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# GEOLOGICAL SURVEY OF CANADA 

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# New and Revised Earthquake Focal Mechanisms of the Charlevoix Seismic Zone, Canada 

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# New and Revised <br> Earthquake Focal Mechanisms of the Charlevoix Seismic Zone, Canada 

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#### Abstract

The Charlevoix Seismic Zone (CSZ) is one of the most active seismic areas of eastern Canada. This report presents a series of new and revised CSZ focal mechanisms for the period 1974-1997. The report documents the methodology used, the input data and the results for 52 mechanisms computed with the program FOCMEC. For most new solutions, P and SH first motion data were used to constrain the mechanisms. The $P$ first motions were read on the vertical components of the digital and analogue records for stations located within 150 km of the CSZ. SH first motions (tranverse horizontal $S$ waves) were read off the two horizontal component data of the Charlevoix Local Telemetered Network (CLTN). Mechanisms of earthquakes with magnitude $>=3.0$ for the period 1989-1997 were computed. For events of magnitude $>=2.0$ recorded between June and November 1996, field data were added to the CLTN to define the focal mechanisms. In addition to these new mechanisms, some published mechanisms were re-computed. Two of the six focal mechanisms from the 1974 field survey appeared well defined, while the other four are less constrained. The August 19, 1979 magnitude $\mathrm{m}_{\mathrm{N}} 5.0$ earthquake was re-analyzed with the current GSC practice for plotting first motions on the focal sphere. Although the original thrust faulting mechanism of the solution remains, the two nodal planes are somewhat different than the ones published. Revisions to the mechanisms published by the Geological Survey of Canada and by Li et al. (1995) are also presented. Finally, the three mechanisms of Lamontagne and Ranalli (1997) are presented. The tectonic implications of these mechanisms will be discussed in a future paper.


## Résumé

La zone sismique de Charlevoix (ZSC) est une des régions sismiques les plus actives de l'Est du Canada. Ce rapport présente une série de mécanismes au foyer de la ZSC qui sont nouveaux ou révisés et ce, pour la période 1974-1997. Ce rapport documente la méthodologie utilisée, les données entrées et les résultats pour quelque 52 mécanismes calculés avec le programme FOCMEC. Pour la plupart des nouvelles solutions, les premiers mouvements de $P$ et de SH furent utilisés pour contraindre les mécanismes. Les premiers mouvements de P furent lus sur des enregistrements numériques et analogiques de postes localisés à moins de 150 km de 1 a ZSC. Les premiers mouvements de SH furent lus à partir des données tri-axiales du réseau local télémétrique de Charlevoix (RLTC). Des mécanismes des séismes de magnitude $>=3.0$ de la période 1988-1997 furent calculés. Pour les événements de magnitude $>=2.0$ enregistrés entre juin et novembre 1996, des données de terrain furent ajoutées à celles du RLTC pour obtenir les mécanismes au foyer. En plus de ces nouveaux mécanismes, quelques autres déjà publiés furent recalculés. Deux des six mécanismes au foyer du levé de terrain de 1974 sont bien définis alors que les quatre autres sont moins bien contraints. Le séisme de magnitude $\mathrm{m}_{\mathrm{N}} 5,0$ du 19 août 1979 fut réanalysé avec la méthode courante pour positionner les premiers mouvements sur la sphère focale. Quoique le mécanisme de faille inverse est préservé, les deux plans nodaux sont quelque peu différents de ceux publiés. Des révisions aux mécanismes publiés par la Commission géologique du Canada et par Li et al. (1995) sont aussi présentés. Finalement, les trois mécanismes de Lamontagne et Ranalli (1997) sont montrés. Les implications tectoniques de ces
mécanismes seront discutés dans un article à venir.

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1- Introduction.
a) Purpose of the report.

Earthquake focal meichanisms can bring to light the relationships between earthquake sources and active faults. They are indicators of the nature of faulting and of the ambient stress system at the earthquake focus. Thus, they are unique sources of seismotectonic information.

This report shows the results of 52 focal mechanism calculations for earthquakes of the Charlevoix Seismic Zone. Focal mechanisms of micro-earthquakes are generally calculated using P first motions. In eastern Canada however, the large inter-station spacing limits the calculations to earthquakes that are at least magnitude 4.0. For smaller earthquakes, P arrivals are generally emergent on stations at regional distances. With the addition of SH first motions in the near field, focal mechanisms can be calculated for events in the magnitude 3.0 to 4.0 range. Most mechanisms of this report are new ones (58\%) computed with P first motions and SH first motions. About $40 \%$ of these are well constrained. The others are updated mechanisms of six earthquakes of the 1974 field survey, the 1979 Magnitude 5.0 earthquake, and some previously published ones.

This report provides the basic parameters used in the computations of these mechanisms. It also proposes a methodology to be used in similar studies. The tectonic implications of these mechanisms will be treated in an forthcoming paper.
b) Earthquake monitoring in the Charlevoix Seismic Zone.

The Charlevoix Seismic Zone (CSZ) of Québec, Canada, is one of the most seismically active areas of Eastern Canada. Historically, it has been the site of a number of moderate to large earthquakes (Figure 1). Since November 1976, between six to eight digital stations have monitored the area (Figure 2A; 2B). This array has been central to the current understanding of the CSZ seismotectonics. As of 1997, the permanent network of the Charlevoix Region (called the CLTN: Charlevoix Local Telemetered Network) has seven 3-component stations (one broadband: LMQ; and six short-period: A11, A16, A21, A54, A61 and A64; Figure 2B). Four additional stations are located within 150 km of the active zone (one digital: DAQ and four analogue: SHQ, SLQ, CIQ and QCQ; Figures 2 B and 2 C ; ). During the period mid-June to midNovember 1996, up to 8 additional analogue and digital field seismographs were in operation (Lamontagne et al., 1997 for details; Figure 2D).
c) Earthquake locations.

All hypocentre locations of this study were routinely computed with the CLTN phases only. The only exception is the June to November 1996 period, when additional phases from up to 6 field stations were added. Earthquakes were located using the "standard" GSC velocity model, which assumes a 36 km thick crust with $6.2 \mathrm{~km} / \mathrm{s}$ Pg velocity and $3.57 \mathrm{~km} / \mathrm{s} \mathrm{Sg}$ velocity. Mantle velocities are $8.2 \mathrm{~km} / \mathrm{s}$ for P and $4.7 \mathrm{~km} / \mathrm{s}$ for S . Take-off angles and azimuths are based on this
model. For a focal depth of $18 \mathrm{~km}, \mathrm{Pg}$ is the first wave to arrive up to about 150 km epicentral distance. Beyond this distance, the first arrival is assumed to be Pn for which a take-off angle of $49^{\circ}$ is assumed.

In Charlevoix, a half space velocity model does not take into account the strong lateral velocity change introduced by the Appalachian nappes. A dipping boundary model representing the interface between the Precambrian and the Appalachian nappes does not change significantly the take-off angles and azimuths for south shore stations (Lamontagne, 1987).
d) Determination of P-first motions.

For the digital stations of the Canadian National Seismograph Network (CNSN), most P-first motions were read by the author. Some additional first motions were read from the analogue seismograms. In all cases, the author only used the maximum number of conspicuous first motions. For station CIQ (Chicoutimi, Qué), the first motions were read by Reynald Du Berger of the Université du Québec à Chicoutimi.
e) Instrument polarity.

The CNSN vertical component polarities are checked about once a year using teleseisms. or nuclear test sources. Polarity of the CLTN stations were correct. Similar checks were made for the analogue stations. The seismometers and cables were never changed during the period 19881997 which insures consistency in the polarities (Gilles Girouard, pers. comm.). To illustrate the polarity correctness, Figure 3 presents the first motions for a South American earthquake recorded on March 25, 1997. Note the similarity of first motion on all components.
f) Methodology.

The program FOCMEC of Snoke et al. (1984) uses a grid search algorithm that finds all mechanisms that match a series of conditions. In this report, the conditions are the number of misfits for P and SH first motions and the search increment for the b axis. The program is run interactively. The results are displayed on a lower hemisphere equi-area projection. In general, the search was made using a one degree $b$-axis increment. In cases where too many solutions existed, 2 degree, then, 5 degree increments were used. For each event, the parameters that were used are listed in the appendices.

2- New focal mechanisms.
a) Convention for SH first motions.

SH first motions can only be read from rotated traces. This was done with the software package SAC (Seismic Analysis Code; Lawrence Livermore National Laboratory). To automate the process, a Perl Script was written to rotate the two horizontal component time series files with the SAC's function ROTATE. The description of the SAC function ROTATE in Tapley and Tull
(1990) is:
"Pairs of data components are rotated in this command. Each pair must have the same station name, event name, and sampling rate... Both components must be horizontals when the TO option is used. This means that the CMPAZ must be defined and that the CMPINC must be $90^{\circ}$. After the rotation is completed, the first component of each pair will be directed along the angle given after the TO keyword. If the TO GCP (TO Great Circle Path) option is used, this component will be directed along the angle given by the station-event back azimuth plus or minus $180^{\circ}$. This component therefore points from the event towards the station. The station and event coordinates (STLA, STLO, EVLA, and EVLO) must be defined so that the back azimuth can be calculated."

The following SAC instructions are used in the script.
cut start_time end_time
r time-series_n time-series_e
lp be co 11.4 npoles 6
chnhdr evla lat_value evlo long_value rotate to gcp
p1 relative perplot 2
| defines start and end times of data
| Reads in horizontal time series files ( $\mathrm{n}=$ north-south $\mathrm{e}=$ east-west).
| filter traces with a Butterworth filter to simulate pre-1995 CLTN response.
| change epicentre coordinates in header
| rotate traces to "Great Circle Path"
| plot 2 traces with relative time scale.

In conclusion, two rotated traces are obtained:
a) the radial component, where:

Up: away from the event.
Down: Towards the event.
and the transverse component, where
Up: Towards the right, back to event (> for FOCMEC).
Down: Towards the left, back to event (< for FOCMEC).
The following figures illustrate that the convention is respected. On September 24, 1996 at 23:40 U.T., an earthquake of magnitude 3.0 occurred in the Charlevoix Seismic Zone (Figure 4). The event was recorded by most stations of the 1996 summer field survey. Station A80P was located almost due West of the epicentre (Azimuth N275 ). The E-W trace shows an impulsive Westdirected Pg motion (Figure 5, bottom trace). This motion is directed at $275^{\circ}$ as expected (Figure 6). Traces were rotated into the radial and transverse components (Figure 7). The top trace shows the radial component and the lower one the transverse. As can be seen, the first motion is away from the event (up on upper trace), while the transverse component has very little motion at the peak of the P first break (as expected). For the same event, station A76P was located directly North of the epicentre (Azimuth N $0.3^{\circ} \mathrm{E}$; Figure 4). The first motion was mainly directed to the North, away from the epicentre (Figure 8), with a small NNE component, i.e. to the right with our back to the event (Figure 9). The motion is away from the epicentre (Figure 10, top) and the
small right component with our back to the epicentre (Figure 10, bottom). The motion would have been read as a ( $>$ ).

To illustrate that FOCMEC is using the right sign convention, Figure 11 shows the radiation pattern for P and SH expected for a vertical NS striking strike-slip earthquake. FOCMEC gives 0 error for the solution shown. If a station located at $\mathrm{N} 85^{\circ} \mathrm{E}$ is considered, a (<) SH motion is expected, i.e. a left motion with our back to the event. With the SAC function ROTATE, the radial trace is oriented $\mathrm{N} 85^{\circ}$ (i.e. station-event back azimuth) and the transverse component is oriented N175 . The Y-axis is pointing South. The SH first motion is nearly due North, it is plotted Down, i.e. giving a (<) first motion on the SAC plot. Thus, the expected and the SAC derived results are the same.

SH first motions were found to be fairly reliable. During the 1996 summer field survey, two focal mechanism could be determined using the P first motions only (events $96071418: 46$ and 960924 23:41; both are described in Appendix 2). In the first case, 3 SH out of 7 did not fit the solution, while 2 out of 9 did not fit the second solution. From these results, it was decided that the $P$ first motions would be preferred over the SH in the determination of the solutions. Thus, a solution with fairly well constrained planes based on P is necessary to get a reliable solution.
b) Listing and displaying the results.

Focal mechanisms were computed as followed. First, the seismic traces for P and transverse SH waves were plotted. From these, the first motions were picked and the pikfile was updated. The updated pickfiles are now in the Canadian seismicity database. From the P first motions only, a FOCMEC run was done, usually with a 5 degree $b$-axis increment. In most cases, due to the poor constraints, numerous solutions were found. In a few rare cases, one $P$ first motion was wrong. In a second step, using all P and SH first motions, another FOCMEC run was made. If no solution was found using a 1 degree increment, one SH misfit was accepted (P-first motions were considered more reliable). If no solutions was found, one additional SH misfit was accepted until some solutions existed. Naturally, if one $P$ was found to be wrong in the calculation with $P$ first motions only, one P misfit was our starting point for the P and SH calculations.

The variations in the $\mathrm{P}, \mathrm{T}$ and B axes were used to quantify the constraints on the nodal planes. Our method was inspired by the work of Moustafa (1992). The P, T and B axes were treated as vectors for which an average direction, plunge and length were computed. The average length is a measure of the dispersion of the axes, i.e. the best solutions have lengths close to 1 . The solutions were rated as follows:

| Quality | Considered <br> as: | Average <br> length <br> P, T, B | Corresponding <br> variation <br> in degrees <br> around average <br> position | Maximum <br> P <br> errors <br> $(\%)$ | Maximum <br> SH <br> errors <br> $(\%)$ |
| :---: | :--- | :---: | :---: | :--- | :--- |
| A | Reliable | $>0.994$ | +-10 | $<10$ | $<50$ |
| B | Reliable | $>0.988$ | +-15 | $<25$ | $<75$ |
| C | Weakly <br> constrained | $>0.979$ | +-20 | $<50$ | 100 |
| X | Rejected | $<=0.979$ | $>+-20$. | $>50$ | 100 |
| O | Cannot be <br> computed | -------- | ------ | ------ | ------ |

One should note that the three conditions had to be matched for the event to be of the corresponding quality. This rating scheme agreed with a visual inspection of the focal mechanisms. In a few cases, it was found that the $\mathrm{P}, \mathrm{T}$ and B axes were well constrained but that the distribution of first motions did not warrant a high quality rating. In that case, the solution was rated " X ". It was also found that very few P and SH were misfits and that the $\mathrm{P}, \mathrm{T}$, and B were the most important constraints. In other words, the high proportions of misfits for P and SH were rarely determining the quality of the solution.

For every event, three figures were produced that showed the focal mechanisms, the first motion picks and the epicentral map. Figure 12 shows an example of such an output.

## i) Focal mechanisms.

For all solutions, the first figure shows the FOCMEC results in five focal spheres (Figure 12A). Starting in the upper left and going clockwise, the first sphere shows the series of solutions obtained with P and SH first motions (entitled " $P, S H$ and $P$-Nodal"). The second shows the solutions obtained using the P first motions uniquely (entitled "Solution with P FM only"). Unless well constrained with $P$ first motions only (rather rare), the increment for the $b$ axis was $5^{\circ}$. The lower right one shows the SH first motions and the SH "nodal" lines computed with the P and SH solutions (entitled "SH motions and Lines"). The lower left one shows all first motions (entitled "First Motions Only"). Finally, the central mechanism is the average solution using the P and SH families of solutions (entitled "Best Solution"). One should also note that the exact position of the first motion on the focal sphere is not in the centre but in the lower left corner of the $C$ and $D$ first motion symbols.
ii) First motion picks.

The second figure in the series (Figure 12B) shows the digital vertical traces of the P arrivals (left window) and the transverse horizontal traces of the $S$ arrivals (right window). The station name can be found in the left portion of the trace. The first motion reading is shown in the left portion as well as where it was read (vertical bar). An "X" means that no first motion was read.
iii) Epicentral map.

The third figure (Figure 12C) shows an epicentral map of all earthquakes of magnitude 1 and larger for the period 1978-1996. The event is shown with its average focal mechanism solution. The stations that provided first motion readings are shown with a symbol that correspond to the number of P and SH first motions.
c) Results.
i) Earthquakes with magnitude $>=3.0$

Table 1 lists all events of magnitude 3.0 for the period November 1988 to April 1997. Most have a focal mechanism calculated for the first time. The results for the 10 quality A and B events are shown in Figure 13 the base information is shown in Appendix 1. The ones that had been previously calculated by other authors (shown by a * in Table 1) will be discussed in Section 3C.
ii) Earthquakes recorded during the 1996 summer field survey.

A total of 15 mechanisms were computed with the data recorded during the 1996 summer field survey. A total of 8 events were of quality A and B and are shown in Figure 14. The additional data was central to the focal mechanism calculations for events as small as $\mathrm{m}_{\mathrm{N}} 2.0$. The base information for all events are shown in Appendix 2.

3- Re-analysis of previously published focal mechanisms.
a) The 1974 Field Survey.

In the 1974 experiment, six of the 34 events had sufficient P-first motions to have a focal mechanism computed (Figure 15). Leblanc and Buchbinder (1977) warned readers that "except for the 20/06/74 event, these events are neither unique nor tightly defined". These original mechanisms were computed with the program of Wickens and Hodgson (1967), later modified by A.E. Stevens, that "presents up to 5 of the best pairs of nodal planes" (Leblanc and Buchbinder, 1977). A preferred solution was chosen from these.

The focal mechanisms were re-computed using the program FOCMEC. Take-off angles and azimuths were the same as in Leblanc and Buchbinder (1977) and were based on the standard

GSC velocity model. Since all first motions were read from stations within 130 km distance, they all correspond to direct Pg arrivals. The outputs of the solutions are presented in Appendix 3.

The mechanisms are not equally constrained. Two of the six mechanisms are well constrained (74/06/09 and 74/06/23; Figure 16A), two mechanisms have two main families of solutions (74/06/20 and 74/06/30) and the last two are very poorly constrained (74/07/02 and 74/07/13; Figure 16B). The two best-constrained mechanisms (74/06/09 and 74/06/23) are similar to the original solutions of Leblanc and Buchbinder (1977) and to the re-computed solutions of Adams et al. (1989). The 74/06/09 solution is a mixed strike-slip--reverse faulting type while the other is almost a pure reverse faulting type. For the two events which have two families of solutions, the 74/06/20 event has a non-traditional normal-faulting mechanisms.
b) The 19 August 1979 , mbLg 5.0 earthquake.

