DEPARTMENT OF THE INTERIOR
CANADA

HONOURABLE T. A. CRERAR, *Minister* J. M. WARDLE, *Deputy Minister*

# PUBLICATIONS

OF THE

# Dominion Observatory

## OTTAWA

R. MELDRUM STEWART, *Director*

VOL. XI, No. 3

# Gravity and Isostasy in Canada

BY

A. H. MILLER AND W. G. HUGHSON

OTTAWA
J. O. PATENAUDE, I.S.O.
PRINTER TO THE KING'S MOST EXCELLENT MAJESTY
1936

*Price, 40 cents.*

## CONTENTS



## TABLES



## MAP

# Gravity and Isostasy in Canada

BY

A. H. MILLER AND W. G. HUGHSON

ABSTRACT

About one-third of Canada has been covered by 128 gravity stations established in the southern part of Canada and in the basin of Mackenzie river. Reductions by the Free Air, Bouguer, Hayford, and Airy methods show that the area as a whole is in practically complete isostatic equilibrium. This also applies to British Columbia and to the mountainous part of Alberta. The results agree somewhat better with the Airy than with the Hayford reduction. The most probable depths for both methods have been computed separately for 22 stations in the mountains as well as for 126 stations, the total number reduced isostatically. All the important results are tabulated and are in part shown graphically in two curves and on a gravity map which shows the anomalies for both United States and Canadian stations.

## INTRODUCTION

This report deals with the results of all gravity work performed in Canada since 1914. Although gravity determinations were begun by the Dominion Observatory as early as 1902 it was not until 1914 that important field work was undertaken. Numerous reports[1] on the subject have appeared from time to time in official publications and also in other journals. Altogether 128 stations have been established. They cover a belt on the average 350 miles wide along the international boundary from Halifax to Victoria and also the basin of Mackenzie river. There is approximately one station to every hundred-mile square, the total area covered being about one-third that of the whole country. The more important results for all stations are given in tables 1, 2, and 3. Tables 4 and 5 give the results for only those stations for which this information has not previously been published. Volume VIII, Nos. 6 and 9, should be consulted for information corresponding to that given in table 5. In order to reduce the size of the publication the rather lengthy table, "Pendulum Observations and Reductions", has been omitted from this report.

Among the 128 stations are 29 not previously reported upon, established in 1927 and 1930 after the publication of the last report. With the single exception of Brockton Point, which is only about one mile from the other gravity station in Vancouver at the C.P.R. depot, the reductions for topography and compensation have been made for all these 29 new stations. As was previously done in the case of Ottawa and 11 stations in Western Canada, the corrections for topography and compensation for 29 stations (Nos. 2 to 30 inclusive), observed in Eastern Canada in 1914 and 1915, have been recomputed. In the original computations no record can be found of the individual corrections for separate zones. New maps have also become available in the meantime. Altogether 126 of the 128 stations have been reduced isostatically and the corresponding corrections for separate zones are either published in this report or have been published previously in the two reports mentioned above. There have been omitted in the isostatic reductions only two stations, North Bend, B.C., due to lack of topographic maps, and Brockton Point on account of its proximity to the other station in Vancouver. It is apparent from the results that the isostatic anomalies for the two Vancouver stations are approximately the same.

## Gravity Anomalies and Reduction Methods

The anomalies (table 1) have been computed by four methods of reduction, using the international formula for gravity at sea-level adopted at Stockholm in 1930 by the Section of Geodesy of the International Union of Geodesy and Geophysics. The observed values for all the stations have also been completely revised, using the value 980·622 for Ottawa adopted since the international determinations at Ottawa, Greenwich, Potsdam, and Washington in 1928. The anomaly for a station is the observed value minus the computed value. The Free Air, Bouguer, and Hayford isostatic reductions have been explained in some detail in Vol. VIII, No. 6. In the Free Air method of obtaining the computed value at the station only one correction to gravity at sea-level is made, namely that due to elevation of the station (table 1). In the Bouguer method this negative correction is also made, together with a further positive correction for topography, which is regarded as an infinite plane or slab of thickness equal to the elevation of the station. In the isostatic methods the complete topographical effects for the entire earth are estimated by the use of tables[2] in combination with readings of contour or relief maps for each station. For distant zones, in reductions recently made, use has been made by the writers of a 30-inch terrestrial globe, designed specially for the purpose, showing land elevations and sea depths. In addition to corrections for elevation and topography, with the isostatic methods a further correction is made for topographical compensation. In both the Airy and Hayford methods the compensation amounts, for land zones, to a deficiency in mass equal to the topography to be compensated or the material in the crust above sea-level. For zones at or very near sea-level there is no topography to be compensated and the compensation is therefore zero for such zones. For ocean zones the compensation is positive, being equivalent to an excess of mass to make up for the lower density of water. In the Hayford method the compensation is considered to be distributed uniformly down to the depth of compensation. On this view variations in the height of the solid crust of the earth are caused by variations in density of the outer crust. In contrast to the Hayford hypothesis of uniform depth and varying density the Airy hypothesis supposes a crust of variable thickness but of uniform density. Compensation is brought about by change in thickness of the crust, which, being lighter than the more or less plastic (to long-continued forces) substratum, floats in it very much as an iceberg in the sea. On the Airy hypothesis variation in elevation is related to varying thickness of the crust and the compensation is confined within comparatively narrow vertical limits at the bottom of the crust, the lighter crust displacing heavier substratum or *vice versa* according to whether the zone is land or ocean. In contrast to its meaning on the Hayford hypothesis, the term *depth of compensation* on the Airy hypothesis denotes a variable quantity differing considerably for mountainous regions and oceanic areas. In comparisons in this report, between Hayford and Airy solutions, depth of compensation on the Airy hypothesis indicates the thickness of crust at sea-level which, on the hypothesis, would be deduced from the particular Airy solution concerned in the reduction. At sea-level the thickness of crust and the depth of compensation are the same. Although not an exact average depth for any particular Airy solution it is nevertheless approximately so and is intermediate between oceanic and mountain depths. In both reductions 2·67 has been taken for the density of topography

and for all the Airy reductions included in this report a density difference of 0·6 between crust and substratum has been assumed. For crustal thicknesses not covered by Heiskanen's tables special tables were computed by Hughson.

## Local and Regional Anomalies

The results are an indication that, on the whole, the area covered by the observations is in isostatic equilibrium. There are, notwithstanding, areas of definite anomaly. Some are local in character and in certain cases are apparently related to the geology. It is likely that these are due to masses of anomalous density near the surface and may well be completely, or very nearly completely, compensated. It is less certain that the areas of more regional anomaly, if regarded independently, are in equilibrium. From a purely mathematical viewpoint these anomalies are obviously capable of explanation by any of the following assumptions: (1) partial lack of compensation, (2) abnormal density (10 per cent or more) covering areas up to 200 miles or more in diameter and extending to depths of 20,000 feet or even farther, (3) partial lack of compensation coupled with abnormal density. The answer as to which is most likely depends upon the load, having regard to areal extent, that the rigidity of the crust can bear, and upon the existence or non-existence of the assumed abnormal densities. There is an area of regional positive anomaly in Western Canada covered entirely by sedimentary formations. The part of it of largest anomaly is in Saskatchewan and has been interpreted by geologists[3] as being due to a buried highland of heavy Paleozoic rock. There are extensive negative areas in Ontario. Part in southern Ontario is covered by sedimentary and presumably lighter rock several thousand feet thick. There is a large area of negative anomaly within the Precambrian shield where the anomalies are in some cases larger than any within the sedimentary formations of southern Ontario.

## Probable Depth and Manner of Isostatic Compensation. Gravity Formulae

The results (tables 1 and 2 and the curves) are plainly in better agreement with the isostatic methods than with either of the other two. Also, of the two isostatic methods the results are in somewhat better agreement with the Airy reduction. For the whole country the Airy method reduces the sum of the squares of the residual anomalies, for the best solutions in each case, by nearly 3 per cent. For 22 Cordilleran stations the corresponding reduction is 11 per cent.

In the mountains the most probable Airy depth of compensation is about 40 kilometres and the corresponding Hayford depth about 115 kilometres. A previous solution for 20 stations in the mountains, but not perhaps quite so well suited for the purpose, gave approximately 100 kilometres for the Hayford depth (Vol. VIII, No. 9, p. 249). For the part of the country covered by all the observations the most probable Airy depth is approximately 35 kilometres and the Hayford depth 85 kilometres. On the Airy hypothesis these figures correspond to an average crustal thickness, over the entire area covered by all the observations, of approximately 37 kilometres and to an average thickness in the mountains of about 50 kilometres. The results (table 2) also show that, with proper correction in each case to gravity at the equator, the three gravity formulæ fit the observa-

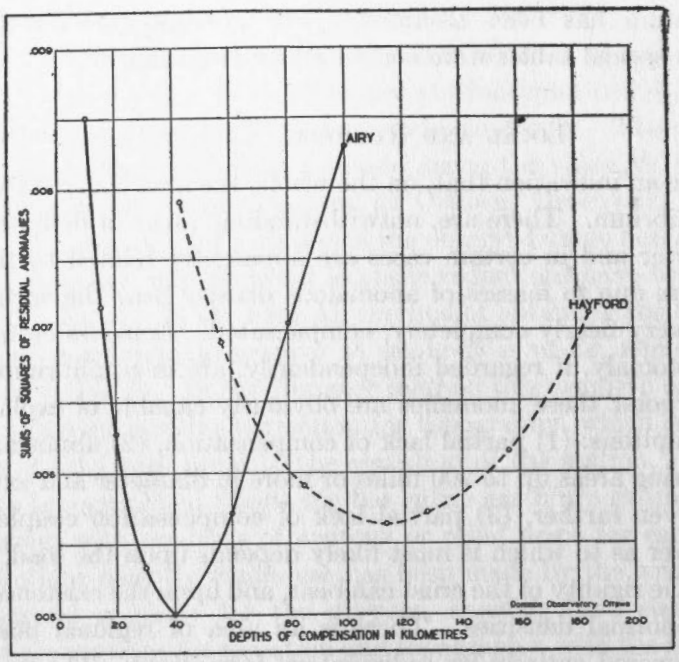


FIGURE 1.—Graphical determination of depths of compensation from 22 stations in the Canadian Cordillera.

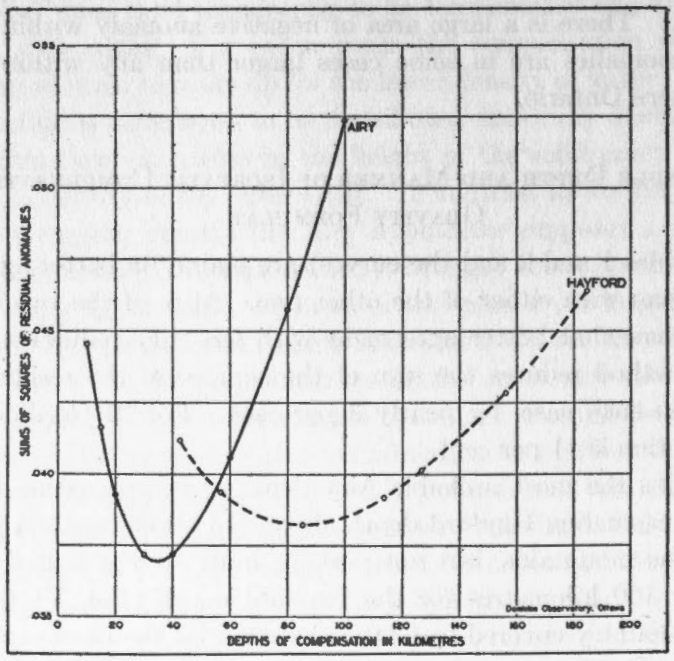


FIGURE 2.—Graphical determination of depths of compensation from 126 stations in Canada.

tions almost equally well, although Helmert's formula actually gives the smallest residuals by a very small margin. At 85·3 kilometres, the most probable Hayford depth of compensation, no correction is required to the international formula, +·012 to Helmert's formula, and +·008 to Bowie's formula.

## Periods of Pendulums

During the seasons of 1927 and 1930 the apparatus gave less satisfaction than usual in so far as constancy of pendulum periods is concerned. At the first field station of 1927 (Chelmsford) a sudden decrease of period of about $100 \times 10^{-7}$ second took place in the periods of all pendulums on knife edge I but not upon knife edge II, which was not used until the second station (Sudbury) was reached. Apparently some physical change took place in knife edge I but what it was or what caused it is uncertain. The change may have resulted from an oversight on the part of the observer. At the conclusion of the swings with one pendulum it was found necessary to repack the stuffing box of the pendulum lifting device. In replacing this part it was not noticed that the operating rod passing through the stuffing box was screwed out to the limit. So when the next pendulum was lowered (carefully as usual) instead of being arrested in the usual manner by the two prongs and then being let down by the gradual slow motion it was by mistake set directly on the knife edge without going through the usual intermediate step. It was immediately following this that the changes in periods on this knife edge occurred. At this station the apparatus during swings was subject to an unusual amount of vibration due to passing trains, which were more effective in this respect due to the fact that the town is underlain by quicksand. Observations were made several times for the purpose but it could not be demonstrated that the passing of the trains produced any effect on the periods or swings of the pendulums. It is more likely that the direct lowering of the pendulum on the knife edge was the cause of the change. Although no change in the appearance of the knife edge was discernible it is possible that scraping that might have occurred may have modified the surface sufficiently to cause the change. Schmerwitz[4] has shown that changes in period of the amount observed in this case can be caused by variation in curvature of the edge due to wear. Following Chelmsford, observations were taken at one more station (Sudbury), this time on both knife edges, and then return was made to Ottawa for restandardization. For the rest of the season the periods remained constant on knife edge I but gradually decreased by over $60 \times 10^{-7}$ second on knife edge II. In 1930 little change took place in the periods on knife edge I but considerable decrease (average $68 \times 10^{-7}$ second) took place with knife edge II.

## Gravity Map and Illustrations

The illustrations accompanying this report were prepared by Mr. F. C. Weskett under the supervision of Mr. F. D. Henderson, both of the observatory staff. Mr. Henderson also assisted with the computation and checking of the isostatic reductions. Mr. G. P. Hatton also gave considerable assistance in the checking of certain computations. The anomalies for Canada on the gravity anomaly map are those given in table 1 for a depth of compensation of 113·7 kilometres. The positions of the contours in the United States are taken from Fig. 11, Special Publication No. 40, U.S.C. and G.S.

### Change in Observation Routine

In order to eliminate a considerable amount of computation and observation the gaining (1 second in 50 seconds) chronometer used for time comparison with the wireless signals has in recent work been compared directly with the pendulums without the interposition of sidereal chronometers. With the gaining chronometer the coincidence interval is only about 50 seconds (up to up, or down to down). In order to compute the number of coincidences in the usual 12 hours' swing greater accuracy is in this case necessary in the preliminary determination of length of coincidence interval. For this purpose, in addition to the usual observations at the beginning and end of swing, observations were also taken at the tenth (double) and fiftieth (double) coincidence following the initial and preceding the final coincidence. Special tables were constructed to facilitate the computation of the results in the field. Using mean time signals it would be more direct to determine the period of the pendulum in mean time. As it is the usual custom to express the periods in fractions of a sidereal second, and as this has always been the practice in previous observatory work, it was considered desirable for the present at least to conform to the usual custom.

### Variation of Period of Pendulum with Arc

In connection with the astronomical work of the observatory at Brockton Point, Vancouver, in 1926, where pendulum No. 3 was used as a clock to check the rate of the Howard clock between time observations, a special set of observations was subsequently taken at Ottawa to determine for different arcs the accuracy of the usual arc correction. The results together with the usual corrections are given in table 6. It is evident from the figures in rows 3 and 5 (more particularly row 3) that after all the corrections are applied there is still a correction required for arc. Assuming this correction to be proportional to arc the most probable value, $2{\cdot}17 \times 10^{-7}$ sec. per mm., is obtained from the periods in row 3. The periods in row 4 resulting from this last correction differ from the mean by little more than the probable error of determination in any particular case and on the average by an amount which is less than the average probable error. The values in row 5 are averages obtained from the figures in row 3 and not the values that might be computed directly from the observed coincidences.

The arc correction formula (Borda) is based on the assumption that the sine of the semi-arc (for these small angles also the semi-arc) decreases exponentially. The figures in row 2, table 6, show that this is not precisely the case for most of the intermediate swings. The average probable error of the observed arcs in row 1 is ·02 mm. The divergence from the exponential law (see table 7 for the magnitude of the arc correction) would seem to be insufficient to account for the observed discrepancies in the period. Compared with a vacuum the indicated total pressure correction is only $13 \times 10^{-7}$ second for the pressure at which the swings were taken. It does not seem likely that the larger observed differences are due to an effect of pressure varying with arc. The displacement of the knife edge due to flexure varies directly with the arc but there is probably little variation of the effective length of the pendulum for the different observed arcs. It is likely that the cause of the residual variation in period with arc is due to change in curvature of the knife edge. The knife edge has been used in all work carried on by the observatory since

the purchase of the apparatus in 1902. It is somewhat worn in the centre (parallel to the edge), that is to say its radius of curvature is greater for smaller arcs of swing. For larger swings the average radius of curvature will be smaller. It is sufficient that the effective radius should vary by only one micron to produce a change in period of $10 \times 10^{-7}$ second.

Similar experiments were made by Putnam[5] who observed somewhat similar effects on a less-used knife edge. After experiments with knife edges of various widths and angles he attributed effects similar to those observed with knife edge I to the fact that "different portions of the knife edge are brought into use" as the arc is varied. The results emphasize the importance in field work (also pointed out by Putnam) of maintaining the same arcs of swing in the field as at the base standardization. With this precaution no error is introduced in the determinations. Otherwise a correction such as that indicated in the table will be required.

## Flexure or Sway Correction

In connection with the corrections that are applied to the observed pendulum periods, it is of interest to note that the experimentally determined value of the flexure coefficient obtained by Burger[6] leads to a flexure correction in almost exact agreement with the theoretical value from the formula

$$\Delta T \text{ (Flexure correction)} = T \frac{\Delta l}{2l} = \frac{\Delta l}{100}$$

Where $\Delta l$ is the increase in effective length of the pendulum and $l$ is the length of the simple equivalent pendulum = 25 cm. for observatory pendulums. The displacement of the knife edge for a swing of 5 millimetres (total arc) when the apparatus is erected on a good support is generally found to be of the order of magnitude measured by Burger, namely ·058 fringe width of sodium light, corresponding to an actual displacement of $\cdot 029 \times 5893 \times 10^{-8}$ cm. $= 170 \cdot 9 \times 10^{-8}$ cm. The distance between the knife edge and the arc scale is 287·5 mm. For the displacement and arc observed in the above case $\frac{\Delta l}{170 \cdot 9 \times 10^{-8}} = \frac{287 \cdot 5}{5}$ or $\Delta l = 9827 \times 10^{-8}$ cm., and therefore $\Delta T = \frac{\Delta l}{100} = 9 \cdot 83 \times 10^{-7}$ second, in close agreement with the value $5 \cdot 8 \times 1 \cdot 73 \times 10^{-7} = 10 \cdot 03 \times 10^{-7}$ second from Burger's empirical formula.

It follows from the above that

$$\Delta T = \frac{D_{cm}}{A} \times 2 \cdot 875$$

$$= \frac{D_f}{A} \times \frac{\lambda}{2} \times 2 \cdot 875$$

$$= \frac{D_f}{A} \times 2947 \times 2 \cdot 875 \times 10^{-8} \text{ (when sodium light is used)}$$

$$= 847 \cdot 3 \times \frac{D_f}{A} \times 10^{-7} \text{ second}$$

a convenient formula for flexure determinations, where $D_{cm}$ = displacement in cms. and $D_r$ = displacement in fringe widths of the knife edge resulting from a swing of arc A, where A is the total or twice the semi-arc and is expressed in millimetres.

## Descriptions of Stations (Explanation)

The list, accompanying this report, includes all gravity stations established since those listed in Vol. VIII, No. 9. Descriptions of stations previously occupied appear in earlier reports. Port Arthur, No. 14, is included in the present list. It was re-occupied in 1930 and its elevation redetermined from a bench mark of the Geodetic Survey of Canada.

Dominion Observatory,

Ottawa, March, 1934

## REFERENCES

1. KLOTZ, OTTO J.—

"Report upon Field Astronomical Observations and Description of Half-Seconds Pendulum Apparatus", *Report of the Chief Astronomer*, Appendix 2, pp. 14-34, 1905.

"Gravity, Seismology, and Magnetic Work", *Report of the Chief Astronomer*, Appendix 3, pp. 15-40, 1907.

"Gravity", *Annual Report of the Association of Ontario Land Surveyors, 1909*, pp. 162-169.

"Gravity Stations 1914", *Journal of the Royal Astronomical Society of Canada*, Vol. IX, pp. 176-179, 1915.

STEWART, LOUIS B.—

"Gravity Determinations in Labrador", *Transactions of the Royal Astronomical Society of Canada for 1905*, pp. 70-78.

MCDIARMID, F. A.—

"Gravity", *Publications of the Dominion Observatory*, Vol. II, No. 10, pp. 197-269, 1915.

"Gravity", *Publications of the Dominion Observatory*, Vol. III, No. 9, pp. 353-370, 1918.

"Gravity", *Journal of the Royal Astronomical Society of Canada*, Vol. X, pp. 537-552, 1916.

MILLER, A. H.—

"Gravity", *Publications of the Dominion Observatory*, Vol. V, No. 10, pp. 381-409, 1922.

"Gravity in Northwestern Canada", *Publications of the Dominion Observatory*, Vol. VIII, No. 6, pp. 83-110, 1924.

"Gravity in Western Canada", *Publications of the Dominion Observatory*, Vol. VIII, No. 9, pp. 241-330, 1929.

"A Determination of the Relative Values of Gravity at Potsdam, Greenwich, Ottawa, and Washington", *Publications of the Dominion Observatory*, Vol. XI, No. 2, pp. 59-76, 1931.

