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TEST PROGRAM

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GAGETOWN LOW NO_X/SO_X BURNER PROJECT

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ERL 87-1000

ENERGY RESEARCH LABORATORIES CPUB

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by

G.K. Lee* and R.J. Philp**

ABSTRACT

Canada, Denmark, Sweden and the United States are collaborating in a three-stage project, under the auspices of the International Energy Agency to develop and evaluate the performance of a low NO_X/SO_X burner for pulverized coal. Stage I, which involved small-scale burner tests with 45 coals from around the world, established that over 70% of the NO_X from pulverized coal flames was derived from the fuel nitrogen and that the conversion of fuel nitrogen to NO_X could be suppressed by proper air staging. In Stage II, the concept of air staging was translated into a prototype design for a NO_X coal burner and large-scale boiler simulator trials were conducted on four coals, two of which included sorbent injection to reduce SO_2 emissions. Stage III, now in progress, involves full-scale demonstration trials on low NO_X/SO_X burners installed in a front-wall-fired boiler in each country using the same general test procedures.

Under Stage III, five bituminous-coal fired boilers of different capacities are being evaluated for NO_X/SO_X reductions under closely controlled operational conditions to validate the trends observed in Stage II. One of the two Canadian boilers selected is the No. 2 Unit at the Central Heating Plant of Canadian Forces Base Gagetown. This Unit, rated at 20 MWt, supplies hot water for a district heating system.

This report gives a detailed outline of the test objectives, the general work plan and the measurement and sampling procedures that will be used during the field trials on Gagetown Unit No. 2

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<u>Contents</u>

4

1) Test Plan	1
1.1.1) Low NOx	
1.2) Baseline Tests	
1.3.1) Low NOx	Screening and Optimization 2 2
1.4) Long Term Test	
2) Test Schedule	
3) Test Coal: Specific	cations3
4) Measurements	
4.1.1) Function Tests	
4.2) Probe	
4.2.1) Furnace Tempera 4.2.1.1) Suction Pyron 4.2.1.2) Bare Thermoco	neter
4.2.2) Furnace Radiat	ion
4.3) Stack Measurement	ts
4.4) Pre-Test	

1) <u>TEST PLAN</u>

-4

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The following tentative test plan is based on the availability of material and human resources, the test period that is available and the heating demand requirements.

1.1) Function Tests

Screen operation of burner and preliminary evaluation of performance.

Schedule: commence Jan. 15, 1987

1.1.1) Low NOx Due to previous testing only minor tuning is expected. Critical parameters are carbon burnout and NOx.

1.1.2) Sorbent Injection Assess SO2 capture at a Ca/S of 2.5 using the same injection velocities as in previous testing.

1.2) Baseline Tests

Repetition of function tests, but with more extensive test procedure.

Scheduling: commence Feb. 1, 1988.

Test Matrix

		Test	No.	
Parameter	1	2	З	4
sorbent injection	Ν	N	Y	Y
boiler load	1/2	Full	1/2	Full

N: No Y: Yes 1/2: half load, lower burner only Full: full load, both burners

1.3) Parametric Tests: Screening and Optimization

The objectives are to determine the limits of the parameters and the influence on boiler output. Only half load measurements required to ascertain effects will be made in the screening tests. Optimization tests at full load will cover a reduced range and testing will be more extensive.

1.3.1) Low NOx

Test Matrix

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			Test No.		
Parameters	1	2	3	4	5
Sec/Tert Air	V	F	F	F	F
Swirl	F	V	F	F	F
Primary Air	F	F	V	F	F
Injection air	F	F	F	V	F
Core Air *	F	F	F	F	V

F: Fixed, Parameter at baseline (low NOx) operating conditions V: Variable, 3-5 settings *: if practical

1.3.2) Sorbent Injection

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Test Matrix

		Test No.	
Parameters	1	2	3
Injection velocity	V	F	F
Ca/S	F	V	F
Sorbent type	· L	L	H

V: variable F: fixed

L: limestone H: hydroxide

1.4) Long Term Test

The boiler will be operated for 2 days at full load. Limestone at a Ca/S ratio of 2.5 will be injected and optimized burner settings will be employed.