The August 19, 1979 mbLg 5.0 earthquake is the largest CSZ earthquake within the time period 1952-1996. Using P-first motions, a fairly well constrained focal mechanism was determined (Hasegawa and Wetmiller, 1980; Figure 17). One of the very few CSZ focal mechanisms, the solution was referred to in numerous studies of the CSZ and of eastern North American seismotectonics. The southeast steeply-dipping nodal plane ( $76^{\circ}$ ) was interpreted to be the fault plane, with a trend similar to the St. Lawrence paleorift faults.

Due to its seismotectonic importance, this focal mechanism was recomputed using the program FOCMEC. Due to the loss of the original data set, first motion data were assembled from the GSC analogue and digital playouts, including paper playouts of the Charlevoix Local Network. In addition, first motions were obtained from the ISC Bulletin for regional and teleseismic phases and from the original photocopies of seismograms and notes for northeast U.S. stations. A total of 45 P-first motions were gathered, a little more than the 39 used in Hasegawa and Wetmiller (1980).

Compared with today's convention for a lower hemisphere projection, some $P$ first motions were not plotted in the same positions in Hasegawa and Wetmiller (1980). In that paper, the azimuth of the $P$ phase was not reversed for a station located between $1^{\circ}$ and $2^{\circ}$ epicentral distance (i.e. between about 110 and 220 km ). With today's convention, the first motion positions are reversed, i.e. assumed to be upper focal sphere, up to about 166 km epicentral distance, assuming a focal depth of 10 km and a velocity model described in the section 1 . This convention changed the first motion positions for stations CHQ, QCQ and CBM. In some cases, it is possible to tell if the first arrival is a Pg or a Pn . At distances between 135 and 166 km , the Pg should be emergent, whereas the Pn should be impulsive. Since CHV and QCQ are analogue stations with high microseisms, we cannot tell if the first motion is Pn or Pg by looking at the amplitude of the first arrival. Nodal planes computed without the CHQ, QCQ and CBM first motions were not very different than the ones obtained with them.

With FOCMEC, a $1^{\circ}$ search gave 32 solutions (Figure 18). Ten first motions out of forty-five are misfits to the solution (stations: CBM, JKM, BNH, MSNY, SCH, ECM, MRG, AAM, BLA and

BNG; see Appendix 3 for solution details). The solution depends strongly on the northeastern U.S. data plotted in the southwestern quadrant and on the James Bay stations PBQ (C), LBQ (D) and LGQ (D).

Although both the original and the new solution show predominantly reverse faulting, the positions of the nodal planes are somewhat different. The new solution shows one plane steeply dipping to the west and one plane more shallowly dipping towards the southeast.
c) Other published mechanisms.

Our versions of the following mechanisms can be found in Appendix 1.
i) By the Geological Survey of Canada.

While most magnitude $>=3.0$ earthquake mechanisms are new, a few however, had already been calculated by J. Adams, W. McNeil or R.J. Wetmiller of the GSC. The figures that were published in the Canadian Earthquake Summaries are given in Appendix 4. Some of our mechanisms are similar to the ones previously calculated ( $890309 ; 890311 ; 900311 ; 900313$ ) while others are significantly different (900421; 900423; 901026; 901106 all quality "C" or "X" in our study). The previously computed ones relied on P first motions (including at times, emergent first motions at regional distances) and on $\mathrm{P} / \mathrm{Sv}$ ratios. As the earthquakes become smaller in magnitude, picking emergent $P$ first motions can cause spurious solutions.
ii) By Li, Doll and Toksöz (1995).

The paper by Li, Doll and Toksöz (1995) presents four different focal mechanisms (901021; 920310; 9890309; and 9890311; Figure 19). These mechanisms were computed using P and SH first motions. In these solutions, the plotting of the first motions for stations within 150 km was wrong. For direct $P$ and $S$ phases, the azimuths were not reversed, which imply that the mechanisms are questionable especially for the 901021 and 920310 solutions that depend heavily on the CLTN data. Our solutions for the same events can be found in Appendix 1. It appears that some SH first motions were read quite liberally by Li et al. (1995), which may explain the differences seen in the resulting mechanisms.
iii) Lamontagne and Ranalli (1997)

For a sub-zone near station A61, Lamontagne and Ranalli (1997) published three focal mechanisms for three small events (magnitude 2.6: 891208; 1.9: 910703 and 2.6: 930330). While the general tectonic style is well defined, the nodal planes are moderately constrained. The solutions are shown in Figure 20 and described in Appendix 5.

4- Conclusions.
With the current CSZ seismograph network, earthquake focal mechanisms can be computed for
events as small as magnitude $\mathrm{m}_{\mathrm{N}}$ 3.0. This can be done by adding constraints with SH first motions. Approximately $50 \%$ of the mechanisms in that magnitude range can be considered reliable. The 8 additional seismograph stations of the 1996 summer field survey added much needed P and SH first motions. They allowed the calculation of focal mechanisms for events as small as magnitude $m_{N} 2.0$. With the recalculation of some previously published mechanisms, we are able to update the previously published ones shown in Figure 21 by discarding some poorly defined solutions. In addition, we are now able to propose a series of 20 well defined mechanisms for the CSZ (Figure 22). In this paper, we have developed a methodology that can be applied to future earthquakes in Charlevoix. The forthcoming study will invert the stress system from the new and old focal mechanisms.

## 5- Recommendations.

More than 30 years of earthquake recording in Charlevoix has produced a fair number of focal mechanisms. It is possible to compute focal mechanisms for earthquakes as small as magnitude 3.0. These solutions, however, are strongly dependent on the correctness of every first motion reading. In order to make the solutions more robust, the number of stations within 100 km of the seismic zone should be increased especially in the NE and SW quadrants. The 1996 summer field survey showed that with about 6 additional stations, focal mechanisms can be computed for events as small as magnitude 2.0. Clearly, additional stations are needed to derive well defined focal mechanisms from which seismo-tectonic conclusions can be drawn.

The use of $\mathrm{Sv} / \mathrm{P}$ ratios should be studied in more detail. We have a series of focal mechanisms computed with $\mathrm{Sv} / \mathrm{P}$ ratios. Although they can theoretically be used, the robustness of $\mathrm{Sv} / \mathrm{P}$ ratios have never been demonstrated. From this study, some focal mechanisms well constrained with $P$ first motions only could be used for this purpose.

For events below magnitude 4.0, P first motions readings from stations at regional distances are difficult to read due to their emerging character. In addition, the velocity models between the CSZ and these stations is at best approximate. A better defined velocity model is necessary to obtain reliable mechanisms and should be defined by other studies.

## Acknowledgments.

Epicentral maps were prepared with the public domain GIS software Xmap8 written by J.M. Lees. The author thanks Reynald Du Berger of the UQAC (Université du Québec à Chicoutimi) for reading many first motions on the station CIQ and the two GSC reviewers of the Open File, R.J. Wetmiller and J.A. Drysdale.

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Table 1: Focal mechanisms of earthquakes of magnitude 3.0 and larger.

| Q Date Time yymmdd hhmm ss | Latitude ( N ) | Long. (oW) | $\begin{aligned} & \text { Dept } \\ & (\mathrm{km}) \end{aligned}$ | th Mag | Sta/Pha | References: |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A 890131143948.20 | 47.4426 | -70.6710 | 19.69 | $3.1 \mathrm{~m}_{\mathrm{N}}$ | 7/012 |  |
| X 890309094132.26 | 47.7171 | -69.8569 | 10.52 | 4.3 mN | 6/011 | 123 |
| X 890311083152.16 | 47.7182 | -69.8699 | 10.41 | 4.4 mN | 7/012 | 123 |
| B 891013140442.80 | 47.3926 | -70.1330 | 22.74 | 3.2 mN | 6/012 |  |
| A 891122230251.72 | 47.4559 | -70.3420 | 7.39 | 3.4 mN | 7/014 |  |
| A 900303020603.38 | 47.8559 | -69.9765 | 20.85 | 3.6 mN | 8/015 | 4 |
| A 900313191039.34 | 47.5338 | -70.1366 | 15.38 | 3.2 mN | 7/014 | 4 |
| C 900421012304.12 | 47.5532 | -70.0698 | 9.56 | 3.1 mN | 7/014 | 5 |
| X 900423002804.78 | 47.4143 | -70.1787 | 8.04 | 3.0 mN | 7/014 |  |
| A 901021133843.20 | 47.3975 | -70.3644 | 15.85 | 3.3 mN | 7/013 | 5 |
| X 901026091351.51 | 47.5692 | -69.9848 | 10.96 | 3.1 mN | 6/012 |  |
| X 901106113010.76 | 47.3943 | -70.1506 | 14.19 | 3.4 mN | 6/011 | 6 |
| X 901218071046.23 | 47.2627 | -70.3359 | 9.38 | 3.3 mN | 7/013 | 6 |
| 0910703092642.32 | 47.5290 | -70.1464 | 18.44 | 3.0 mN | CLTN | a not saved. |
| C 911208030030.12 | 47.7792 | -69.8643 | 23.05 | 4.3 mN | 7/013 |  |
| X 920310054532.64 | 47.7167 | -69.8574 | 9.96 | 3.3 mN | 7/013 | 3 |
| X 920501003751.49 | 47.4463 | -70.4069 | 2.67 | 3.2 mN | 6/011 |  |
| A 930304220221.84 | 47.5145 | -70.3621 | 4.39 | 3.1 mN | 6/011 |  |
| X 930807212531.92 | 47.6681 | -69.8893 | 7.75 | 3.1 mN | 7/014 |  |
| $0 \quad 931201124715.89$ | 47.4671 | -70.1584 | 18.0 g | 3.5 mN | No CLT | data. |
| X 931230230147.69 | 47.4532 | -70.3609 | 5.94 | 3.8 mN | 6/012 |  |
| A 940925005329.46 | 47.7518 | -69.9612 | 12.18 | 4.3 mN | 6/012 |  |
| B 941201130247.14 | 47.4374 | -70.3138 | 10.77 | 3.0 mN | 5/009 |  |
| C 960512115321.91 | 47.5161 | -70.0281 | 14.82 | 3.1 mN | 7/014 |  |
| X 960607094142.83 | 47.5299 | -69.9417 | 13.32 | 3.1 mN | 7/014 |  |
| A 970110192727.56 | 47.5094 | -70.1965 | 17.06 | 3.2 mN | 7/014 |  |
| X 970114044732.39 | 47.6574 | -69.8765 | 14.96 | 3.1 mN | 7/014 |  |
| 1- Drysdale et al. (1989); |  |  |  |  |  |  |
| 2- Wetmiller and Adams (1990). |  |  |  |  |  |  |
| 3- Li et al. (1995). |  |  |  |  |  |  |
| 4- Drysdale et al. (1990); |  |  |  |  |  |  |
| 5- Drysdale et al. (1991a). |  |  |  |  |  |  |
| 6- Drysdale et al. (1991b). |  |  |  |  |  |  |

Q: Quality.
A: Very good
B: Good
C: Fair
X: Rejected
0: Cannot be computed.
Total: $8 \mathrm{~A} ; 2 \mathrm{~B} ; 3 \mathrm{C} ; 12 \mathrm{X} ; 2 \mathrm{O}$

Table 2: Focal mechanisms of earthquakes recorded during the 1996 summer field survey.
$\left.\begin{array}{lccccccc}\text { Q } & \begin{array}{c}\text { Date } \\ \text { yymmdd hhmm ss }\end{array} & \begin{array}{c}\text { Latitude } \\ (\circ \mathrm{N})\end{array} & \begin{array}{c}\text { Longitude } \\ (\circ \mathrm{W})\end{array} & \begin{array}{c}\text { Depth } \\ (\mathrm{km})\end{array} & \text { Mag } & \text { Sta/Pha } \\ \text { A } & 960617 & 1118 & 30.66 & 47.5328 & -70.1463 & 14.11 & 1.9 \mathrm{mN}\end{array}\right) 8 / 016$

Q: Quality.
A: Very good
B: Good
C: Fair
X: Rejected 0 : Cannot be computed.

Total: 7 A; 1 B; 4 C; 3 X.

## Figures.

Figure 1: Location map of the Charlevoix Seismic Zone. The earthquakes shown are the ones of the seismicity map of Canada (Anglin et al., 1990).

Figure 2A: Time-history of the Charlevoix network for the period 1970-1997. Acronyms used: field exp.: field experiments of Leblanc et al. (1973) and Leblanc and Buchbinder (1977); 2) CLTN: Charlevoix Local Telemetered Network; 3) CNSN: Canadian National Seismograph Network; 4) sp: short period; 5) bb: broad-band; 6) CHX network: Charlevoix Short-Period Local Network ( 6 stations + A56).

Figure 2B: Seismograph Network of Charlevoix. Stations LPQ and POC are not currently operational.

Figure 2C: Seismograph stations surrounding Charlevoix.
Figure 2D: Seismograph stations used during the June-November 1996 field survey. The white triangles are the digital seismograph sites, while pasq and rsfq are two analogue recorder stations.

Figure 3. Polarity check for the South American earthquake of March 25, 1997 at 16 UT. The figure shows P arrivals on the vertical components (left window), and the corresponding radial motion of the P wave for CLTN stations only (right window).

Figure 4. Location map of the 960924 23:40 U.T. earthquake and the 1996 summer seismograph stations. Station A80P is located almost exactly west of the epicentre.

Figure 5. Horizontal seismic traces recorded at site A80 with similar Y scales (N-S, upper ; E-W lower).

Figure 6. Corresponding particle motions of the seismic traces.
Figure 7. Rotated traces of the horizontal seismic traces with similar Y scales (radial: upper; transverse: lower). Note that the maximum amplitude on the radial corresponds to a very small amplitude on the transverse.

Figure 8. Similar to Figure 5 for station A76P.
Figure 9. Similar to Figure 6 for station A76P.
Figure 10. Similar to Figure 7 for station A76P.
Figure 11. Theoretical P and SH first motions for a strike-slip mechanism on a north-south fault plane.

Figure 12. Example of an output for a focal mechanism computed with P and SH first motions. The first two pages are the text.

Figure 12A: Focal mechanisms.
Figure 12B: First motion picks.
Figure 12C: Epicentral map.
Figure 13. Location map of the 10 quality $A$ and $B$ focal mechanisms for events of magnitude $>=3.0$.

Figure 14. Location map of the 8 quality A and B focal mechanisms for summer 1996 events.
Figure 15. Focal mechanisms for the 1974 field survey and for the $1979 \mathrm{~m}_{\mathrm{N}} 5.0$ earthquake (published in Lamontagne (1987).

Figure 16A: The two well constrained focal mechanisms for the 1974 field survey ( $5^{\circ} \mathrm{b}$-axis search).

Figure 16B: The four poorly constrained mechanisms for the 1974 field survey ( $5^{\circ}$ b-axis search).

Figure 17. The focal mechanism of the $\mathrm{m}_{\mathrm{N}} 1979$ earthquake as published in Hasegawa and Wetmiller (1980).

Figure 18. The new focal mechanism for the $\mathrm{m}_{\mathrm{N}} 5.01979$ earthquake.
Figure 19. Focal mechanisms of Li et al. (1995).
Figure 20. Focal mechanisms published in Lamontagne and Ranalli (1997).
Figure 21. Modified figure of Lamontagne and Ranalli (1997). Poorly constrained mechanisms of 1974 are crossed while the two acceptable ones are checked. Events 890309 and 890311 were found to have one poorly constrained nodal plane and were rated as "X". For the $1979 \mathrm{~m}_{\mathrm{N}} 5.0$ event, the two nodal planes found in this study are shown on the previous solution. The other mechanisms are not part of this report.

Figure 22. Quality " A " and " B " solutions found in this study.


[^0]

Figure 2,7


Figure 2B


Figure 2C


Figure 2D


960924 23:40 U.T.


Figure 4


$29$






## Figure 12. Text

Earthquake of 199609242341 Magnitude 3.1MN

1- Earthquake information and list of first motions.


COMMENTS:

Felt, CHARLEVOIX SEISMIC ZONE, QUE.
Felt in St-Irenee, St-Hilarion, La Malbaie, and Clermont.
\$ Felt info from local radio station.
$\$$ CIQ FM from R. Du Berger, Chicoutimi.
$\$$ QCQ FM is unclear.
\$
\$ The Sg lines of some stations include the SH FM.
\$ The convention used is the Virginia Tech convention used in FOCMEC:
\$ <: SH first motion to left (back to event) impulsive
\$ >: SH first motion to right (back to event) impulsive
\$ Preliminary Focmec computed by ML.
\$ SH FM not picked on: A11 and A21.

| Sta | Fha | Dist <br> $(k m)$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | ---: | :---: | :---: |
| A58P | PG | 3 | 139 | -14 | C |
| A58P | SG | 3 | 139 | -14 | < |
| LMQ | PG | 6 | 271 | -26 | C |
| LIQ | SG | 6 | 271 | -26 | $>$ |
| A84P | PG | 9 | 211 | -34 | C |
| A84P | SG | 9 | 211 | -34 | $>$ |
| A76P | PG | 11 | 0 | -40 | C |
| A76P | SG | 11 | 0 | -40 | $>$ |
| GHQ | PG | 14 | 298 | -46 | C |
| A54 | PG | 16 | 232 | -52 | C |
| A54 | SG | 16 | 232 | -52 | $>$ |
| A16 | PG | 20 | 116 | -57 | D |
| A16 | SG | 20 | 116 | -57 | $<$ |
| A61 | PG | 20 | 35 | -57 | C |
| A61 | SG | 20 | 35 | -57 | $<$ |
| A80P | PG | 21 | 275 | -59 | C |
| A80P | SG | 21 | 275 | -59 | $>$ |
| A11 | PG | 34 | 174 | -69 | D |
| RSFQ | PG | 36 | 223 | -70 | D |
| A64 | PG | 41 | 40 | -72 | D |
| A64 | SG | 41 | 40 | -72 | $<$ |
| A21 | PG | 45 | 67 | -74 | C |
| DAD | PG | 88 | 302 | -82 | D |
| LIQ | PG | 90 | 333 | -82 | D |
| SLD | PG | 94 | 81 | -82 | D |

## Figure 12: text

Number of P first motions: 16
Number of SH first motions: 9

2- Most Representative Solution.