"Dominion Observatory Work in the Mackenzie District", *Journal of the Royal Astronomical Society of Canada*, Vol. XVII, pp. 197-210, 1923.

"Gravity Results in the Mackenzie Basin", *Ibid.*, pp. 367-373.

"Gravity and Isostasy", *Journal of the Royal Astronomical Society of Canada*, Vol. XX, pp. 327-334, 1926.

"Isostasy in British Columbia", *Proceedings of the Third Pan-Pacific Science Congress*, Vol. I, pp. 607-617, Tokyo, 1926.

"Gravity in Western Canada", *Transactions of the Royal Society of Canada, Third Series*, Vol. XXI, Section IV, pp. 175-187, 1927.

"The Gravity Survey of Canada", *Bulletin of the National Research Council*, No. 68, pp. 35-38, Washington, D.C., 1929.

ALCOCK, F. J. and MILLER, A. H.—

"Plumb-line Deflections and Gravity Anomalies in Gaspé Peninsula and Their Significance", *Transactions of the Royal Society of Canada, Third Series*, Vol. XXVI, Section IV, pp. 321-333, 1932.

MILLER, A. H. and HUGHSON, W. G.—

"The Isostatic Equilibrium of the Pacific Coast of Canada", *Proceedings of the Fifth Pacific Science Congress*, Vol. II, pp. 1169-1173, Toronto, 1933.

REFERENCES—*Concluded*

2. HAYFORD, JOHN F. and BOWIE, WILLIAM—
"The Effect of Topography and Isostatic Compensation upon the Intensity of Gravity", *Special Publication No. 10, U.S. Coast and Geodetic Survey, 1912.*

BOWIE, WILLIAM—
"Investigations of Gravity and Isostasy", *Special Publication No. 40, U.S. Coast and Geodetic Survey, 1917.*

HEISKANEN, W.—
"Untersuchungen über Schwerkraft und Isostasie", *Publication No. 4, Geodetic Institute of Finland, 1924.*
"Isostatic Tables for the Reduction of Gravimetric Observations Calculated on the Basis of Airy's Hypothesis", *Bulletin geodesique, Section of Geodesy of International Union of Geodesy and Geophysics*, No. 30, 1931.

3. WICKENDEN, R. T. D.—
"Notes on Some Deep Wells in Saskatchewan", *Transactions of the Royal Society of Canada, Third Series*, Vol. XXVI, Section IV, pp. 177-196 (see pp. 194-196), 1932.

HUME, G. S.—
"Oil and Gas in Western Canada", *Economic Geology, Series No. 5* (Second Edition), 359 pages (see p. 266), 1933.

4. SCHMERWITZ, GERHARD—
"Messung von Schneidenkrümmungsradien", *Zeitschrift für Instrumentenkunde*, 52 Jahrgang, Heft 1, pp. 1-14 (see pp. 7-8), 1932.

5. PUTNAM, G. R.—
"Relative Determination of Gravity with Half-second Pendulums, and other Pendulum Investigations", *U.S. Coast and Geodetic Survey Report for 1894*, Part II, Appendix No. 1, pp. 7-55 (see pp. 40-42).

6. BURGER, W. H.—
"The Measurement of the Flexure of Pendulum Supports with the Interferometer", *U.S. Coast and Geodetic Survey Report for 1910*, Appendix No. 6, pp. 431-449.

## DESCRIPTIONS OF STATIONS

No. 14, Port Arthur, Ont. (1930).—The apparatus was set up in the southwest corner of the basement of the Masonic Temple, Arthur street. It was 3·5 feet below the elevation of G.S.C.B.M. No. 95-E. This station was also occupied by F. A. McDiarmid in 1914.

No. 100, Vancouver (Brockton Point), B.C. (1926).—In connection with the world longitude determinations the apparatus was set up on a concrete pier about 3 feet above the level of the ground and about 2 feet 4 inches above the level of the floor of the clock room built on to the south side of Brockton Point Observatory. It is approximately 12 feet south and 6 feet west of the astronomical pier. According to information supplied by the Vancouver Sewage Board the top of the pier is 36·5 feet above mean sea-level.

No. 101, Chelmsford, Ont. (1927).—The apparatus was set up on the concrete floor in the northeast section of the basement of the Algoma hotel. It was 6 feet 10 inches below the level of the rail at the station and 4 feet below the surrounding level.

No. 102, Sudbury, Ont. (1927).—The apparatus was set up on the concrete floor in the northeast corner of the assay room at the southwest corner of Sudbury Mining and Technical School. It was about 1700 feet west and 3300 feet north of the C.P.R. station. It was 1 foot 8 inches above the elevation of G.S.C.B.M. 454-A in the west end of Sudbury Court House.

No. 103, Hearst, Ont. (1927).—The apparatus was set up on the concrete floor in the west end of Mr. K. M. Sharp's poultry house. It was 1680 feet north and 2320 feet west of the astronomical station. It was 5 feet 6 inches below the level of the rail at the station.

No. 104, Nakina, Ont. (1927).—The apparatus was set up on the concrete floor of a small room used as a kitchen in the northeasterly part of the basement of Nakina school. It was 8 feet 4 inches below the level of the rail at the station and 5 feet below the surrounding level.

No. 105, Armstrong, Ont. (1927).—The apparatus was set up on a concrete pier, flush with the floor, in the centre of the main room on the west side of Wm. Randall's cottage. It was about 1000 feet east of the station and was 10 feet above the level of the rail at the station.

No. 106, Sioux Lookout, Ont. (1927).—The apparatus was set up on the concrete floor in the room in the west end of the basement of the Masonic hall. It was 870 feet north and 50 feet east of the C.N. station, and was 10 feet above the level of the rail at the station. It was 6 feet below the surrounding level.

No. 107, Berens River, Man. (1927).—The apparatus was set up on a concrete pier, flush with the floor, in the most northerly of the buildings forming the Hudson's Bay Company trading post at Berens river. This building was used partly as a storehouse and partly as an Indian dwelling. It was about 100 feet north of the office building and about 7 feet above the level of lake Winnipeg.

## DESCRIPTIONS OF STATIONS—*Continued*

No. 108, Grand Rapids, Man. (1927).—The apparatus was set up on a concrete pier flush with the floor in the second from the river front of the group of log buildings forming J. G. Campbell's trading post. This building was used partly as a dwelling and partly as a storehouse. The pier was 21 feet above the level of Saskatchewan river in front of Campbell's post on August 13, 1927.

No. 109, Norway House, Man. (1927).—The apparatus was set up on the outcrop of rock in the east end of the old detention house at the Hudson's Bay Company post. This stone building is on the south side of the quadrangle and about 200 feet westerly from the building that was then used for the sale of merchandise. On August 5, 1927, it was about 7 feet above the water level in front of the Hudson's Bay Company wharf at the post.

No. 110, Nokomis, Sask. (1927).—The apparatus was set up on the concrete floor in the basement of the more easterly of the two overflow (cottage) buildings of Nokomis school. These buildings are on the south side of the street and directly opposite the school. The apparatus was six inches below the level of the rail at the station and about four feet below the surrounding level.

No. 111, North Battleford, Sask. (1927).—The apparatus was set up on the concrete floor of the basement of the post office at King and First streets about 6 feet below the surrounding level. The elevation of the station was estimated from the description in Publication No. 27 of the Geodetic Survey of Canada of G.S.C.B.M. No. 829-C established in the wall of the post office in 1928 one year after the occupation of the station. It is possible the adopted elevation may be one or two feet in error.

No. 112, Kindersley, Sask. (1927).—The apparatus was set up on the concrete floor in the northwesterly room of the basement of Kindersley school. It was 35 feet 4 inches above the level of the rail at the station and about 4 feet below the surrounding level.

No. 113, Prince George, B.C. (1927).—The apparatus was set up on the concrete floor in the basement of a store building owned by R. MacLeod. This building was on the main street about 1000 feet west of the station and a few hundred feet south of the track. The pier was 3 feet 7 inches above the level of the rail at the station.

No. 114, Endako, B.C. (1927).—The apparatus was set up on a concrete pier, flush with the floor, erected in a house owned by Mrs. P. Cousins, across the street from the Anglican church about 400 yards north of the station. It was 13 feet above the level of the rail at the station.

No. 115, Smithers, B.C. (1927).—The apparatus was set up on the concrete floor in the westerly room of the garage of the B.C. roads department. It was 17 feet above the level of the rail at the station. The building is on the north side of the highway about one-half mile along the main street and highway in an easterly direction from the station.

## DESCRIPTIONS OF STATIONS—*Continued*

No. 116, Montreal, Que. (1928).—The apparatus was set up on the concrete floor of the room in the northeasterly corner of the basement of Macdonald Physics Building of McGill University. The elevation of the station was obtained from G.S.C.B.M. No. 548-A in the wall of the Macdonald Engineering Building by Professor James Weir.

No. 117, Pembroke, Ont. (1930).—The apparatus was set up on the concrete floor in the furnace room of the Collegiate Institute, Pembroke street West. It was 13·9 feet below the level of G.S.C.B.M. No. 1826.

No. 118, Haliburton, Ont. (1930).—The apparatus was set up on the concrete floor in the southeast corner of the basement of the Grand Central hotel, east half of Lot 3, Block L, of the town plot of Haliburton. It was 20·6 feet above the level of the rail in front of the C.N.R. station.

No. 119, Kincardine, Ont. (1930).—The apparatus was set up on the concrete floor in the southeast corner of the basement of the public school, lots 17 and 18, Princess street. It was 3·5 feet above the level of G.S.C.B.M. No. 52-R.

No. 120, Biscotasing, Ont. (1930).—The apparatus was set up on a concrete pier erected in the southwest corner of the basement of the Hudson's Bay Company house, Lot 65, Block B, Lake street. It was 20·3 feet above the level of the rail in front of the C.P.R. station.

No. 121, White River, Ont. (1930).—The apparatus was set up on the concrete floor in the northwest corner of the basement of the public school, Lot 2, Block "B", as shown on the C.P.R. map of White River. It was 3 feet below the elevation of G.S.C.B.M. No. 723-A.

No. 122, Schreiber, Ont. (1930).—The apparatus was set up on the concrete floor on the western side of the basement of the public and continuation school, Winnipeg street. It was 12·7 feet above the elevation of G.S.C.B.M. No. 764.

No. 123, Federal Mine, Que. (1930).—The apparatus was set up on a concrete pier erected in the southeast corner of the boiler house at number one shaft of the Federal Lead and Zinc Mine, Lemieux township, Gaspe county. The elevation of the station was estimated from the topographical map, Publication No. 1934 of the Geological Survey of Canada. It is possible that the adopted elevation, 1736 feet, may be considerably in error.

No. 124, Cascapedia, Que. (1930).—The apparatus was set up on a concrete pier erected in the northeast corner of Mr. C. Campbell's residence, No. 316a, on part of Lot 19, Grande Cascapedia range, township of New Richmond. It was 6·4 feet below the level of the rail in front of the C.N.R. station.

No. 125, Lac au Saumon, Que. (1930).—The apparatus was set up on the floor in the eastern corner of the basement of Mr. Henry Lane's residence, Church street, part of Lot 32, first range of Humqui. It was 4·2 feet above the level of the rail in front of the C.N.R. station.

## DESCRIPTIONS OF STATIONS—*Concluded*

No. 126, La Tuque, Que. (1930).—The apparatus was set up on the concrete floor in the eastern corner of the basement of the Roman Catholic presbytery, Lots 24-A-58 and 24-A-59, Range 1, Canton Malhiot, Champlain county. It was 7·8 feet below the elevation of G.S.C.B.M. No. 1428.

No. 127, Parent, Que. (1930).—The apparatus was set up on the concrete floor in the southwest corner of the basement of the residence of Mr. O'Neill (C.N.R. agent), Lot 161, Block K, Canton Lamy, Champlain county. It was 1·3 feet above the elevation of G.S.C.B.M. No. 1372.

No. 128, Taschereau, Que. (1930).—The apparatus was set up on the concrete floor in the basement of an unused storehouse located in the yards of the Canadian National Railway. The building is about 300 feet west of G.S.C.B.M. No. 1275. The pier was 9 feet below the elevation of this bench mark.

## TABLE I—PRINCIPAL FACTS FOR GRAVITY STATIONS

### (a) In Nova Scotia

| Number and Station | Longitude | Latitude | Altitude | | Computed Gravity at Sea Level | Corrections for | | Computed Gravity | Observed Gravity | Gravity Anomalies | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | Ft. | M. | | Altitude | Topography and Isostatic Compensation | | | Hayford 113·7 km. | Airy 40 km. | Free Air | Bouguer |
| | ° ′ | ° ′ | | | | | | | | | | | |
| 22 Sydney | 60 11·8 | 46 08·4 | 39 | 12 | 980·732 | −·004 | +·018 | 980·746 | 980·735 | −·011 | −·001 | +·007 | +·006 |
| 23 Truro | 63 16·5 | 45 21·7 | 59 | 18 | 980·662 | −·006 | +·013 | 980·669 | 980·666 | −·003 | +·004 | +·010 | +·008 |
| 24 Halifax | 63 33·8 | 44 40·8 | 30 | 9 | 980·601 | −·003 | +·019 | 980·617 | 980·578 | −·039 | −·032 | −·020 | −·021 |
| 25 Yarmouth | 66 07·2 | 43 50·1 | 30 | 9 | 980·524 | −·003 | +·022 | 980·543 | 980·547 | +·004 | +·011 | +·026 | +·025 |
| Mean anomaly with regard to sign (Nova Scotia Stations) | | | | | | | | | | −·012 | −·005 | +·006 | +·005 |
| Mean anomaly without regard to sign (Nova Scotia Stations) | | | | | | | | | | ·014 | ·012 | ·016 | ·015 |

### (b) In Prince Edward Island

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 21 Charlottetown | 63 07·5 | 46 13·9 | 26 | 8 | 980·741 | −·002 | +·012 | 980·751 | 980·737 | −·014 | −·010 | −·002 | −·003 |

### (c) In New Brunswick

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 20 Moncton | 64 47·2 | 46 05·1 | 46 | 14 | 980·727 | −·004 | +·007 | 980·730 | 980·732 | +·002 | +·006 | +·009 | +·008 |
| 28 Bathurst | 65 39·0 | 47 37·2 | 16 | 5 | 980·866 | −·002 | −·004 | 980·860 | 980·840 | −·020 | −·017 | −·024 | −·025 |
| 19 St. John | 66 05·0 | 45 16·1 | 108 | 33 | 980·654 | −·010 | +·008 | 980·652 | 980·667 | +·015 | +·018 | +·023 | +·019 |
| 26 Woodstock | 67 34·5 | 46 09·0 | 184 | 56 | 980·733 | −·017 | −·001 | 980·715 | 980·703 | −·012 | −·008 | −·013 | −·019 |
| 27 Edmundston | 68 19·5 | 47 22·2 | 486 | 148 | 980·843 | −·046 | −·005 | 980·792 | 980·778 | −·014 | −·010 | −·019 | −·036 |
| Mean anomaly with regard to sign (New Brunswick Stations) | | | | | | | | | | −·006 | −·002 | −·005 | −·011 |
| Mean anomaly without regard to sign (New Brunswick Stations) | | | | | | | | | | ·013 | ·012 | ·018 | ·021 |

TABLE I—PRINCIPAL FACTS FOR GRAVITY STATIONS—*Continued*

(*d*) In Quebec

| | Number and Station | Longitude | Latitude | Altitude | | Computed Gravity at Sea Level | Corrections for | | Computed Gravity | Observed Gravity | Gravity Anomalies | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | | Ft. | M. | | Altitude | Topography and Isostatic Compensation | | | Hayford 113·7 km. | Airy 40 km. | Free Air | Bouguer |
| | | ° ′ | ° ′ | | | | | | | | | | | |
| 29 | Percé | 64 12·8 | 48 31·6 | 20 | 6 | 980·947 | −·002 | +·004 | 980·949 | 980·954 | +·005 | +·005 | +·009 | +·008 |
| 124 | Cascapedia | 65 52·5 | 48 15·2 | 37 | 11 | 980·923 | −·003 | −·011 | 980·909 | 980·910 | +·001 | +·006 | −·010 | −·011 |
| 123 | Federal Mine | 66 08·4 | 48 46·4 | 1,736 | 529 | 980·969 | −·163 | +·033 | 980·839 | 980·857 | +·018 | +·022 | +·051 | −·008 |
| 125 | Lac au Saumon | 67 21·0 | 48 25·0 | 507 | 155 | 980·937 | −·048 | −·001 | 980·888 | 980·865 | −·023 | −·018 | −·024 | −·041 |
| 5 | Tadoussac | 69 43·0 | 48 08·4 | 39 | 12 | 980·912 | −·004 | −·020 | 980·888 | 980·908 | +·020 | +·023 | ·000 | −·001 |
| 6 | Portneuf | 71 53·8 | 46 42·5 | 194 | 59 | 980·784 | −·018 | −·011 | 980·755 | 980·767 | +·012 | +·015 | +·001 | −·006 |
| 4 | Roberval | 72 13·5 | 48 30·9 | 351 | 107 | 980·946 | −·033 | −·016 | 980·897 | 980·872 | −·025 | −·021 | −·041 | −·053 |
| 126 | La Tuque | 72 47·3 | 47 26·0 | 555 | 169 | 980·849 | −·052 | −·007 | 980·790 | 980·783 | −·007 | −·004 | −·014 | −·033 |
| 116 | Montreal | 73 34·0 | 45 30·0 | 137 | 42 | 980·675 | −·013 | −·009 | 980·653 | 980·652 | −·001 | ·000 | −·010 | −·014 |
| 8 | Ste. Anne-de-Bellevue | 73 56·5 | 45 24·5 | 112 | 34 | 980·666 | −·010 | −·010 | 980·646 | 980·667 | +·021 | +·022 | +·011 | +·007 |
| 7 | St. Jerome | 74 00·0 | 45 46·6 | 351 | 107 | 980·700 | −·033 | −·006 | 980·661 | 980·685 | +·024 | +·026 | +·018 | +·006 |
| 127 | Parent | 74 36·5 | 47 55·2 | 1,401 | 427 | 980·893 | −·132 | +·012 | 980·773 | 980·775 | +·002 | +·005 | +·014 | −·034 |
| 2 | Maniwaki | 75 58·8 | 46 22·5 | 554 | 169 | 980·753 | −·052 | −·009 | 980·692 | 980·692 | ·000 | +·005 | −·009 | −·028 |
| 128 | Taschereau | 78 40·9 | 48 39·7 | 1,008 | 307 | 980·959 | −·095 | +·007 | 980·871 | 980·825 | −·046 | −·042 | −·039 | −·073 |
| | Mean anomaly with regard to sign (Quebec Stations) | | | | | | | | | | ·000 | +·003 | −·003 | −·020 |
| | Mean anomaly without regard to sign (Quebec Stations) | | | | | | | | | | ·015 | ·015 | ·018 | ·023 |

(*e*) In Ontario

| | | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 1 | Ottawa | 75 43·0 | 45 23·6 | 271 | 83 | 980·665 | −·026 | −·008 | 980·631 | 980·622 | −·009 | −·008 | −·017 | −·026 |
| 3 | Kingston | 76 28·8 | 44 13·6 | 259 | 79 | 980·560 | −·024 | −·004 | 980·532 | 980·534 | +·002 | +·004 | −·002 | −·011 |
| 117 | Pembroke | 77 06·7 | 45 49·7 | 399 | 122 | 980·704 | −·038 | −·006 | 980·660 | 980·634 | −·026 | −·023 | −·032 | −·046 |
| 118 | Haliburton | 78 30·7 | 45 02·7 | 1,071 | 326 | 980·633 | −·101 | +·012 | 980·544 | 980·524 | −·020 | −·016 | −·008 | −·045 |
| 9 | Mattawa | 78 42·3 | 46 18·7 | 558 | 170 | 980·748 | −·052 | −·010 | 980·686 | 980·654 | −·032 | −·028 | −·042 | −·061 |
| 16 | Whitby | 78 56·5 | 43 52·7 | 276 | 84 | 980·528 | −·026 | −·005 | 980·497 | 980·465 | −·032 | −·030 | −·037 | −·046 |

| | | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 10 | New Liskeard | 79 40·3 | 47 30·6 | 636 | 194 | 980·856 | −·060 | −·006 | 980·790 | 980·792 | +·002 | +·005 | −·004 | −·026 |
| 15 | Rose Point | 80 02·5 | 45 19·0 | 600 | 183 | 980·658 | −·056 | −·002 | 980·600 | 980·610 | +·010 | +·012 | +·008 | −·012 |
| 17 | Woodstock | 80 47·0 | 43 08·6 | 981 | 299 | 980·462 | −·093 | +·004 | 980·373 | 980·356 | −·017 | −·012 | −·013 | −·047 |
| 102 | Sudbury | 81 00·0 | 46 29·8 | 885 | 270 | 980·764 | −·083 | +·002 | 980·683 | 980·684 | +·001 | +·004 | +·003 | −·027 |
| 11 | Cochrane | 81 01·3 | 49 03·7 | 909 | 277 | 980·995 | −·085 | +·005 | 980·915 | 980·887 | −·028 | −·027 | −·023 | −·054 |
| 101 | Chelmsford | 81 11·8 | 46 35·0 | 882 | 269 | 980·772 | −·083 | ·000 | 980·689 | 980·695 | +·006 | +·007 | +·006 | −·024 |
| 119 | Kincardine | 81 38·5 | 44 10·5 | 659 | 201 | 980·555 | −·062 | +·005 | 980·498 | 980·476 | −·022 | −·021 | −·017 | −·040 |
| 120 | Biscotasing | 82 06·3 | 47 17·9 | 1,354 | 413 | 980·837 | −·127 | +·014 | 980·724 | 980·706 | −·018 | −·016 | −·004 | −·050 |
| 18 | Windsor | 83 02·5 | 42 19·1 | 584 | 178 | 980·388 | −·055 | −·001 | 980·332 | 980·345 | +·013 | +·015 | +·012 | −·008 |
| 13 | Chapleau | 83 24·3 | 47 50·4 | 1,411 | 430 | 980·885 | −·133 | +·009 | 980·761 | 980·770 | +·009 | +·012 | +·018 | −·030 |
| 103 | Hearst | 83 40·3 | 49 41·6 | 798 | 243 | 981·051 | −·075 | +·002 | 980·978 | 980·972 | −·006 | −·004 | −·004 | −·031 |
| 12 | Sault Ste. Marie | 84 19·5 | 46 30·4 | 610 | 186 | 980·765 | −·057 | −·003 | 980·705 | 980·684 | −·021 | −·019 | −·024 | −·045 |
| 121 | White River | 85 16·9 | 48 35·2 | 1,219 | 372 | 980·952 | −·115 | +·012 | 980·849 | 980·820 | −·029 | −·026 | −·017 | −·059 |
| 104 | Nakina | 86 41·6 | 50 11·0 | 1,013 | 309 | 981·095 | −·095 | +·003 | 981·003 | 980·987 | −·016 | −·013 | −·013 | −·047 |
| 122 | Schreiber | 87 15·7 | 48 49·0 | 993 | 303 | 980·973 | −·094 | +·013 | 980·892 | 980·879 | −·013 | −·013 | ·000 | −·034 |
| 105 | Armstrong | 89 02·7 | 50 17·0 | 1,130 | 344 | 981·104 | −·106 | ·000 | 980·998 | 981·013 | +·015 | +·017 | +·015 | −·023 |
| 14 | Port Arthur | 89 13·3 | 48 26·1 | 653 | 199 | 980·939 | −·061 | −·005 | 980·873 | 980·827 | −·046 | −·045 | −·051 | −·073 |
| 106 | Sioux Lookout | 91 54·8 | 50 05·3 | 1,208 | 368 | 981·087 | −·114 | +·002 | 980·975 | 980·982 | +·007 | +·009 | +·009 | −·032 |
| 30 | Kenora | 94 30·0 | 49 46·0 | 1,083 | 330 | 981·058 | −·102 | −·004 | 980·952 | 980·978 | +·026 | +·029 | +·022 | −·015 |
| | Mean anomaly with regard to sign (Ontario Stations) | | | | | | | | | | −·010 | −·007 | −·009 | −·036 |
| | Mean anomaly without regard to sign (Ontario Stations) | | | | | | | | | | ·017 | ·017 | ·016 | ·036 |

