20, 1961 | 56.6 N | 152.3 \% | 46 | N 31 E | N 59 w | $72^{\circ}$ | . 939 | -. 342 | N 53 W | * 37 E | $71^{\circ}$ | . 945 | -. 326 | N9 9 |  | b | a |
| February 12, 1961 | 43.9 N | 147.6 E | 45 | N 44 E | N 134 E | 74* | . 101 | +. 994 | N 62 E | * 28 w | $17^{*}$ | . 333 | +. 942 | \% 4.5 E | 5 | $b$ | a |
| February 26, 1961 | 31.6 N | 131.2 E | 54 | ~ 30 E | \% 120 E | $64^{\circ}$ | . 651 | +:758 | N 33 w | N 123 * | $47^{\circ}$ | . 800 | +.599 | N 171 \% | $36^{\circ}$ | a | b |
| March 28, 1961 | 0.2 N | 123.6 E | 83 | N 31 E | N 121 E |  |  |  | Not der | ed |  |  |  |  |  |  | - |
|  | ternative | solution |  | M 81 w | \% 171 * | $64^{\circ}$ | .904 | +.414 | $\cdots 3$ \% | \% 87 E |  | . 881 | +. 472 | M 143 E | 5s* | b | a |
| June 1, 1961 | 10.4 m | 39.9 E | 33 |  | - Not d |  |  |  | v $24 \times$ | N 114 * |  |  |  |  |  |  |  |
| June 11, 1961 | 27.9 N | 54.6 E | 37 | N 59 E | N 149 E | $58^{\circ}$ | . 832 | +. 553 | N 51 | N 39 E | 62* | . 793 | +. 800 | N 98 E |  | b | a |
|  | ternative | solution |  | \% 33 - | x 123 * | $40^{\circ}$ | . 404 | +. 914 | M 3 \% | M 87 E | $55 *$ | . 321 | +.946 | w 166 E | $15^{\circ}$ | b | a |
| July 18, 1961 | 29.4 N | 131.6 E | 21 | \% 14 E | N 104 E | 36* | . 218 | -. 975 | - 31 E | N 59 * | $55^{\circ}$ | .156 | -. 987 | N 25 E | $8^{\circ}$ | a | b |
| August 11, 1961 | 43.0 N | 145.0 \% | 50 | \% 28 | N 92 E | $58^{\circ}$ | .458 | +.88y | N 46 E | * 44 | $41^{\circ}$ | . 589 | +. 807 | \% 17 E | $23^{\circ}$ | b | a |
| August 19A, 1961 | 10.8 s | 71.0 * | 649 | ल 3 - | ¢ 87 E | $51^{\circ}$ | . 968 | -. 245 | N 84 " | \% 174 * | $79^{*}$ | . 767 | -. 641 | N 109 E | $49^{\circ}$ | b | a |
|  | ternative | solution |  | M 17 E | -107E | 62* | . 929 | -. 368 | N 62 - | N 152 w | $71^{\circ}$ | . 868 | -. 496 | N 147 E | $55^{*}$ | - | 2 |
| August 198, 1961 | 36.2 N | 136.5 E | 17 | N 91 | , 81 E | $60^{\circ}$ | . 248 | +. 968 | N 19 E | N 71 * | $33^{\circ}$ | . 396 | +. 918 | N1: | $13^{*}$ | b | . |
|  | ternative | colution |  | \% 25 B | \% 115 : | $31^{*}$ | . 524 | +. 851 | \% 12 " | \% 102 * | $64^{\circ}$ | . 300 | +. 953 | N 176 E | $16^{\circ}$ | a | b |
| August 31A, 1961 | 10.6 s | 70.9 | 628 | 1145 | * 135 E | $8{ }^{*}$ | . 208 | -. 423 | N 43 \# | * 133 \% | $65^{\circ}$ | . 998 | -. 057 | N 141 * | $65^{\circ}$ | b | a |
| August 318, 1961 | 10.4 s | 70.7 \% | 629 | \% 50 E | N 148 E | 84* |  |  | Not d | ed |  |  |  |  |  |  | $\rightarrow$ |
| September 1, 1961 | 59.5 s | 27.3 \% | 131 |  |  |  |  |  | Wot |  |  |  |  |  |  |  | - |
| February 14, 1962 | 38.1 s | 73.1 . | 44 | 1847 | N 43 " | $38^{\circ}$ | . 880 | +. 474 | * 20 \% | N 70 E | $73^{\circ}$ | . 586 | +. 824 | N 9 \% |  | 2 |  |
| Alternative solution |  |  |  | N 30 E | N 60 * | $83^{\circ}$ | . 997 | +. 070 | N 60 \% | M 30 E | $88^{\circ}$ | . 992 | +. 122 | N 27 - | $82^{\circ}$ | a | b |
| March 7, 1962 | 19.3 s | 145.3 E | 680 | * 52 " | \% 142 * | 54* | . 226 | -. 974 | N 33 \# | M 57 E | $38{ }^{*}$ | . 297 | -. 954 | N 135 E | 9* | - | b |
| April 12, 1962 | 38.2 m | 142.3 E | 68 | \% 48 x | * 130 ह | $87^{*}$ | . 090 | +. 895 | N 10 \# | N 100 \% | ${ }^{\circ}$ | . 865 | +. 500 | N 131 * | $5{ }^{\circ}$ | a | b |
| April 23, 1962 | 42.9 N | 143.4 E | 25 | N 64 E | * 154 \% | 77* | . 404 | +. 814 | N 2 E | N 88 \# | $27^{\circ}$ | . 868 | +. 495 | N 121 * | $23^{\circ}$ | * | b |
| Alternative solution |  |  |  | M 882 | $\cdots 2$ - | $85^{\circ}$ | . 280 | -. 959 | * 18 \# | N 108 : | 17* | . 954 | -. 298 | N 91 \% | 17* | * | b |
| May 7, 1962 | 45.3 n | 146.7 \% | 25 | N 58 E | N 148 E | $55^{\circ}$ | . 713 | +. 700 | N 3 " | N 93 . | 55* | . 713 | +. 700 | N 152 w | $36^{\circ}$ | a | b |
| May 11, 1962 | 17.0 m | 99.7 \% | 25 | - 49 I | \% 139 E | $36^{\circ}$ | . 987 | -. 159 | N 50 \# | \% 40 E | $86^{\circ}$ | . 433 | -. 900 | \% 128 E | $25^{*}$ | 1 | b |
| May 21, 1962 | 37.3 m | 96.0 E | 25 |  |  |  |  |  | not | d |  |  |  |  |  |  |  |
| July 6, 1962 | 36.6 m | 30.4 E | 203 | N 82 E | N 8 " | 15* | . 000 | +1.000 | N 87 - | N 177 \% | $75^{\circ}$ | . 000 | +. 999 | N 87 w | $3{ }^{\bullet}$ | 1 | 1 |
| July 28, 1962 | 7.5 \% | 82.7 \% | 21 |  |  |  |  |  | N 8 | N 98 * | $83^{\circ}$ | Not d | defined |  |  |  |  |
| July 30A, 1962 | 3.38 | 143.9 E | 25 |  |  |  |  |  | Not | $\square$ |  |  |  |  |  |  |  |
| July 308, 1962 | 5.0 \% | 76.3 \% | 45 | N 208 | \% 110 E | $8^{\circ}$ | .970 | *. 241 | N 70 \# | N 20 E | $76^{\circ}$ | . 998 | +. 017 | N 21 E | $75^{\circ}$ | - | - |




[^0]:    *Canadian Contribution No. 56 to the International Upper Mantle Project.