A total of 100 solutions were found using ab axis increment of 1 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

| dip, strike, rake | 67.37 | 246.26 | 79.16 |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| dip, strike, rake | 24.97 | 92.73 | 114.29 | : auxiliary plane |  |
| lower hem. trend, plunge of $a, n$ | 2.73 | 65.03 | 156.26 | 22.63 |  |
| lower hem. trend \& plunge of b | 250.48 | 10.00 |  |  |  |
| lower hem. trend, plunge of $p, t$ | 344.49 | 21.65 | 137.22 | 65.94 |  |

Average $B, P$, and $T$ axes:

|  | B | P | T |  |
| :--- | ---: | ---: | ---: | ---: |
| Mean trend: |  |  |  |  |
| Mean Plunge: | 250 | N | 343 | N |
| Vector Magnitude: |  | 7 | 20 | 69 |
| Mean length of resulting vector: | 100 | 100 | 100 |  |

3- Misfits.

All 16 P first motions agreed with the solution. Out of 9 SH first motions, a total of 2 did not fit the solutions (22/100).

| Station | Number |  |
| :---: | :---: | :---: |
| Name | of misfits | Percentage |
| of wrongs |  |  |

4- Rating of the focal mechanism.

The solution has an $A$ rating based on the small number of $P$ and $S H$ misfits ( $0 / 100$ and $22 / 100$ respectively) and on the good constraints on the P , T and B axes (value of 0.996 ).

Figure 12 A


Figure 12 B



Figure 12C

## Location Map



$$
\text { Figure } 13
$$

Focal Mechanisms M3+ Qual: AB


Figure 14

1996 Field Survey Q: A B



Fig. . P-wave nodal solution of micro-earthquakes from the 1974 survey (Leblanc and Buchbinder 1977) and of the August 19, 1979, earthquake (Hasegawa and Wetmiller 1980). Open dot and plus sign denote dilatational and compressional first motion, respectively. The maximum compressive stress axis $(P)$ and the maximum tensile stress ( $T$ ) are also indicated. The centre of the focal sphere is represented by $\times$. The dagrams are equal-area projections of the lower hemisphere. Modified from Leblanc and Buchbinder (1977) and Hasegawa and Wetmiller (1980).
From Lamontagne (1987)

Figure 15


74/06/23
Figure 16A


740620


740702


740630


740714

Figure 16 B


Ficure 7


$$
\text { Figure } 18
$$




Figure 19


- Figure Focal mechanisms computed using first motion data ( $C, D$ ) and transverse $S H$ polarities (,+- ). Possible variations in the nodal planes are shown as grey lines. Note the normal faulting mechanism of event 930330. Event 891208 is part of Triplet A. From Lamontagne and Ranalli (1997)

$$
\text { Figure } 20
$$



- Figure . Lower hemisphere focal mechanism solutions of the CSZ. Regions with compressional first motions are shaded. The maximum and minimum pressure axes are shown as $P$ and $T$, respectively. The dates of the events and the magnitudes ( $M$ ) of the two largest events are given. Mechanisms are from: (a) Bent, 1992; (b) Hasegawa and Wetmiller, 1980; (c) Lamontagne, 1987; (e) and ( f : Wetmiller and Adams, 1990; ( g ), ( h ), ( i ), ( j ), ( l$)$, ( m ): in Leblanc and Buchbinder, 1977; ( k ) and ( n ) in Adams et al., 1988; (d), and Figure 21 (0) in Adams et al., 1989.

Figure 22

Focal Mec Qual A B


Appendix 1: Focal mechanisms of earthquakes of magnitude 3.0 and larger.
Q Date Time Latitude Long. Depth Mag Sta/Pha References: yymmdd hhmm ss ( ${ }^{\circ} \mathrm{N}$ ) ( OW ) (km)

|  | 890131143948.20 | 47.4426 | -70.6710 | 19.69 | 3.1 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| X | 890309094132.26 | 47.7171 | -69.8569 | 10.52 | 4.3 mN | 6/011 | 123 |
| X | 890311083152.16 | 47.7182 | -69.8699 | 10.41 | 4.4 mN | 7/012 | 123 |
| B | 891013140442.80 | 47.3926 | -70.1330 | 22.74 | 3.2 mN | 6/012 |  |
| A | 891122230251.72 | 47.4559 | -70.3420 | 7.39 | 3.4 mN | 7/014 |  |
| A | 900303020603.38 | 47.8559 | -69.9765 | 20.85 | 3.6 mN | 8/015 | 4 |
| A | 900313191039.34 | 47.5338 | -70.1366 | 15.38 | 3.2 mN | 7/014 | 4 |
| C | 900421012304.12 | 47.5532 | -70.0698 | 9.56 | 3.1 mN | 7/014 | 5 |
| X | 900423002804.78 | 47.4143 | -70.1787 | 8.04 | 3.0 mN | 7/014 |  |
| A | 901021133843.20 | 47.3975 | -70.3644 | 15.85 | 3.3 mN | 7/013 | 5 |
| X | 901026091351.51 | 47.5692 | -69.9848 | 10.96 | 3.1 mN | 6/012 |  |
| X | 901106113010.76 | 47.3943 | -70.1506 | 14.19 | 3.4 mN | 6/011 | 6 |
| X | 901218071046.23 | 47.2627 | -70.3359 | 9.38 | 3.3 mN | 7/013 | 6 |
| 0 | 910703092642.32 | 47.5290 | -70.1464 | 18.44 | 3.0 mN | CLTN | saved. |
| C | 911208030030.12 | 47.7792 | -69.8643 | 23.05 | 4.3 mN | 7/013 |  |
| X | 920310054532.64 | 47.7167 | -69.8574 | 9.96 | 3.3 mN | 7/013 | 3 |
| X | 920501003751.49 | 47.4463 | -70.4069 | 2.67 | 3.2 mN | 6/011 |  |
| A | 930304220221.84 | 47.5145 | -70.3621 | 4.39 | 3.1 mN | 6/011 |  |
| X | 930807212531.92 | 47.6681 | -69.8893 | 7.75 | 3.1 mN | 7/014 |  |
| 0 | 931201124715.89 | 47.4671 | -70.1584 | 18.0 g | 3.5 mN | No CLT |  |
| X | 931230230147.69 | 47.4532 | -70.3609 | 5.94 | 3.8 mN | 6/012 |  |
| A | 940925005329.46 | 47.7518 | -69.9612 | 12.18 | 4.3 mN | 6/012 |  |
| B | 941201130247.14 | 47.4374 | -70.3138 | 10.77 | 3.0 mN | 5/009 |  |
| C | 960512115321.91 | 47.5161 | -70.0281 | 14.82 | 3.1 mN | 7/014 |  |
| X | 960607094142.83 | 47.5299 | -69.9417 | 13.32 | 3.1 mN | 7/014 |  |
| A | 970110192727.56 | 47.5094 | -70.1965 | 17.06 | 3.2 mN | 7/014 |  |
| X | 970114044732.39 | 47.6574 | -69.8765 | 14.96 | 3.1 mN | 7/014 |  |
| 1- Drysdale et al. (1989); |  |  |  |  |  |  |  |
| 2- Wetmiller and Adams (1990). |  |  |  |  |  |  |  |
| $3-\mathrm{Li}$ et al. (1995). |  |  |  |  |  |  |  |
| 4- Drysdale et al. (1990); |  |  |  |  |  |  |  |
| 5 - Drysdale et al. (1991a). |  |  |  |  |  |  |  |
| 6- Drysdale et al. (1991b). |  |  |  |  |  |  |  |

Q : Quality.
A: Very good
B: Good
C: Fair
X: Rejected
0 : Cannot be computed.
Total: 8 A; 2 B; 3 C; $12 \mathrm{X} ; 2$ O

Earthquake of 198901311439 Magnitude 3.1MN

1- Earthquake information and list of first motions.

| Date | Time <br> hhmm | Ss | Latitude | Longitude | Depth <br> (km) | Mag | Sta/Pha |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 890131 | 1439 | 48.20 | 47.4426 | -70.6710 | 19.69 | 3.1MN | 7/012 |

COMMENTS:
CHARLEVOIX, QUEBEC; FELT IN SAINT-HILARION, BAIE-SAINT-PAUL LES EBOULEMENTS AND LA MALBAIE
\$
\$ The Sg lines of some stations include the SH FM.
\$ The convention used is the Virginia Tech convention used in FOCMEC:
\$ <: SH first motion to left (back to event) impulsive
\$ >: SH first motion to right (back to event) impulsive
\$ Preliminary Focmec computed by ML.

| Sta | Pha | Dist <br> $(k m)$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | ---: | :---: | ---: |
| A54 | PG | 20 | 85 | -45 | C |
| LMQ | PG | 28 | 66 | -55 | D |
| A11 | PG | 42 | 122 | -65 | D |
| A11 | SG | 42 | 122 | -65 | $>$ |
| A16 | PG | 50 | 86 | -69 | D |
| LPQ | PG | 51 | 102 | -69 | D |
| A61 | PG | 52 | 57 | -69 | D |
| A61 | SG | 52 | 57 | -69 | < |
| DAQ | PG | 72 | 324 | -75 | D |
| A64 | PG | 72 | 54 | -75 | D |
| A21 | PG | 79 | 68 | -76 | D |
| A21 | SG | 79 | 68 | -76 | > |
| CQ22 | PG | 92 | 333 | -78 | D |
| CQ8 | PG | 99 | 333 | -79 | D |
| SLQ | PG | 128 | 78 | -81 | D |
|  |  |  |  |  |  |
|  | Number of | P | first motions: | 12 |  |
|  | Number of | SH first motions: | 3 |  |  |

2- Most Representative Solution.
A total of 65 solutions were found using a b axis increment of 1 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

| dip,strike, rake | 42.47 | 152.63 | 79.60 |  |
| :--- | :--- | :--- | :--- | :--- |
| dip,strike, rake | 48.38 | 346.60 | 99.38 | :auxiliary plane |


| lower hem. trend, plunge of $a, n$ | 256.60 | 41.62 | 62.63 | 47.53 |
| :--- | :--- | :---: | :---: | :---: | :---: |
| lower hem. trend \& plunge of $b$ | 160.34 | 7.00 |  |  |
| lower hem. trend, plunge of $p, t$ | 69.97 | 2.98 | 317.07 | 82.39 |

Average $B, P$, and $T$ axes:

| Mean trend: | N | 159 | N | 249 |
| :--- | :---: | :---: | :---: | :---: |
| Mean Plunge: | 10 | 1 | N | 343 |
| Vector Magnitude: | 65 | 65 | 80 |  |
| Mean length of resulting vector: | 0.999 | 0.999 | 65 |  |
| 3- Misfits. |  |  | 0.999 |  |

All 12 P first motions agreed with the solution.
All 3 SH first motions agreed with the solution.
4- Rating of the focal mechanism.
The solution has an $A$ rating based on the small number of $P$ and $S H$ misfits ( $0 / 100$ and $0 / 100$ respectively) and on the good constraints on the $P$, $T$ and $B$ axes (value of 0.999).


$55$

## Location Map



Earthquake of 198903090941 Magnitude 4.25 MN

1- Earthquake information and list of first motions.

| DateTime <br> hhmm ss | Latitude | Longitude | Depth <br> $(\mathrm{km})$ | Mag | Sta/Pha |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 890309 | 0941 | 32.26 | 47.7171 | -69.8569 | 10.52 | 4.25 MN |

COMMENTS:

CHARLEVOIX-KAMOURASKA, QUE.; FELT IN LA MALBAIE (IV) AND BAIE-SAINT-PAUL. ALSO FELT ON THE SOUTH SHORE IN RIVIERE-OUELLE AND KAMOURASKA. MAG (EDR) 3.9 MB (1 OBS)
\$ TRQ,GRQ,WBO,CKO DOWN, MNQ SPIKY
\$ LPQ DEAD AT START ? A2l dead.
\$ CLTN CLOCK CORRECT ?
\$FOCAL MECHANISM PUBLISHED IN
\$WETMILLER AND ADAMS (1990): "AN EARTHQUAKE DOUBLET IN THE CHARLEVOIX
\$SEISMIC ZONE" IN CURRENT RESEARCH, PART B, GSC, PAPER 90-1, P. 105-I13.
\$ADDITIONAL FIRST MOTIONS USED:
\$HTQ SZ PN XCO942 03.07 E L
\$GSQ SZ PN XB0942 09.04 + L
\$MNQ SZ PN XA0942 17.79 C L
\$SIC SZ PN XB0942 20.30 + L
\$GGN SZ PN XB0942 24.12 - L
\$GAC SZ PN XB0942 38.46-L
\$HAL SZ PN XB0942 51.20 + L
\$GBN SZ PN XB0943 02.00 - L
\$EEO SZ PN XB0943 03.44 C L
\$JAQ SZ PN XA0943 14.10 D L
\$SCH SZ PN XA0943 17.20-L
\$KAO SZ PN XB0943 31.50 - L
\$GTO SZ PN XC0944 12.50 E L
$\$$ RATIO $=1.432 \mathrm{LPQ} 414023 \mathrm{C} 0.17 \quad 2228.83 \quad 7823.174145520 .12 \quad 60224.83$
$\$ \operatorname{RATIO}=1.399$ DAQ 424955D 0.13 $-3308.12 \quad 3308.1242 \quad 298 \quad 0.13 \quad 82963.88$
\$RATIO $=0.746$ A11 414196D 0.16 $\quad-7989.04 \quad 12426.964148910 .20 \quad 44554.96$
$\begin{array}{lllllllllll} \\ \$ R A T I O & =1.893 & \text { A16 } 413742 \mathrm{C} & 0.13 & 2876.80 & 37068.80 & 414100 & 0.12 & 224972.80\end{array}$
$\$$ RATIO $=1.265$ A54 414050D 0.17 -17228.71 $25107.294146860 .13 \quad 317100.72$
$\$ R A T I O=0.059$ A61 413565D 0.14 $-572643.251102620 .754138130 .12 \quad 656156.75$
\$RATIO $=1.217$ A64 413491D 0.15 -45529.60 $64870.404136830 .10 \quad 751078.38$
\$
\$ The Sg lines of some stations include the SH FM.
\$ The convention used is the Virginia Tech convention used in FOCMEC:
\$ <: SH first motion to left (back to event) impulsive
\$ >: SH first motion to right (back to event) impulsive
\$ Preliminary Focmec also computed by ML.

| Sta | Pha | Dist <br> $(k m)$ | Azim | Take-off <br> Angle | FM |
| :---: | :---: | :---: | :---: | :---: | :---: |
| A64 | PG | 12 | 348 | -50 | D |


| A64 | SG | 12 | 348 | -50 | $>$ |
| :--- | ---: | ---: | ---: | ---: | ---: |
| A61 | PG | 18 | 261 | -59 | D |
| A61 | SG | 18 | 261 | -59 | $<$ |
| A16 | PG | 30 | 202 | -70 | C |
| A16 | SG | 30 | 202 | -70 | $<$ |
| LMQ | PG | 40 | 242 | -75 | D |
| LPQ | PG | 43 | 196 | -76 | C |
| A54 | PG | 51 | 236 | -78 | D |
| A54 | SG | 51 | 236 | -78 | $>$ |
| A11 | PG | 59 | 206 | -80 | D |
| SLQ | PG | 64 | 95 | -81 | D |
| DAQ | PG | 107 | 285 | -84 | D |
| EBN | PG | 125 | 102 | -85 | D |
| JOQ | PG | 129 | 307 | -85 | D |
| QCQ | PG | 150 | 226 | -86 | D |
| DPQ | PN | 250 | 244 | 49 | C |
| KLN | PN | 281 | 109 | 49 | D |

Number of $P$ first motions: 14
Number of $S H$ first motions: 4

2- Most Representative Solution.

A total of 910 solutions were found using a b axis increment of 2 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.


Average $B, P$, and $T$ axes:
B P T

| Mean trend: | N | 195 | N | 98 |
| :--- | :---: | :---: | :---: | :---: |
| Mean Plunge: | 14 | N | 311 |  |
| Vector Magnitude: | 871 | 24 | 60 |  |
| Mean length of resulting vector: | 0.957 | 892 | 889 |  |

3- Misfits.

All 14 p first motions agreed with the solution.
Out of 4 SH first motions, a total of 1 did not fit the solutions (25/100).

| StationNumber <br> Name of misfits | Percentage <br> of wrongs |  |
| :---: | :---: | :---: |
| A54 | 910 | 100 |

4- Rating of the focal mechanism.

The solution is rejected (rating $X$ ) based on the high number of $P$ and SH misfits ( $0 / 100$ and $25 / 100$ respectively) and the absence of constraints on the $P, T$ and $B$ axes (value of 0.971).