(*f*) In Manitoba

| | | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 72 | Riverton | 96 59·8 | 50 59·5 | 724 | 221 | 981·167 | −·068 | −·006 | 981·093 | 981·085 | −·008 | −·008 | −·014 | −·039 |
| 107 | Berens River | 97 00·9 | 52 21·4 | 720 | 219 | 981·287 | −·068 | −·002 | 981·217 | 981·203 | −·014 | −·013 | −·016 | −·041 |
| 31 | Winnipeg | 97 08·0 | 49 54·4 | 754 | 230 | 981·070 | −·071 | −·008 | 980·991 | 980·993 | +·002 | +·001 | −·006 | −·032 |
| 109 | Norway House | 97 50·0 | 53 58·8 | 720 | 219 | 981·427 | −·068 | −·003 | 981·356 | 981·349 | −·007 | −·007 | −·010 | −·035 |
| 74 | Manitou | 98 32·3 | 49 14·3 | 1,607 | 490 | 981·011 | −·151 | +·008 | 980·868 | 980·899 | +·031 | +·030 | +·039 | −·016 |
| 73 | Gypsumville | 98 37·9 | 51 46·1 | 857 | 261 | 981·235 | −·081 | −·004 | 981·150 | 981·133 | −·017 | −·017 | −·021 | −·050 |
| 108 | Grand Rapids | 99 16·0 | 53 10·4 | 736 | 224 | 981·358 | −·069 | −·004 | 981·285 | 981·302 | +·017 | +·018 | +·013 | −·012 |
| 32 | Brandon | 99 56·8 | 49 50·9 | 1,216 | 371 | 981·065 | −·114 | −·009 | 980·942 | 980·958 | +·016 | +·016 | +·007 | −·035 |
| 52 | Dauphin | 100 03·0 | 51 08·7 | 963 | 294 | 981·180 | −·091 | −·012 | 981·077 | 981·066 | −·011 | −·009 | −·023 | −·056 |
| 75 | Melita | 100 59·2 | 49 16·3 | 1,452 | 443 | 981·014 | −·137 | −·005 | 980·872 | 980·886 | +·014 | +·014 | +·009 | −·041 |
| 54 | The Pas | 101 14·7 | 53 49·7 | 872 | 266 | 981·414 | −·082 | −·004 | 981·328 | 981·341 | +·013 | +·014 | +·009 | −·021 |
| 53 | Swan River | 101 15·7 | 52 06·4 | 1,107 | 337 | 981·265 | −·104 | −·009 | 981·152 | 981·170 | +·018 | +·021 | +·009 | −·029 |
| | Mean anomaly with regard to sign (Manitoba Stations) | | | | | | | | | | +·005 | +·005 | ·000 | −·034 |
| | Mean anomaly without regard to sign (Manitoba Stations) | | | | | | | | | | ·014 | ·014 | ·015 | ·034 |

TABLE I—PRINCIPAL FACTS FOR GRAVITY STATIONS—*Continued*

(*g*) In Saskatchewan

| | Number and Station | Longitude | Latitude | Altitude | | Computed Gravity at Sea Level | Corrections for | | Computed Gravity | Observed Gravity | Gravity Anomalies | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | | Ft. | M. | | Altitude | Topography and Isostatic Compensation | | | Hayford 113·7 km. | Airy 40 km. | Free Air | Bouguer |
| | | ° ′ | ° ′ | | | | | | | | | | | |
| 78 | Moosomin | 101 40·3 | 50 08·7 | 1,892 | 577 | 981·092 | −·178 | +·006 | 980·920 | 980·932 | +·012 | +·011 | +·018 | −·047 |
| 79 | Yorkton | 102 27·3 | 51 12·8 | 1,650 | 503 | 981·186 | −·155 | +·001 | 981·032 | 981·052 | +·020 | +·020 | +·021 | −·035 |
| 76 | Estevan | 102 59·4 | 49 08·4 | 1,860 | 567 | 981·002 | −·175 | −·002 | 980·825 | 980·860 | +·035 | +·035 | +·033 | −·031 |
| 77 | Indian Head | 103 40·0 | 50 31·9 | 1,919 | 585 | 981·126 | −·181 | +·001 | 980·946 | 980·973 | +·027 | +·027 | +·028 | −·038 |
| 110 | Nokomis | 105 00·1 | 51 30·7 | 1,716 | 523 | 981·212 | −·161 | ·000 | 981·051 | 981·064 | +·013 | +·015 | +·013 | −·045 |
| 33 | Moosejaw | 105 31·8 | 50 23·7 | 1,774 | 541 | 981·114 | −·167 | −·007 | 980·940 | 980·945 | +·005 | +·005 | −·002 | −·063 |
| 55 | Prince Albert | 105 45·3 | 53 12·3 | 1,398 | 426 | 981·360 | −·131 | −·004 | 981·225 | 981·236 | +·011 | +·011 | +·007 | −·041 |
| 80 | Elbow | 106 35·5 | 51 07·2 | 1,929 | 588 | 981·178 | −·181 | ·000 | 980·997 | 980·993 | −·004 | −·005 | −·004 | −·070 |
| 56 | Saskatoon | 106 38·1 | 52 07·8 | 1,629 | 497 | 981·267 | −·153 | −·003 | 981·111 | 981·138 | +·027 | +·028 | +·024 | −·032 |
| 81 | Swift Current | 107 48·1 | 50 17·4 | 2,498 | 761 | 981·104 | −·235 | +·004 | 980·873 | 980·882 | +·009 | +·009 | +·013 | −·072 |
| 111 | North Battleford | 108 18·0 | 52 46·7 | 1,700 | 518 | 981·323 | −·160 | −·007 | 981·156 | 981·183 | +·027 | +·030 | +·020 | −·038 |
| 112 | Kindersley | 109 09·0 | 51 28·3 | 2,268 | 691 | 981·209 | −·213 | +·004 | 981·000 | 980·999 | −·001 | +·001 | +·003 | −·074 |
| | Mean anomaly with regard to sign (Saskatchewan Stations) | | | | | | | | | | +·015 | +·016 | +·015 | −·049 |
| | Mean anomaly without regard to sign (Saskatchewan Stations) | | | | | | | | | | ·016 | ·016 | ·016 | ·049 |
| | (*h*) In Alberta | | | | | | | | | | | | | |
| 34 | Medicine Hat | 110 40·0 | 50 02·4 | 2,178 | 664 | 981·082 | −·205 | −·014 | 980·863 | 980·870 | +·007 | +·009 | −·007 | −·081 |
| 57 | Vermilion | 110 50·8 | 53 21·4 | 2,016 | 614 | 981·374 | −·189 | −·001 | 981·184 | 981·185 | +·001 | +·003 | ·000 | −·069 |
| 51 | Chipewyan | 111 08·8 | 58 42·7 | 750 | 229 | 981·822 | −·071 | −·012 | 981·739 | 981·727 | −·012 | −·013 | −·024 | −·050 |
| 62 | Waterways | 111 15·3 | 56 40·5 | 820 | 250 | 981·655 | −·077 | −·024 | 981·554 | 981·555 | +·001 | +·003 | −·023 | −·051 |
| 84 | Coronation | 111 26·6 | 52 05·8 | 2,593 | 790 | 981·264 | −·244 | +·004 | 981·024 | 981·102 | −·012 | −·011 | −·008 | −·097 |
| 61 | Lac la Biche | 111 58·3 | 54 46·5 | 1,801 | 549 | 981·495 | −·169 | −·004 | 981·322 | 981·322 | ·000 | +·003 | −·004 | −·065 |
| 82 | Bassano | 112 28·2 | 50 47·5 | 2,601 | 793 | 981·149 | −·245 | −·008 | 980·896 | 980·900 | +·004 | +·005 | −·004 | −·093 |
| 71 | Lethbridge | 112 50·3 | 49 41·7 | 2,971 | 906 | 981·051 | −·280 | −·012 | 980·759 | 980·760 | +·001 | +·005 | −·011 | −·113 |

| | | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 58 | Edmonton | 113 31·0 | 53 31·6 | 2,197 | 670 | 981·388 | −·207 | −·005 | 981·176 | 981·173 | −·003 | −·001 | −·008 | −·083 |
| 83 | Red Deer | 113 47·7 | 52 16·3 | 2,810 | 856 | 981·279 | −·264 | −·005 | 981·010 | 980·995 | −·015 | −·012 | −·020 | −·116 |
| 35 | Calgary | 114 03·8 | 51 02·7 | 3,433 | 1,046 | 981·171 | −·323 | −·006 | 980·842 | 980·825 | −·017 | −·015 | −·023 | −·140 |
| 70 | Blairmore | 114 26·2 | 49 36·5 | 4,222 | 1,287 | 981·044 | −·397 | −·021 | 980·626 | 980·638 | +·012 | +·015 | −·009 | −·153 |
| 60 | Kinuso | 115 25·9 | 55 19·9 | 1,922 | 586 | 981·543 | −·181 | −·010 | 981·352 | 981·353 | +·001 | +·003 | −·009 | −·075 |
| 36 | Banff | 115 34·5 | 51 10·9 | 4,527 | 1,380 | 981·183 | −·426 | −·033 | 980·724 | 980·755 | +·031 | +·036 | −·002 | −·157 |
| 63 | Edson | 116 25·8 | 53 35·3 | 3,038 | 926 | 981·394 | −·286 | −·010 | 981·098 | 981·106 | +·008 | +·012 | −·002 | −·106 |
| 43 | Peace River | 117 17·3 | 56 14·1 | 1,063 | 324 | 981·619 | −·100 | −·038 | 981·481 | 981·486 | +·005 | +·006 | −·033 | −·069 |
| 64 | Jasper | 118 04·7 | 52 52·6 | 3,476 | 1,059 | 981·332 | −·327 | −·057 | 980·948 | 980·932 | −·016 | −·008 | −·073 | −·192 |
| 59 | Grande Prairie | 118 47·5 | 55 10·3 | 2,154 | 657 | 981·529 | −·203 | −·013 | 981·313 | 981·321 | +·008 | +·009 | −·005 | −·079 |
| | Mean anomaly with regard to sign (Alberta Stations) | | | | | | | | | | ·000 | +·003 | −·015 | −·099 |
| | Mean anomaly without regard to sign (Alberta Stations) | | | | | | | | | | ·009 | ·009 | ·015 | ·099 |

(*i*) In British Columbia

| | | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 69 | Cranbrook | 115 45·3 | 49 30·6 | 3,004 | 916 | 981·035 | −·283 | −·053 | 980·699 | 980·716 | +·017 | +·029 | −·036 | −·139 |
| 86 | Invermere | 116 03·4 | 50 30·2 | 2,715 | 828 | 981·123 | −·256 | −·086 | 980·781 | 980·767 | −·014 | −·003 | −·100 | −·193 |
| 85 | Paradise Mine | 116 19·8 | 50 28·4 | 7,470 | 2,277 | 981·121 | −·703 | +·066 | 980·484 | 980·472 | −·012 | −·011 | +·054 | −·201 |
| 37 | Field | 116 29·8 | 51 23·7 | 4,081 | 1,244 | 981·202 | −·384 | −·066 | 980·752 | 980·750 | −·002 | +·005 | −·068 | −·207 |
| 68 | Nelson | 117 17·2 | 49 29·5 | 1,823 | 556 | 981·033 | −·172 | −·094 | 980·767 | 980·755 | −·012 | −·004 | −·106 | −·168 |
| 38 | Glacier | 117 29·5 | 51 15·7 | 4,094 | 1,248 | 981·190 | −·385 | −·056 | 980·749 | 980·744 | −·005 | ·000 | −·061 | −·201 |
| 39 | Revelstoke | 118 11·8 | 50 59·8 | 1,486 | 453 | 981·167 | −·140 | −·112 | 980·915 | 980·905 | −·010 | +·001 | −·122 | −·173 |
| 67 | Phoenix | 118 36·3 | 49 05·8 | 4,529 | 1,380 | 980·998 | −·426 | +·028 | 980·600 | 980·624 | +·024 | +·027 | +·052 | −·103 |
| 87 | Vernon | 119 16·4 | 50 15·9 | 1,236 | 377 | 981·102 | −·116 | −·073 | 980·913 | 980·906 | −·007 | +·001 | −·080 | −·122 |
| 65 | Mt. Olie | 120 12·2 | 51 24·7 | 1,269 | 387 | 981·204 | −·119 | −·073 | 981·012 | 981·008 | −·004 | ·000 | −·077 | −·120 |
| 40 | Kamloops | 120 19·5 | 50 40·7 | 1,155 | 352 | 981·139 | −·109 | −·072 | 980·958 | 980·949 | −·009 | −·002 | −·081 | −·121 |
| 66 | Princeton | 120 30·4 | 49 27·1 | 2,086 | 636 | 981·030 | −·196 | −·042 | 980·792 | 980·778 | −·014 | −·006 | −·056 | −·127 |
| 41 | North Bend | 121 27·0 | 49 52·3 | 497 | 151 | 981·067 | −·047 | ..... | ..... | 980·891 | ..... | ..... | −·129 | −·146 |
| 88 | Barkerville | 121 29·8 | 53 03·8 | 4,227 | 1,288 | 981·348 | −·397 | +·007 | 980·958 | 980·950 | −·008 | −·006 | −·001 | −·145 |
| 89 | Tyaughton Creek | 122 42·0 | 50 56·9 | 2,084 | 635 | 981·163 | −·196 | −·090 | 980·877 | 980·849 | −·028 | −·021 | −·118 | −·189 |
| 113 | Prince George | 122 43·0 | 53 56·0 | 1,872 | 571 | 981·423 | −·176 | −·026 | 981·221 | 981·211 | −·010 | −·005 | −·036 | −·100 |
| 91 | Cloverdale | 122 44·0 | 49 06·5 | 10 | 3 | 980·999 | −·001 | −·045 | 980·953 | 980·939 | −·014 | −·013 | −·059 | −·059 |
| 42 | Vancouver (C.P.R. Stn.) | 123 06·8 | 49 16·8 | 31 | 9 | 981·014 | −·003 | −·054 | 980·957 | 980·952 | −·005 | −·001 | −·059 | −·060 |
| 100 | Vancouver (Brockton Point) | 123 07·1 | 49 17·8 | 37 | 11 | 981·016 | −·003 | ..... | ..... | 980·951 | ..... | ..... | −·062 | −·063 |
| 92 | Victoria | 123 19·5 | 48 24·8 | 219 | 67 | 980·937 | −·021 | −·014 | 980·902 | 980·952 | +·050 | +·052 | +·036 | +·028 |
| 48 | Liard River | 123 47·5 | 59 58·7 | 525 | 160 | 981·922 | −·049 | −·059 | 981·814 | 981·794 | −·020 | −·016 | −·079 | −·097 |
| 90 | Union Bay | 124 53·0 | 49 34·9 | 10 | 3 | 981·041 | −·001 | −·044 | 980·996 | 981·033 | +·037 | +·046 | −·007 | −·007 |
| 114 | Endako | 124 57·0 | 54 04·0 | 2,259 | 689 | 981·435 | −·213 | −·013 | 981·209 | 981·175 | −·034 | −·028 | −·047 | −·124 |
| 93 | Banfield | 125 08·7 | 48 49·9 | 30 | 9 | 980·974 | −·003 | −·007 | 980·964 | 980·981 | +·017 | +·019 | +·010 | +·009 |
| 94 | Nootka | 126 37·6 | 49 35·5 | 75 | 23 | 981·042 | −·007 | −·002 | 981·033 | 981·029 | −·004 | ·000 | −·006 | −·009 |

TABLE I—PRINCIPAL FACTS FOR GRAVITY STATIONS—*Continued*

(*i*) In British Columbia—*Concluded*

| | Number and Station | Longitude | Latitude | Altitude | | Computed Gravity at Sea Level | Corrections for | | Computed Gravity | Observed Gravity | Gravity Anomalies | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | | Ft. | M. | | Altitude | Topography and Isostatic Compensation | | | Hayford 113·7 km. | Airy 40 km. | Free Air | Bouguer |
| | | ° ′ | ° ′ | | | | | | | | | | | |
| 115 | Smithers | 127 11·0 | 54 47·0 | 1,642 | 500 | 981·496 | −·154 | −·021 | 981·321 | 981·289 | −·032 | −·023 | −·053 | −·109 |
| 95 | Quatsino | 127 37·4 | 50 32·0 | 41 | 12 | 981·126 | −·004 | −·004 | 981·118 | 981·125 | +·007 | +·011 | +·003 | +·002 |
| 99 | Ocean Falls | 127 42·9 | 52 21·3 | 60 | 18 | 981·286 | −·006 | −·057 | 981·223 | 981·232 | +·009 | +·014 | −·048 | −·050 |
| 97 | Stewart | 129 58·3 | 55 57·2 | 44 | 13 | 981·595 | −·004 | −·120 | 981·471 | 981·452 | −·019 | −·007 | −·139 | −·140 |
| 96 | Prince Rupert | 130 19·8 | 54 18·7 | 79 | 24 | 981·456 | −·007 | −·026 | 981·423 | 981·436 | +·013 | +·017 | −·013 | −·016 |
| 98 | Masset | 132 08·8 | 54 00·7 | 30 | 9 | 981·430 | −·003 | +·024 | 981·451 | 981·435 | −·016 | −·012 | +·008 | +·007 |
| | Mean anomaly with regard to sign (British Columbia Stations) | | | | | | | | | | −·004 | +·002 | −·048 | −·101 |
| | Mean anomaly without regard to sign (British Columbia Stations) | | | | | | | | | | ·016 | ·013 | ·058 | ·104 |
| | (*j*) In Northwest Territories | | | | | | | | | | | | | |
| 47 | Resolution | 113 40·5 | 61 10·1 | 500 | 152 | 982·014 | −·047 | −·009 | 981·958 | 981·946 | −·012 | −·013 | −·021 | −·038 |
| 44 | Providence | 117 39·3 | 61 21·2 | 512 | 156 | 982·028 | −·048 | −·018 | 981·962 | 981·959 | −·003 | −·003 | −·021 | −·038 |
| 45 | Simpson | 121 20·8 | 61 51·7 | 433 | 132 | 982·067 | −·041 | −·023 | 982·003 | 982·008 | +·005 | +·004 | −·018 | −·033 |
| 46 | Norman | 125 34·3 | 64 54·0 | 285 | 87 | 982·287 | −·027 | −·036 | 982·224 | 982·218 | −·006 | −·004 | −·042 | −·052 |
| 49 | Good Hope | 128 38·3 | 66 15·3 | 195 | 59 | 982·380 | −·018 | −·029 | 982·333 | 982·344 | +·011 | +·011 | −·018 | −·025 |
| 50 | Arctic Red River | 133 44·3 | 67 26·6 | 135 | 41 | 982·457 | −·013 | −·026 | 982·418 | 982·438 | +·020 | +·019 | −·006 | −·011 |
| | Mean anomaly with regard to sign (Northwest Territories Stations) | | | | | | | | | | +·003 | +·002 | −·021 | −·033 |
| | Mean anomaly without regard to sign (Northwest Territories Stations) | | | | | | | | | | ·010 | ·009 | ·021 | ·033 |
| | Mean anomaly with regard to sign (All Stations) | | | | | | | | | | −·002 | +·002 | −·015 | −·057 |
| | Mean anomaly without regard to sign (All Stations) | | | | | | | | | | ·014 | ·014 | ·026 | ·060 |