2) <u>TEST SCHEDULE</u>

It is estimated that 27 test days are required to complete the program, excluding those required for the function tests. The test sequence and schedule is shown in the attached figure.

3) TEST COAL: SPECIFICATIONS

V.M.: 33-35% Ash : 8-12% S : 21/2-3%

4) MEASUREMENTS

4.1) Log

4.1.1) Function Tests

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Date:
Time:
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Boiler Measurements:
Firing Configuration: Upper Burner, Y/N:
                       Lower Burner, Y/N:
MW Flow (0-25 \text{ MW}):
Water Flow (0-100%):
Air Flow (0-100%):
Furnace draft, +100/-100 Pa =
Air Heater:
     Gas Inlet Temp., °C =
     Gas Outlet Temp., oC =
     Air Inlet Temp., °C =
     Air Outlet Temp., °C =
Flue Gas O_2, % =
Lower burner, oil flow, %:
              secondary air flow, %:
              tertiary air flow, %:
              exhaustor, %:
Lower mill, primary air flow, %:
 (No. 1)
            coal feeder, %:
            pressure, inlet, +250/-1000 Pa:
                       outlet, 0/2.5 kPa:
            motor amperes, A:
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Fest Schedule: Tentative																										
		•	2	4	-		-	•	•				Days				_	_								07
Test	1	2	3	4	5	b	1	в .	Э	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27
Parametric Screening																										
Sec/Tert.																										
Swirl																										
Core		-																								
Primary																										
Injection				-																						
Sorbent Injection Velocity																										
Ca/S						-																				
Baseline, Test Sequence No.1 Sorbent,Load	•																							•		
N,1/2																										
N, Full							•																			
Y, 1/2															•											
Y,Full																										
Parametric Optimization					÷																					
Sec/Tert									-																	
Swirl													-													
Çcte Primary								`																		
Injection																•										•
Sorbent Injection velocity																										
Ca/S																										
Baseline Test Sequence, No.2																										
Sorbent, Load																										
N, 1/2																										
N,Full Y,1/2																										
Y,Full																										
Long Term Test																										
Optimized condition																										
											•															
arametric Optimization																										
Sorbent Type, Ca/S																				,						
								•																		
				-																						

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Upper burner, oil flow, %: secondary air flow, %: tertiary air flow, %: exhaustor, %: Upper mill, primary air flow, %: (No. 2) coal feeder, %: pressure, inlet, +250/-1000 Pa: outlet, 0/2.5 kPa: motor amperes, A: I.D. Fan motor, A: F.D. Fan motor, A: Forced draft duct pressure, %: Oxygen trim, %: Air heater bypass, %: Primary air, lower burner, %: upper burner, %: Secondary air, lower burner, %: upper burner, %: Coal/air temp, °C: lower burner mill: upper burner mill: Water flow, Inlet, %: Outlet, %: temp., Inlet, °C: Outlet, °C: press., kPa guage: <u>Burner</u>: Settings Lower Secondary air swirler, mm.: Position, secondary air, mm.: tertiary air, mm.: core air, mm.: Flame Description: Sorbent Injection: Feed rate, % = Time: Totalizer Count: Time: Totalizer Count: Air flow: E.C. Measurements:

Upper

<u>E.C. Heasuren</u> SO₂, ppm: NO_x, ppm: THC, ppm: CO, ppm: O₂, %: CO₂, %:

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Samples, check list: Coal, Raw: Pulverized: Sorbent: Fly Ash: 4.1.2) Baseline/Parametric Optimization Tests Date: Time: Boiler Measurements: Firing Configuration: Upper Burner, Y/N: Lower Burner, Y/N: MW Flow (0-25 MW): Water Flow (0-100%): Air Flow (0-100%): Furnace draft, +100/-100 Pa = Air Heater: Gas Inlet Temp., °C Ξ Gas Outlet Temp., °C = Air Inlet Temp., °C = Air Outlet Temp., $\circ C =$ Flue Gas O_2 , % = Lower burner, oil flow, %: secondary air flow, %: tertiary air flow, %: exhaustor, %: Lower mill, primary air flow, %: (No. 1) coal feeder, %: pressure, inlet, +250/-1000 Pa: outlet, 0/2.5 kPa: motor amperes, A: Upper burner, oil flow, %: secondary air flow, %: tertiary air flow, %: exhaustor, %: Upper mill, primary air flow, %: (No. 2) coal feeder, %: pressure, inlet, +250/-1000 Pa: outlet, 0/2.5 kPa: motor amperes, A: I.D. Fan motor, A: F.D. Fan motor, A: Forced draft duct pressure, %: Oxygen trim, %: Air heater bypass, %: Primary air, lower burner, %: upper burner, %: Secondary air, lower burner, %: upper burner, %:

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Coal/air temp, °C: lower burner mill: upper burner mill: Water flow, Inlet, %: Outlet, %: temp., Inlet, °C: Outlet, °C: press., kPa guage: Pressure drop, convective tube bank, " WC = air preheater, " WC = furnace/preheater outlet, " WC = Soot blowing cycle: Combustion air humidity, wet bulb, °C = dry bult, °C = relative humidity, % = Furnace deposits, description: Burner: Settings Lower Upper Secondary air swirler, mm.: Position, secondary air, mm.: tertiary air, mm.: core air, mm.: Pressure, tertiary air windbox, "WC = Orifice and Venturi Measurements: (1) Primary Air, Lower Burner (DP-127A):
 pressure differential, "WC =
 pressure at lower tap, "WC = (2) Core, Secondary and Tertiary Air, Lower Burner (DP-129A) pressure differential, " WC = pressure at lower tap, " WC = (3) Primary Air, Upper Burner (DP-128A): pressure differential, "WC = pressure at lower tap, "WC = (4) Core, Secondary and Tertiary air, Upper Burner (DP-130A) pressure differential, " WC = pressure at lower tap, " WC = Flame Description: Sorbent Injection: Feed rate, %: Time: Totalizer Count: Time: Totalizer Count: Air flow: Compressor: injection, A = fluidizing, A =

E.C. Measurements: SO2, ppm: NOx, ppm: THC, ppm: CO, ppm: O2, %: CO2, %: Fly ash mass loading, kg/h: Particle size distribution Ash mass balance: Ash from cyclone separators, kg: Time, start: finish: Bottom ash, kg: Time, start: finish: Samples, check list: Coal, Raw: Pulverized: Sorbent: Ash from cyclone separators: Bottom ash: Fly ash: 4.2) Probe 4.2.1) Furnace Temperature 4.2.1.1) Suction Pyrometer O.D.: 2.5" Length: 8' 4", maximum insertion Procedure: 1) Tests: 1.1) Parametric Screening: Injection air flow: one measurement at typical flow 1.2) Baseline test: full load, with and without limestone injection 1.3) Parametric Optimization: Either for injection air or sorbent injection velocity tests, depending upon outcome of 1.2 2) Location of measurements:

2.1) L.1.1, L.2.1: at wall and every 1.5' to a maximum insertion of 6' in each port, 5 measurements/port
2.2) L.1.2, L.2.2: at 1.5' and 6', 2 measurements/port
2.3) R.1.2, R.2.2: at 1.5' and 4.5', 2 measurements/port

Port locations:

See attached figure

Port No.:

- L.1.1: LHS, elevation no. 1 (lower), front -port located on LHS of boiler (facing) -approximately 9" below centre line of lower burner, and 10" from quarl exit
- L.1.2: LHS, elevation no. 1 (lower), rear -port located on LHS of boiler (facing) -approximately 9" below centre line of lower burner, and 19" from rear wall
- L.2.1: LHS, elevation no. 2, front -port located on LHS of 'boiler (facing) -approximately 28" above centre line of upper burner, and 10" from quarl exit
- L.2.2: LHS, elevation no. 2, rear -port located on LHS of boiler (facing) -approximately 28" above centre line of upper burner, and 19" from rear wall
 - L.3: LHS, elevation no. 3, convection tube bank inlet -port located on LHS of boiler (facing) -approximately 44" from the first tube bank, and on the centre line, or port slightly above
 - L.4: LHS, elevation no. 4, outlet of convection tube bank
- R.1.2: same as L.1.2, but located on RHS
- R.2.2: same as L.2.2, but located on RHS
 - R.3: same as L.3, but located on RHS
 - R.4: same as L.4, but located on RHS
- R.x.y: corresponding ports on the opposite side of the boiler

4.2.1.2) <u>Bare Thermocouple</u>

Bare thermocouples located at every 1.5' and supported by air cooled pipe to be used for measurements in ports L.3, L.4, R.3 and R.4.