## Location Map



Earthquake of 198903110831 Magnitude 4.4MN

1- Earthquake information and list of first motions.

| Date | Time <br> hhmm ss | Latitude | Longitude | Depth <br> $(\mathrm{km})$ | Mag | Sta/Pha |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 890311 | 0831 | 52.16 | 47.7182 | -69.8699 | 10.41 | 4.4 MN |

COMMENTS:
CHARLEVOIX-KAMOURASKA, QUE. FELT
IN LA MALBAIE, BAIE-SAINT-PAUL, ON THE SOUTH SHORE
AND IN THE SAGUENAY REGION. CLOSE TO MAG. 4.3 EVENT
TWO DAYS EARLIER.
\$ EDR QUOTES GSC PRELIMINARY SOLUTION
\$A21 down.
\$
\$Additional Phases used by Wetmiller and Adams (1990):
\$GSQ SZ PN XB0832 28.27 C L
\$HTQ SZ PN XB0832 21.80 C L
\$GGN SZ PN XB0832 43.18 D L
\$TRQ SZ PN XA0832 45.82 C L
\$JAQ SZ PN XB0833 33.57 D L
\$YKA SZ PN XB0837 50.00 C L
\$SIC SZ PN XB0832 41.00-L
\$LMN SZ PN XB0832 51.06 - L
\$HAL SZ PN XB0833 11.00 - L
\$CKO SZ PN XB0833 10.68 + L
\$GBN SZ PN XB0833 21.90-L
\$KAO SZ PN XB0833 51.20-L
$\begin{array}{llllllllllll}\$ R A T I O= & 0.983 & \text { LPQ } 325964 C & 0.23 & 4885.50 & 12082.50 & 32 & 495 & 0.19 & 47005.50\end{array}$
$\$$ RATIO $=1.329$ DAQ $320886 \mathrm{D} 0.19 \quad-4371.84 \quad 5044.16 \quad 3222220.15 \quad 93252.16$
\$RATIO $=\begin{array}{llllllllllllll}0.842 & \text { All } & 320180 D & 0.18 & -5065.64 & 5889.64 & 32 & 877 & 0.22 & 35193.64\end{array}$
$\$ \mathrm{RATIO}=1.094$ A16 $325726 \mathrm{C} \quad 0.16 \quad 12168.37 \quad 36263.63 \quad 32 \quad 88 \quad 0.16 \quad 151256.38$
$\$$ RATIO $=1.235$ A54 320034D 0.16 -16321.58 $\quad 23358.42 \quad 32 \quad 670 \quad 0.10 \quad 280382.44$
\$RATIO $=0.150$ A61 $315548 \mathrm{D} 0.15-580846.44 \quad 893713.56315797 \quad 0.10 \quad 819985.56$
$\begin{array}{lllllllllllllll} \\ \$ R A T I O= & 1.211 & \text { A64 } & 315473 D & 0.15 & -88760.11 & 114887.89 & 315663 & 0.16 & 1442744.13\end{array}$
\$
\$ The Sg lines of some stations include the SH FM.
\$ The convention used is the Virginia Tech convention used in FOCMEC:
$\$<: S H$ first motion to left (back to event) impulsive \$ >: SH first motion to right (back to event) impulsive \$ Preliminary Focmec computed by ML.

| Sta | Pha | Dist <br> $(k m)$ | Azim | Take-off <br> Angle | FM |
| :--- | :---: | :---: | :---: | :---: | :---: |
| A64 | PG | 12 | 352 | -49 | D |
| A64 | SG | 12 | 352 | -49 | > |
| A61 | PG | 17 | 260 | -58 | D |
| A61 | SG | 17 | 260 | -58 | < |


| A16 | PG | 29 | 200 | -70 | C |
| :--- | ---: | ---: | ---: | ---: | ---: |
| A16 | SG | 29 | 200 | -70 | < |
| LMQ | PG | 39 | 241 | -75 | D |
| LPQ | PG | 43 | 194 | -76 | C |
| A54 | PG | 50 | 235 | -78 | D |
| A11 | PG | 58 | 205 | -80 | D |
| SLQ | PG | 65 | 95 | -81 | D |
| DAQ | PG | 106 | 285 | -84 | D |
| EBN | PG | 126 | 102 | -85 | D |
| JOQ | PG | 128 | 307 | -85 | D |
| QCQ | PG | 149 | 226 | -86 | D |
| DPQ | PN | 249 | 243 | 49 | C |
| KLN | PN | 282 | 109 | 49 | D |
| GRQ | PN | 471 | 257 | 49 | C |
| EEO | PN | 708 | 264 | 49 | C |

Number of $P$ first motions: 16 Number of SH first motions: 3

## 2- Most Representative Solution.

A total of 853 solutions were found using a b axis increment of 2 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

| dip, strike, rake | 72.05 | 14.75 | 85.79 |  |  |  |
| :--- | :--- | ---: | ---: | :--- | :--- | :--- |
| dip, strike, rake | 18.42 | 208.16 | 102.75 | : auxiliary plane |  |  |
| lower hem. trend, plunge of $\mathrm{a}, \mathrm{n}$ | 118.16 | 71.58 | 284.75 | 17.95 |  |  |
| lower hem. trend \& plunge of b | 16.04 | 4.00 |  |  |  |  |
| lower hem. trend, plunge of $\mathrm{p}, \mathrm{t}$ | 108.08 | 26.93 | 278.25 | 62.73 |  |  |

Average $B, P$, and $T$ axes:
B

| Mean trend: | N | 195 | N | 97 |
| :--- | :---: | :---: | :---: | :---: |
| Mean Plunge: | 15 | 26 | N | 309 |
| Vector Magnitude: | 816 | 837 | 58 |  |
| Mean length of resulting vector: | 0.957 | 0.981 | 835 |  |

```
3- Misfits.
```

All 16 p first motions agreed with the solution.
All 3 SH first motions agreed with the solution.
4- Rating of the focal mechanism.
The solution is rejected (rating $X$ ) based on the high number of $P$ and SH misfits ( $0 / 100$ and $0 / 100$ respectively) and the absence of constraints on the $P, T$ and $B$ axes (value of 0.972 ).



66

## Location Map



Earthquake of 198910131404 Magnitude 3.2MN

1- Earthquake information and list of first motions.

| Date | Time <br> hhmm ss | Latitude | Longitude | Depth <br> $(\mathrm{km})$ | Mag | Sta/Pha |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: |
| 891013 | 1404 | 42.80 | 47.3926 | -70.1330 | 22.74 | 3.2 MN |

COMMENTS:

CHARLEVOIX, QUEBEC; FELT ON THE NORTH SHORE
AT ST-HILARION, BAIE-SAINT-PAUL, LA MALBAIE, LES EBOULEMENTS.
$\$$ SLQ dead.
\$ Other first motions in original pikfile:
\$KLN SZ PN XA1405 24.13 E L
SGGN SZ PN XA1405 32.83 + L
\$TRQ SZ Trac Y1404 43.80 L
\$LMN SZ PN XA1405 42.68 + L
\$
\$ The Sg lines of some stations include the SH FM.
\$ The convention used is the Virginia Tech convention used in FOCMEC:
\$ <: SH first motion to left (back to event) impulsive
\$ >: SH first motion to right (back to event) impulsive
\$ Preliminary Focmec computed by ML.

| Sta | Pha | Dist <br> $(\mathrm{km})$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | ---: | :---: | :---: |
| LPQ | PG | 11 | 122 | -26 | C |
| A16 | PG | 13 | 48 | -30 | C |
| A16 | SG | 13 | 48 | -30 | $<$ |
| A11 | PG | 17 | 196 | -37 | C |
| A54 | PG | 22 | 289 | -44 | D |
| A54 | SG | 22 | 289 | -44 | $<$ |
| LMQ | PG | 23 | 320 | -45 | D |
| A6I | PG | 34 | 6 | -56 | D |
| A61 | SG | 34 | 6 | -56 | $>$ |
| A21 | PG | 48 | 44 | -65 | C |
| A64 | PG | 52 | 20 | -66 | D |
| DAQ | PG | 105 | 308 | -78 | D |
| CIQ | PG | 110 | 334 | -78 | D |

Number of P first motions: 10 Number of SH first motions: 3

2- Most Representative Solution.
A total of 44 solutions were found using a b axis increment of 1 degree. The following parameters describe the most representative solution, which was derived

```
from the average B, P, and T axes listed below.
\begin{tabular}{lcccccc} 
dip, strike, rake & 44.12 & 195.00 & 68.18 & & & \\
dip, strike, rake & 49.73 & 44.15 & 109.83 & \multicolumn{4}{c}{ : auxiliary plane } \\
lower hem. trend, plunge of & a, n & 314.15 & 40.27 & 105.00 & 45.88 \\
lower hem. trend \& plunge of b & 211.03 & 15.00 & & \\
lower hem. trend, plunge of p,t & 120.26 & 2.90 & 19.59 & 74.71
\end{tabular}
```

Average B, $P$, and $T$ axes:
B P T

| Mean trend: | N | 215 | N |
| :--- | :---: | :---: | :---: |
| Mean Plunge: | 3124 | N | 31 |
| Vector Magnitude: | 43 | 2 | 59 |
| Mean length of resulting vector: | 0.983 | 44 | 43 |
|  |  | 0.999 | 0.983 |
| 3- Misfits. |  |  |  |

All 10 P first motions agreed with the solution.
All 3 SH first motions agreed with the solution.
4- Rating of the focal mechanism.
The solution has a $B$ rating based on the number of $P$ and $S H$ misfits
( $0 / 100$ and $0 / 100$ respectively) and on the constraints on the $P, T$ and
$B$ axes (value of 0.988).



## Location Map



Earthquake of 198911222302 Magnitude 3.4MN

1- Earthquake information and list of first motions.

| Date | Time <br> hhmm |  | Latitude | Longitude | Depth <br> (km) | Mag | Sta/Pha |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 891122 | 2302 | 51.72 | 47.4559 | -70.3420 | 7.39 | 3.4MN | 7/014 |

COMMENTS:

CHARLEVOIX-KAMOURASKA, QUE.; FELT (IV)
IN BAIE-ST-PAUL, LA MALBAIE, LES EBOULEMENTS, ST-IRENEE
FELT (III) IN ST-HILARION,
AND ON THE SOUTH SHORE AT ST-PASCAL, RIVIERE-OUELLE, KAMOURASKA.
\$ FELT INFO FROM LMQ OPERATOR AND EROM RADIO STATIONS.
\$
\$ The Sg lines of some stations include the SH FM.
\$ The convention used is the Virginia Tech convention used in FOCMEC:
\$ <: SH first motion to left (back to event) impulsive
\$ >: SH first motion to right (back to event) impulsive
\$ Preliminary Focmec computed by ML.

| Sta | Pha | Dist <br> $(k m)$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | ---: | ---: | ---: | ---: |
| A54 | PG | 5 | 271 | -36 | C |
| A54 | SG | 5 | 271 | -36 | $>$ |
| LMQ | PG | 10 | 6 | -54 | C |
| A16 | PG | 25 | 86 | -74 | D |
| A16 | SG | 25 | 86 | -74 | < |
| Al1 | PG | 26 | 155 | -74 | D |
| Al1 | SG | 26 | 155 | -74 | $>$ |
| LPQ | PG | 28 | 117 | -75 | D |
| A61 | PG | 32 | 36 | -77 | D |
| A61 | SG | 32 | 36 | -77 | $>$ |
| A64 | PG | 53 | 39 | -82 | D |
| A21 | PG | 56 | 60 | -82 | D |
| DAQ | PG | 88 | 310 | -85 | D |
| CIQ | PG | 97 | 340 | -86 | D |
| SLQ | PG | 103 | 76 | -86 | D |
| QCQ | PG | 103 | 224 | -86 | D |

Number of P first motions: 12
Number of SH first motions: 4

2- Most Representative Solution.
A total of 846 solutions were found using $a b$ axis increment of 1 degree. The following parameters describe the most representative solution, which was derived
from the average $B, P$, and $T$ axes listed below.

| dip, strike, rake | 60.13 | 230.77 | 84.23 |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| dip, strike, rake | 30.38 | 62.23 | 99.92 | : auxiliary plane |  |  |
| lower hem. trend, plunge of | a, n | 332.23 | 59.62 | 140.77 | 29.87 |  |
| lower hem. trend \& plunge of b | 233.65 | 5.00 |  |  |  |  |
| lower hem. trend, plunge of $\mathrm{p}, \mathrm{t}$ | 324.99 | 14.94 | 125.63 | 74.21 |  |  |

Average $B, P$, and $T$ axes:

|  | B |  | P |  | T |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mean trend: | N | 235 | N | 328 | N | 125 |
| Mean Plunge: |  | 7 |  | 19 |  | 69 |
| Vector Magnitude: |  | 844 |  | 842 |  | 842 |
| Mean length of resulting vector: |  | 0.997 |  | 0.995 |  | 0.996 |

All 12 P first motions agreed with the solution.
All 4 SH first motions agreed with the solution.

4- Rating of the focal mechanism.

The solution has an A rating based on the small number of $P$ and $S H$ misfits ( $0 / 100$ and $0 / 100$ respectively) and on the good constraints on the $P$, $T$ and $B$ axes (value of 0.996 ).




## Location Map



Lـــلـนـ 20.0 km

Earthquake of 199003030206 Magnitude 3.6MN

1- Earthquake information and list of first motions.

| Date | Time <br> hhmm Ss | Latitude | Longitude | Depth <br> $(\mathrm{km})$ | Mag | Sta/Pha |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: |
| 900303 | 0206 | 03.38 | 47.8559 | -69.9765 | 20.85 | 3.6 MN |

COMMENTS:

CHARLEVOIX, QUE.; AFTERSHOCK AT 02:09
FELT IN CHARLEVOIX FROM SAINT-SIMEON TO LES EBOULEMENTS
ALSO REPORTED FELT IN RIVIERE-DU-LOUP
\$ HTQ,MNQ,JAQ DOWN
\$ Focmec by W. McNeil and J. Adams in National Summary Jan. -March 1990.
\$TRQ SZ PN XA0206 56.77 D L
$\$$ The Sg lines of some stations include the SH $\mathrm{F} M$.
\$ The convention used is the Virginia Tech convention used in FOCMEC:
\$ <: SH first motion to left (back to event) impulsive
\$ >: SH first motion to right (back to event) impulsive
\$ Preliminary Focmec computed by ML

| Sta | Pha | Dist <br> $(\mathrm{km})$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | :---: | :---: | :---: |
| A64 | PG | 7 | 118 | -19 | C |
| A61 | PG | 20 | 205 | -44 | C |
| A61 | SG | 20 | 205 | -44 | $>$ |
| A21 | PG | 27 | 128 | -53 | D |
| A16 | PG | 43 | 183 | -64 | C |
| A16 | SG | 43 | 183 | -64 | > |
| LMQ | PG | 43 | 218 | -64 | C |
| A54 | PG | 55 | 217 | -69 | C |
| LPQ | PG | 57 | 182 | -70 | D |
| A11 | PG | 70 | 194 | -74 | D |
| SLQ | PG | 76 | 106 | -75 | D |
| CIQ | PG | 76 | 308 | -75 | D |
| DAQ | PG | 95 | 278 | -78 | D |
| EBN | PG | 138 | 108 | -81 | D |
| QCQ | PG | 155 | 220 | -82 | D |
| DPQ | PN | 249 | 239 | 49 | C |
|  |  |  |  |  |  |
|  | Number of | P first motions: | 14 |  |  |
|  | Number of | SH first motions: | 2 |  |  |

2- Most Representative Solution.
A total of 28 solutions were found using a b axis increment of 1 degree. The following parameters describe the most representative solution, which was derived

```
from the average B, P, and T axes listed below.
    dip,strike,rake 48.01 32.10 88.65
    dip,strike,rake 42.01 214.11 91.49 :auxiliary plane
    lower hem. trend, plunge of a,n 124.11 4, 47.99 302.10 41.99
    lower hem. trend & plunge of b 33.00 1.00
    lower hem. trend, plunge of p,t 
```

Average $B, P$, and $T$ axes:

|  | B |  | P |  | T |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mean trend: | N | 30 | N | 120 | N | 236 |
| Mean Plunge: |  | 2 |  | 1 |  | 88 |
| Vector Magnitude: |  | 28 |  | 28 |  | 28 |
| Mean length of resulting vector: |  | 0.999 |  | 0.999 |  | 0.999 |

```
3- Misfits.
```

All 14 p first motions agreed with the solution.
All 2 SH first motions agreed with the solution.
4- Rating of the focal mechanism.
The solution has an $A$ rating based on the small number of $P$ and $S H$ misfits
( $0 / 100$ and $0 / 100$ respectively) and on the good constraints on the $P, T$ and
$B$ axes (value of 0.999 ).


19900303 02:06 U.T.



## $P$ Phases on Vertical Components



## Location Map



Earthquake of 199003131910 Magnitude 3.2MN

1- Earthquake information and list of first motions.

| Date | Time <br> hhmm ss | Latitude | Longitude | Depth <br> $(\mathrm{km})$ | Mag | Sta/Pha |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: |
| 900313 | 1910 | 39.34 | 47.5338 | -70.1366 | 15.38 | 3.2 MN |

COMMENTS:

NEAR LA MALBAIE; FELT IN LA MALBAIE AND POINTE-AU-PIC
CHARLEVOIX, QUE.
FORESHOCK AT 18:47 (MAG 2.4)
\$ Focmec published by $W$. McNeil and J. Adams
\$ in the National Summary of January-March 1990.
\$ They used: A64 D.
\$
\$ The Sg lines of some stations include the SH FM.
\$ The convention used is the Virginia Tech convention used in FOCMEC:
\$ <: SH first motion to left (back to event) impulsive
\$ >: SH first motion to right (back to event) impulsive
\$ Preliminary Focmec computed by ML.

| Sta | Pha | Dist <br> $(k m)$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | ---: | ---: | ---: | ---: |
| A16 | PG | 12 | 126 | -38 | C |
| A16 | SG | 12 | 126 | -38 | < |
| LMQ | PG | 14 | 276 | -43 | D |
| A61 | PG | 18 | 11 | -50 | D |
| A61 | SG | 18 | 11 | -50 | $>$ |
| A54 | PG | 22 | 248 | -56 | D |
| A54 | SG | 22 | 248 | -56 | < |
| LPQ | PG | 23 | 156 | -57 | D |
| A11 | PG | 33 | 188 | -65 | D |
| A64 | PG | 37 | 29 | -68 | C |
| A64 | SG | 37 | 29 | -68 | > |
| A21 | PG | 39 | 60 | -68 | C |
| A21 | SG | 39 | 60 | -68 | $>$ |
| SLQ | PG | 86 | 80 | -80 | D |
| CIQ | PG | 96 | 330 | -81 | D |
| DAQ | PG | 96 | 300 | -81 | D |
| EBN | PG | 143 | 92 | -84 | D |

Number of P first motions: 12
Number of SH first motions: 5

2- Most Representative Solution.

A total of 100 solutions were found using ab axis increment of 1 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

| dip, strike, rake | 65.30 | 34.42 | 64.53 |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| dip, strike, rake | 34.90 | 263.16 | 133.08 | : auxiliary plane |  |  |
| lower hem. trend, plunge of $\mathrm{a}, \mathrm{n}$ | 173.16 | 55.10 | 304.42 | 24.70 |  |  |
| lower hem. trend \& plunge of b | 45.68 | 23.00 |  |  |  |  |
| lower hem. trend, plunge of $\mathrm{p}, \mathrm{t}$ | 142.92 | 16.53 | 265.43 | 61.10 |  |  |

Average $B, P$, and $T$ axes:
B P T

| Mean trend: | N | 50 | N | 145 |
| :--- | :---: | :---: | :---: | :---: |
| Mean Plunge: | 17 | 14 | N | 272 |
| Vector Magnitude: | 100 | 100 | 68 |  |
| Mean length of resulting vector: | 0.996 | 0.999 | 100 |  |

3- Misfits.
Out of 12 p first motions, one did not fit the solutions ( $8 / 100$ )

| Station | Number |
| :---: | :---: |
| Name of misfits of wrongs |  |


| A54 | 1 | 1 |
| :--- | ---: | ---: |
| A61 | 5 | 5 |
| LPQ | 10 | 10 |
| SEQ | 84 | 84 |

All 5 SH first motions agreed with the solution.
4- Rating of the focal mechanism.
The solution has an $A$ rating based on the small number of $P$ and $S H$ misfits ( $8 / 100$ and $0 / 100$ respectively) and on the good constraints on the $P, T$ and $B$ axes (value of 0.998 ).