TABLE II.—MEAN ANOMALIES AND SUMS OF SQUARES OF RESIDUAL ANOMALIES FROM INTERNATIONAL* GRAVITY FORMULA FOR 126 STATIONS IN CANADA FOR VARIOUS REDUCTIONS

| — | Airy | | | | | | | | Hayford | | | | | | | Free Air | Bouguer |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | 10 km. | 15 km. | 20 km. | 30 km. | 40 km. | 60 km. | 80 km. | 100 km. | 42·6 km. | 56·9 km. | 85·3 km. | 113·7 km. | 127·9 km. | 156·25 km. | 184·6 km. | | |
| Mean anomaly with regard to sign..... | +·004 | +·004 | +·004 | +·003 | +·002 | ·000 | −·003 | −·006 | +·001 | +·001 | ·000 | −·002 | −·002 | −·003 | −·006 | −·014 | −·057 |
| Mean anomaly without regard to sign.. | ·015 | ·015 | ·015 | ·014 | ·014 | ·014 | ·015 | ·017 | ·014 | ·014 | ·014 | ·014 | ·014 | ·015 | ·016 | ·025 | ·059 |
| Sums of squares of residual anomalies in units of $10^{-6}$..... | 44,533 | 41,617 | 39,273 | 37,177 | 37,191 | 40,570 | 45,727 | 52,377 | 41,185 | 39,364 | 38,224 | 39,191 | 40,149 | 42,850 | 46,397 | 146,360 | 353,981 |

*$\gamma_o = 978{\cdot}049\ (1 + {\cdot}0052884\ \sin^2\phi - {\cdot}0000059\ \sin^2 2\phi)$

TABLE III.—MEAN ANOMALIES AND SUMS OF SQUARES OF RESIDUAL ANOMALIES FOR 126 STATIONS IN CANADA FOR VARIOUS DEPTHS OF HAYFORD COMPENSATION FROM HELMERT* AND BOWIE** GRAVITY FORMULAE

| — | Helmert | | | | | | | Bowie | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | 42·6 km. | 56·9 km. | 85·3 km. | 113·7 km. | 127·9 km. | 156·25 km. | 184·6 km. | 42·6 km. | 56·9 km. | 85·3 km. | 113·7 km. | 127·9 km. | 156·25 km. | 184·6 km. |
| Mean anomaly with regard to sign..... | + ·013 | + ·013 | + ·012 | + ·011 | + ·010 | + ·008 | + ·006 | + ·008 | + ·008 | + ·008 | + ·006 | + ·006 | + ·004 | + ·002 |
| Mean anomaly without regard to sign..... | ·018 | ·017 | ·017 | ·016 | ·016 | ·016 | ·016 | ·016 | ·016 | ·015 | ·015 | ·015 | ·015 | ·016 |
| Sums of squares of residual anomalies in units of $10^{-6}$..... | 41,442 | 39,535 | 38,066 | 38,910 | 39,677 | 42,316 | 45,747 | 41,674 | 39,687 | 38,183 | 39,333 | 40,203 | 42,790 | 46,166 |

*$\gamma_o = 978{\cdot}030\ (1 + {\cdot}005302\ \sin^2\phi - {\cdot}000007\ \sin^2 2\phi)$

**$\gamma_o = 978{\cdot}039\ (1 + {\cdot}005294\ \sin^2\phi - {\cdot}000007\ \sin^2 2\phi)$

## TABLE IV

## PERIODS OF PENDULUMS AT ALL STATIONS ESTABLISHED IN CANADA SINCE JANUARY, 1927

| | Number and Station | Knife Edge | Periods of Pendulums in Seconds | | | Value of $g$ in Dynes | | | Weighted Mean | Observer |
|---|---|---|---|---|---|---|---|---|---|---|
| | | | 1 | 2 | 3 | 1 | 2 | 3 | | |
| 1 | Ottawa (May, 1927) | 1 | ·5013490 | ·5014621 | ·5014371 | | | | 980·622 | A. H. Miller |
| | | 2 | ·5013435 | ·5014536 | ·5014321 | | | | | " |
| 101 | Chelmsford | 1 | ·5013231 | ·5014336 | ·5014103 | 980·698 | 980·697 | 980·690 | 980·695 | " |
| 102 | Sudbury | 1 | | ·5014366 | ·5014108 | | 980·685 | 970·688 | 980·684 | " |
| | | 2 | | ·5014386 | ·5014174 | | 980·682 | 980·681 | | " |
| 1 | Ottawa (June-July, 1927) | 1 | ·5013424 | ·5014528 | ·5014276 | | | | 980·622 | " |
| | | 2 | ·5013458 | ·5014544 | ·5014326 | | | | | |
| 103 | Hearst | 2 | | ·5013645 | ·5013418 | | 980·970 | 980·974 | 980·972 | " |
| 104 | Nakina | 2 | | ·5013598 | ·5013381 | | 980·987 | 980·987 | 980·987 | " |
| 105 | Armstrong | 2 | | ·5013525 | ·5013313 | | 981·014 | 981·011 | 981·013 | " |
| 106 | Sioux Lookout | 1 | | ·5013611 | | | 980·983 | | 980·982 | " |
| | | 2 | | ·5013609 | ·5013379 | | 980·979 | 980·984 | | |
| 107 | Berens River | 2 | | ·5013033 | ·5012814 | | 981·203 | 981·202 | 981·203 | " |
| 108 | Grand Rapids | 2 | | ·5012785 | ·5012545 | | 981·298 | 981·306 | 981·302 | " |
| 109 | Norway House | 1 | | ·5012674 | | | 981·349 | | 981·349 | " |
| | | 2 | | ·5012655 | ·5012429 | | 981·348 | 981·350 | | |
| 110 | Nokomis | 1 | | ·5013413 | ·5013152 | | 981·060 | 981·064 | 981·064 | A. H. Miller |
| | | 2 | | ·5013380 | ·5013139 | | 981·063 | 981·070 | | |
| 111 | North Battleford | 1 | | ·5013109 | ·5012848 | | 981·179 | 981·182 | 981·183 | " |
| | | 2 | | ·5013063 | ·5012837 | | 981·185 | 981·187 | | |
| 112 | Kindersley | 1 | | ·5013572 | ·5013320 | | 980·998 | 980·998 | 980·999 | " |
| | | 2 | | ·5013538 | ·5013306 | | 980·998 | 981·001 | | |
| 113 | Prince George | 1 | | ·5013032 | ·5012773 | | 981·209 | 981·212 | 981·211 | " |
| | | 2 | | ·5012984 | ·5012764 | | 981·212 | 981·211 | | |
| 114 | Endako | 1 | | ·5013119 | ·5012870 | | 981·175 | 981·174 | 981·175 | " |
| | | 2 | | ·5013069 | ·5012860 | | 981·177 | 981·172 | | |
| 115 | Smithers | 2 | | ·5012775 | ·5012559 | | 981·291 | 981·287 | 981·289 | " |
| 1 | Ottawa (Nov., 1927) | 1 | ·5013431 | ·5014538 | ·5014285 | | | | 980·622 | " |
| | | 2 | | ·5014482 | ·5014256 | | | | | |
| 1 | Ottawa (Jan., 1928) | 1 | | ·5014531 | ·5014280 | | | | 980·622 | " |
| | | 2 | | ·5014481 | ·5014258 | | | | | |
| 116 | Montreal | 1 | | ·5014444 | ·5014202 | | 980·654 | 980·651 | 980·652 | " |
| | | 2 | | ·5014399 | ·5014170 | | 980·652 | 980·652 | | |
| 1 | Ottawa (Feb., 1928) | 1 | | ·5014521 | ·5014271 | | | | 980·622 | " |
| | | 2 | | ·5014469 | ·5014237 | | | | | |
| 1 | Ottawa (May-June, 1928) | 1 | ·5013433 | ·5014541 | ·5014283 | | | | 980·622 | " |
| | | 2 | ·5013399 | ·5014489 | ·5014266 | | | | | |
| 1 | Ottawa (Jan., 1929) | 1 | ·5013415 | ·5014531 | ·5014273 | | | | 980·622 | " |
| | | 2 | ·5013402 | ·5014484 | ·5014261 | | | | | |
| 1 | Ottawa (Mar., 1929) | 1 | ·5013424 | ·5014528 | ·5014278 | | | | 980·622 | " |
| | | 2 | ·5013399 | ·5014484 | ·5014264 | | | | | |
| 1 | Ottawa (June, 1930) | 1 | ·5013412 | ·5014537 | ·5014282 | | | | 980·622 | W. G. Hughson |
| | | 2 | ·5013467 | ·5014538 | ·5014334 | | | | | |

TABLE IV—*Concluded*

| Number and Station | Knife Edge | Periods of Pendulums in Seconds | | | Value of $g$ in Dynes | | | Weighted Mean | Observer |
|---|---|---|---|---|---|---|---|---|---|
| | | 1 | 2 | 3 | 1 | 2 | 3 | | |
| 117 Pembroke | 1 | ..... | ·5014502 | ·5014244 | ..... | 980·632 | 980·636 | 980·634 | W G. Hughson |
| | 2 | ..... | ·5014486 | ·5014262 | ..... | 980·632 | 980·635 | | |
| 118 Haliburton | 1 | ..... | ·5014702 | ·5014538 | ..... | 980·519 | 980·521 | 980·524 | " |
| | 2 | ..... | ·5014754 | ·5014536 | ..... | 980·527 | 980·527 | | |
| 119 Kincardine | 1 | ..... | ·5014906 | ·5014664 | ..... | 980·474 | 980·472 | 980·476 | " |
| | 2 | ..... | ·5014885 | ·5014657 | ..... | 980·476 | 980·480 | | |
| 120 Biscotasing | 1 | ..... | ·5014286 | ·5014046 | ..... | 980·717 | 980·713 | 980·706 | " |
| | 2 | ..... | ·5014314 | ·5014104 | ..... | 980·699 | 980·696 | | |
| 121 White River | 1 | ..... | ·5014029 | ·5013774 | ..... | 980·817 | 980·820 | 980·820 | " |
| | 2 | ..... | ·5014004 | ·5013774 | ..... | 980·820 | 980·826 | | |
| 122 Schreiber | 1 | ..... | ·5013856 | ·5013618 | ..... | 980·885 | 980·881 | 980·879 | " |
| | 2 | ..... | ·5013862 | ·5013646 | ..... | 980·876 | 980·876 | | |
| 14 Port Arthur | 1 | ..... | ·5014000 | ·5013755 | ..... | 980·829 | 980·827 | 980·830 | " |
| | 2 | ..... | ·5013963 | ·5013764 | ..... | 980·836 | 980·829 | | |
| 123 Federal Mine | 1 | ·5012826 | ·5013938 | ·5013700 | 980·851 | 980·853 | 980·849 | 980·857 | " |
| | 2 | ·5012821 | ·5013899 | ·5013666 | 980·861 | 980·861 | 980·868 | | |
| 124 Cascapedia | 1 | ..... | ·5013802 | ·5013542 | ..... | 980·906 | 980·910 | 980·910 | " |
| | 2 | ..... | ·5013773 | ·5013544 | ..... | 980·910 | 980·915 | | |
| 125 Lac au Saumon | 1 | ..... | ·5013895 | ·5013635 | ..... | 980·870 | 980·874 | 980·865 | " |
| | 2 | ..... | ·5013910 | ·5013688 | ..... | 980·857 | 980·859 | | |
| 126 La Tuque | 1 | ..... | ·5014096 | ·5013901 | ..... | 980·791 | 980·770 | 980·783 | " |
| | 2 | ..... | ·5014103 | ·5013866 | ..... | 980·781 | 980·789 | | |
| | 1 | ..... | ·5014107 | ·5013886 | ..... | 980·787 | 980·776 | | |
| 127 Parent | 1 | ..... | ·5014148 | ·5013905 | ..... | 980·771 | 980·768 | 980·775 | " |
| | 2 | ..... | ·5014110 | ·5013888 | ..... | 980·779 | 980·781 | | " |
| 128 Taschereau | 1 | ..... | ·5013998 | ·5013744 | ..... | 980·829 | 980·831 | 980·825 | " |
| | 2 | ..... | ·5014002 | ·5013790 | ..... | 980·821 | 980·819 | | |
| 1 Ottawa (Oct., 1930) | 1 | ·5013412 | ·5014520 | ·5014277 | ..... | ..... | ..... | 980·622 | " |
| | 2 | ·5013397 | ·5014483 | ·5014255 | ..... | ..... | ..... | | |

## TABLE V

### AVERAGE ELEVATIONS AND CORRECTIONS FOR TOPOGRAPHY AND COMPENSATION FOR SEPARATE ZONES

The unit for the corrections in this table is ·0001 dyne.

| Zone | Elevation in Feet | Topography | Compensation | Topography and Compensation | Elevation in Feet | Topography | Compensation | Topography and Compensation |
|---|---|---|---|---|---|---|---|---|
| | Maniwaki, Que., No. 2 | | | | Kingston, Ont., No. 3 | | | |
| A | 566 | + 2 | 0 | + 2 | 259 | + 2 | 0 | + 2 |
| B | 570 | + 56 | 0 | + 56 | 260 | + 44 | 0 | + 44 |
| C | 575 | + 69 | 0 | + 69 | 256 | + 24 | 0 | + 24 |
| D | 585 | + 40 | 0 | + 40 | 256 | + 10 | 0 | + 10 |
| E | 610 | + 16 | 0 | + 16 | 283 | + 5 | 0 | + 5 |
| F | 630 | + 6 | 0 | + 6 | 273 | 0 | 0 | 0 |
| G | 670 | 0 | 0 | 0 | 281 | 0 | 0 | 0 |
| H | 720 | 0 | 0 | 0 | 278 | 0 | 0 | 0 |
| I | 800 | 0 | 0 | 0 | 296 | 0 | 0 | 0 |
| J | 930 | 0 | − 15 | − 15 | 300 | 0 | − 5 | − 5 |
| K | 1,256 | 0 | − 20 | − 20 | 318 | 0 | − 6 | − 6 |
| L | 1,300 | 0 | − 31 | − 31 | 337 | 0 | − 8 | − 8 |
| M | 1,245 | 0 | − 69 | − 69 | 331 | 0 | − 19 | − 19 |
| N | 1,181 | 0 | − 62 | − 62 | 505 | 0 | − 28 | − 28 |
| O | 1,028 | 0 | − 57 | − 57 | 799 | 0 | − 45 | − 45 |
| 18 | ..... | ..... | ..... | − 11 | ..... | ..... | ..... | − 10 |
| 17 | ..... | ..... | ..... | − 10 | ..... | ..... | ..... | − 11 |
| 16 | ..... | ..... | ..... | − 10 | ..... | ..... | ..... | − 11 |
| 15 | ..... | ..... | ..... | − 9 | ..... | ..... | ..... | − 11 |
| 14 | ..... | ..... | ..... | − 9 | ..... | ..... | ..... | − 12 |
| 13 | ..... | ..... | ..... | − 17 | ..... | ..... | ..... | − 14 |
| 12 | ..... | ..... | ..... | − 10 | ..... | ..... | ..... | − 7 |
| 11 | ..... | ..... | ..... | − 5 | ..... | ..... | ..... | − 5 |
| 10 | ..... | ..... | ..... | + 4 | ..... | ..... | ..... | + 6 |
| 9 | ..... | ..... | ..... | + 7 | ..... | ..... | ..... | + 8 |
| 8 | ..... | ..... | ..... | + 13 | ..... | ..... | ..... | + 13 |
| 7 | ..... | ..... | ..... | + 6 | ..... | ..... | ..... | + 7 |
| 6 | ..... | ..... | ..... | + 6* | ..... | ..... | ..... | + 7* |
| 5 | ..... | ..... | ..... | + 7* | ..... | ..... | ..... | + 7* |
| 4 | ..... | ..... | ..... | + 5* | ..... | ..... | ..... | + 5* |
| 3 | ..... | ..... | ..... | + 5* | ..... | ..... | ..... | + 5* |
| 2 | ..... | ..... | ..... | + 4* | ..... | ..... | ..... | + 4* |
| 1 | ..... | ..... | ..... | + 1* | ..... | ..... | ..... | + 1* |
| | | Total..... | | − 88 | | Total..... | | − 44 |

*These values have been interpolated from those obtained for neighbouring stations.

TABLE V—*Continued*

AVERAGE ELEVATIONS AND CORRECTIONS FOR TOPOGRAPHY AND COMPENSATION FOR SEPARATE ZONES

The unit for the corrections in this table is ·0001 dyne.

| Zone | Elevation in Feet | Topography | Compensation | Topography and Compensation | Elevation in Feet | Topography | Compensation | Topography and Compensation |
|---|---|---|---|---|---|---|---|---|
| | Roberval, Que., No. 4 | | | | Tadoussac, Que., No. 5 | | | |
| A | 350 | + 2 | 0 | + 2 | 40 | + 2 | 0 | + 2 |
| B | 350 | + 52 | 0 | + 52 | 40 | + 12 | 0 | + 12 |
| C | 350 | + 40 | 0 | + 40 | 45 | 0 | 0 | 0 |
| D | 360 | + 18 | 0 | + 18 | 28 | + 1 | 0 | + 1 |
| E | 370 | + 8 | 0 | + 8 | 38 | + 1 | 0 | + 1 |
| F | 385 | 0 | 0 | 0 | 120 | 0 | 0 | 0 |
| G | 405 | 0 | 0 | 0 | 145 | 0 | 0 | 0 |
| H | 435 | 0 | 0 | 0 | 180 | 0 | 0 | 0 |
| I | 480 | 0 | 0 | 0 | 264 | 0 | 0 | 0 |
| J | 557 | 0 | − 9 | − 9 | 325 | 0 | − 5 | − 5 |
| K | 592 | 0 | − 12 | − 12 | 572 | 0 | − 11 | − 11 |
| L | 829 | 0 | − 20 | − 20 | 748 | 0 | − 18 | − 18 |
| M | 1,052 | 0 | − 59 | − 59 | 821 | 0 | − 46 | − 46 |
| N | 1,339 | 0 | − 70 | − 70 | 1,105 | 0 | − 57 | − 57 |
| O | 1,391 | 0 | − 78 | − 78 | 1,103 | 0 | − 62 | − 62 |
| 18 | | | | − 14 | | | | − 10 |
| 17 | | | | − 11 | | | | − 11 |
| 16 | | | | − 12 | | | | − 11 |
| 15 | | | | − 12 | | | | − 11 |
| 14 | | | | − 12 | | | | − 10 |
| 13 | | | | − 16 | | | | − 15 |
| 12 | | | | − 9 | | | | − 9 |
| 11 | | | | − 5 | | | | − 3 |
| 10 | | | | + 2 | | | | + 4 |
| 9 | | | | + 7 | | | | + 13 |
| 8 | | | | + 16 | | | | + 17 |
| 7 | | | | + 6 | | | | + 6 |
| 6 | | | | + 5* | | | | + 5* |
| 5 | | | | + 7* | | | | + 6* |
| 4 | | | | + 5* | | | | + 5* |
| 3 | | | | + 5* | | | | + 5* |
| 2 | | | | + 4* | | | | + 4* |
| 1 | | | | + 1* | | | | + 1* |
| | | Total | | −161 | | Total | | −197 |

*These values have been interpolated from those obtained for neighbouring stations.

TABLE V—*Continued*

AVERAGE ELEVATIONS AND CORRECTIONS FOR TOPOGRAPHY AND COMPENSATION FOR SEPARATE ZONES

The units for the corrections in this table is ·0001 dyne.

| Zone | Elevation in Feet | Topography | Compensation | Topography and Compensation | Elevation in Feet | Topography | Compensation | Topography and Compensation |
|---|---|---|---|---|---|---|---|---|
| | Portneuf, Que., No. 6 | | | | St. Jerome, Que., No. 7 | | | |
| A | 194 | + 2 | 0 | + 2 | 300 | + 2 | 0 | + 2 |
| B | 164 | + 35 | 0 | + 35 | 300 | + 48 | 0 | + 48 |
| C | 166 | + 14 | 0 | + 14 | 300 | + 32 | 0 | + 32 |
| D | 179 | + 7 | 0 | + 7 | 298 | + 12 | 0 | + 12 |
| E | 186 | + 4 | 0 | + 4 | 283 | + 6 | 0 | + 6 |
| F | 225 | 0 | 0 | 0 | 279 | 0 | 0 | 0 |
| G | 217 | 0 | 0 | 0 | 278 | 0 | 0 | 0 |
| H | 212 | 0 | 0 | 0 | 288 | 0 | 0 | 0 |
| I | 205 | 0 | 0 | 0 | 326 | 0 | 0 | 0 |
| J | 214 | 0 | − 4 | − 4 | 353 | 0 | − 6 | − 6 |
| K | 262 | 0 | − 5 | − 5 | 410 | 0 | − 8 | − 8 |
| L | 410 | 0 | − 10 | − 10 | 370 | 0 | − 9 | − 9 |
| M | 618 | 0 | − 35 | − 35 | 491 | 0 | − 27 | − 27 |
| N | 817 | 0 | − 44 | − 44 | 628 | 0 | − 35 | − 35 |
| O | 1,147 | 0 | − 63 | − 63 | 839 | 0 | − 47 | − 47 |
| 18 | | | | − 12 | | | | − 11 |
| 17 | | | | − 11 | | | | − 10 |
| 16 | | | | − 11 | | | | − 12 |
| 15 | | | | − 11 | | | | − 14 |
| 14 | | | | − 12 | | | | − 12 |
| 13 | | | | − 15 | | | | − 15 |
| 12 | | | | − 7 | | | | − 7 |
| 11 | | | | + 2 | | | | − 3 |
| 10 | | | | + 7 | | | | + 3 |
| 9 | | | | + 9 | | | | + 8 |
| 8 | | | | + 16 | | | | + 13 |
| 7 | | | | + 6 | | | | + 5 |
| 6 | | | | + 5* | | | | + 6* |
| 5 | | | | + 6* | | | | + 7* |
| 4 | | | | + 5* | | | | + 5* |
| 3 | | | | + 5* | | | | + 5* |
| 2 | | | | + 4* | | | | + 4* |
| 1 | | | | + 1* | | | | + 1* |
| | | Total | | −112 | | Total | | − 59 |

*These values have been interpolated from those obtained for neighbouring stations.