4.2.2) Furnace Radiation

Ellipsoidal Radiometer

Procedure:

1) Tests:

1.1) Baseline test: full load, with and without limestone injection

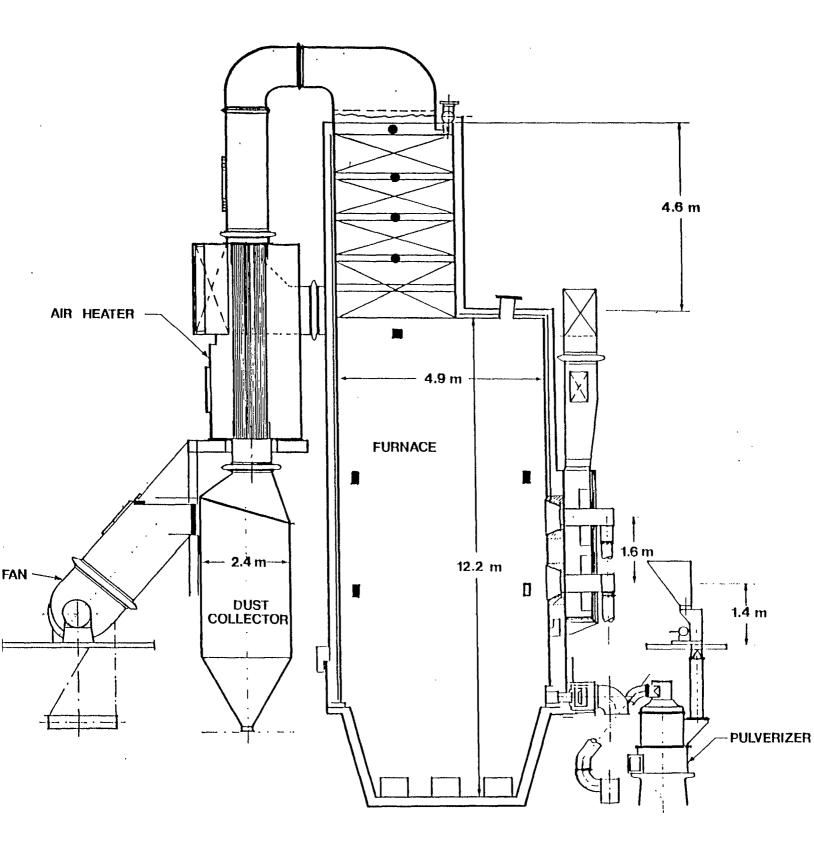
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1.2) Parametric Optimization:

Either for injection air or sorbent injection velocity tests, depending upon outcome of 1.1 2) Location of measurements:

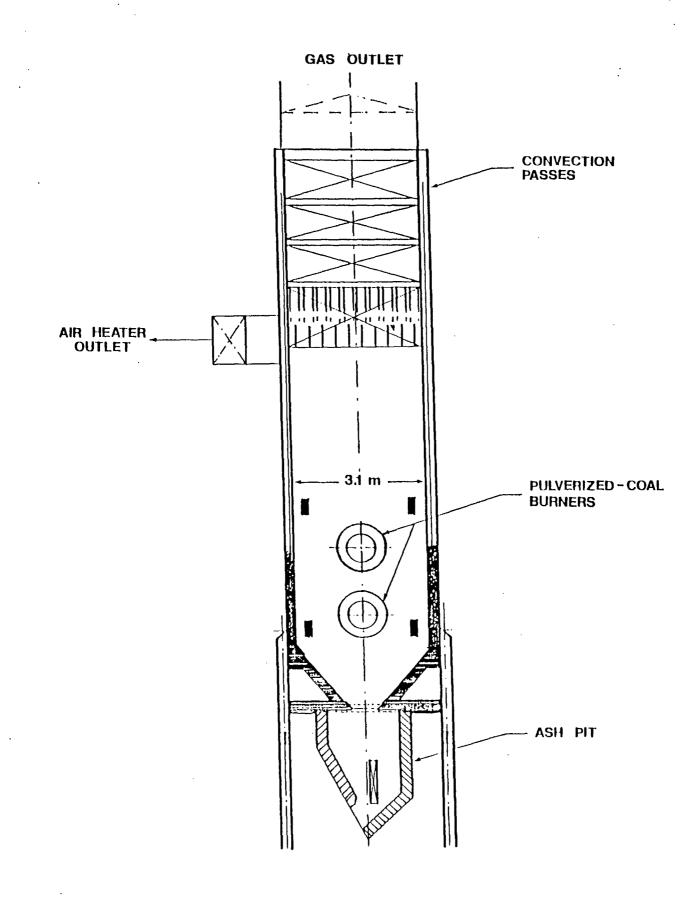
2.1) L.1.1, L.2.1: at wall

2.2) L.1.2, L.2.2, L.3: at wall



Side View: No.2 Generator - Gagetown CHP

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Front View: No.2 Generator - Gagetown CHP

4.3) Stack Measurements

Flue gas will be monitored continously for SOx, NOx, CO, O2, CO2 and THC downstream of the I.D. fan. Particulates will also be sampled using standard isokinetic techniques so that loading may be determined. Laboratory particles size analysis will be conducted on the solids.

4.4) <u>PRE-TEST</u>

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4.4.1) Calibrate orifice and venturi: lower burner air flows

4.4.2) Calibrate sorbent injection

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TABLE 1 March 1987 Gagetown Tests prior to boiler cleaning

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Test	P2	P7	ЪЭ	P10	P11
Date Time: Start End	Feb 28 15:12 16:55	Mar 2 12:55 14:28	Mar 3 14:20 15:45	Mar 4 10:22 11:48	Mar 4 13:16 15:00
Coal Type Boiler Output, MW	Test 9.9	Test 11.8	Base 9.6	Base 10	Base 10
SO2, PPM NOx, PPM Ca/S Mole Ratio SO2 Absorption, % Calcium Efficiency	$2163 \\ 492 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $	$986 \\ 391 \\ 1.4 \\ 50.7 \\ 0.37$	827 347 0 0 0	281 276 2.25 59. 0.26	$181 \\ 261 \\ 1.85 \\ 77.8 \\ 0.42$
AH Outlet: Temp. C O2, % (vol.)	282 6	288 3	260 2.9	$\begin{array}{c} 272\\2.4\end{array}$	271 2.7
Carbon in Bottom Ash, % (1) Carbon in Fly Ash, % (1)	7 28.1	2.2 9.7	6.8 66.7	$\begin{array}{c} 4.9\\ 21.6\end{array}$	5 16
Coal Feedrate, kg/h Oil Flowrate, l/h % of Total Energy Input Limestone Feedrate, kg/h Total Air, kg/h Dry Flue Gas, kg/h H2O in Flue Gas, kg/h	$1608 \\ 40 \\ 3.3 \\ 0 \\ 20200 \\ 21200 \\ 730 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1600 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 $	$1757 \\ 40 \\ 3.0 \\ 223 \\ 18500 \\ 20400 \\ 780$	$1271 \\ 40 \\ 3.5 \\ 0 \\ 15900 \\ 16600 \\ 610 \\ $	1255403.6981530016000600	$1236 \\ 40 \\ 3.6 \\ 96 \\ 15500 \\ 16200 \\ 600 $
Boiler Efficiency, % Dry Gas, H2 & H2O Loss, % Unburned C in Ash Loss, % Calcining Loss, % Radiation Loss, %	77.717.14.400.8	$82.8 \\ 15.4 \\ 1.0 \\ 0.8 \\ 0.8$			$ 84.7 \\ 13.9 \\ 0.5 \\ 0.4 \\ 0.8 $
Coal Analysis: C H N O S Ash Moisture Calorific Value, MJ/kg	$\begin{array}{r} 68.64\\ 4.42\\ 1.23\\ 7.55\\ 3.15\\ 10.93\\ 4.08\\ 28.75 \end{array}$	72.094.61.396.462.919.642.9130.08	81.02 5.1 1.62 6.04 1.28 3.31 1.63 33.69	81.73 5.12 1.61 5.98 1.06 3.02 1.48 33.89	$\begin{array}{c} 80.93 \\ 5.09 \\ 1.66 \\ 6.43 \\ 1.26 \\ 3.13 \\ 1.5 \\ 33.66 \end{array}$