## Location Map



Earthquake of 199004210123 Magnitude 3.1MN

1- Earthquake information and list of first motions.

| DateTime <br> hhmm Ss | Latitude | Longitude | Depth <br> $(\mathrm{km})$ | Mag | Sta/Pha |  |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: |
| 900421 | 0123 | 04.12 | 47.5532 | -70.0698 | 9.56 | 3.1 MN |

COMMENTS:

12 KM SE OF LA MALBAIE, CHARLEVOIX, QUE.
FELT AT ST-HILARION, LA MALBAIE
POINTE-AU-PIC, LES EBOULEMENTS.
\$ MECHANISM DONE BY $W$. MCNEIL. PHASES ADDED NOT CHECKED BY JD
\$Additional phases used by wayne Moneil:
\$DAQ SZ PG X0123 19.57 + I
\$DPQ SZ PN X0123 38.99 + L
\$KLN SZ PN X0123 45.63 + L
\$EBN SZ PG X0123 26.95 - L
\$QCQ SZ PG X0123 33.50 C L
\$
\$ The Sg lines of some stations include the SH FM.
\$ The convention used is the Virginia Tech convention used in FOCMEC:
\$ <: SH first motion to left (back to event) impulsive
\$ >: SH first motion to right (back to event) impulsive
\$ Preliminary Focmec computed by ML.

| Sta | Pha | Dist <br> $(k m)$ | Azim | Take-off <br> Angle | FM |
| :--- | :---: | :---: | :---: | :---: | :---: |
| A16 | PG | 10 | 153 | -47 | C |
| A16 | SG | 10 | 153 | -47 | < |
| A61 | PG | 16 | 354 | -58 | C |
| A61 | SG | 16 | 354 | -58 | $>$ |
| LMQ | PG | 19 | 268 | -64 | D |
| LPQ | PG | 24 | 169 | -68 | D |
| A54 | PG | 28 | 248 | -71 | D |
| A54 | SG | 28 | 248 | -71 | $>$ |
| A21 | PG | 33 | 60 | -74 | D |
| A64 | PG | 33 | 24 | -74 | D |
| A11 | PG | 36 | 196 | -75 | D |
| SLQ | PG | 81 | 81 | -83 | D |
|  |  |  |  |  |  |
|  | Number of | P first motions: | 9 |  |  |
|  | Number of | SH first motions: | 3 |  |  |

2- Most Representative Solution.
A total of 602 solutions were found using $a b$ axis increment of 2 degree. The
following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

| dip, strike, rake | 70.01 | 320.16 | 87.87 |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| dip, strike, rake | 20.10 | 146.37 | 95.83 | : auxiliary plane |  |  |
| lower hem. trend, plunge of $\mathrm{a}, \mathrm{n}$ | 56.37 | 69.90 | 230.16 | 19.99 |  |  |
| lower hem. trend \& plunge of $b$ | 320.89 | 2.00 |  |  |  |  |
| lower hem. trend, plunge of p,t | 51.82 | 24.98 | 226.61 | 64.93 |  |  |

Average $B, P$, and $T$ axes:

|  | B | P | T |  |
| :--- | :--- | :--- | :--- | ---: |
| Mean trend: | N | 147 | N | 54 |
| Mean Plunge: |  | 7 | N | 252 |
| Vector Magnitude: | 591 | 59 | 65 |  |
| Mean length of resulting vector: | 0.982 | 0.991 | 594 |  |
| 3- Misfits. |  |  | 0.987 |  |

All 9 p first motions agreed with the solution.
All 3 SH first motions agreed with the solution.
4- Rating of the focal mechanism.
The solution has a $C$ rating based on the high number of $P$ and $S H$ misfits ( $0 / 100$ and $0 / 100$ respectively) and on the poor constraints on the $P, T$ and $B$ axes (value of 0.987 ).




## Location Map



Earthquake of 199004230028 Magnitude 3.0MN

1- Earthquake information and list of first motions.

| Date | Time | Latitude | Longitude | Depth <br> hhmm ss |  | Mag |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |$\quad$ Sta/Pha

COMMENTS:

```
    24 KM E OF BAIE-SAINT-PAUL, CHARLEVOIX, QUE.
CHARLEVOIX-KAMOURASKA, QUEBEC.; FELT LOCALLY
AT L'ILE AUX COUDRES, SAINT-HILARION, LES EBOULEMENTS, SAINT-IRENEE,
BAIE-SAINT-PAUL. NOT FELT AT LA MALBAIE.
$ SLQ dead.
$
$ The Sg lines of some stations include the SH FM.
$ The convention used is the Virginia Tech convention used in FOCMEC:
$ <: SH first motion to left (back to event) impulsive
$ >: SH first motion to right (back to event) impulsive
$ Preliminary Focmec computed by ML.
```

| Sta | Pha | Dist <br> $(\mathrm{km})$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | ---: | :---: | :---: |
| A16 | PG | 14 | 64 | -61 | D |
| A16 | SG | 14 | 64 | -61 | < |
| LPQ | PG | 15 | 123 | -62 | D |
| A54 | PG | 18 | 285 | -66 | D |
| A54 | SG | 18 | 285 | -66 | > |
| LMQ | PG | 19 | 323 | -67 | D |
| A11 | PG | 19 | 184 | -67 | C |
| A61 | PG | 32 | 12 | -76 | C |
| A21 | PG | 49 | 49 | -81 | D |
| A64 | PG | 51 | 25 | -81 | C |
| DAQ | PG | 101 | 308 | -85 | D |
| CIQ | PG | 106 | 335 | -86 | D |

Number of P first motions: 10 Number of SH first motions: 2

2- Most Representative Solution.

A total of 382 solutions were found using a b axis increment of 2 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

| dip,strike, rake | 40.66 | 6.72 | 77.67 |  |
| :--- | ---: | ---: | ---: | ---: |
| dip,strike, rake | 50.47 | 202.79 | 100.40 | :auxiliary plane |


| lower hem. trend, plunge of $a, n$ | 112.79 | 39.53 | 276.72 | 49.34 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| lower hem. trend \& plunge of b | 16.13 | 8.00 |  |  |
| lower hem. trend, plunge of $\mathrm{p}, \mathrm{t}$ | 285.44 | 4.95 | 163.98 | 80.57 |

Average $B, P$, and $T$ axes:
B $\quad \mathrm{P}$

| Mean trend: | N | 10 | N | 99 |
| :--- | :---: | :---: | :---: | :---: |
| Mean Plunge: |  | 3 | N | 234 |
| Vector Magnitude: | 332 | 380 | 87 |  |
| Mean length of resulting vector: | 0.870 | 0.994 | 357 |  |

3- Misfits.

All 10 P first motions agreed with the solution.
All 2 SH first motions agreed with the solution.

4- Rating of the focal mechanism.
The solution is rejected (rating $X$ ) based on the high number of $P$ and SH misfits ( $0 / 100$ and $0 / 100$ respectively) and the absence of constraints on the $P, T$ and $B$ axes (value of 0.933 ).



## Location Map



Earthquake of 199010211338 Magnitude 3.3MN

1- Earthquake information and list of first motions.

| DateTime <br> hhmm ss | Latitude | Longitude | Depth <br> $(\mathrm{km})$ | Mag | Sta/Pha |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 901021 | 1338 | 43.20 | 47.3975 | -70.3644 | 15.85 | 3.3 MN |

COMMENTS:

CHARLEVOIX, QUE.; FELT AT BAIE-SAINT-PAUL
\$ LPQ; HTQ; GSQ; GRQ; CKO; EEO; down.
\$
\$ The Sg lines of some stations include the SH FM.
\$ The convention used is the Virginia Tech convention used in FOCMEC:
\$ <: SH first motion to left (back to event) impulsive
\$ >: SH first motion to right (back to event) impulsive
\$ Preliminary Focmec computed by ML.
\$JOQ SZ PG YY . C

| Sta | Pha | Dist <br> $(k m)$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | ---: | ---: | ---: | ---: |
| A54 | PG | 8 | 331 | -25 | D |
| A54 | SG | 8 | 331 | -25 | $>$ |
| LMQ | PG | 17 | 10 | -47 | C |
| A11 | PG | 21 | 144 | -53 | C |
| A16 | PG | 28 | 73 | -61 | C |
| A61 | PG | 39 | 32 | -68 | C |
| A61 | SG | 39 | 32 | -68 | < |
| A64 | PG | 59 | 36 | -75 | D |
| A64 | SG | 59 | 36 | -75 | > |
| A21 | PG | 61 | 56 | -76 | D |
| A21 | SG | 61 | 56 | -76 | C |
| DAQ | PG | 91 | 314 | -80 | D |
| CIQ | PG | 102 | 342 | -81 | D |
| SLQ | PG | 106 | 73 | -82 | D |

Number of P first motions: 10 Number of SH first motions: 4

2- Most Representative Solution.

A total of 434 solutions were found using a b axis increment of 1 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

```
dip,strike,rake 24.25 163.41 53.91
dip,strike,rake 70.62 22.05 104.86 :auxiliary plane
```

```
lower hem. trend, plunge of a,n 292.05 19.38 19, 73.41 65.75
lower hem. trend & plunge of b 197.02 14.00
lower hem. trend, plunge of p,t 
```

Average $B, P$, and $T$ axes:
B P T

| Mean trend: | N | 194 | $N$ | 96 |
| :--- | :---: | :---: | :---: | ---: |
| Mean Plunge: | 16 | 27 | N |  |
| Vector Magnitude: | 432 | 432 | 59 |  |
| Mean length of resulting vector: | 0.996 | 0.996 | 433 |  |

3- Misfits.

All 10 P first motions agreed with the solution.
Out of 4 SH first motions, a total of 1 did not fit the solutions (25/100).

| Station <br> NameNumber misfits | Percentage <br> of wrongs |  |
| :---: | :---: | :---: |
| A64 | 434 | 100 |

4- Rating of the focal mechanism.
The solution has an $A$ rating based on the small number of $P$ and sh misfits
( $0 / 100$ and $25 / 100$ respectively) and on the good constraints on the $P$, $T$ and $B$ axes (value of 0.996 ).


19901021 13:38 U.T.



## Location Map



Earthquake of 199010260913 Magnitude 3.1MN

1- Earthquake information and list of first motions.

| Date Time | Latitude | Longitude | Depth |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| hhmm ss |  | Mag | Sta/Pha |  |  |  |
| 9010260913 | 51.51 | 47.5692 | -69.9848 | 10.96 | 3.1 MN | $6 / 012$ |

COMMENTS:

CHARLEVOIX, QUE.; FELT AT SAINT-HILARION, LA MALBAIE
AND POINTE-AU-PIC.
\$ Focmec published by W. McNeil and J. Adams
\$ in the National Summary of January-March 1990.
\$
\$ The Sg lines of some stations include the SH FM.
\$ The convention used is the Virginia Tech convention used in FOCMEC:
\$ <: SH first motion to left (back to event) impulsive \$ >: SH first motion to right (back to event) impulsive \$ Preliminary Focmec computed by ML.

| Sta | Pha | Dist <br> $(k m)$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | ---: | :---: | :---: |
| A16 | PG | 11 | 188 | -45 | D |
| A16 | SG | 11 | 188 | -45 | < |
| A61 | PG | 16 | 330 | -55 | C |
| A61 | SG | 16 | 330 | -55 | $>$ |
| LMQ | PG | 26 | 265 | -67 | D |
| A21 | PG | 27 | 56 | -68 | D |
| A64 | PG | 29 | 14 | -70 | C |
| A64 | SG | 29 | 14 | -70 | < |
| A54 | PG | 35 | 249 | -72 | D |
| A11 | PG | 40 | 204 | -75 | D |
| SLQ | PG | 74 | 81 | -82 | D |
| CIQ | PG | 99 | 323 | -84 | D |
| DAQ | PG | 104 | 296 | -84 | D |

Number of P first motions: 10
Number of SH first motions: 3

2- Most Representative Solution.
A total of 420 solutions were found using a b axis increment of 2 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

```
dip,strike,rake
22.76 141.93 74.33
dip,strike,rake 68.13 338.85 96.47 :auxiliary plane
```

| lower hem. trend, plunge of $a, n$ | 248.85 | 21.87 | 51.93 | 67.24 |
| :--- | :--- | :---: | :---: | :---: | :---: |
| lower hem. trend \& plunge of b | 156.43 | 6.00 |  |  |
| lower hem. trend, plunge of $\mathrm{p}, \mathrm{t}$ | 63.89 | 22.87 | 260.27 | 66.27 |

Average $B, P$, and $T$ axes:
B
P
T

| Mean trend: | N | 340 | N | 74 |
| :--- | :---: | :---: | ---: | ---: |
| Mean Plunge: | 15 | 15 | N | 209 |
| Vector Magnitude: | 405 | 414 | 67 |  |
| Mean length of resulting vector: | 0.964 | 0.985 | 412 |  |

3- Misfits.

All 10 P first motions agreed with the solution.
All 3 SH first motions agreed with the solution.
4- Rating of the focal mechanism.
The solution is rejected (rating $X$ ) based on the high number of $p$ and sH misfits ( $0 / 100$ and $0 / 100$ respectively) and the absence of constraints on the $P, T$ and $B$ axes (value of 0.976 ).



## Location Map



```
Earthquake of 19901106 1130 Magnitude 3.4MN
```

1- Earthquake information and list of first motions.

| Date | Time hhmm |  | Latitude | Longitude | Depth <br> (km) | Mag | Sta/Pha |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 901106 | 1130 | 10.76 | 47.3943 | -70.1506 | 14.19 | 3.4 MN |  |

COMMENTS:

```
    26 KM E OF BAIE-SAINT-PAUL, CHARLEVOIX, QUE.
CHARLEVOIX-KAMOURASKA, QUE. FELT AT LA POCATIERE WHERE PEOPLE
REPORTED THEY HEARD A BOOM FOLLOWED BY A SHORT VIBRATION. ALSO FELT AT
STE-HELENE AND OTHER COMMUNITIES NEAR LA POCATIERE.
$ QCQ too weak for first motion.
$ Focmec published by W. McNeil and J. Adams
$ in the National Summary of October-December 1990.
$
$ The Sg lines of some stations include the SH FM.
$ The convention used is the Virginia Tech convention used in FOCMEC:
$ <: SH first motion to left (back to event) impulsive
$ >: SH first motion to right (back to event) impulsive
$ Preliminary Fommec computed by ML.
```

| Sta | Pha | Dist <br> $(k m)$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | ---: | :---: | :---: |
| A16 | PG | 14 | 52 | -44 | C |
| A16 | SG | 14 | 52 | -44 | $<$ |
| A11 | PG | 17 | 192 | -51 | C |
| A54 | PG | 21 | 289 | -56 | D |
| A54 | SG | 21 | 289 | -56 | < |
| LMQ | PG | 22 | 322 | -57 | C |
| A61 | PG | 34 | 8 | -67 | D |
| A61 | SG | 34 | 8 | -67 | $>$ |
| A21 | PG | 49 | 45 | -74 | C |
| A64 | PG | 52 | 22 | -75 | D |
| SLQ | PG | 91 | 70 | -81 | C |
| DAQ | PG | 104 | 308 | -82 | D |
| CIQ | PG | 109 | 334 | -83 | D |

Number of P first motions: 10 Number of SH first motions: 3

2- Most Representative Solution.

A total of 367 solutions were found using a b axis increment of 1 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

| dip, strike, rake | 68.76 | 209.02 | 56.46 |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| dip, strike, rake | 39.03 | 90.37 | 144.88 | : auxiliary plane |  |  |
| lower hem. trend, plunge of $\mathrm{a}, \mathrm{n}$ | 0.37 | 50.97 | 119.02 | 21.24 |  |  |
| lower hem. trend \& plunge of b | 222.52 | 31.00 |  |  |  |  |
| lower hem. trend, plunge of p,t | 323.14 | 17.05 | 77.77 | 53.66 |  |  |

Average $B, P$, and $T$ axes:


All 3 SH first motions agreed with the solution.
4- Rating of the focal mechanism.
The solution is rejected (X rating) because of the large number of solutions.




## Location Map



```
1- Earthquake information and list of first motions.
\begin{tabular}{ccccccc} 
Date & Time & Latitude & Longitude & \begin{tabular}{c} 
Depth \\
hhmm ss
\end{tabular} & & Mag
\end{tabular}\(\quad\) Sta/Pha
```

COMMENTS :

```
CHARLEVOIX, QUE. 8 KM NW OF ST-JEAN-PORT-JOLI
```

NOT REPORTED FELT
\$ GRQ, CKO LMN NOISY; SLQ down.
\$
\$ The Sg lines of some stations include the SH FM.
\$ The convention used is the Virginia Tech convention used in FOCMEC:
\$ <: SH first motion to left (back to event) impulsive
\$ >: SH first motion to right (back to event) impulsive
\$ Preliminary Focmec computed by ML.

| Sta | Pha | Dist <br> $(k m)$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | ---: | :---: | :---: |
| A11 | PG | 11 | 102 | -49 | D |
| A11 | SG | 11 | 102 | -49 | $>$ |
| A54 | PG | 22 | 345 | -67 | C |
| A54 | SG | 22 | 345 | -67 | $>$ |
| LMQ | PG | 32 | 1 | -74 | C |
| A16 | PG | 34 | 47 | -75 | D |
| A16 | SG | 34 | 47 | -75 | < |
| A61 | PG | 51 | 21 | -80 | C |
| A61 | SG | 51 | 21 | -80 | $>$ |
| A21 | PG | 69 | 45 | -82 | C |
| A64 | PG | 71 | 28 | -82 | D |
| A64 | SG | 71 | 28 | -82 | $>$ |
| DAQ | PG | 104 | 319 | -85 | D |
| CIQ | PG | 117 | 343 | -85 | D |

Number of P first motions: 9 Number of SH first motions: 5

2- Most Representative Solution.