TABLE V—*Continued*

AVERAGE ELEVATIONS AND CORRECTIONS FOR TOPOGRAPHY AND COMPENSATION FOR SEPARATE ZONES

The unit for the corrections in this table is ·0001 dyne.

| Zone | Elevation in Feet | Topography | Compensation | Topography and Compensation | Elevation in Feet | Topography | Compensation | Topography and Compensation |
|---|---|---|---|---|---|---|---|---|
| | Ste. Anne-de-Bellevue, Que., No. 8 | | | | Mattawa, Ont., No. 9 | | | |
| A | 112 | + 2 | 0 | + 2 | 552 | + 2 | 0 | + 2 |
| B | 115 | + 26 | 0 | + 26 | 562 | + 56 | 0 | + 56 |
| C | 108 | + 5 | 0 | + 5 | 565 | + 66 | 0 | + 66 |
| D | 98 | + 4 | 0 | + 4 | 565 | + 38 | 0 | + 38 |
| E | 93 | + 2 | 0 | + 2 | 565 | + 15 | 0 | + 15 |
| F | 94 | 0 | 0 | 0 | 580 | + 4 | 0 | + 4 |
| G | 100 | 0 | 0 | 0 | 590 | 0 | 0 | 0 |
| H | 97 | 0 | 0 | 0 | 600 | 0 | 0 | 0 |
| I | 85 | 0 | 0 | 0 | 700 | 0 | 0 | 0 |
| J | 112 | 0 | − 2 | − 2 | 900 | 0 | − 14 | − 14 |
| K | 138 | 0 | − 3 | − 3 | 975 | 0 | − 19 | − 19 |
| L | 175 | 0 | − 4 | − 4 | 1,069 | 0 | − 26 | − 26 |
| M | 295 | 0 | − 17 | − 17 | 1,142 | 0 | − 64 | − 64 |
| N | 567 | 0 | − 31 | − 31 | 1,172 | 0 | − 62 | − 62 |
| O | 948 | 0 | − 53 | − 53 | 1,099 | 0 | − 62 | − 62 |
| 18 | | | | − 10 | | | | − 10 |
| 17 | | | | − 11 | | | | − 9 |
| 16 | | | | − 12 | | | | − 9 |
| 15 | | | | − 13 | | | | − 9 |
| 14 | | | | − 13 | | | | − 9 |
| 13 | | | | − 16 | | | | − 16 |
| 12 | | | | − 7 | | | | − 10 |
| 11 | | | | − 3 | | | | − 6 |
| 10 | | | | + 5 | | | | − 4 |
| 9 | | | | + 8 | | | | + 3 |
| 8 | | | | + 13 | | | | + 10 |
| 7 | | | | + 5 | | | | + 5 |
| 6 | | | | + 6* | | | | + 6* |
| 5 | | | | + 7* | | | | + 8* |
| 4 | | | | + 5* | | | | + 5* |
| 3 | | | | + 5* | | | | + 5* |
| 2 | | | | + 4* | | | | + 3* |
| 1 | | | | + 1* | | | | + 1* |
| | | Total | | − 97 | | Total | | −102 |

*These values have been interpolated from those obtained for neighbouring stations.

TABLE V—*Continued*

AVERAGE ELEVATIONS AND CORRECTIONS FOR TOPOGRAPHY AND COMPENSATION FOR SEPARATE ZONES

The unit for the corrections in this table is ·0001 dyne.

| Zone | Elevation in Feet | Topography | Compensation | Topography and Compensation | Elevation in Feet | Topography | Compensation | Topography and Compensation |
|---|---|---|---|---|---|---|---|---|
| | New Liskeard, Ont., No. 10 | | | | Cochrane, Ont., No. 11 | | | |
| A | 630 | + 2 | 0 | + 2 | 909 | + 2 | 0 | + 2 |
| B | 635 | + 58 | 0 | + 58 | 915 | + 63 | 0 | + 63 |
| C | 635 | + 75 | 0 | + 75 | 910 | + 97 | 0 | + 97 |
| D | 635 | + 46 | 0 | + 46 | 900 | + 72 | 0 | + 72 |
| E | 635 | + 18 | 0 | + 18 | 900 | + 32 | 0 | + 32 |
| F | 710 | + 8 | 0 | + 8 | 900 | + 12 | 0 | + 12 |
| G | 720 | 0 | 0 | 0 | 900 | 0 | 0 | 0 |
| H | 730 | 0 | 0 | 0 | 900 | 0 | 0 | 0 |
| I | 750 | 0 | 0 | 0 | 900 | 0 | 0 | 0 |
| J | 750 | 0 | − 12 | − 12 | 900 | 0 | − 14 | − 14 |
| K | 859 | 0 | − 17 | − 17 | 900 | 0 | − 18 | − 18 |
| L | 850 | 0 | − 20 | − 20 | 900 | 0 | − 22 | − 22 |
| M | 983 | 0 | − 55 | − 55 | 691 | 0 | − 39 | − 39 |
| N | 1,148 | 0 | − 60 | − 60 | 773 | 0 | − 39 | − 39 |
| O | 1,041 | 0 | − 58 | − 58 | 930 | 0 | − 52 | − 52 |
| 18 | | | | − 11 | | | | − 8 |
| 17 | | | | − 11 | | | | − 8 |
| 16 | | | | − 11 | | | | − 8 |
| 15 | | | | − 10 | | | | − 8 |
| 14 | | | | − 10 | | | | − 8 |
| 13 | | | | − 14 | | | | − 12 |
| 12 | | | | − 9 | | | | − 9 |
| 11 | | | | − 8 | | | | − 8 |
| 10 | | | | − 4 | | | | − 6 |
| 9 | | | | + 3 | | | | − 2 |
| 8 | | | | + 10 | | | | + 4 |
| 7 | | | | + 4 | | | | + 5 |
| 6 | | | | + 5* | | | | + 4 |
| 5 | | | | + 8* | | | | + 9 |
| 4 | | | | + 5* | | | | + 5 |
| 3 | | | | + 5* | | | | + 5 |
| 2 | | | | + 3* | | | | + 3 |
| 1 | | | | + 1* | | | | + 1 |
| | | Total | | − 59 | | Total | | + 53 |

*These values have been interpolated from those obtained for neighbouring stations.

TABLE V—*Continued*

AVERAGE ELEVATIONS AND CORRECTIONS FOR TOPOGRAPHY AND COMPENSATION FOR SEPARATE ZONES

The unit for the corrections in this table is ·0001 dyne.

| Zone | Elevation in Feet | Topography | Compensation | Topography and Compensation | Elevation in Feet | Topography | Compensation | Topography and Compensation |
|---|---|---|---|---|---|---|---|---|
| | Sault Ste. Marie, Ont., No. 12 | | | | Chapleau, Ont., No. 13 | | | |
| A | 612 | + 2 | 0 | + 2 | 1,406 | + 2 | 0 | + 2 |
| B | 625 | + 57 | 0 | + 57 | 1,412 | + 64 | 0 | + 64 |
| C | 625 | + 74 | 0 | + 74 | 1,415 | +121 | 0 | +121 |
| D | 625 | + 45 | 0 | + 45 | 1,415 | +132 | 0 | +132 |
| E | 625 | + 17 | 0 | + 17 | 1,420 | + 72 | 0 | + 72 |
| F | 625 | + 6 | 0 | + 6 | 1,430 | + 29 | 0 | + 29 |
| G | 650 | 0 | 0 | 0 | 1,440 | + 11 | 0 | + 11 |
| H | 700 | 0 | 0 | 0 | 1,450 | + 16 | − 16 | 0 |
| I | 750 | 0 | 0 | 0 | 1,465 | + 20 | − 20 | 0 |
| J | 750 | 0 | − 12 | − 12 | 1,475 | 0 | − 16 | − 16 |
| K | 750 | 0 | − 15 | − 15 | 1,500 | 0 | − 20 | − 20 |
| L | 750 | 0 | − 18 | − 18 | 1,500 | 0 | − 36 | − 36 |
| M | 839 | 0 | − 47 | − 47 | 1,500 | 0 | − 84 | − 84 |
| N | 833 | 0 | − 49 | − 49 | 1,500 | 0 | − 80 | − 80 |
| O | 849 | 0 | − 48 | − 48 | 1,227 | 0 | − 69 | − 69 |
| 18 | | | | − 9 | | | | − 10 |
| 17 | | | | − 9 | | | | − 9 |
| 16 | | | | − 9 | | | | − 7 |
| 15 | | | | − 9 | | | | − 6 |
| 14 | | | | − 8 | | | | − 7 |
| 13 | | | | − 14 | | | | − 13 |
| 12 | | | | − 9 | | | | − 9 |
| 11 | | | | − 8 | | | | − 9 |
| 10 | | | | − 7 | | | | − 6 |
| 9 | | | | − 2 | | | | − 3 |
| 8 | | | | + 4 | | | | + 6 |
| 7 | | | | + 5 | | | | + 5 |
| 6 | | | | + 6* | | | | + 5* |
| 5 | | | | + 9* | | | | + 9* |
| 4 | | | | + 6* | | | | + 5* |
| 3 | | | | + 5* | | | | + 5* |
| 2 | | | | + 3* | | | | + 3* |
| 1 | | | | + 1* | | | | + 1* |
| | | Total | | − 33 | | Total | | + 86 |

*These values have been interpolated from those obtained for neighbouring stations.

TABLE V—*Continued*

AVERAGE ELEVATIONS AND CORRECTIONS FOR TOPOGRAPHY AND COMPENSATION FOR SEPARATE ZONES

The units for the corrections in this table is ·0001 dyne.

| Zone | Elevation in Feet | Topography | Compensation | Topography and Compensation | Elevation in Feet | Topography | Compensation | Topography and Compensation |
|---|---|---|---|---|---|---|---|---|
| | Port Arthur, Ont., No. 14 | | | | Rose Point, Ont., No. 15 | | | |
| A | 654 | + 2 | 0 | + 2 | 598 | + 2 | 0 | + 2 |
| B | 643 | + 56 | 0 | + 56 | 600 | + 57 | 0 | + 57 |
| C | 630 | + 74 | 0 | + 74 | 600 | + 72 | 0 | + 72 |
| D | 630 | + 46 | 0 | + 46 | 600 | + 42 | 0 | + 42 |
| E | 630 | + 16 | 0 | + 16 | 600 | + 16 | 0 | + 16 |
| F | 630 | + 6 | 0 | + 6 | 600 | + 5 | 0 | + 5 |
| G | 640 | 0 | 0 | 0 | 610 | 0 | 0 | 0 |
| H | 640 | 0 | 0 | 0 | 620 | 0 | 0 | 0 |
| I | 650 | 0 | 0 | 0 | 625 | 0 | 0 | 0 |
| J | 690 | 0 | − 11 | − 11 | 675 | 0 | − 11 | − 11 |
| K | 660 | 0 | − 13 | − 13 | 675 | 0 | − 14 | − 14 |
| L | 790 | 0 | − 20 | − 20 | 669 | 0 | − 16 | − 16 |
| M | 990 | 0 | − 55 | − 55 | 733 | 0 | − 41 | − 41 |
| N | 880 | 0 | − 46 | − 46 | 818 | 0 | − 44 | − 44 |
| O | 740 | 0 | − 42 | − 42 | 932 | 0 | − 52 | − 52 |
| 18 | | | | − 9 | | | | − 10 |
| 17 | | | | − 10 | | | | − 9 |
| 16 | | | | − 10 | | | | − 7 |
| 15 | | | | − 12 | | | | − 9 |
| 14 | | | | − 12 | | | | − 9 |
| 13 | | | | − 17 | | | | − 16 |
| 12 | | | | − 9 | | | | − 9 |
| 11 | | | | − 8 | | | | − 7 |
| 10 | | | | − 6 | | | | − 4 |
| 9 | | | | − 6 | | | | + 4 |
| 8 | | | | 0 | | | | + 7 |
| 7 | | | | + 6 | | | | + 6 |
| 6 | | | | + 7* | | | | + 6* |
| 5 | | | | + 9* | | | | + 8* |
| 4 | | | | + 6* | | | | + 5* |
| 3 | | | | + 5* | | | | + 5* |
| 2 | | | | + 3* | | | | + 3* |
| 1 | | | | + 1* | | | | + 1* |
| | | Total | | − 49 | | Total | | − 19 |

*These values have been interpolated from those obtained for neighbouring stations.

TABLE V—*Continued*

AVERAGE ELEVATIONS AND CORRECTIONS FOR TOPOGRAPHY AND COMPENSATION FOR SEPARATE ZONES

The unit for the corrections in this table is ·0001 dyne.

| Zone | Elevation in Feet | Topography | Compensation | Topography and Compensation | Elevation in Feet | Topography | Compensation | Topography and Compensation |
|---|---|---|---|---|---|---|---|---|
| | Whitby, Ont., No. 16 | | | | Woodstock, Ont., No. 17 | | | |
| A | 284 | + 2 | 0 | + 2 | 981 | + 2 | 0 | + 2 |
| B | 290 | + 47 | 0 | + 47 | 1,000 | + 62 | 0 | + 62 |
| C | 290 | + 30 | 0 | + 30 | 999 | +104 | 0 | +104 |
| D | 290 | + 11 | 0 | + 11 | 978 | + 81 | 0 | + 81 |
| E | 293 | + 6 | 0 | + 6 | 991 | + 38 | 0 | + 38 |
| F | 300 | 0 | 0 | 0 | 992 | + 15 | 0 | + 15 |
| G | 316 | 0 | 0 | 0 | 1,021 | + 1 | 0 | + 1 |
| H | 325 | 0 | 0 | 0 | 1,044 | 0 | 0 | 0 |
| I | 337 | 0 | 0 | 0 | 1,022 | 0 | 0 | 0 |
| J | 360 | 0 | − 6 | − 6 | 1,028 | 0 | − 16 | − 16 |
| K | 431 | 0 | − 9 | − 9 | 1,238 | 0 | − 20 | − 20 |
| L | 491 | 0 | − 12 | − 12 | 1,088 | 0 | − 26 | − 26 |
| M | 433 | 0 | − 24 | − 24 | 1,446 | 0 | − 81 | − 81 |
| N | 592 | 0 | − 32 | − 32 | 872 | 0 | − 47 | − 47 |
| O | 931 | 0 | − 52 | − 52 | 740 | 0 | − 41 | − 41 |
| 18 | ..... | ..... | ..... | − 10 | ..... | ..... | ..... | − 8 |
| 17 | ..... | ..... | ..... | − 8 | ..... | ..... | ..... | − 8 |
| 16 | ..... | ..... | ..... | − 8 | ..... | ..... | ..... | − 9 |
| 15 | ..... | ..... | ..... | − 9 | ..... | ..... | ..... | − 10 |
| 14 | ..... | ..... | ..... | − 10 | ..... | ..... | ..... | − 10 |
| 13 | ..... | ..... | ..... | − 13 | ..... | ..... | ..... | − 16 |
| 12 | ..... | ..... | ..... | − 7 | ..... | ..... | ..... | − 8 |
| 11 | ..... | ..... | ..... | − 1 | ..... | ..... | ..... | − 5 |
| 10 | ..... | ..... | ..... | + 5 | ..... | ..... | ..... | − 3 |
| 9 | ..... | ..... | ..... | + 6 | ..... | ..... | ..... | + 3 |
| 8 | ..... | ..... | ..... | + 10 | ..... | ..... | ..... | + 7 |
| 7 | ..... | ..... | ..... | + 5 | ..... | ..... | ..... | + 5 |
| 6 | ..... | ..... | ..... | + 7* | ..... | ..... | ..... | + 7* |
| 5 | ..... | ..... | ..... | + 8* | ..... | ..... | ..... | + 8* |
| 4 | ..... | ..... | ..... | + 5* | ..... | ..... | ..... | + 5* |
| 3 | ..... | ..... | ..... | + 5* | ..... | ..... | ..... | + 5* |
| 2 | ..... | ..... | ..... | + 4* | ..... | ..... | ..... | + 3* |
| 1 | ..... | ..... | ..... | + 1* | ..... | ..... | ..... | + 1* |
| | | Total..... | | − 49 | | Total..... | | + 39 |

*These values have been interpolated from those obtained for neighbouring stations.

TABLE V—*Continued*

AVERAGE ELEVATIONS AND CORRECTIONS FOR TOPOGRAPHY AND COMPENSATION FOR SEPARATE ZONES

The unit for the corrections in this table is ·0001 dyne.

| Zone | Elevation in Feet | Topography | Compensation | Topography and Compensation | Elevation in Feet | Topography | Compensation | Topography and Compensation |
|---|---|---|---|---|---|---|---|---|
| | Windsor, Ont., No. 18 | | | | St. John, N.B., No. 19 | | | |
| A | 584 | + 2 | 0 | + 2 | 108 | + 2 | 0 | + 2 |
| B | 590 | + 57 | 0 | + 57 | 75 | + 18 | 0 | + 18 |
| C | 587 | + 72 | 0 | + 72 | 64 | + 3 | 0 | + 3 |
| D | 583 | + 40 | 0 | + 40 | 42 | + 2 | 0 | + 2 |
| E | 586 | + 15 | 0 | + 15 | 24 | 0 | 0 | 0 |
| F | 592 | + 5 | 0 | + 5 | 91 | 0 | 0 | 0 |
| G | 600 | 0 | 0 | 0 | 60 | 0 | 0 | 0 |
| H | 602 | 0 | 0 | 0 | 48 | 0 | 0 | 0 |
| I | 604 | 0 | 0 | 0 | 56 | 0 | 0 | 0 |
| J | 603 | 0 | − 10 | − 10 | 90 | 0 | − 2 | − 2 |
| K | 616 | 0 | − 12 | − 12 | 91 | 0 | − 2 | − 2 |
| L | 616 | 0 | − 15 | − 15 | 97 | 0 | − 3 | − 3 |
| M | 695 | 0 | − 39 | − 39 | 75 | 0 | − 5 | − 5 |
| N | 743 | 0 | − 40 | − 40 | 167 | 0 | − 11 | − 11 |
| O | 740 | 0 | − 41 | − 41 | 318 | 0 | − 18 | − 18 |
| 18 | | | | − 10 | | | | − 2 |
| 17 | | | | − 10 | | | | − 2 |
| 16 | | | | − 12 | | | | − 2 |
| 15 | | | | − 10 | | | | − 3 |
| 14 | | | | − 9 | | | | − 3 |
| 13 | | | | − 15 | | | | + 4 |
| 12 | | | | − 11 | | | | + 10 |
| 11 | | | | − 9 | | | | + 18 |
| 10 | | | | − 2 | | | | + 16 |
| 9 | | | | + 3 | | | | + 14 |
| 8 | | | | + 5 | | | | + 18 |
| 7 | | | | + 4 | | | | + 6 |
| 6 | | | | + 7 | | | | + 6* |
| 5 | | | | + 8 | | | | + 5* |
| 4 | | | | + 6 | | | | + 5* |
| 3 | | | | + 5 | | | | + 5* |
| 2 | | | | + 3 | | | | + 4* |
| 1 | | | | + 1 | | | | + 1* |
| | | Total | | − 12 | | Total | | + 84 |

*These values have been interpolated from those obtained for neighbouring stations.

TABLE V—*Continued*

AVERAGE ELEVATIONS AND CORRECTIONS FOR TOPOGRAPHY AND COMPENSATION FOR SEPARATE ZONES

The unit for the corrections in this table is ·0001 dyne.

| Zone | Elevation in Feet | Topography | Compensation | Topography and Compensation | Elevation in Feet | Topography | Compensation | Topography and Compensation |
|---|---|---|---|---|---|---|---|---|
| | Moncton, N.B., No. 20 | | | | Charlottetown, P.E.I., No. 21 | | | |
| A | 46 | + 2 | 0 | + 2 | 26 | + 2 | 0 | + 2 |
| B | 52 | + 13 | 0 | + 13 | 25 | + 6 | 0 | + 6 |
| C | 52 | 0 | 0 | 0 | 7 | 0 | 0 | 0 |
| D | 51 | + 2 | 0 | + 2 | 22 | + 1 | 0 | + 1 |
| E | 53 | + 1 | 0 | + 1 | 13 | 0 | 0 | 0 |
| F | 66 | 0 | 0 | 0 | 8 | 0 | 0 | 0 |
| G | 75 | 0 | 0 | 0 | 22 | 0 | 0 | 0 |
| H | 95 | 0 | 0 | 0 | 24 | 0 | 0 | 0 |
| I | 135 | 0 | 0 | 0 | 32 | 0 | 0 | 0 |
| J | 230 | 0 | − 4 | − 4 | 28 | 0 | − 1 | − 1 |
| K | 256 | 0 | − 5 | − 5 | 65 | 0 | − 1 | − 1 |
| L | 286 | 0 | − 7 | − 7 | 11 | 0 | 0 | 0 |
| M | 272 | 0 | − 16 | − 16 | 0 | 0 | 0 | 0 |
| N | 195 | 0 | − 12 | − 12 | 54 | 0 | − 4 | − 4 |
| O | 205 | 0 | − 12 | − 12 | 166 | 0 | − 10 | − 10 |
| 18 | | | | − 3 | | | | − 2 |
| 17 | | | | − 2 | | | | − 2 |
| 16 | | | | − 2 | | | | 0 |
| 15 | | | | − 3 | | | | 0 |
| 14 | | | | − 4 | | | | − 1 |
| 13 | | | | + 5 | | | | + 9 |
| 12 | | | | + 10 | | | | + 14 |
| 11 | | | | + 18 | | | | + 18 |
| 10 | | | | + 18 | | | | + 19 |
| 9 | | | | + 17 | | | | + 18 |
| 8 | | | | + 19 | | | | + 19 |
| 7 | | | | + 7 | | | | + 7 |
| 6 | | | | + 6* | | | | + 6* |
| 5 | | | | + 5* | | | | + 4* |
| 4 | | | | + 5* | | | | + 5* |
| 3 | | | | + 6* | | | | + 6* |
| 2 | | | | + 4* | | | | + 4* |
| 1 | | | | + 1* | | | | + 1* |
| | | Total | | + 69 | | Total | | +118 |

*These values have been interpolated from those obtained for neighbouring stations.