(1) 10% of input ash removed from ash pit

TABLE 2 March 1987 Gagetown Tests after boiler cleaning

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Test	P13	P16a	P16b	P17	P19
Date Time: Start End	Mar 11 14:29 15:37			Mar 13 9:13 10:40	Mar 13 14:54 16:27
Coal Type Boiler Output, MW	Base 10.7		Base 10.5	Base 17.4	Base 17
SO2, PPM NOx, PPM Ca/S Mole Ratio SO2 Absorption, % Calcium Efficiency	764 364 0 0 0	$227 \\ 420 \\ 2.7 \\ 65.7 \\ 0.24$	$2.4 \\ 73.7$	784 400 0 0 0	$357 \\ 363 \\ 3.6 \\ 54.5 \\ 0.15$
AH Outlet: Temp. C O2, % (vol.)	186 3	$\begin{array}{c} 169 \\ 5.2 \end{array}$	$\begin{array}{c} 170 \\ 5.1 \end{array}$	177 4.0	177 3.8
Carbon in Bottom Ash, % (1) Carbon in Fly Ash, % (1)	$\begin{array}{c} 28.3 \\ 71.6 \end{array}$	7.5 22.5	7.5 22.5	2 61.2	2 21.8
Coal Feedrate, kg/h Oil Flowrate, 1/h % of Total Energy Input Limestone Feedrate, kg/h Total Air, kg/h Dry Flue Gas, kg/h H2O in Flue Gas, kg/h	1355403.301690017700640	$1310 \\ 40 \\ 3.5 \\ 120 \\ 17800 \\ 18600 \\ 610$	40 3.6 123 17700 18400	$2148 \\ 65 \\ 3.4 \\ 0 \\ 28300 \\ 29500 \\ 1020 \\$	2040 65 3.6 237 26700 27800 970
Boiler Efficiency, % Dry Gas, H2 & H2O Loss, % Unburned C in Ash Loss, % Calcining Loss, % Radiation Loss, %		87.7 10.3 1.2 0.5 0.8	$ \begin{array}{r} 88.2 \\ 10.3 \\ 0.7 \\ 0.5 \\ 0.8 \\ \end{array} $		$ \begin{array}{r} 88.3 \\ 10.2 \\ 0.7 \\ 0.6 \\ 0.8 \end{array} $
Coal Analysis: C H N O S Ash Moisture Calorific Value, MJ/kg	$\begin{array}{c} 81.32 \\ 5.04 \\ 1.58 \\ 6.55 \\ 1.14 \\ 2.46 \\ 1.91 \\ 33.81 \end{array}$	$79.26 \\ 4.94 \\ 1.69 \\ 6.50 \\ 1.03 \\ 4.44 \\ 2.12 \\ 32.92$	$\begin{array}{c} 80.66\\ 4.96\\ 1.5\\ 6.8\\ 1.24\\ 2.72\\ 2.12\\ 33.51 \end{array}$	$\begin{array}{r} 81.38\\ 5.04\\ 1.67\\ 6.26\\ 1.16\\ 2.52\\ 1.97\\ 33.93 \end{array}$	$\begin{array}{c} 81.47 \\ 5.09 \\ 1.65 \\ 6.14 \\ 0.99 \\ 2.80 \\ 1.86 \\ 33.97 \end{array}$

(1) 10% of input ash removed from ash pit