One solution was found using $a b$ axis increment of 1 degree.
The
following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

```
dip,strike,rake 74.04 222.48 85.84
```



Average $B, P$, and $T$ axes:


All 9 p first motions agreed with the solution.
Out of 5 SH first motions, a total of 1 did not fit the solutions (20/100).

| Station | Number | Percentage |
| :---: | :---: | :---: |
| Name of misfits | of wrongs |  |

4- Rating of the focal mechanism.
Although most characteristics of this solution correspond to an A rating (small number of $P$ and $S H$ misfits and on the good constraints on the $P, T$ and $B$ axes, the poor distribution on the focal sphere makes the nodal planes poorly defined. Thus, this solution is rated as X .





Earthquake of 199112080300 Magnitude 4.3MN

1- Earthquake information and list of first motions.

| Date | Time <br> hhmm ss | Latitude | Longitude | Depth <br> $(\mathrm{km})$ | Mag | Sta/Pha |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: |
| 911208 | 0300 | 30.12 | 47.7792 | -69.8643 | 23.05 | 4.3 MN |

## COMMENTS:

```
25 KM W OF RIVIERE-DU-LOUP, QUE.
FELT IN CHARLEVOIX-KAMOURASKA, ST-HILARION, LA MALBAIE, CAP-A-L'AIGLE,
POINTE-AU-PIC, CLERMONT, ILE AUX COUDRES. FELT AT RIVIERE-DU-LOUP, CHICOUTIMI,
LA BAIE, ROBERVAL.
$ SLQ NO RECORD; QCQ EMERGENT.
$ 5 KM S OF ST-SIMEON, QUE. }5\textrm{KM S DE ST-SIMEON, QUE.
$
$ The Sg lines of some stations include the SH FM.
$ The convention used is the Virginia Tech convention used in FOCMEC:
$ <: SH first motion to left (back to event) impulsive
$ >: SH first motion to right (back to event) impulsive
$ Preliminary Focmec computed by ML
$ emergent fm on DPQ (C); GSQ (D); ICQ (D) and CNQ (D).
```

| Sta | Pha | Dist <br> $(\mathrm{km})$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | ---: | ---: | ---: | ---: |
| A64 | PG | 6 | 338 | -14 | C |
| A64 | SG | 6 | 338 | -14 | C |
| A21 | PG | 16 | 123 | -34 | C |
| A21 | SG | 16 | 123 | -34 | < |
| A61 | PG | 19 | 240 | -40 | C |
| A61 | SG | 19 | 240 | -40 | < |
| A16 | PG | 36 | 197 | -57 | D |
| LMQ | PG | 43 | 234 | -62 | C |
| A54 | PG | 55 | 229 | -67 | C |
| A11 | PG | 65 | 203 | -70 | C |
| CIQ | PG | 88 | 309 | -75 | D |
| DAQ | PG | 105 | 282 | -78 | D |

Number of P first motions: 9 Number of SH first motions: 3

2- Most Representative Solution.

A total of 1385 solutions were found using a b axis increment of 1 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

| dip, strike, rake | 79.73 | 17.90 | 21.81 |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| dip, strike, rake | 68.56 | 283.82 | 168.96 | : auxiliary plane |  |  |
| lower hem. trend, plunge of $\mathrm{a}, \mathrm{n}$ | 193.82 | 21.44 | 287.90 | 10.27 |  |  |
| lower hem. trend \& plunge of b | 41.92 | 66.00 |  |  |  |  |
| lower hem. trend, plunge of $\mathrm{p}, \mathrm{t}$ | 149.38 | 7.61 | 242.57 | 22.62 |  |  |

Average $B, P$, and $T$ axes:
B P T

| Mean trend: | N | 46 | N |
| :--- | :---: | :---: | :---: |
| Mean plunge: | 63 | 144 | N |
| Vector Magnitude: | 1375 | 436 |  |
| Mean length of resulting vector: | 0.993 | 1378 | 27 |
|  |  | 0.995 | 1373 |
| 3- Misfits. |  |  | 0.992 |

All 9 first motions agreed with the solution.
out of 3 sH first motions, a total of 1 did not fit the solutions (33/100).
Station Number Percentage
Name of misfits of wrongs
A64 $1385 \quad 100$

4- Rating of the focal mechanism.
Although the solution has a $B$ rating based on the number of $P$ and $S H$ misfits ( $0 / 100$ and $33 / 100$ respectively) and on the constraints on the $P, T$ and B axes (value of 0.993), we prefer to assign a $C$ rating to the solution due to the two distinct families of solutions found.




## Location Map



1- Earthquake information and list of first motions.

| Date Time | Latitude | Longitude | Depth | Mag | Sta/Pha |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| hhmm ss |  |  |  |  |  |

COMMENTS:

```
    23 KM E OF LA MALBAIE, CHARLEVOIX, QUE.
FELT AT SAINT-FIDELE
$ 9 KM E OF ST-FIDELE, QUE.
$47.830-69.970 MN=3.3 0545326 10031992 15 20 13 10.00
$ MN=3.3 FROM AUTO LOCATION
$ DAQ DOWN; JOQ fm unreadable.
$ The Sg lines of some stations include the SH FM.
$
$ The convention used is the Virginia Tech convention used in FOCMEC:
$ <: SH first motion to left (back to event) impulsive
$ >: SH first motion to right (back to event) impulsive
$ Preliminary Focmec computed by ML.
$ focmec published in Li et al. 1996 BSSA.
$ Li et al. propose that it is a double-event.
$ Li et al. suggest SH fm are: All < ; A64 < .
```

| Sta | Pha | Dist <br> $(k m)$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | ---: | :---: | :---: |
| A64 | PG | 12 | 348 | -51 | C |
| A21 | PG | 13 | 97 | -52 | D |
| A21 | SG | 13 | 97 | -52 | $>$ |
| A61 | PG | 18 | 261 | -61 | D |
| A61 | SG | 18 | 261 | -61 | > |
| A16 | PG | 30 | 202 | -71 | D |
| A16 | SG | 30 | 202 | -71 | < |
| LMQ | PG | 40 | 242 | -76 | D |
| A54 | PG | 51 | 236 | -79 | D |
| A54 | SG | 51 | 236 | -79 | C |
| A11 | PG | 59 | 206 | -80 | D |
| SLQ | PG | 64 | 95 | -81 | D |
| CIQ | PG | 93 | 312 | -84 | C |

Number of p first motions: 9 Number of SH first motions: 4

2- Most Representative Solution.
A total of 487 solutions were found using a baxis increment of 5 degree. The
following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

| dip, strike, rake | 63.94 | 300.77 | 44.31 |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| dip, strike, rake | 51.13 | 187.55 | 145.64 | : auxiliary plane |  |  |
| lower hem. trend, plunge of $\mathrm{a}, \mathrm{n}$ | 97.55 | 38.87 | 210.77 | 26.06 |  |  |
| lower hem. trend \& plunge of $b$ | 325.00 | 40.00 |  |  |  |  |
| lower hem. trend, plunge of $p, t$ | 61.47 | 7.64 | 160.34 | 48.97 |  |  |

Average $B, P$, and $T$ axes:

|  | B | P | T |  |
| :--- | :--- | :--- | :--- | ---: |
| Mean trend: | N | 329 | N | 66 |
| Mean Plunge: | 61 | N | 157 |  |
| Vector Magnitude: | 414 | 467 | 29 |  |
| Mean length of resulting vector: | 0.849 | 0.959 | 454 |  |
| 3- Misfits. |  |  | 0.931 |  |

All 9 p first motions agreed with the solution.
All 4 SH first motions agreed with the solution.
4- Rating of the focal mechanism.
The solution is rejected (rating $X$ ) based on the high number of $p$ and $S H$ misfits ( $0 / 100$ and $0 / 100$ respectively) and the absence of constraints on the $P, T$ and $B$ axes (value of 0.913 ).



## Location Map



Earthquake of 199205010037 Magnitude 3.2MN

1- Earthquake information and list of first motions.

| Date | Time <br> hhmm SS | Latitude | Longitude | Depth | Mag | Sta/Pha |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: |
| 920501 | 0037 | 51.49 | 47.4463 | -70.4069 | 2.67 | 3.2 MN |

COMMENTS:

6 KM E OF BAIE-SAINT-PAUL, CHARLEVOIX, QUE.
FELT STRONGEST AT ILE AUX COUDRES, ALSO FELT AT SAINT-HILARION, BAIE-ST-PAUL, LES EBOULEMENTS, SAINT-URBAIN.
\$ FROM AUTO LOCATION
$\$+47.460-70.496 F 1 M N=3.300375050105199200 .0290 .036 \quad 0.017 \quad 21 \quad 01.02 \quad 210.00$
\$ A54 DEAD
\$ CIQ down.
\$ NOTE: the focal depth may not be very accurate as A54 is down.
\$
\$ The Sg lines of some stations include the SH FM.
\$ The convention used is the Virginia Tech convention used in FOCMEC:
\$ <: SH first motion to left (back to event) impulsive
\$ >: SH first motion to right (back to event) impulsive \$ Preliminary Focmec computed by ML.

| Sta | Pha | Dist <br> $(\mathrm{km})$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | ---: | :---: | :---: |
| LMQ | PG | 13 | 28 | -78 | D |
| All | PG | 28 | 145 | -84 | D |
| A16 | PG | 30 | 85 | -85 | C |
| A16 | SG | 30 | 85 | -85 | < |
| A61 | PG | 36 | 41 | -86 | D |
| A64 | PG | 57 | 42 | -87 | D |
| A21 | PG | 61 | 62 | -88 | C |
| DAQ | PG | 85 | 313 | -88 | D |
| SLQ | PG | 108 | 76 | -89 | D |
| DPQ | PN | 199 | 246 | 49 | D |
|  |  |  |  |  |  |
|  | Number of | P first motions: | 9 |  |  |

2- Most Representative Solution.

A total of 5 solutions were found using a b axis increment of 1 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

$$
\begin{array}{llll}
\text { dip,strike,rake } & 6.40 \quad 217.14 \quad 51.26
\end{array}
$$

| dip, strike, rake | 85.01 | 76.06 | 94.02 | : auxiliary plane |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | ---: |
| lower hem. trend, plunge of $a, n$ | 346.06 | 4.99 | 127.14 | 83.60 |  |  |
| lower hem. trend \& plunge of $b$ | 255.71 | 4.00 |  |  |  |  |
| lower hem. trend, plunge of p,t | 162.36 | 39.88 | 350.46 | 49.83 |  |  |

Average $B, P$, and $T$ axes:
B P T

| Mean trend: | N | 254 | N | 161 |
| :--- | ---: | ---: | ---: | ---: |
| Mean Plunge: | 4 | N | 349 |  |
| Vector Magnitude: | 5 | 50 | 50 |  |
| Mean length of resulting vector: | 1.000 | 5 | 5 |  |

3- Misfits.

All 9 first motions agreed with the solution.
All 1 SH first motions agreed with the solution.

4- Rating of the focal mechanism.
Although the solution could have an $A$ rating based on the small number of P and SH misfits ( $0 / 100$ and $0 / 100$ respectively) and on the good constraints on the $P, T$ and $B$ axes (value of 1.000 ), we believe that the poor distribution of first motions makes it an $X$ (rejected) solution.



## Location Map



Earthquake of 199303042202 Magnitude 3.1MN

1- Earthquake information and list of first motions.

| Date Time | Latitude | Longitude | Depth <br> hhmm ss |  | Mag | Sta/Pha |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 930304 | 2202 | 21.84 | 47.5145 | -70.3621 | 4.39 | 3.1 MN |

COMMENTS :

```
LA MALBAIE, CHARLEVOIX, QUE. FELT IN ISLE AUX COUDRES, ST-HILARION
LES EBOULEMENT, ST-URBAIN AND BAIE-ST-PAUL.
$ TRQ NOISY; NO MAGNITUDE; LMN DEAD
$ LMQ PHASES X'ED OUT DUE TO SUSPECTED TIMING DESCREPANCY
$ BETWEEN CNSN AND CLTN, AND TO FIR-FILTER RINGING BEFORE PG
$ MNT,GSQ SG INDISTINCT
$ CIQ first motion read by Reynald Du Berger in Chicoutimi.
$ Sg on A2l has large residual but is quite clear.
$
$ The Sg lines of some stations include the SH FM.
$ The convention used is the Virginia Tech convention used in FOCMEC:
$ <; SH first motion to left (back to event) impulsive
$ >: SH first motion to right (back to event) impulsive
$ Preliminary Focmec computed by ML.
```

| Sta | Pha | Dist <br> (km) | Azim | Take-off <br> Angle | FM |
| :--- | ---: | ---: | ---: | ---: | ---: |
| LMQ | PG | 5 | 35 | -46 | D |
| A54 | PG | 7 | 210 | -60 | D |
| A54 | SG | 7 | 210 | -60 | $<$ |
| SHQ | PG | 10 | 344 | -67 | C |
| A16 | PG | 27 | 100 | -81 | D |
| A16 | SG | 27 | 100 | -81 | $>$ |
| A61 | PG | 29 | 46 | -81 | D |
| A11 | PG | 33 | 158 | -82 | C |
| LPQ | PG | 33 | 126 | -82 | C |
| A64 | PG | 50 | 45 | -85 | D |
| A64 | SG | 50 | 45 | -85 | $>$ |
| A21 | PG | 55 | 67 | -85 | D |
| DAQ | PG | 83 | 308 | -87 | C |
| CIQ | PG | 90 | 339 | -87 | C |
| SLQ | PG | 103 | 80 | -88 | D |

Number of P first motions: 12 Number of SH first motions: 3

A total of 343 solutions were found using ab axis increment of 1 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

| dip, strike, rake | 59.55 | 279.68 | 39.09 |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| dip, strike, rake | 57.08 | 167.30 | 142.86 | : auxiliary plane |  |  |
| lower hem. trend, plunge of $\mathrm{a}, \mathrm{n}$ | 77.30 | 32.92 | 189.68 | 30.45 |  |  |
| lower hem. trend \& plunge of b | 311.64 | 42.00 |  |  |  |  |
| lower hem. trend, plunge of $\mathrm{p}, \mathrm{t}$ | 42.98 | 1.49 | 134.63 | 47.96 |  |  |

Average $B, P$, and $T$ axes:

B P T

| Mean trend: | N | 314 | N |
| :--- | :---: | :---: | ---: |
| Mean Plunge: | 45 | 1 | N |
| Vector Magnitude: | 340 | 341 | 45 |
| Mean length of resulting vector: | 0.993 | 0.995 | 342 |

3- Misfits.

All 12 P first motions agreed with the solution.
All 3 SH first motions agreed with the solution.
4- Rating of the focal mechanism.

The solution has an $A$ rating based on the small number of $P$ and $S H$ misfits ( $0 / 100$ and $0 / 100$ respectively) and on the good constraints on the $p$, $T$ and $B$ axes (value of 0.994 ).



## Location Map



Earthquake of 199308072125 Magnitude 3.1MN

1- Earthquake information and list of first motions.

| Date | Time | Latitude | Longitude | Depth | Mag | Sta/Pha |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: |
| hhmm ss |  |  |  |  |  |  |
| 930807 | 2125 | 31.92 | 47.6681 | -69.8893 | 7.75 | 3.1 MN |

COMMENTS:

```
    19 KM E OF LA MALBAIE, CHARLEVOIX, QUE.
$ LPQ PHASES X'ED OUT DUE TO SUSPECTED TIMING DESCREPANCY
$ BETWEEN CNSN AND CLTN, AND TO FIR-FILTER RINGING BEFORE PG
$ ECTN RESCANNED BY PFC USING DAN 1.83I; SLIGHT CHANGES TO PN,SG PHASES
$ PN NOT VISIBLE AT MNT
$ LPQ DATA NOT SAVED; SG AND AMPLITUDE UNAVAILABLE
$ CIQ first motion read by Reynald Du Berger in Chicoutimi.
$ SLQ down.
$
$ The Sg lines of some stations include the SH FM.
$ The convention used is the Virginia Tech convention used in FOCMEC:
$ <: SH first motion to left (back to event) impulsive
$ >: SH first motion to right (back to event) impulsive
```

| Sta | Pha | Dist <br> $(\mathrm{km})$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | ---: | :---: | :---: |
| A61 | PG | 15 | 280 | -63 | D |
| A61 | SG | 15 | 280 | -63 | $>$ |
| A21 | PG | 16 | 75 | -63 | D |
| A21 | SG | 16 | 75 | -63 | < |
| A64 | PG | 18 | 359 | -66 | C |
| A16 | PG | 24 | 202 | -72 | C |
| LMQ | PG | 36 | 248 | -78 | D |
| SHQ | PG | 39 | 260 | -79 | D |
| A54 | PG | 46 | 239 | -80 | D |
| A11 | PG | 53 | 206 | -82 | D |
| CIQ | PG | 95 | 315 | -85 | D |
| DAQ | PG | 107 | 288 | -86 | D |

Number of P first motions: 10 Number of SH first motions: 2

2- Most Representative Solution.
A total of 1144 solutions were found using a $b$ axis increment of 2 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

```
dip,strike,rake 53.32 164.64 72.44
dip,strike,rake 40.13 12.55 112.05 :auxiliary plane
```



```
lower hem, trend & plunge of b 175.34 14.00
lower hem. trend, plunge of p,t 267.04 
```

Average $B, P$, and $T$ axes:
B P T

| Mean trend: | N | 21 | N | 273 |
| :--- | :---: | :---: | :---: | :---: |
| Mean Plunge: |  | 10 | 6 | 72 |
| Vector Magnitude: | 397 | 1124 | 84 |  |
| Mean length of resulting vector: | 0.347 | 0.982 | 1116 |  |

3- Misfits.

All 10 P first motions agreed with the solution.
All 2 SH first motions agreed with the solution.
4- Rating of the focal mechanism.
The solution is rejected (rating $X$ ) based on the high number of $P$ and SH misfits ( $0 / 100$ and $0 / 100$ respectively) and the absence of constraints on the $P, T$ and $B$ axes (value of 0.768 ).