TABLE V—*Continued*

AVERAGE ELEVATIONS AND CORRECTIONS FOR TOPOGRAPHY AND COMPENSATION FOR SEPARATE ZONES

The units for the corrections in this table is ·0001 dyne.

| Zone | Elevation in Feet | Topography | Compensation | Topography and Compensation | Elevation in Feet | Topography | Compensation | Topography and Compensation |
|---|---|---|---|---|---|---|---|---|
| | Sydney, N.S., No. 22 | | | | Truro, N.S., No. 23 | | | |
| A | 39 | + 2 | 0 | + 2 | 59 | + 2 | 0 | + 2 |
| B | 40 | + 12 | 0 | + 12 | 60 | + 16 | 0 | + 16 |
| C | 27 | + 1 | 0 | + 1 | 60 | + 2 | 0 | + 2 |
| D | 26 | 0 | 0 | 0 | 60 | + 2 | 0 | + 2 |
| E | 6 | 0 | 0 | 0 | 65 | + 1 | 0 | + 1 |
| F | 58 | 0 | 0 | 0 | 75 | 0 | 0 | 0 |
| G | 110 | 0 | 0 | 0 | 85 | 0 | 0 | 0 |
| H | 138 | 0 | 0 | 0 | 100 | 0 | 0 | 0 |
| I | 136 | 0 | 0 | 0 | 140 | 0 | 0 | 0 |
| J | 265 | 0 | − 4 | − 4 | 275 | 0 | − 4 | − 4 |
| K | 321 | 0 | − 6 | − 6 | 246 | 0 | − 5 | − 5 |
| L | 212 | 0 | − 6 | − 6 | 415 | 0 | − 10 | − 10 |
| M | 228 | 0 | − 15 | − 15 | 381 | 0 | − 21 | − 21 |
| N | 24 | 0 | − 2 | − 2 | 211 | 0 | − 14 | − 14 |
| O | −313 | 0 | + 14 | + 14 | 30 | 0 | − 3 | − 3 |
| 18 | | | | + 3 | | | | − 1 |
| 17 | | | | + 2 | | | | 0 |
| 16 | | | | + 2 | | | | 0 |
| 15 | | | | + 1 | | | | 0 |
| 14 | | | | + 6 | | | | + 5 |
| 13 | | | | + 27 | | | | + 25 |
| 12 | | | | + 21 | | | | + 25 |
| 11 | | | | + 21 | | | | + 22 |
| 10 | | | | + 23 | | | | + 20 |
| 9 | | | | + 21 | | | | + 18 |
| 8 | | | | + 20 | | | | + 19 |
| 7 | | | | + 8 | | | | + 7 |
| 6 | | | | + 6* | | | | + 6* |
| 5 | | | | + 4* | | | | + 4* |
| 4 | | | | + 5* | | | | + 5* |
| 3 | | | | + 6* | | | | + 6* |
| 2 | | | | + 4* | | | | + 4* |
| 1 | | | | + 1* | | | | + 1* |
| | | Total | | +177 | | Total | | +132 |

*These values have been interpolated from those obtained for neighbouring stations.

TABLE V—*Continued*

AVERAGE ELEVATIONS AND CORRECTIONS FOR TOPOGRAPHY AND COMPENSATION FOR SEPARATE ZONES

The unit for the corrections in this table is ·0001 dyne.

| Zone | Elevation in Feet | Topography | Compensation | Topography and Compensation | Elevation in Feet | Topography | Compensation | Topography and Compensation |
|---|---|---|---|---|---|---|---|---|
| | Halifax, N.S., No. 24 | | | | Yarmouth, N.S., No. 25 | | | |
| A | 30 | + 2 | 0 | + 2 | 30 | + 2 | 0 | + 2 |
| B | 38 | + 7 | 0 | + 7 | 30 | + 8 | 0 | + 8 |
| C | 41 | 0 | 0 | 0 | 30 | 0 | 0 | 0 |
| D | 49 | − 2 | 0 | − 2 | 30 | + 1 | 0 | + 1 |
| E | 24 | 0 | 0 | 0 | 13 | 0 | 0 | 0 |
| F | 34 | 0 | 0 | 0 | 25 | 0 | 0 | 0 |
| G | 78 | 0 | 0 | 0 | 25 | 0 | 0 | 0 |
| H | 105 | 0 | 0 | 0 | 28 | 0 | 0 | 0 |
| I | 156 | 0 | 0 | 0 | 26 | 0 | 0 | 0 |
| J | 154 | 0 | − 3 | − 3 | − 6 | 0 | 0 | 0 |
| K | 125 | 0 | − 3 | − 3 | − 14 | 0 | 0 | 0 |
| L | 87 | 0 | − 3 | − 3 | − 29 | 0 | + 1 | + 1 |
| M | 58 | 0 | − 7 | − 7 | − 19 | 0 | − 3 | − 3 |
| N | − 4 | 0 | − 5 | − 5 | −198 | 0 | + 4 | + 4 |
| O | − 81 | 0 | − 1 | − 1 | −305 | 0 | + 8 | + 8 |
| 18 | ..... | ..... | ..... | 0 | ..... | ..... | ..... | + 1 |
| 17 | ..... | ..... | ..... | 0 | ..... | ..... | ..... | + 2 |
| 16 | ..... | ..... | ..... | + 6 | ..... | ..... | ..... | + 6 |
| 15 | ..... | ..... | ..... | + 14 | ..... | ..... | ..... | + 9 |
| 14 | ..... | ..... | ..... | + 18 | ..... | ..... | ..... | + 12 |
| 13 | ..... | ..... | ..... | + 35 | ..... | ..... | ..... | + 27 |
| 12 | ..... | ..... | ..... | + 29 | ..... | ..... | ..... | + 26 |
| 11 | ..... | ..... | ..... | + 23 | ..... | ..... | ..... | + 26 |
| 10 | ..... | ..... | ..... | + 18 | ..... | ..... | ..... | + 20 |
| 9 | ..... | ..... | ..... | + 15 | ..... | ..... | ..... | + 14 |
| 8 | ..... | ..... | ..... | + 18 | ..... | ..... | ..... | + 20 |
| 7 | ..... | ..... | ..... | + 7 | ..... | ..... | ..... | + 8 |
| 6 | ..... | ..... | ..... | + 6 | ..... | ..... | ..... | + 6* |
| 5 | ..... | ..... | ..... | + 4 | ..... | ..... | ..... | + 5* |
| 4 | ..... | ..... | ..... | + 5 | ..... | ..... | ..... | + 5* |
| 3 | ..... | ..... | ..... | + 6 | ..... | ..... | ..... | + 5* |
| 2 | ..... | ..... | ..... | + 4 | ..... | ..... | ..... | + 4* |
| 1 | ..... | ..... | ..... | + 1 | ..... | ..... | ..... | + 1* |
| | | Total..... | | +194 | | Total..... | | +218 |

*These values have been interpolated from those obtained for neighbouring stations.

TABLE V—*Continued*

AVERAGE ELEVATIONS AND CORRECTIONS FOR TOPOGRAPHY AND COMPENSATION FOR SEPARATE ZONES

The unit for the corrections in this table is ·0001 dyne.

| Zone | Elevation in Feet | Topography | Compensation | Topography and Compensation | Elevation in Feet | Topography | Compensation | Topography and Compensation |
|---|---|---|---|---|---|---|---|---|
| | Woodstock, N.B., No. 26 | | | | Edmundston, N.B., No. 27 | | | |
| A | 184 | + 2 | 0 | + 2 | 486 | + 2 | 0 | + 2 |
| B | 185 | + 38 | 0 | + 38 | 500 | + 55 | 0 | + 55 |
| C | 175 | + 14 | 0 | + 14 | 500 | + 59 | 0 | + 59 |
| D | 175 | + 7 | 0 | + 7 | 510 | + 30 | 0 | + 30 |
| E | 175 | + 4 | 0 | + 4 | 520 | + 13 | 0 | + 13 |
| F | 250 | 0 | 0 | 0 | 530 | + 3 | 0 | + 3 |
| G | 300 | 0 | 0 | 0 | 540 | 0 | 0 | 0 |
| H | 300 | 0 | 0 | 0 | 590 | 0 | 0 | 0 |
| I | 300 | 0 | 0 | 0 | 650 | 0 | 0 | 0 |
| J | 300 | 0 | − 5 | − 5 | 750 | 0 | − 12 | − 12 |
| K | 334 | 0 | − 7 | − 7 | 760 | 0 | − 15 | − 15 |
| L | 369 | 0 | − 9 | − 9 | 975 | 0 | − 23 | − 23 |
| M | 589 | 0 | − 33 | − 33 | 1,105 | 0 | − 62 | − 62 |
| N | 536 | 0 | − 31 | − 31 | 1,118 | 0 | − 56 | − 56 |
| O | 710 | 0 | − 40 | − 40 | 795 | 0 | − 45 | − 45 |
| 18 | | | | − 5 | | | | − 10 |
| 17 | | | | − 6 | | | | − 11 |
| 16 | | | | − 6 | | | | − 9 |
| 15 | | | | − 4 | | | | − 9 |
| 14 | | | | + 1 | | | | − 7 |
| 13 | | | | − 6 | | | | − 11 |
| 12 | | | | + 2 | | | | − 7 |
| 11 | | | | + 1 | | | | − 1 |
| 10 | | | | + 13 | | | | + 10 |
| 9 | | | | + 12 | | | | + 11 |
| 8 | | | | + 17 | | | | + 15 |
| 7 | | | | + 7 | | | | + 7 |
| 6 | | | | + 6* | | | | + 5* |
| 5 | | | | + 5* | | | | + 5* |
| 4 | | | | + 5* | | | | + 5* |
| 3 | | | | + 5* | | | | + 5* |
| 2 | | | | + 4* | | | | + 4* |
| 1 | | | | + 1* | | | | + 1* |
| | | | Total | − 8 | | | Total | − 48 |

*These values have been interpolated from those obtained for neighbouring stations.

TABLE V—*Continued*

AVERAGE ELEVATIONS AND CORRECTIONS FOR TOPOGRAPHY AND COMPENSATION FOR SEPARATE ZONES

The unit for the corrections in this table is ·0001 dyne.

| Zone | Elevation in Feet | Topography | Compensation | Topography and Compensation | Elevation in Feet | Topography | Compensation | Topography and Compensation |
|---|---|---|---|---|---|---|---|---|
| | Bathurst, N.B., No. 28 | | | | Percé, Que., No. 29 | | | |
| A | 15 | + 2 | 0 | + 2 | 20 | + 2 | 0 | + 2 |
| B | 15 | + 2 | 0 | + 2 | 20 | + 4 | 0 | + 4 |
| C | 15 | 0 | 0 | 0 | 25 | 0 | 0 | 0 |
| D | − 11 | 0 | 0 | 0 | 20 | + 1 | 0 | + 1 |
| E | − 7 | 0 | 0 | 0 | 25 | 0 | 0 | 0 |
| F | 27 | 0 | 0 | 0 | 94 | + 2 | 0 | + 2 |
| G | 56 | 0 | 0 | 0 | 4 | 0 | 0 | 0 |
| H | 84 | 0 | 0 | 0 | − 47 | 0 | 0 | 0 |
| I | 114 | 0 | 0 | 0 | − 54 | 0 | 0 | 0 |
| J | 144 | 0 | − 2 | − 2 | − 1 | 0 | − 1 | − 1 |
| K | 311 | 0 | − 6 | − 6 | 59 | 0 | − 3 | − 3 |
| L | 348 | 0 | − 8 | − 8 | 32 | 0 | − 2 | − 2 |
| M | 334 | 0 | − 19 | − 19 | 18 | 0 | − 6 | − 6 |
| N | 433 | 0 | − 25 | − 25 | − 50 | 0 | − 4 | − 4 |
| O | 749 | 0 | − 42 | − 42 | 47 | 0 | − 9 | − 9 |
| 18 | | | | − 5 | | | | − 1 |
| 17 | | | | − 2 | | | | − 1 |
| 16 | | | | − 1 | | | | − 3 |
| 15 | | | | − 2 | | | | − 5 |
| 14 | | | | − 5 | | | | − 6 |
| 13 | | | | − 11 | | | | 0 |
| 12 | | | | − 4 | | | | − 8 |
| 11 | | | | + 6 | | | | 0 |
| 10 | | | | + 16 | | | | + 15 |
| 9 | | | | + 14 | | | | + 11 |
| 8 | | | | + 17 | | | | + 19 |
| 7 | | | | + 7 | | | | + 8 |
| 6 | | | | + 6* | | | | + 6* |
| 5 | | | | + 5* | | | | + 5* |
| 4 | | | | + 5* | | | | + 5* |
| 3 | | | | + 6* | | | | + 6* |
| 2 | | | | + 4* | | | | + 4* |
| 1 | | | | + 1* | | | | + 1* |
| | | Total | | − 41 | | Total | | + 40 |

*These values have been interpolated from those obtained for neighbouring stations.

TABLE V—*Continued*

AVERAGE ELEVATIONS AND CORRECTIONS FOR TOPOGRAPHY AND COMPENSATION FOR SEPARATE ZONES

The units for the corrections in this table is ·0001 dyne.

| Zone | Elevation in Feet | Topography | Compensation | Topography and Compensation | Elevation in Feet | Topography | Compensation | Topography and Compensation |
|---|---|---|---|---|---|---|---|---|
| | Kenora, Ont., No. 30 | | | | Chelmsford, Ont., No. 101 | | | |
| A | 1,083 | + 2 | 0 | + 2 | 882 | + 2 | 0 | + 2 |
| B | 1,090 | + 64 | 0 | + 64 | 882 | + 62 | 0 | + 62 |
| C | 1,100 | +108 | 0 | +108 | 882 | + 95 | 0 | + 95 |
| D | 1,100 | + 96 | 0 | + 96 | 882 | + 70 | 0 | + 70 |
| E | 1,100 | + 48 | 0 | + 48 | 882 | + 31 | 0 | + 31 |
| F | 1,100 | + 18 | 0 | + 18 | 882 | + 12 | 0 | + 12 |
| G | 1,100 | + 2 | 0 | + 2 | 879 | 0 | 0 | 0 |
| H | 1,100 | + 3 | − 3 | 0 | 891 | 0 | 0 | 0 |
| I | 1,100 | + 4 | − 4 | 0 | 902 | 0 | 0 | 0 |
| J | 1,100 | 0 | − 16 | − 16 | 939 | 0 | − 15 | − 15 |
| K | 1,100 | 0 | − 20 | − 20 | 965 | 0 | − 19 | − 19 |
| L | 1,100 | 0 | − 26 | − 26 | 981 | 0 | − 24 | − 24 |
| M | 1,400 | 0 | − 78 | − 78 | 949 | 0 | − 53 | − 53 |
| N | 1,362 | 0 | − 71 | − 71 | 1,022 | 0 | − 54 | − 54 |
| O | 1,323 | 0 | − 74 | − 74 | 962 | 0 | − 56 | − 56 |
| 18 | | | | − 13 | | | | − 11 |
| 17 | | | | − 12 | | | | − 10 |
| 16 | | | | − 12 | | | | − 10 |
| 15 | | | | − 12 | | | | − 10 |
| 14 | | | | − 13 | | | | − 10 |
| 13 | | | | − 18 | | | | − 12 |
| 12 | | | | − 13 | | | | − 10 |
| 11 | | | | − 11 | | | | − 9 |
| 10 | | | | − 9 | | | | − 6 |
| 9 | | | | − 9 | | | | 0 |
| 8 | | | | − 11 | | | | + 6 |
| 7 | | | | + 4 | | | | + 5 |
| 6 | | | | + 8* | | | | + 5* |
| 5 | | | | + 10* | | | | + 9* |
| 4 | | | | + 6* | | | | + 5* |
| 3 | | | | + 5* | | | | + 5* |
| 2 | | | | + 3* | | | | + 3* |
| 1 | | | | + 1* | | | | + 1* |
| | | Total | | − 43 | | Total | | + 2 |

*These values have been interpolated from those obtained for neighbouring stations.

TABLE V—*Continued*

AVERAGE ELEVATIONS AND CORRECTIONS FOR TOPOGRAPHY AND COMPENSATION FOR SEPARATE ZONES

The unit for the corrections in this table is ·0001 dyne.

| Zone | Elevation in Feet | Topography | Compensation | Topography and Compensation | Elevation in Feet | Topography | Compensation | Topography and Compensation |
|---|---|---|---|---|---|---|---|---|
| | Sudbury, Ont., No. 102 | | | | Hearst, Ont., No. 103 | | | |
| A | 886 | + 2 | 0 | + 2 | 797 | + 2 | 0 | + 2 |
| B | 886 | + 62 | 0 | + 62 | 797 | + 61 | 0 | + 61 |
| C | 886 | + 95 | 0 | + 95 | 797 | + 88 | 0 | + 88 |
| D | 886 | + 70 | 0 | + 70 | 797 | + 60 | 0 | + 60 |
| E | 871 | + 30 | 0 | + 30 | 797 | + 24 | 0 | + 24 |
| F | 864 | + 12 | 0 | + 12 | 795 | + 10 | 0 | + 10 |
| G | 854 | 0 | 0 | 0 | 795 | 0 | 0 | 0 |
| H | 858 | 0 | 0 | 0 | 798 | 0 | 0 | 0 |
| I | 856 | 0 | 0 | 0 | 798 | 0 | 0 | 0 |
| J | 830 | 0 | − 13 | − 13 | 806 | 0 | − 13 | − 13 |
| K | 838 | 0 | − 17 | − 17 | 812 | 0 | − 16 | − 16 |
| L | 833 | 0 | − 20 | − 20 | 811 | 0 | − 19 | − 19 |
| M | 881 | 0 | − 49 | − 49 | 767 | 0 | − 43 | − 43 |
| N | 988 | 0 | − 52 | − 52 | 762 | 0 | − 42 | − 42 |
| O | 968 | 0 | − 54 | − 54 | 882 | 0 | − 49 | − 49 |
| 18 | | | | − 10 | | | | − 9 |
| 17 | | | | − 11 | | | | − 9 |
| 16 | | | | − 11 | | | | − 9 |
| 15 | | | | − 10 | | | | − 8 |
| 14 | | | | − 10 | | | | − 7 |
| 13 | | | | − 12 | | | | − 11 |
| 12 | | | | − 10 | | | | − 9 |
| 11 | | | | − 9 | | | | − 8 |
| 10 | | | | − 6 | | | | − 6 |
| 9 | | | | 0 | | | | − 3 |
| 8 | | | | + 6 | | | | + 2 |
| 7 | | | | + 5 | | | | + 4 |
| 6 | | | | + 5* | | | | + 5* |
| 5 | | | | + 8* | | | | + 9* |
| 4 | | | | + 5* | | | | + 5* |
| 3 | | | | + 5* | | | | + 5* |
| 2 | | | | + 3* | | | | + 3* |
| 1 | | | | + 1* | | | | + 1* |
| | | Total | | + 15 | | Total | | + 18 |

*These values have been interpolated from those obtained for neighbouring stations.

TABLE V—*Continued*

AVERAGE ELEVATIONS AND CORRECTIONS FOR TOPOGRAPHY AND COMPENSATION FOR SEPARATE ZONES

The unit for the corrections in this table is ·0001 dyne.

| Zone | Elevation in Feet | Topography | Compensation | Topography and Compensation | Elevation in Feet | Topography | Compensation | Topography and Compensation |
|---|---|---|---|---|---|---|---|---|
| | Nakina, Ont., No. 104 | | | | Armstrong, Ont., No. 105 | | | |
| A | 1,010 | + 2 | 0 | + 2 | 1,129 | + 2 | 0 | + 2 |
| B | 1,010 | + 64 | 0 | + 64 | 1,129 | + 65 | 0 | + 65 |
| C | 1,010 | +104 | 0 | +104 | 1,129 | +109 | 0 | +109 |
| D | 1,010 | + 85 | 0 | + 85 | 1,129 | + 99 | 0 | + 99 |
| E | 1,010 | + 41 | 0 | + 41 | 1,129 | + 50 | 0 | + 50 |
| F | 996 | + 15 | 0 | + 15 | 1,129 | + 18 | 0 | + 18 |
| G | 991 | 0 | 0 | 0 | 1,137 | + 3 | 0 | + 3 |
| H | 995 | 0 | 0 | 0 | 1,146 | + 5 | − 5 | 0 |
| I | 995 | 0 | 0 | 0 | 1,130 | + 5 | − 5 | 0 |
| J | 1,012 | 0 | − 16 | − 16 | 1,132 | 0 | − 16 | − 16 |
| K | 1,036 | 0 | − 21 | − 21 | 1,136 | 0 | − 20 | − 20 |
| L | 1,020 | 0 | − 24 | − 24 | 1,104 | 0 | − 26 | − 26 |
| M | 1,014 | 0 | − 57 | − 57 | 1,101 | 0 | − 62 | − 62 |
| N | 1,097 | 0 | − 58 | − 58 | 1,379 | 0 | − 72 | − 72 |
| O | 957 | 0 | − 54 | − 54 | 1,352 | 0 | − 76 | − 76 |
| 18 | | | | − 9 | | | | − 13 |
| 17 | | | | − 9 | | | | − 13 |
| 16 | | | | − 9 | | | | − 11 |
| 15 | | | | − 9 | | | | − 12 |
| 14 | | | | − 9 | | | | − 10 |
| 13 | | | | − 14 | | | | − 13 |
| 12 | | | | − 8 | | | | − 8 |
| 11 | | | | − 6 | | | | − 7 |
| 10 | | | | − 6 | | | | − 6 |
| 9 | | | | − 5 | | | | − 6 |
| 8 | | | | − 1 | | | | − 5 |
| 7 | | | | + 3 | | | | + 3 |
| 6 | | | | + 6* | | | | + 6* |
| 5 | | | | + 9* | | | | + 10* |
| 4 | | | | + 6* | | | | + 6* |
| 3 | | | | + 5* | | | | + 5* |
| 2 | | | | + 3* | | | | + 3* |
| 1 | | | | + 1* | | | | + 1* |
| Total | | | | + 29 | Total | | | + 4 |

*These values have been interpolated from those obtained for neighbouring stations.

TABLE V—*Continued*

AVERAGE ELEVATIONS AND CORRECTIONS FOR TOPOGRAPHY AND COMPENSATION FOR SEPARATE ZONES

The unit for the corrections in this table is ·0001 dyne.

| Zone | Elevation in Feet | Topography | Compensation | Topography and Compensation | Elevation in Feet | Topography | Compensation | Topography and Compensation |
|---|---|---|---|---|---|---|---|---|
| | Sioux Lookout, Ont., No. 106 | | | | Berens River, Man., No. 107 | | | |
| A | 1,207 | + 2 | 0 | + 2 | 718 | + 2 | 0 | + 2 |
| B | 1,207 | + 65 | 0 | + 65 | 718 | + 59 | 0 | + 59 |
| C | 1,207 | +112 | 0 | +112 | 718 | + 81 | 0 | + 81 |
| D | 1,207 | +109 | 0 | +109 | 718 | + 50 | 0 | + 50 |
| E | 1,207 | + 56 | 0 | + 56 | 718 | + 21 | 0 | + 21 |
| F | 1,202 | + 20 | 0 | + 20 | 719 | + 8 | 0 | + 8 |
| G | 1,202 | + 5 | 0 | + 5 | 719 | 0 | 0 | 0 |
| H | 1,205 | + 6 | − 6 | 0 | 717 | 0 | 0 | 0 |
| I | 1,211 | + 8 | − 8 | 0 | 717 | 0 | 0 | 0 |
| J | 1,208 | 0 | − 16 | − 16 | 723 | 0 | − 12 | − 12 |
| K | 1,196 | 0 | − 20 | − 20 | 741 | 0 | − 15 | − 15 |
| L | 1,217 | 0 | − 29 | − 29 | 738 | 0 | − 18 | − 18 |
| M | 1,246 | 0 | − 70 | − 70 | 753 | 0 | − 42 | − 42 |
| N | 1,250 | 0 | − 64 | − 64 | 734 | 0 | − 39 | − 39 |
| O | 1,250 | 0 | − 70 | − 70 | 773 | 0 | − 42 | − 42 |
| 18 | ..... | ..... | ..... | − 13 | ..... | ..... | ..... | − 8 |
| 17 | ..... | ..... | ..... | − 13 | ..... | ..... | ..... | − 8 |
| 16 | ..... | ..... | ..... | − 13 | ..... | ..... | ..... | − 8 |
| 15 | ..... | ..... | ..... | − 13 | ..... | ..... | ..... | − 9 |
| 14 | ..... | ..... | ..... | − 10 | ..... | ..... | ..... | − 10 |
| 13 | ..... | ..... | ..... | − 15 | ..... | ..... | ..... | − 17 |
| 12 | ..... | ..... | ..... | − 9 | ..... | ..... | ..... | − 12 |
| 11 | ..... | ..... | ..... | − 7 | ..... | ..... | ..... | − 10 |
| 10 | ..... | ..... | ..... | − 6 | ..... | ..... | ..... | − 9 |
| 9 | ..... | ..... | ..... | − 6 | ..... | ..... | ..... | − 9 |
| 8 | ..... | ..... | ..... | − 7 | ..... | ..... | ..... | − 12 |
| 7 | ..... | ..... | ..... | + 4 | ..... | ..... | ..... | + 3 |
| 6 | ..... | ..... | ..... | + 7* | ..... | ..... | ..... | + 8* |
| 5 | ..... | ..... | ..... | + 10* | ..... | ..... | ..... | + 10* |
| 4 | ..... | ..... | ..... | + 6* | ..... | ..... | ..... | + 6* |
| 3 | ..... | ..... | ..... | + 5* | ..... | ..... | ..... | + 5* |
| 2 | ..... | ..... | ..... | + 3* | ..... | ..... | ..... | + 3* |
| 1 | ..... | ..... | ..... | + 1* | ..... | ..... | ..... | + 1* |
| | | Total..... | | + 24 | | Total..... | | − 23 |

*These values have been interpolated from those obtained for neighbouring stations.

TABLE V—*Continued*

AVERAGE ELEVATIONS AND CORRECTIONS FOR TOPOGRAPHY AND COMPENSATION FOR SEPARATE ZONES

The units for the corrections in this table is ·0001 dyne.

| Zone | Elevation in Feet | Topography | Compensation | Topography and Compensation | Elevation in Feet | Topography | Compensation | Topography and Compensation |
|---|---|---|---|---|---|---|---|---|
| | Grand Rapids, Man., No. 108 | | | | Norway House, Man., No. 109 | | | |
| A | 735 | + 2 | 0 | + 2 | 718 | + 2 | 0 | + 2 |
| B | 735 | + 60 | 0 | + 60 | 718 | + 59 | 0 | + 59 |
| C | 735 | + 83 | 0 | + 83 | 718 | + 81 | 0 | + 81 |
| D | 735 | + 52 | 0 | + 52 | 718 | + 50 | 0 | + 50 |
| E | 735 | + 21 | 0 | + 21 | 718 | + 21 | 0 | + 21 |
| F | 734 | + 8 | 0 | + 8 | 717 | + 9 | 0 | + 9 |
| G | 735 | 0 | 0 | 0 | 718 | 0 | 0 | 0 |
| H | 768 | 0 | 0 | 0 | 718 | 0 | 0 | 0 |
| I | 769 | 0 | 0 | 0 | 723 | 0 | 0 | 0 |
| J | 778 | 0 | − 12 | − 12 | 730 | 0 | − 12 | − 12 |
| K | 781 | 0 | − 16 | − 16 | 733 | 0 | − 15 | − 15 |
| L | 790 | 0 | − 19 | − 19 | 738 | 0 | − 18 | − 18 |
| M | 815 | 0 | − 46 | − 46 | 742 | 0 | − 42 | − 42 |
| N | 804 | 0 | − 41 | − 41 | 748 | 0 | − 40 | − 40 |
| O | 881 | 0 | − 49 | − 49 | 761 | 0 | − 43 | − 43 |
| 18 | | | | − 10 | | | | − 8 |
| 17 | | | | − 10 | | | | − 8 |
| 16 | | | | − 11 | | | | − 8 |
| 15 | | | | − 11 | | | | − 8 |
| 14 | | | | − 11 | | | | − 10 |
| 13 | | | | − 19 | | | | − 17 |
| 12 | | | | − 13 | | | | − 12 |
| 11 | | | | − 11 | | | | − 14 |
| 10 | | | | − 10 | | | | − 16 |
| 9 | | | | − 10 | | | | − 11 |
| 8 | | | | − 8 | | | | − 6 |
| 7 | | | | + 4 | | | | + 3 |
| 6 | | | | + 8* | | | | + 7* |
| 5 | | | | + 10* | | | | + 10* |
| 4 | | | | + 6* | | | | + 6* |
| 3 | | | | + 5* | | | | + 5* |
| 2 | | | | + 3* | | | | + 4* |
| 1 | | | | + 1* | | | | + 1* |
| | | Total | | − 44 | | Total | | − 30 |

*These values have been interpolated from those obtained for neighbouring stations.

TABLE V—*Continued*

AVERAGE ELEVATIONS AND CORRECTIONS FOR TOPOGRAPHY AND COMPENSATION FOR SEPARATE ZONES

The unit for the corrections in this table is ·0001 dyne.

| Zone | Elevation in Feet | Topography | Compensation | Topography and Compensation | Elevation in Feet | Topography | Compensation | Topography and Compensation |
|---|---|---|---|---|---|---|---|---|
| | Nokomis, Sask., No. 110 | | | | North Battleford, Sask., No. 111 | | | |
| A | 1,716 | + 2 | 0 | + 2 | 1,700 | + 2 | ..... | + 2 |
| B | 1,716 | + 67 | 0 | + 67 | 1,700 | + 67 | ..... | + 67 |
| C | 1,716 | +133 | 0 | +133 | 1,700 | +132 | ..... | +132 |
| D | 1,716 | +158 | 0 | +158 | 1,700 | +156 | ..... | +156 |
| E | 1,720 | +102 | 0 | +102 | 1,700 | +100 | ..... | +100 |
| F | 1,725 | + 49 | − 3 | + 46 | 1,676 | + 46 | − 2 | + 44 |
| G | 1,722 | + 23 | − 5 | + 18 | 1,680 | + 21 | − 4 | + 17 |
| H | 1,718 | + 16 | − 16 | 0 | 1,708 | + 16 | − 16 | 0 |
| I | 1,712 | + 20 | − 20 | 0 | 1,689 | + 20 | − 20 | 0 |
| J | 1,712 | 0 | − 16 | − 16 | 1,742 | 0 | − 16 | − 16 |
| K | 1,697 | 0 | − 20 | − 20 | 1,762 | 0 | − 20 | − 20 |
| L | 1,742 | 0 | − 42 | − 42 | 1,928 | 0 | − 46 | − 46 |
| M | 1,889 | 0 | −106 | −106 | 2,086 | 0 | −117 | −117 |
| N | 1,756 | 0 | − 90 | − 90 | 2,275 | 0 | −114 | −114 |
| O | 1,725 | 0 | − 97 | − 97 | 1,986 | 0 | −111 | −111 |
| 18 | ..... | ..... | ..... | − 19 | ..... | ..... | ..... | − 20 |
| 17 | ..... | ..... | ..... | − 19 | ..... | ..... | ..... | − 19 |
| 16 | ..... | ..... | ..... | − 20 | ..... | ..... | ..... | − 19 |
| 15 | ..... | ..... | ..... | − 20 | ..... | ..... | ..... | − 19 |
| 14 | ..... | ..... | ..... | − 19 | ..... | ..... | ..... | − 20 |
| 13 | ..... | ..... | ..... | − 31 | ..... | ..... | ..... | − 33 |
| 12 | ..... | ..... | ..... | − 19 | ..... | ..... | ..... | − 23 |
| 11 | ..... | ..... | ..... | − 20 | ..... | ..... | ..... | − 20 |
| 10 | ..... | ..... | ..... | − 16 | ..... | ..... | ..... | − 14 |
| 9 | ..... | ..... | ..... | − 9 | ..... | ..... | ..... | − 8 |
| 8 | ..... | ..... | ..... | − 2 | ..... | ..... | ..... | 0 |
| 7 | ..... | ..... | ..... | + 4 | ..... | ..... | ..... | + 2 |
| 6 | ..... | ..... | ..... | + 8* | ..... | ..... | ..... | + 7* |
| 5 | ..... | ..... | ..... | + 10* | ..... | ..... | ..... | + 10* |
| 4 | ..... | ..... | ..... | + 7* | ..... | ..... | ..... | + 7* |
| 3 | ..... | ..... | ..... | + 4* | ..... | ..... | ..... | + 4* |
| 2 | ..... | ..... | ..... | + 3* | ..... | ..... | ..... | + 3* |
| 1 | ..... | ..... | ..... | + 1* | ..... | ..... | ..... | + 1* |
| | | Total..... | | − 2 | | Total..... | | − 67 |

*These values have been interpolated from those obtained for neighbouring stations.

TABLE V—*Continued*

AVERAGE ELEVATIONS AND CORRECTIONS FOR TOPOGRAPHY AND COMPENSATION FOR SEPARATE ZONES

The unit for the corrections in this table is ·0001 dyne.

| Zone | Elevation in Feet | Topography | Compensation | Topography and Compensation | Elevation in Feet | Topography | Compensation | Topography and Compensation |
|---|---|---|---|---|---|---|---|---|
| | Kindersley, Sask., No. 112 | | | | Prince George, B.C., No. 113 | | | |
| A | 2,267 | + 2 | 0 | + 2 | 1,873 | + 2 | 0 | + 2 |
| B | 2,267 | + 68 | 0 | + 68 | 1,873 | + 67 | 0 | + 67 |
| C | 2,267 | +144 | 0 | +144 | 1,873 | +137 | 0 | +137 |
| D | 2,267 | +196 | 0 | +196 | 1,873 | +172 | 0 | +172 |
| E | 2,270 | +166 | − 8 | +158 | 2,000 | +136 | − 8 | +128 |
| F | 2,265 | + 83 | − 10 | + 73 | 2,000 | + 70 | − 10 | + 60 |
| G | 2,275 | + 43 | − 12 | + 31 | 2,000 | + 36 | − 12 | + 24 |
| H | 2,269 | + 25 | − 16 | + 9 | 2,200 | + 22 | − 16 | + 6 |
| I | 2,266 | + 20 | − 20 | 0 | 2,200 | + 20 | − 20 | 0 |
| J | 2,275 | + 4 | − 20 | − 16 | 2,200 | + 3 | − 19 | − 16 |
| K | 2,288 | 0 | − 26 | − 26 | 2,200 | 0 | − 24 | − 24 |
| L | 2,275 | 0 | − 55 | − 55 | 2,312 | 0 | − 55 | − 55 |
| M | 2,236 | + 3 | −126 | −123 | 2,614 | + 9 | −155 | −146 |
| N | 2,406 | 0 | −122 | −122 | 3,125 | 0 | −163 | −163 |
| O | 2,232 | 0 | −107 | −107 | 4,196 | 0 | −202 | −202 |
| 18 | | | | − 22 | | | | − 40 |
| 17 | | | | − 23 | | | | − 38 |
| 16 | | | | − 23 | | | | − 41 |
| 15 | | | | − 23 | | | | − 40 |
| 14 | | | | − 23 | | | | − 40 |
| 13 | | | | − 40 | | | | − 71 |
| 12 | | | | − 30 | | | | − 30 |
| 11 | | | | − 23 | | | | 0 |
| 10 | | | | − 17 | | | | + 2 |
| 9 | | | | − 7 | | | | + 3 |
| 8 | | | | + 2 | | | | + 6 |
| 7 | | | | + 3 | | | | + 7 |
| 6 | | | | + 8* | | | | + 7* |
| 5 | | | | + 10* | | | | + 9* |
| 4 | | | | + 7* | | | | + 7* |
| 3 | | | | + 4* | | | | + 4* |
| 2 | | | | + 3* | | | | + 4* |
| 1 | | | | + 1* | | | | + 1* |
| | | Total | | + 39 | | Total | | −260 |

*These values have been interpolated from those obtained for neighbouring stations.

TABLE V—*Continued*

AVERAGE ELEVATIONS AND CORRECTIONS FOR TOPOGRAPHY AND COMPENSATION FOR SEPARATE ZONES

The unit for the corrections in this table is ·0001 dyne.

| Zone | Elevation in Feet | Topography | Compensation | Topography and Compensation | Elevation in Feet | Topography | Compensation | Topography and Compensation |
|---|---|---|---|---|---|---|---|---|
| | Endako, B.C., No. 114 | | | | Smithers, B.C., No. 115 | | | |
| A | 2,257 | + 2 | 0 | + 2 | 1,640 | + 2 | 0 | + 2 |
| B | 2,260 | + 68 | 0 | + 68 | 1,640 | + 67 | 0 | + 67 |
| C | 2,260 | +144 | 0 | +144 | 1,650 | +130 | 0 | +130 |
| D | 2,260 | +196 | 0 | +196 | 1,700 | +156 | 0 | +156 |
| E | 2,260 | +165 | − 8 | +157 | 2,000 | +136 | − 8 | +128 |
| F | 2,260 | + 83 | − 10 | + 73 | 2,100 | + 75 | − 10 | + 65 |
| G | 2,260 | + 42 | − 12 | + 30 | 2,300 | + 43 | − 12 | + 31 |
| H | 2,260 | + 24 | − 16 | + 8 | 2,500 | + 32 | − 16 | + 16 |
| I | 2,260 | + 20 | − 20 | 0 | 2,750 | + 20 | − 20 | 0 |
| J | 2,260 | + 4 | − 20 | − 16 | 3,000 | + 16 | − 32 | − 16 |
| K | 2,260 | 0 | − 25 | − 25 | 3,400 | + 8 | − 48 | − 40 |
| L | 3,054 | + 1 | − 73 | − 72 | 3,625 | + 13 | − 87 | − 74 |
| M | 3,007 | + 14 | −182 | −168 | 3,714 | + 16 | −222 | −206 |
| N | 3,206 | 0 | −166 | −166 | 3,406 | + 2 | −177 | −175 |
| O | 3,657 | 0 | −177 | −177 | 3,375 | 0 | −161 | −161 |
| 18 | ..... | ..... | ..... | − 36 | ..... | ..... | ..... | − 37 |
| 17 | ..... | ..... | ..... | − 36 | ..... | ..... | ..... | − 36 |
| 16 | ..... | ..... | ..... | − 38 | ..... | ..... | ..... | − 35 |
| 15 | ..... | ..... | ..... | − 36 | ..... | ..... | ..... | − 24 |
| 14 | ..... | ..... | ..... | − 34 | ..... | ..... | ..... | − 22 |
| 13 | ..... | ..... | ..... | − 48 | ..... | ..... | ..... | − 31 |
| 12 | ..... | ..... | ..... | − 13 | ..... | ..... | ..... | − 4 |
| 11 | ..... | ..... | ..... | + 4 | ..... | ..... | ..... | + 4 |
| 10 | ..... | ..... | ..... | + 5 | ..... | ..... | ..... | + 6 |
| 9 | ..... | ..... | ..... | + 4 | ..... | ..... | ..... | + 5 |
| 8 | ..... | ..... | ..... | + 7 | ..... | ..... | ..... | + 8 |
| 7 | ..... | ..... | ..... | + 8 | ..... | ..... | ..... | + 8 |
| 6 | ..... | ..... | ..... | + 7* | ..... | ..... | ..... | + 7* |
| 5 | ..... | ..... | ..... | + 9* | ..... | ..... | ..... | + 8* |
| 4 | ..... | ..... | ..... | + 7* | ..... | ..... | ..... | + 7* |
| 3 | ..... | ..... | ..... | + 4* | ..... | ..... | ..... | + 4* |
| 2 | ..... | ..... | ..... | + 3* | ..... | ..... | ..... | + 3* |
| 1 | ..... | ..... | ..... | + 1* | ..... | ..... | ..... | + 1* |
| | | Total..... | | −128 | | Total..... | | −205 |

*These values have been interpolated from those obtained for neighbouring stations.

TABLE V—*Continued*

AVERAGE ELEVATIONS AND CORRECTIONS FOR TOPOGRAPHY AND COMPENSATION FOR SEPARATE ZONES

The units for the corrections in this table is ·0001 dyne.

| Zone | Elevation in Feet | Topography | Compensation | Topography and Compensation | Elevation in Feet | Topography | Compensation | Topography and Compensation |
|---|---|---|---|---|---|---|---|---|
| | Montreal, Que., No. 116 | | | | Pembroke, Ont., No. 117 | | | |
| A | 128 | + 2 | 0 | + 2 | 399 | + 2 | 0 | + 2 |
| B | 128 | + 28 | 0 | + 28 | 408 | + 56 | 0 | + 56 |
| C | 128 | + 6 | 0 | + 6 | 410 | + 49 | 0 | + 49 |
| D | 155 | + 6 | 0 | + 6 | 392 | + 18 | 0 | + 18 |
| E | 191 | + 4 | 0 | + 4 | 389 | + 8 | 0 | + 8 |
| F | 208 | 0 | 0 | 0 | 393 | 0 | 0 | 0 |
| G | 167 | 0 | 0 | 0 | 409 | 0 | 0 | 0 |
| H | 129 | 0 | 0 | 0 | 409 | 0 | 0 | 0 |
| I | 105 | 0 | 0 | 0 | 427 | 0 | 0 | 0 |
| J | 87 | 0 | − 1 | − 1 | 439 | 0 | − 7 | − 7 |
| K | 87 | 0 | − 2 | − 2 | 452 | 0 | − 9 | − 9 |
| L | 118 | 0 | − 3 | − 3 | 476 | 0 | − 11 | − 11 |
| M | 329 | 0 | − 18 | − 18 | 779 | 0 | − 44 | − 44 |
| N | 556 | 0 | − 31 | − 31 | 1,025 | 0 | − 49 | − 49 |
| O | 941 | 0 | − 53 | − 53 | 936 | 0 | − 52 | − 52 |
| 18 | | | | − 12 | | | | − 8 |
| 17 | | | | − 13 | | | | − 8 |
| 16 | | | | − 12 | | | | − 8 |
| 15 | | | | − 11 | | | | − 7 |
| 14 | | | | − 10 | | | | − 9 |
| 13 | | | | − 14 | | | | − 16 |
| 12 | | | | − 7 | | | | − 10 |
| 11 | | | | − 3 | | | | − 4 |
| 10 | | | | + 5 | | | | + 3 |
| 9 | | | | + 7 | | | | + 6 |
| 8 | | | | + 13 | | | | + 11 |
| 7 | | | | + 5 | | | | + 6 |
| 6 | | | | + 6* | | | | + 6* |
| 5 | | | | + 7* | | | | + 7* |
| 4 | | | | + 5* | | | | + 5* |
| 3 | | | | + 5* | | | | + 5* |
| 2 | | | | + 4* | | | | + 4* |
| 1 | | | | + 1* | | | | + 1* |
| | | Total | | − 86 | | Total | | − 55 |

*These values have been interpolated from those obtained for neighbouring stations.