## Location Map



Earthquake of 199312302301 Magnitude 3.8MN

1- Earthquake information and list of first motions.

| Date | Time <br> hhmm ss | Latitude | Longitude | Depth <br> $(\mathrm{km})$ | Mag | Sta/Pha |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 931230 | 230147.69 | 47.4532 | -70.3609 | 5.94 | 3.8 MN | $6 / 012$ |

COMMENTS:

```
    10 KM E OF BAIE-SAINT-PAUL, CHARLEVOIX, QUE.
FELT AT BAIE-SAINT-PAUL AND LA MALBAIE.
$ LMQ,LPQ PHASES X'ED OUT DUE TO SUSPECTED TIMING DESCREPANCY
$ BETWEEN CNSN AND CLTN, AND TO FIR-FILTER RINGING BEFORE PG
$KAO RECORD CHANGE; NOT ON GTO
$ CIQ first motion read by Reynald Du Berger in Chicoutimi.
$
$ The Sg lines of some stations include the SH FM.
$ The convention used is the Virginia Tech convention used in FOCMEC:
$ <: SH first motion to left (back to event) impulsive
$ >: SH first motion to right (back to event) impulsive
$ Preliminary Focmec computed by ML
```

| Sta | Pha | Dist <br> $(\mathrm{km})$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | ---: | ---: | ---: | ---: |
| A54 | PG | 4 | 276 | -33 | D |
| A54 | SG | 4 | 276 | -33 | $>$ |
| LMQ | PG | 11 | 14 | -61 | D |
| SHQ | PG | 17 | 350 | -71 | C |
| A11 | PG | 26 | 152 | -77 | C |
| A11 | SG | 26 | 152 | -77 | $>$ |
| A16 | PG | 27 | 86 | -78 | D |
| A16 | SG | 27 | 86 | -78 | $>$ |
| LPQ | PG | 29 | 115 | -78 | D |
| A61 | PG | 34 | 37 | -80 | D |
| A61 | SG | 34 | 37 | -80 | < |
| A64 | PG | 54 | 40 | -84 | D |
| A21 | PG | 58 | 61 | -84 | D |
| DAQ | PG | 87 | 311 | -86 | C |
| CIQ | PG | 97 | 341 | -86 | C |
| QCQ | PG | 102 | 223 | -87 | D |
| SLQ | PG | 104 | 76 | -87 | D |
| DPQ | PN | 203 | 246 | 49 | D |

Number of $P$ first motions: 14 Number of SH first motions: 4

A total of 112 solutions were found using a b axis increment of 2 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

| dip, strike, rake | 86.75 | 116.31 | 23.79 |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | ---: |
| dip, strike, rake | 66.25 | 24.88 | 176.45 | : auxiliary plane |  |
| lower hem. trend, plunge of $\mathrm{a}, \mathrm{n}$ | 294.88 | 23.75 | 26.31 | 3.25 |  |
| lower hem. trend \& plunge of b | 123.63 | 66.00 |  |  |  |
| lower hem. trend, plunge of $\mathrm{p}, \mathrm{t}$ | 248.17 | 14.17 | 343.15 | 18.96 |  |

Average $B, P$, and $T$ axes:

|  | B |  | P |  | T |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mean trend: | N | 149 | N | 250 | N | 341 |
| Mean Plunge: |  | 59 |  | 5 |  | 30 |
| Vector Magnitude: |  | 107 |  | 110 |  | 109 |
| Mean length of resulting vector: |  | 0.955 |  | 0.978 |  | 0.969 |

All 14 P first motions agreed with the solution.
All 4 SH first motions agreed with the solution.

4- Rating of the focal mechanism.

The solution is rejected (rating $X$ ) based on the high number of $P$ and $S H$ misfits ( $0 / 100$ and $0 / 100$ respectively) and the absence of constraints on the $P, T$ and $B$ axes (value of 0.967 ).



$146$

## Location Map



Earthquake of 199409250053 Magnitude 4.3MN

1- Earthquake information and list of first motions.

| Date | Time <br> hhmm |  | Latitude | Longitude | Depth <br> (km) | Mag | Sta/Pha |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 940925 | 0053 | 29.46 | 47.7518 | -69.9612 | 12.18 | 4.3MN | 6/012 |

## COMMENTS:

19 KM Ne OF LA MALbAIE, ChARLEVOIX, QUE. CHARLEVOIX-KAMOURASKA, QUE.; LARGELY FELT IN CHARLEVOIX AS WELL AS ON The SOUTH SHORE. IN CHARLEVOIX, REPORTED FELT IN:
ST-hilarion, notre-dame-des-monts, st-Aime-des-lacs, la malbaie, Clermont, POINTE-AU-PIC, LES EBOULEMENTS, BAIE-ST-PAUL, ST-URBAIN,
and on Ile-aux-COUDRES. FELT AS FAR EAST AS NORTHWESTERN NEW
BRUNSWICK, AS FAR NORTH AS LES ESCOUMINS,AS FAR SOUTH AS TO BEAUPORT (1 REPORT)
AND AS FAR WEST AS JONQUIERE.
\$ CIQ READING FROM REYNALD DU BERGER, UQAC.
\$ CHARLEVOIX FELT REPORTS FROM HILARION BERGERON.
\$ SONT PHASES READ BY UWO NOT GSC
\$ N.y. State phases from f. Revetta.
\$ SLTN ADDED BY MGC
\$ SWO BAD SIGNAL; ELO NO RESPONSE CURVE; CODE DISCREPANCY
\$ CIQ first motion read by Reynald Du Berger in Chicoutimi.


$\begin{array}{lllllllllllllllll}\text { \$SWX SZ Trac Y0057 } 24.27 & \text { L } & 0.000 & 0.00 & 867.00 & 266.0 W & 4.40 & \mathrm{MN} & 0.00 & 0.58\end{array}$
\$
\$ The Sg lines of some stations include the SH FM.
\$ The convention used is the virginia Tech convention used in FOCMEC:
\$ <: SH first motion to left (back to event) impulsive
\$ >: SH first motion to right (back to event) impulsive
\$ Preliminary Focmec computed by ML.

| Sta | Pha | Dist <br> $(k m)$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | ---: | :---: | :---: |
| A64 | PG | 10 | 32 | -39 | C |
| A64 | SG | 10 | 32 | -39 | $>$ |
| A61 | PG | 12 | 236 | -44 | C |
| A61 | SG | 12 | 236 | -44 | < |
| A21 | PG | 21 | 105 | -60 | D |
| A21 | SG | 21 | 105 | -60 | $<$ |
| A16 | PG | 31 | 186 | -69 | C |
| SHQ | PG | 37 | 244 | -72 | D |
| A54 | PG | 47 | 226 | -76 | C |
| A54 | SG | 47 | 226 | -76 | > |
| A11 | PG | 59 | 198 | -78 | D |
| SLQ | PG | 72 | 97 | -80 | D |
| CIQ | PG | 85 | 313 | -82 | D |


| DAQ | PG | 99 | 284 | -83 | $D$ |
| ---: | ---: | ---: | ---: | ---: | ---: |
| QCQ | PG | 147 | 223 | -85 | $D$ |

Number of $P$ first motions: 11 Number of SH first motions: 4

2- Most Representative Solution.
A total of 77 solutions were found using a b axis increment of 1 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.


Average $B, P$, and $T$ axes:

B P T

| Mean trend: | N | 217 | N |
| :--- | :---: | :---: | :---: |
| Mean plunge: | 127 | N | 312 |
| Vector Magnitude: | 77 | 9 | 81 |
| Mean length of resulting vector: | 0.999 | 77 | 77 |
|  |  | 0.998 | 0.999 |

All 11 P first motions agreed with the solution.
Out of 4 SH first motions, a total of 1 did not fit the solutions (25/100).

| Station | Number | Percentage |
| :---: | :---: | :---: |
| Name of misfits | of wrongs |  |

4- Rating of the focal mechanism.
The solution has an $A$ rating based on the small number of $P$ and $S H$ misfits ( $0 / 100$ and $25 / 100$ respectively) and on the good constraints on the $P, T$ and $B$ axes (value of 0.999).



## Location Map



Earthquake of 199412011302 Magnitude 3.0MN

1- Earthquake information and list of first motions.

| Date | Time <br> hamm ss | Latitude | Longitude | Depth <br> $(\mathrm{km})$ | Mag | Sta/Pha |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 941201 | 1302 | 47.14 | 47.4374 | -70.3138 | 10.77 | 3.0 MN |

COMMENTS:
CHARLEVOIX, QUE.; FELT AT ILE-AUX-COUDRES, QUE.
\$ NO HORIZONTALS FOR AlI
\$ RG LIKE PHASE ON All AND Alb.
\$ LIQ HAS SOME RINGING; HENCE PHASE READINGS WERE X'ED OUT.
\$ LMQ first motion is uncertain.
\$ PICKS ON A64 LOOK FINE; PROBLEM WITH NETWORK?
\$ CIQ first motion read by Reynald Du Berger in Chicoutimi.
\$
\$ The Sg lines of some stations include the SH FM.
\$ The convention used is the Virginia Tech convention used in FOCMEC:
\$ <: SH first motion to left (back to event) impulsive
\$ >: SH first motion to right (back to event) impulsive
\$ Preliminary Focmec computed by ML.

| Sta | Fha | Dist <br> $(k m)$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | ---: | ---: | :---: | :---: |
| A54 | PG | 8 | 286 | -36 | C |
| A54 | SG | 8 | 286 | -36 | $>$ |
| LMQ | PG | 12 | 356 | -49 | C |
| GHQ | PG | 20 | 340 | -61 | C |
| A11 | PG | 23 | 158 | -65 | C |
| A16 | PG | 23 | 81 | -65 | C |
| A16 | SG | 23 | 81 | -65 | $>$ |
| A61 | PG | 33 | 31 | -72 | D |
| A64 | PG | 54 | 36 | -79 | D |
| A21 | PG | 56 | 58 | -79 | D |
| AQ | PG | 91 | 310 | -83 | C |
| LIQ | PG | 100 | 339 | -84 | C |
| SEQ | PG | 101 | 75 | -84 | C |

Number of P first motions: 11 Number of SH first motions: 2

2- Most Representative Solution.

A total of 197 solutions were found using ab axis increment of 2 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

| dip, strike, rake | 68.69 | 69.61 | -15.26 |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | ---: |
| dip, strike, rake | 75.81 | 165.27 | -157.98 | : auxiliary plane |  |
| lower hem. trend, plunge of $\mathrm{a}, \mathrm{n}$ | 75.27 | 14.19 | 339.61 | 21.31 |  |
| lower hem. trend \& plunge of b | 196.49 | 64.00 |  |  |  |
| lower hem. trend, plunge of $\mathrm{p}, \mathrm{t}$ | 28.70 | 25.49 | 296.40 | 4.80 |  |

Average $B, P$, and $T$ axes:


All 11 P first motions agreed with the solution.
All 2 SH first motions agreed with the solution.
4- Rating of the focal mechanism.
The solution has a $B$ rating based on the number of $P$ and $S H$ misfits
( $0 / 100$ and $0 / 100$ respectively) and on the constraints on the $P, T$ and
$B$ axes (value of 0.988 ).



## Location Map



Earthquake of 199605121153 Magnitude 3.1MN

1- Earthquake information and list of first motions.

| DateTime <br> hhmm ss | Latitude | Longitude | Depth <br> $(\mathrm{km})$ | Mag | Sta/Pha |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 9605121153 | 21.91 | 47.5161 | -70.0281 | 14.82 | 3.1 MN | $7 / 014$ |

COMMENTS :
Felt, CHARLEVOIX SEISMIC ZONE, QUE.
Felt at Saint-Denis on the South Shore.
Also felt on the North shore at St-Irenee and La Malbaie.
\$ DAQ Pg was truncated by a line drop-out.
\$ Maurice called St-Denis Municipal Office; people felt it
\$ as a bump. Charlevoix radio station gave felt info. for the \$ north shore.
\$
\$ The Sg lines of some stations include the SH FM.
\$ The convention used is the Virginia Tech convention used in FOCMEC:
$\$<: S H$ first motion to left (back to event) impulsive
\$ >: SH first motion to right (back to event) impulsive
\$ Preliminary Focmec computed by ML.
\$ CIQ first motion by Reynald Du Berger, UQAC.

| Sta | Pha | Dist <br> $(\mathrm{km})$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | ---: | :---: | :---: |
| A16 | PG | 5 | 162 | -20 | C |
| A16 | SG | 5 | 162 | -20 | > |
| A61 | PG | 20 | 347 | -54 | D |
| LMQ | PG | 23 | 279 | -57 | D |
| A54 | PG | 30 | 257 | -64 | D |
| A21 | PG | 33 | 51 | -66 | D |
| A21 | SG | 33 | 51 | -66 | C |
| A11 | PG | 33 | 203 | -66 | C |
| A64 | PG | 36 | 16 | -68 | D |
| A64 | SG | 36 | 16 | -68 | C |
| CIQ | PG | 102 | 326 | -82 | D |

Number of $P$ first motions: 8 Number of SH first motions: 3

2- Most Representative Solution.
A total of 662 solutions were found using a b axis increment of 2 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

| dip, strike, rake | 48.92 | 163.13 | 57.34 |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| dip, strike, rake | 50.61 | 27.41 | 121.76 | : auxiliary plane |  |  |
| lower hem. trend, plunge of $\mathrm{a}, \mathrm{n}$ | 297.41 | 39.39 | 73.13 | 41.08 |  |  |
| lower hem. trend \& plunge of b | 185.97 | 24.00 |  |  |  |  |
| lower hem. trend, plunge of $p, t$ | 95.56 | 0.91 | 3.51 | 65.98 |  |  |

Average $B, P$, and $T$ axes:

B P T

| Mean trend: | N | 178 | N | 270 |
| :--- | :---: | :---: | :---: | :---: |
| Mean Plunge: | 31 | 4 | N | 5 |
| Vector Magnitude: | 650 | 649 | 59 |  |
| Mean length of resulting vector: | 0.981 | 0.981 | 655 |  |
|  |  |  | 0.989 |  |

All 8 P first motions agreed with the solution.
All 3 SH first motions agreed with the solution.
4- Rating of the focal mechanism.

The solution has a $C$ rating based on the high number of $P$ and $S H$ misfits ( $0 / 100$ and $0 / 100$ respectively) and on the poor constraints on the $P, T$ and B axes (value of 0.984).




## Location Map



Earthquake of 199606070941 Magnitude 3.08MN

1- Earthquake information and list of first motions.

| DateTime <br> hamm Ss | Latitude | Longitude | Depth <br> $(\mathrm{km})$ | Mag | Sta/Pha |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 960607 | 094142.84 | 47.5299 | -69.9417 | 13.31 | 3.08 MN | $7 / 014$ |

## COMMENTS:

Felt, CHARLEVOIX SEISMIC ZONE, QUE.
Reported felt on the South shore at St-Denis and St-Pascal.
On the North Shore: St-Irenee, Pointe-au-Pic et St-Hilarion.
\$Felt info from radio announcers in Kamouraska and Charlevoix.
\$
\$ The Sg lines of some stations include the SH FM.
\$ The convention used is the Virginia Tech convention used in FOCMEC:
\$ <: SH first motion to left (back to event) impulsive
\$ >: SH first motion to right (back to event) impulsive
\$ Preliminary Focmec computed by ML.
\$ CIQ fm from reynald Du Berger.

| Sta | Fha | Dist <br> $(k m)$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | ---: | :---: | :---: |
| A16 | PG | 8 | 216 | -32 | C |
| A16 | SG | 8 | 216 | -32 | > |
| A61 | PG | 21 | 328 | -58 | C |
| A61 | SG | 21 | 328 | -58 | $>$ |
| A21 | PG | 27 | 44 | -64 | D |
| A21 | SG | 27 | 44 | -64 | < |
| LMQ | PG | 29 | 274 | -65 | D |
| LMQ | SG | 29 | 274 | -65 | $>$ |
| A64 | PG | 33 | 6 | -68 | C |
| GHQ | PG | 36 | 284 | -70 | D |
| A54 | PG | 36 | 257 | -70 | D |
| A54 | SG | 36 | 257 | -70 | $>$ |
| A11 | PG | 37 | 211 | -70 | C |
| SLD | PG | 72 | 78 | -80 | D |
| LIQ | PG | 104 | 323 | -83 | D |
| AQ | PG | 109 | 297 | -83 | D |

Number of P first motions: 11 Number of SH first motions: 5

2- Most Representative Solution.
A total of 205 solutions were found using $a b$ axis increment of 2 degree. The following parameters describe the most representative solution, which was derived
from the average $B, P$, and $T$ axes listed below.

| dip, strike, rake | 28.58 | 352.89 | 77.38 |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| dip, strike, rake | 62.17 | 187.19 | 96.79 | : auxiliary plane |  |  |
| lower hem. trend, plunge of $\mathrm{a}, \mathrm{n}$ | 97.19 | 27.83 | 262.89 | 61.42 |  |  |
| lower hem. trend \& plunge of b | 4.01 | 6.00 |  |  |  |  |
| lower hem. trend, plunge of $p, \mathrm{t}$ | 272.18 | 16.90 | 112.89 | 72.00 |  |  |

Average $B, P$, and $T$ axes:

|  | B | P | T |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Mean trend: | N | 15 | N | 277 | N |
| Mean Plunge: | 9 | 118 |  |  |  |
| Vector Magnitude: | 133 | 203 | 72 |  |  |
| Mean length of resulting vector: | 0.647 | 0.992 | 203 |  |  |
| 3- Misfits. |  |  | 0.990 |  |  |

All 11 P first motions agreed with the solution.
Out of 5 sH first motions, a total of 1 did not fit the solutions (20/100).

| Station <br> NameNumber misfits | Percentage <br> of wrongs |  |
| :---: | :---: | :---: |
| A54 | 205 | 100 |

4- Rating of the focal mechanism.

The solution is rejected (rating $X$ ) based on the high number of $P$ and sH misfits ( $0 / 100$ and $20 / 100$ respectively) and the absence of constraints on the $P, T$ and $B$ axes (value of 0.876 ).


19960607 09:41 U.T.