TABLE V—*Continued*

AVERAGE ELEVATIONS AND CORRECTIONS FOR TOPOGRAPHY AND COMPENSATION FOR SEPARATE ZONES

The unit for the corrections in this table is ·0001 dyne.

| Zone | Elevation in Feet | Topography | Compensation | Topography and Compensation | Elevation in Feet | Topography | Compensation | Topography and Compensation |
|---|---|---|---|---|---|---|---|---|
| | Haliburton, Ont., No. 118 | | | | Kincardine, Ont., No. 119 | | | |
| A | 1,071 | + 2 | ..... | + 2 | 659 | + 2 | 0 | + 2 |
| B | 1,070 | + 64 | ..... | + 64 | 665 | + 59 | 0 | + 59 |
| C | 1,062 | +106 | ..... | +106 | 652 | + 76 | 0 | + 76 |
| D | 1,077 | + 89 | ..... | + 89 | 650 | + 48 | 0 | + 48 |
| E | 1,175 | + 59 | ..... | + 59 | 624 | + 17 | 0 | + 17 |
| F | 1,170 | + 22 | ..... | + 22 | 606 | + 5 | 0 | + 5 |
| G | 1,217 | + 5 | ..... | + 5 | 602 | 0 | 0 | 0 |
| H | 1,169 | + 5 | − 5 | 0 | 602 | 0 | 0 | 0 |
| I | 1,230 | + 9 | − 9 | 0 | 600 | 0 | 0 | 0 |
| J | 1,188 | 0 | − 16 | − 16 | 595 | 0 | − 10 | − 10 |
| K | 1,175 | 0 | − 20 | − 20 | 606 | 0 | − 12 | − 12 |
| L | 1,162 | 0 | − 28 | − 28 | 583 | 0 | − 14 | − 14 |
| M | 1,136 | 0 | − 64 | − 64 | 546 | 0 | − 31 | − 31 |
| N | 994 | 0 | − 51 | − 51 | 597 | 0 | − 33 | − 33 |
| O | 675 | 0 | − 39 | − 39 | 589 | 0 | − 33 | − 33 |
| 18 | ..... | ..... | ..... | − 5 | ..... | ..... | ..... | − 6 |
| 17 | ..... | ..... | ..... | − 6 | ..... | ..... | ..... | − 6 |
| 16 | ..... | ..... | ..... | − 7 | ..... | ..... | ..... | − 6 |
| 15 | ..... | ..... | ..... | − 8 | ..... | ..... | ..... | − 8 |
| 14 | ..... | ..... | ..... | − 10 | ..... | ..... | ..... | − 9 |
| 13 | ..... | ..... | ..... | − 17 | ..... | ..... | ..... | − 16 |
| 12 | ..... | ..... | ..... | − 8 | ..... | ..... | ..... | − 11 |
| 11 | ..... | ..... | ..... | − 5 | ..... | ..... | ..... | − 6 |
| 10 | ..... | ..... | ..... | + 2 | ..... | ..... | ..... | − 3 |
| 9 | ..... | ..... | ..... | + 6 | ..... | ..... | ..... | + 5 |
| 8 | ..... | ..... | ..... | + 10 | ..... | ..... | ..... | + 8 |
| 7 | ..... | ..... | ..... | + 6* | ..... | ..... | ..... | + 5* |
| 6 | ..... | ..... | ..... | + 6* | ..... | ..... | ..... | + 7* |
| 5 | ..... | ..... | ..... | + 8* | ..... | ..... | ..... | + 8* |
| 4 | ..... | ..... | ..... | + 5* | ..... | ..... | ..... | + 6* |
| 3 | ..... | ..... | ..... | + 5* | ..... | ..... | ..... | + 5* |
| 2 | ..... | ..... | ..... | + 4* | ..... | ..... | ..... | + 3* |
| 1 | ..... | ..... | ..... | + 1* | ..... | ..... | ..... | + 1* |
| | | | Total..... | +116 | | | Total..... | + 51 |

*These values have been interpolated from those obtained for neighbouring stations.

TABLE V—*Continued*

AVERAGE ELEVATIONS AND CORRECTIONS FOR TOPOGRAPHY AND COMPENSATION FOR SEPARATE ZONES

The units for the corrections in this table is ·0001 dyne.

| Zone | Elevation in Feet | Topography | Compensation | Topography and Compensation | Elevation in Feet | Topography | Compensation | Topography and Compensation |
|---|---|---|---|---|---|---|---|---|
| | Biscotasing, Ont., No. 120 | | | | White River, Ont., No. 121 | | | |
| A | 1,354 | + 2 | 0 | + 2 | 1,219 | + 2 | 0 | + 2 |
| B | 1,358 | + 65 | 0 | + 65 | 1,220 | + 65 | 0 | + 65 |
| C | 1,345 | +121 | 0 | +121 | 1,225 | +114 | 0 | +114 |
| D | 1,338 | +125 | 0 | +125 | 1,218 | +111 | 0 | +111 |
| E | 1,330 | + 66 | 0 | + 66 | 1,218 | + 57 | 0 | + 57 |
| F | 1,340 | + 27 | 0 | + 27 | 1,215 | + 21 | 0 | + 21 |
| G | 1,340 | + 8 | 0 | + 8 | 1,225 | + 5 | 0 | + 5 |
| H | 1,341 | + 11 | − 11 | 0 | 1,252 | + 8 | − 8 | 0 |
| I | 1,334 | + 20 | − 20 | 0 | 1,241 | + 10 | − 10 | 0 |
| J | 1,339 | 0 | − 16 | − 16 | 1,275 | 0 | − 16 | − 16 |
| K | 1,340 | 0 | − 20 | − 20 | 1,240 | 0 | − 20 | − 20 |
| L | 1,295 | 0 | − 31 | − 31 | 1,267 | 0 | − 30 | − 30 |
| M | 1,186 | 0 | − 66 | − 66 | 1,179 | 0 | − 66 | − 66 |
| N | 1,194 | 0 | − 57 | − 57 | 869 | 0 | − 45 | − 45 |
| O | 982 | 0 | − 54 | − 54 | 741 | 0 | − 45 | − 45 |
| 18 | | | | − 8 | | | | − 6 |
| 17 | | | | − 7 | | | | − 7 |
| 16 | | | | − 6 | | | | − 7 |
| 15 | | | | − 7 | | | | − 8 |
| 14 | | | | − 8 | | | | − 9 |
| 13 | | | | − 12 | | | | − 13 |
| 12 | | | | − 6 | | | | − 8 |
| 11 | | | | − 9 | | | | − 7 |
| 10 | | | | − 7 | | | | − 8 |
| 9 | | | | 0 | | | | − 5 |
| 8 | | | | + 7 | | | | + 5 |
| 7 | | | | + 5* | | | | + 5* |
| 6 | | | | + 5* | | | | + 6* |
| 5 | | | | + 9* | | | | + 9* |
| 4 | | | | + 5* | | | | + 6* |
| 3 | | | | + 5* | | | | + 5* |
| 2 | | | | + 3* | | | | + 3* |
| 1 | | | | + 1* | | | | + 1* |
| | | | Total | +140 | | | Total | +115 |

*These values have been interpolated from those obtained for neighbouring stations.

TABLE V—*Continued*

AVERAGE ELEVATIONS AND CORRECTIONS FOR TOPOGRAPHY AND COMPENSATION FOR SEPARATE ZONES

The unit for the corrections in this table is ·0001 dyne.

| Zone | Elevation in Feet | Topography | Compensation | Topography and Compensation | Elevation in Feet | Topography | Compensation | Topography and Compensation |
|---|---|---|---|---|---|---|---|---|
| | Schreiber, Ont., No. 122 | | | | Federal Mine, Gaspé County, Que., No. 123 | | | |
| A | 993 | + 2 | 0 | + 2 | 1,736 | + 2 | 0 | + 2 |
| B | 1,000 | + 64 | 0 | + 64 | 1,725 | + 67 | 0 | + 67 |
| C | 1,000 | +104 | 0 | +104 | 1,658 | +121 | 0 | +121 |
| D | 1,000 | + 84 | 0 | + 84 | 1,565 | +156 | 0 | +156 |
| E | 1,038 | + 43 | 0 | + 43 | 1,651 | + 92 | 0 | + 92 |
| F | 1,040 | + 16 | 0 | + 16 | 1,764 | + 52 | − 4 | + 48 |
| G | 1,025 | + 3 | 0 | + 3 | 1,677 | + 22 | − 5 | + 17 |
| H | 975 | + 3 | − 3 | 0 | 1,755 | + 11 | − 13 | − 2 |
| I | 875 | + 4 | − 4 | 0 | 1,785 | + 18 | − 20 | − 2 |
| J | 750 | 0 | − 11 | − 11 | 2,094 | + 1 | − 17 | − 16 |
| K | 725 | 0 | − 13 | − 13 | 2,000 | − 5 | − 24 | − 29 |
| L | 692 | 0 | − 17 | − 17 | 2,383 | + 3 | − 57 | − 54 |
| M | 500 | 0 | − 28 | − 28 | 1,171 | 0 | − 66 | − 66 |
| N | 538 | 0 | − 25 | − 25 | 425 | 0 | − 23 | − 23 |
| O | 702 | 0 | − 40 | − 40 | 318 | 0 | − 19 | − 19 |
| 18 | | | | − 8 | | | | − 2 |
| 17 | | | | − 8 | | | | − 5 |
| 16 | | | | − 8 | | | | − 4 |
| 15 | | | | − 9 | | | | − 6 |
| 14 | | | | − 10 | | | | − 6 |
| 13 | | | | − 14 | | | | − 12 |
| 12 | | | | − 8 | | | | − 7 |
| 11 | | | | − 6 | | | | − 1 |
| 10 | | | | − 7 | | | | + 11 |
| 9 | | | | − 7 | | | | + 15 |
| 8 | | | | − 1 | | | | + 18* |
| 7 | | | | + 4 | | | | + 7* |
| 6 | | | | + 6* | | | | + 6* |
| 5 | | | | + 9* | | | | + 5* |
| 4 | | | | + 6* | | | | + 5* |
| 3 | | | | + 5* | | | | + 6* |
| 2 | | | | + 3* | | | | + 4* |
| 1 | | | | + 1* | | | | + 1* |
| | | Total | | +130 | | Total | | +327 |

*These values have been interpolated from those obtained for neighbouring stations.

TABLE V—*Continued*

AVERAGE ELEVATIONS AND CORRECTIONS FOR TOPOGRAPHY AND COMPENSATION FOR SEPARATE ZONES

The unit for the corrections in this table is ·0001 dyne.

| Zone | Elevation in Feet | Topography | Compensation | Topography and Compensation | Elevation in Feet | Topography | Compensation | Topography and Compensation |
|---|---|---|---|---|---|---|---|---|
| | Cascapedia, Que., No. 124 | | | | Lac au Saumon, Que., No. 125 | | | |
| A | 37 | + 2 | 0 | + 2 | 507 | + 2 | 0 | + 2 |
| B | 42 | + 12 | 0 | + 12 | 510 | + 56 | 0 | + 56 |
| C | 40 | 0 | 0 | 0 | 519 | + 61 | 0 | + 61 |
| D | 40 | + 2 | 0 | + 2 | 518 | + 32 | 0 | + 32 |
| E | 62 | + 1 | 0 | + 1 | 540 | + 13 | 0 | + 13 |
| F | 78 | 0 | 0 | 0 | 555 | + 4 | 0 | + 4 |
| G | 283 | 0 | 0 | 0 | 652 | 0 | 0 | 0 |
| H | 350 | 0 | 0 | 0 | 831 | 0 | 0 | 0 |
| I | 565 | 0 | 0 | 0 | 985 | + 6 | − 6 | 0 |
| J | 588 | 0 | − 9 | − 9 | 869 | 0 | − 14 | − 14 |
| K | 655 | 0 | − 12 | − 12 | 1,070 | 0 | − 20 | − 20 |
| L | 862 | 0 | − 23 | − 23 | 1,162 | 0 | − 28 | − 28 |
| M | 864 | 0 | − 48 | − 48 | 1,071 | 0 | − 61 | − 61 |
| N | 1,088 | 0 | − 55 | − 55 | 900 | 0 | − 47 | − 47 |
| O | 329 | 0 | − 20 | − 20 | 654 | 0 | − 36 | − 36 |
| 18 | | | | − 2 | | | | − 5 |
| 17 | | | | − 2 | | | | − 5 |
| 16 | | | | − 4 | | | | − 5 |
| 15 | | | | − 5 | | | | − 5 |
| 14 | | | | − 5 | | | | − 7 |
| 13 | | | | − 13 | | | | − 11 |
| 12 | | | | − 7 | | | | − 7 |
| 11 | | | | + 4 | | | | + 1 |
| 10 | | | | + 10 | | | | + 6 |
| 9 | | | | + 13 | | | | + 15 |
| 8 | | | | + 18* | | | | + 17* |
| 7 | | | | + 7* | | | | + 7* |
| 6 | | | | + 6* | | | | + 6* |
| 5 | | | | + 5* | | | | + 5* |
| 4 | | | | + 5* | | | | + 5* |
| 3 | | | | + 6* | | | | + 5* |
| 2 | | | | + 4* | | | | + 4* |
| 1 | | | | + 1* | | | | + 1* |
| | | Total | | −109 | | Total | | − 11 |

*These values have been interpolated from those obtained for neighbouring stations.

TABLE V—*Continued*

AVERAGE ELEVATIONS AND CORRECTIONS FOR TOPOGRAPHY AND COMPENSATION FOR SEPARATE ZONES

The unit for the corrections in this table is ·0001 dyne.

| Zone | Elevation in Feet | Topography | Compensation | Topography and Compensation | Elevation in Feet | Topography | Compensation | Topography and Compensation |
|---|---|---|---|---|---|---|---|---|
| | La Tuque, Que., No. 126 | | | | Parent, Que., No. 127 | | | |
| A | 555 | + 2 | 0 | + 2 | 1,401 | + 2 | 0 | + 2 |
| B | 560 | + 57 | 0 | + 57 | 1,405 | + 65 | 0 | + 65 |
| C | 545 | + 64 | 0 | + 64 | 1,389 | +123 | 0 | +123 |
| D | 537 | + 34 | 0 | + 34 | 1,380 | +130 | 0 | +130 |
| E | 511 | + 12 | 0 | + 12 | 1,390 | + 71 | 0 | + 71 |
| F | 465 | + 2 | 0 | + 2 | 1,394 | + 30 | 0 | + 30 |
| G | 475 | 0 | 0 | 0 | 1,458 | + 12 | 0 | + 12 |
| H | 597 | 0 | 0 | 0 | 1,512 | + 16 | − 16 | 0 |
| I | 675 | 0 | 0 | 0 | 1,625 | + 20 | − 20 | 0 |
| J | 828 | 0 | − 13 | − 13 | 1,600 | 0 | − 16 | − 16 |
| K | 985 | 0 | − 20 | − 20 | 1,620 | 0 | − 20 | − 20 |
| L | 996 | 0 | − 24 | − 24 | 1,483 | 0 | − 36 | − 36 |
| M | 943 | 0 | − 53 | − 53 | 1,386 | 0 | − 78 | − 78 |
| N | 1,125 | 0 | − 64 | − 64 | 1,369 | 0 | − 72 | − 72 |
| O | 1,014 | 0 | − 57 | − 57 | 1,189 | 0 | − 67 | − 67 |
| 18 | | | | − 8 | | | | − 10 |
| 17 | | | | − 9 | | | | − 9 |
| 16 | | | | − 10 | | | | − 8 |
| 15 | | | | − 10 | | | | − 9 |
| 14 | | | | − 10 | | | | − 9 |
| 13 | | | | − 15 | | | | − 16 |
| 12 | | | | − 7 | | | | − 7 |
| 11 | | | | − 5 | | | | − 4 |
| 10 | | | | + 5 | | | | 0 |
| 9 | | | | + 7 | | | | + 6 |
| 8 | | | | + 17 | | | | + 13 |
| 7 | | | | + 6* | | | | + 6* |
| 6 | | | | + 5* | | | | + 5* |
| 5 | | | | + 7* | | | | + 7* |
| 4 | | | | + 5* | | | | + 5* |
| 3 | | | | + 5* | | | | + 5* |
| 2 | | | | + 4* | | | | + 4* |
| 1 | | | | + 1* | | | | + 1* |
| | | Total | | − 72 | | Total | | +124 |

*These values have been interpolated from those obtained for neighbouring stations.

TABLE V—*Concluded*

AVERAGE ELEVATIONS AND CORRECTIONS FOR TOPOGRAPHY AND COMPENSATION FOR SEPARATE ZONES

The unit for the corrections in this table is ·0001 dyne.

| Zone | Elevation in Feet | Topography | Compensation | Topography and Compensation |
|---|---|---|---|---|
| | Taschereau, Que., No. 128 | | | |
| A | 1,008 | + 2 | 0 | + 2 |
| B | 1,013 | + 64 | 0 | + 64 |
| C | 1,013 | +105 | 0 | +105 |
| D | 1,015 | + 86 | 0 | + 86 |
| E | 1,012 | + 41 | 0 | + 41 |
| F | 1,016 | + 15 | 0 | + 15 |
| G | 1,019 | 0 | 0 | 0 |
| H | 1,058 | + 2 | − 2 | 0 |
| I | 1,088 | + 4 | − 4 | 0 |
| J | 1,138 | 0 | − 16 | − 16 |
| K | 1,115 | 0 | − 20 | − 20 |
| L | 1,117 | 0 | − 27 | − 27 |
| M | 1,064 | 0 | − 59 | − 59 |
| N | 856 | 0 | − 43 | − 43 |
| O | 864 | 0 | − 48 | − 48 |
| 18 | | | | − 8 |
| 17 | | | | − 9 |
| 16 | | | | − 9 |
| 15 | | | | − 9 |
| 14 | | | | − 9 |
| 13 | | | | − 13 |
| 12 | | | | − 6 |
| 11 | | | | − 7 |
| 10 | | | | − 4 |
| 9 | | | | + 1 |
| 8 | | | | + 9 |
| 7 | | | | + 5* |
| 6 | | | | + 5* |
| 5 | | | | + 8* |
| 4 | | | | + 5* |
| 3 | | | | + 5* |
| 2 | | | | + 3* |
| 1 | | | | + 1* |
| | | | Total | + 68 |

*These values have been interpolated from those obtained for neighbouring stations.

## TABLE VI

PERIODS IN SECONDS × $10^7$ OF PENDULUM NO. 3 FOR DECREASING ARCS ON KNIFE EDGE I FROM 6 CONTINUOUS SWINGS OF 24 HOURS EACH AT AN AVERAGE PRESSURE OF 12·8 MILLIMETRES OF MERCURY FROM OBSERVATIONS BY A. H. MILLER AND J. P. HENDERSON

| | | | | | | | | | Mean |
|---|---|---|---|---|---|---|---|---|---|
| Observed initial and final amplitude in millimetres (1 mm. = 11′ 33″) | 8·0—6·4 | 6·4—5·0 | 5·0—4·0 | 4·0—3·1 | 3·1—2·4 | 2·4—1·9 | 1·9—1·3 | 1·3—1·0 | |
| Corresponding computed amplitudes assuming the sine of the semi arc to decrease exponentially | 8·0—6·2 | 6·2—4·8 | 4·8—3·7 | 3·7—2·8 | 2·8—2·2 | 2·2—1·7 | 1·7—1·3 | 1·3—1·0 | |
| Observed periods corrected for arc*, temperature**, pressure† and flexure†† | 5014291 ±2·1 | 5014285 ±1·0 | 5014284 ±1·7 | 5014284 ±1·6 | 5014280 ±1·9 | 5014282 ±1·4 | 5014276 ±2·1 | 5014277 ±1·3 | 5014282 |
| Periods corrected as above with an additional arc correction of 2·17 × $10^{-7}$s. per mm. of arc | 5014275 | 5014273 | 5014274 | 5014276 | 5014274 | 5014277 | 5014273 | 5014275 | 5014275 |
| Corrected periods for swings with final arc of 1 mm. and initial arcs of 8·0, 6·4, 5·0, 4·0, 3·1, 2·4, 1·9, 1·3 mm. respectively | 5014282·4 ±0·6 | 5014281·1 ±0·6 | 5014280·5 ±0·7 | 5014279·8 ±0·8 | 5014278·8 ±0·9 | 5014278·3 ±0·9 | 5014276·5 ±1·2 | 5014277·0 ±1·3 | 5014279·3 |
| Periods corrected by an additional arc correction of 2.17 × $10^{-7}$s. | 5014272·6 | 5014273·1 | 5014274·0 | 5014274·4 | 5014274·4 | 5014274·6 | 5014273·4 | 5014274·5 | 5014273·9 |

*Arc Correction $= \frac{T_o(\mathrm{Sin}^2\alpha_1 - \mathrm{Sin}^2\alpha_2)}{32(\log_e \mathrm{Sin}\,\alpha_1 - \log_e \mathrm{Sin}\,\alpha_2)}$ †Pressure Correction $= +1{\cdot}01 \times 10^{-7}(60 - \frac{p}{1+\alpha t})$sec.

**Temperature Correction $= -41{\cdot}55 \times 10^{-7}$s. per degree centigrade.

††Flexure Correction = 1·73 × $10^{-7}$ sec. per ·01 fringe displacement of sodium light for 5 mm. arc = also theoretically $T\frac{\Delta l}{2l} = 847{\cdot}3\frac{D_y}{A} \times 10^{-7}$ Rate Correction = Uncorrected Period × $\frac{86400}{86400 - \mathrm{Rate}}$

## TABLE VII—ARC CORRECTIONS IN UNITS OF $10^{-7}$ SEC. FROM FORMULA

$$\Delta T = T_o \frac{(\mathrm{Sin}^2 \alpha_1 - \mathrm{Sin}^2 \alpha_2)}{32(\log_e \mathrm{Sin}\ \alpha_1 - \log_e \mathrm{Sin}\ \alpha_2)}$$

| Initial total arc in millimetres | Final total arc in millimetres | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 |
| 10 | 79·8 | 71·4 | 63·3 | 55·5 | 47·9 | 40·6 | 33·5 | 26·4 | 19·0 |
| 9 | .... | 63·8 | 56·4 | 49·1 | 42·1 | 35·5 | 29·0 | 22·6 | 16·1 |
| 8 | .... | .... | 49·8 | 43·1 | 36·7 | 30·7 | 24·8 | 19·1 | 13·4 |
| 7 | .... | .... | .... | 37·3 | 31·5 | 26·1 | 20·9 | 15·9 | 10·9 |
| 6 | .... | .... | .... | .... | 26·7 | 21·8 | 17·2 | 12·9 | 8·6 |
| 5 | .... | .... | .... | .... | .... | 17·9 | 13·9 | 10·1 | 6·6 |
| 4 | .... | .... | .... | .... | .... | .... | 10·8 | 7·7 | 4·8 |
| 3 | .... | .... | .... | .... | .... | .... | .... | 5·5 | 3·2 |
| 2 | .... | .... | .... | .... | .... | .... | .... | .... | 1·9 |

Reqn. 7185