## Location Map



Earthquake of 199701101927 Magnitude 3.21MN

1- Earthquake information and list of first motions.

| DateTime <br> hhmm ss | Latitude | Longitude | Depth <br> $(\mathrm{km})$ | Mag | Sta/Pha |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 970110 | 1927 | 27.56 | 47.5094 | -70.1965 | 17.06 | 3.21 MN |

COMMENTS :

Felt, CHARLEVOIX SEISMIC ZONE, QUE.
Felt in St-Irenee, St-Joseph-de-la-Rive and St-Hilarion.
16 km S from LA MALBAIE, QUE.
\$ maurice talked with local radio station to get felt info.
\$ CIQ first motion read by $R$. Du Berger.
\$
\$ The Sg lines of some stations include the SH FM.
\$ The convention used is the Virginia Tech convention used in FOCMEC:
\$ <: SH first motion to left (back to event) impulsive
\$ >: SH first motion to right (back to event) impulsive
\$ Preliminary Focmec computed by ML.

| Sta | Pha | Dist <br> $(k m)$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | ---: | :---: | ---: |
| LMQ | PG | 11 | 294 | -32 | D |
| LMQ | SG | 11 | 294 | -32 | $>$ |
| A16 | PG | 15 | 107 | -41 | C |
| A16 | SG | 15 | 107 | -41 | $>$ |
| A54 | PG | 17 | 250 | -45 | D |
| A54 | SG | 17 | 250 | -45 | $>$ |
| SHQ | PG | 19 | 304 | -48 | D |
| A61 | PG | 22 | 21 | -52 | C |
| A61 | SG | 22 | 21 | -52 | $>$ |
| A11 | PG | 30 | 180 | -60 | D |
| A64 | PG | 42 | 33 | -68 | D |
| A21 | PG | 44 | 60 | -69 | D |
| DAQ | PG | 93 | 303 | -80 | D |
| CIQ | PG | 96 | 333 | -80 | C |
|  |  |  |  |  |  |
|  | Number of | P first motions: | 10 |  |  |
|  | Number of | SH first motions: | 4 |  |  |

2- Most Representative Solution.
A total of 104 solutions were found using a b axis increment of 2 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

```
lrrr,strike,rake 
lower hem. trend, plunge of a,n
lower hem, trend & plunge of b 155.99 26.00
lower hem. trend, plunge of p,t 
```

Average $B, P$, and $T$ axes:

|  | B | P | T |  |
| :--- | ---: | :--- | ---: | ---: |
| Mean trend: | N | 156 | N | 58 |
| Mean Plunge: | 20 | N | 286 |  |
| Vector Magnitude: | 104 | 21 | 60 |  |
| Mean length of resulting vector: | 0.996 | 0.997 | 104 |  |
| 3- Misfits. |  |  | 0.997 |  |

All 10 P first motions agreed with the solution.
All 4 SH first motions agreed with the solution.
4- Rating of the focal mechanism.
The solution has an $A$ rating based on the small number of $p$ and $S H$ misfits ( $0 / 100$ and $0 / 100$ respectively) and on the good constraints on the $P$, $T$ and $B$ axes (value of 0.997 ).




## Location Map



Earthquake of 199701140447 Magnitude 3.1MN

1- Earthquake information and list of first motions.

| Date | Time <br> hamm | Latitude | Longitude | Depth <br> $(\mathrm{km})$ | Mag | Sta/Pha |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 970114 | 0447 | 32.42 | 47.6569 | -69.8765 | 14.74 | 3.1 MN |

```
COMMENTS:
```

CHARLEVOIX SEISMIC ZONE, QUE.
21 km E from LA MALBAIE, QUE.
Weakly felt in St-Fidele.
\$ Maurice talked to local media. No phone calls from residents to radio stations
\$ Talked to St-Fidele Town Hall; felt by one person.
\$ CIQ first motion read by $R$. Du Berger.
\$
\$ The Sg lines of some stations include the SH FM.
S The convention used is the Virginia Tech convention used in FOCMEC:
$\$<: S H$ first motion to left (back to event) impulsive
\$ >: SH first motion to right (back to event) impulsive
\$ Preliminary Focmec computed by ML.

| Sta | Ph | Dist <br> $(\mathrm{km})$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | ---: | :---: | :---: |
| A21 | PG | 15 | 70 | -45 | D |
| A61 | PG | 17 | 284 | -48 | C |
| A61 | SG | 17 | 284 | -48 | $>$ |
| A64 | PG | 19 | 356 | -52 | D |
| A64 | SG | 19 | 356 | -52 | < |
| A16 | PG | 23 | 205 | -57 | D |
| A16 | SG | 23 | 205 | -57 | $>$ |
| LMQ | PG | 36 | 250 | -68 | C |
| LMQ | SG | 36 | 250 | -68 | $>$ |
| GHQ | PG | 40 | 262 | -70 | C |
| A54 | PG | 46 | 241 | -72 | C |
| A54 | SG | 46 | 241 | -72 | $>$ |
| A11 | PG | 52 | 208 | -74 | D |
| SEQ | PG | 65 | 89 | -77 | C |
| LIQ | PG | 97 | 315 | -81 | C |
| AQ | PG | 108 | 289 | -82 | C |

Number of P first motions: 11 Number of SH first motions: 5

2- Most Representative Solution.

A total of 137 solutions were found using ab axis increment of 5 degree. The
following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

| dip, strike, rake | 50.73 | 255.98 | 8.29 |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| dip, strike, rake | 83.59 | 160.71 | 140.43 | : auxiliary plane |  |
| lower hem. trend, plunge of $\mathrm{a}, \mathrm{n}$ | 70.71 | 6.41 | 165.98 | 39.27 |  |
| lower hem. trend \& plunge of b | 333.02 | 50.00 |  |  |  |
| lower hem. trend, plunge of p,t | 214.81 | 21.63 | 110.59 | 31.77 |  |

Average $B, P$, and $T$ axes:





## Location Map



Appendix 2: Focal mechanisms of earthquakes recorded during the 1996 summer field survey.


Q: Quality.
A: Very good
B: Good
C: Fair
X: Rejected
0 : Cannot be computed.

Focal Mechanisms from 1996 Field Survey


Earthquake of 199606171118 Magnitude 1.9 MN

1- Earthquake information and list of first motions.

| Date | Time <br> hamm ss | Latitude | Longitude | Depth <br> $(\mathrm{km})$ | Mag | Sta/Pha |
| :---: | :--- | :---: | :---: | ---: | :---: | ---: |
| 960617 | 1118 | 30.66 | 47.5328 | -70.1463 | 14.11 | 1.9 MN |

COMMENTS:

CHARLEVOIX SEISMIC ZONE, QUE.
\$
\$ The Sg lines of some stations include the SH FM.
$\$$ The convention used is the Virginia Tech convention used in FOCMEC:
\$ <: SH first motion to left (back to event) impulsive \$ >: SH first motion to right (back to event) impulsive \$ Preliminary Focmec computed by ML. \$ time corrections to be added as soon as station \$ conditions get clarified.

| Sta | Fha | Dist <br> $(k m)$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | ---: | :---: | ---: |
| A16 | PG | 13 | 123 | -42 | C |
| A16 | SG | 13 | 123 | -42 | $<$ |
| LMQ | PG | 14 | 277 | -44 | C |
| A81P | PG | 14 | 243 | -44 | C |
| A81P | SG | 14 | 243 | -44 | $>$ |
| A61 | PG | 18 | 13 | -52 | D |
| A61 | SG | 18 | 13 | -52 | $>$ |
| A82P | PG | 20 | 295 | -55 | D |
| A54 | PG | 22 | 247 | -57 | C |
| A54 | SG | 22 | 247 | -57 | $<$ |
| A80P | PG | 29 | 277 | -64 | D |
| A80P | SG | 29 | 277 | -64 | $<$ |
| A11 | PG | 33 | 187 | -66 | D |
| A11 | SG | 33 | 187 | -66 | $<$ |
| A64 | PG | 38 | 30 | -70 | D |
| A64 | SG | 38 | 30 | -70 | $>$ |
| A21 | PG | 39 | 61 | -70 | D |
| AQ | PG | 95 | 301 | -82 | D |
|  |  |  |  |  |  |
|  | Number of | P first motions: | Il |  |  |
|  | Number of | SH first motions: | 7 |  |  |

2- Most Representative Solution.

A total of 347 solutions were found using ab axis increment of 1 degree. The following parameters describe the most representative solution, which was derived

```
from the average B, P, and T axes listed below.
\begin{tabular}{lllllll} 
dip, strike, rake & 61.94 & 72.82 & 74.09 & & & \\
dip, strike, rake & 31.94 & 284.04 & 117.22 & \multicolumn{2}{c}{ : auxiliary plane } \\
lower hem. trend, plunge of \(\mathrm{a}, \mathrm{n}\) & 194.04 & 58.06 & 342.82 & 28.06 \\
lower hem. trend \& plunge of b & 80.46 & 14.00 & & \\
lower hem. trend, plunge of p,t & 174.43 & 15.51 & 310.30 & 68.86
\end{tabular}
```

Average $B, P$, and $T$ axes:

|  | B |  | P | T |
| :--- | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| Mean trend: | N | 84 | N | 178 |
| Mean Plunge: | 16 | 16 | N | 310 |
| Vector Magnitude: | 346 | 346 | 67 |  |
| Mean length of resulting vector: | 0.996 | 0.996 | 346 |  |

3- Misfits.

All 11 P first motions agreed with the solution.
Out of 7 sH first motions, a total of 1 did not fit the solutions (14/100).

| Station | Number | Percentage |
| :---: | :---: | :---: |
| Name of misfits | of wrongs |  |

4- Rating of the focal mechanism.

The solution has an $A$ rating based on the small number of $P$ and $S H$ misfits ( $0 / 100$ and $14 / 100$ respectively) and on the good constraints on the $P, T$ and $B$ axes (value of 0.997 ).



## Location Map



Earthquake of 199606241311 Magnitude 1.6MN

1- Earthquake information and list of first motions.

| DateTime <br> hhmm Ss | Latitude | Longitude | Depth <br> $(\mathrm{km})$ | Mag | Sta/Pha |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 960624 | 1311 | 16.55 | 47.4862 | -70.1239 | 14.36 |

COMMENTS:

CHARLEVOIX SEISMIC ZONE, QUE.
\$
\$ The Sg lines of some stations include the SH FM.
\$ The convention used is the Virginia Tech convention used in FOCMEC:
\$ <: SH first motion to left (back to event) impulsive
\$ >: SH first motion to right (back to event) impulsive
\$ Preliminary Focmec computed by ML.
\$ Time drift of station A81P is -0.07 sec
\$ Time drift of station A76P is 0.01 sec
\$ Time drift of station A82P is 0.03 sec
$\$$ Time drift of station A80p is -0.58 sec

| Sta | Pha | Dist <br> $(k m)$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | :---: | :---: | :---: |
| A16 | PG | 9 | 101 | -32 | C |
| A16 | SG | 9 | 101 | -32 | $<$ |
| A81P | PG | 14 | 265 | -44 | C |
| A81P | SG | 14 | 265 | -44 | < |
| LMQ | PG | 17 | 294 | -49 | D |
| A54 | PG | 22 | 261 | -57 | D |
| A54 | SG | 22 | 261 | -57 | < |
| A61 | PG | 23 | 6 | -58 | D |
| A61 | SG | 23 | 6 | -58 | $>$ |
| A82P | PG | 24 | 305 | -59 | D |
| A80P | PG | 31 | 286 | -65 | D |

Number of P first motions: 7 Number of SH first motions: 4

2- Most Representative Solution.
A total of 58 solutions were found using a b axis increment of 5 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

| dip, strike, rake | 55.15 | 46.37 | 83.90 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| dip, strike, rake | 35.31 | 236.96 | 98.67 | : auxiliary plane |  |
| lower hem. trend, plunge of | a, $n$ | 146.96 | 54.69 | 316.37 | 34.85 |

```
lower hem. trend & plunge of b 49.86 5.00
lower hem. trend, plunge of p,t 140.74 1, 9.96 293.56 78.83
```

Average $B, P$, and $T$ axes:

B

| Mean trend: | N | 58 | N | 150 | N |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Mean Plunge: | 16 | 6 | 71 |  |  |
| Vector Magnitude: | 56 | 57 | 55 |  |  |
| Mean length of resulting vector: | 0.958 |  | 0.975 | 0.947 |  |

3- Misfits.

All 7 P first motions agreed with the solution.
All 0 SH first motions agreed with the solution.

4- Rating of the focal mechanism.

The solution is rejected (rating $X$ ) based on the high number of $P$ and SH misfits ( $0 / 100$ and $0 / 100$ respectively) and the absence of constraints on the $P, T$ and $B$ axes (value of 0.960 ).




## Location Map



1- Earthquake information and list of first motions.

| Date Time | Latitude | Longitude | Depth <br> hhmm ss |  | Mag | Sta/Pha |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 960704 | 1227 | 07.48 | 47.6197 | -70.1352 | 5.28 | 2.0 MN |

COMMENTS:

CHARLEVOIX SEISMIC ZONE, QUE.
\$ triggered $A 80 \mathrm{P}$ and A 82 P ;
\$ A82P fm is uncertain.
\$ Time drift of station A82P is 0.00 sec
$\$$ Time drift of station A80P is -0.05 sec
\$ The Sg lines of some stations include the SH FM .
\$ The convention used is the Virginia Tech convention used in FOCMEC:
$\$<: S H$ first motion to left (back to event) impulsive
\$ >: SH first motion to right (back to event) impulsive
\$ Focmec computed by MI is poorly constrained.

| Sta | Pha | Dist <br> $(\mathrm{km})$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | ---: | :---: | :---: |
| A61 | PG | 9 | 23 | -59 | C |
| A61 | SG | 9 | 23 | -59 | $>$ |
| LMQ | PG | 16 | 241 | -72 | C |
| A82P | SG | 19 | 266 | -74 | $<$ |
| A16 | PG | 19 | 150 | -75 | D |
| A16 | SG | 19 | 150 | -75 | $<$ |
| A64 | PG | 29 | 38 | -80 | C |
| A64 | SG | 29 | 38 | -80 | $>$ |
| A80P | SG | 30 | 258 | -80 | $>$ |
| A21 | PG | 35 | 74 | -81 | C |

Number of $P$ first motions: 5
Number of SH first motions: 5
2- Rating of the solution.

The solution has an $X$ rating (rejected) due to the absence of constraints on the positions of the nodal planes.



## Location Map



Earthquake of 199607140715 Magnitude 2.2MN

1- Earthquake information and list of first motions.

| DateTime <br> hhmm ss | Latitude | Longitude | Depth <br> $(\mathrm{km})$ | Mag | Sta/Pha |  |
| :---: | :--- | :--- | :--- | ---: | :--- | ---: |
| 960714 | 0715 | 02.89 | 47.4829 | -70.0503 | 13.71 | 2.2 MN |

COMMENTS:

CHARLEVOIX SEISMIC ZONE, QUE.
20 km S from LA MALBAIE, QUE.
\$ 3 field stations triggered: A76P, A80P, and A58P.
\$ Time drift of station A58P is 0.09 sec
\$ Time drift of station A76P is -0.03 sec
$\$$ Time drift of station A80p is 0.09 sec
\$ The Sg lines of some stations include the SH FM.
\$ The convention used is the Virginia Tech convention used in FOCMEC:
\$ <: SH first motion to left (back to event) impulsive
\$ >: SH first motion to right (back to event) impulsive
\$ Preliminary Focmec computed by ML.

| Sta | Pha | Dist <br> $(\mathrm{km})$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | ---: | :---: | :---: |
| A16 | PG | 4 | 112 | -15 | C |
| A16 | SG | 4 | 112 | -15 | $>$ |
| A58P | PG | 13 | 291 | -44 | C |
| LMQ | PG | 22 | 289 | -58 | D |
| A76P | PG | 23 | 321 | -59 | D |
| A76P | SG | 23 | 321 | -59 | $>$ |
| A61 | PG | 24 | 353 | -60 | C |
| A61 | SG | 24 | 353 | -60 | $<$ |
| A54 | PG | 27 | 264 | -64 | D |
| A54 | SG | 27 | 264 | -64 | $>$ |
| A11 | PG | 29 | 203 | -65 | C |
| A21 | PG | 37 | 48 | -70 | D |
| A21 | SG | 37 | 48 | -70 | $<$ |
| A80P | PG | 37 | 284 | -70 | D |
| A80P | SG | 37 | 284 | -70 | $>$ |
| A64 | PG | 40 | 17 | -71 | C |
| A64 | SG | 40 | 17 | -71 | $>$ |
|  |  |  |  |  |  |
|  | Number of | P first motions: | 10 |  |  |
|  | Number of | SH first motions: | 7 |  |  |

2- Most Representative Solution.

A total of 442 solutions were found using a b axis increment of 1 degree. The
following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

| dip, strike, rake | 69.65 | 147.52 | 46.72 |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | ---: |
| dip, strike, rake | 46.96 | 37.25 | 151.58 | : auxiliary plane |  |  |
| lower hem. trend, plunge of $a, n$ | 307.25 | 43.04 | 57.52 | 20.35 |  |  |
| lower hem. trend \& plunge of $b$ | 165.65 | 40.00 |  |  |  |  |
| lower hem. trend, plunge of pot | 267.45 | 13.69 | 12.47 | 46.77 |  |  |

Average $B, P$, and $T$ axes:


All 10 P first motions agreed with the solution.
Out of 7 SH first motions, a total of 2 did not fit the solutions (28/100).

| Station Number | Percentage |
| :---: | :--- |
| Name of misfits of wrongs |  |


| A54 | 442 | 100 |
| :--- | :--- | :--- |
| A64 | 442 | 100 |

4- Rating of the focal mechanism.

The solution has an $A$ rating based on the small number of $P$ and $S H$ misfits ( $0 / 100$ and $28 / 100$ respectively) and on the good constraints on the $P, T$ and $B$ axes (value of 0.998 ).




## Location Map



Earthquake of 199607141846 Magnitude 3.4MN

1- Earthquake information and list of first motions.

| DateTime <br> hhmm ss | Latitude | Longitude | Depth <br> $(\mathrm{km})$ | Mag | Sta/Pha |  |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: |
| 960714 | 1846 | 49.22 | 47.6938 | -69.9927 | 7.26 | 3.4 MN |

## COMMENTS:

CHARLEVOIX SEISMIC ZONE, QUE.
13 km E from LA MALBAIE, QUE.
Felt in La Malbaie, Clermont, St-Irenee, St-Hilarion, St-Fidele, Pointe-au-Pic and Port-au-Saumon.
\$ Felt info from $M$. Bergeron
\$ Talked to radio station (418) 457-3333
$\$$ who had received calls from Clermont.
$\$$ No first motion readable on ICQ and TRQ.
$\$$ CIQ data from R. Du Berger, Chicoutimi.
\$ all phases were doubled-checked.
\$ Field data $X$-ed out due to large residuals.
\$ Time drift of station A76P is -0.03 sec
$\$$ Time drift of station A58P is 0.09 sec
$\$$ Time drift of station A82P is -0.38 sec
\$ Time drift of station A80P is 0.10 sec
\$ PASQ fm from smoker records.
\$ The Sg lines of some stations include the SH FM.
\$ The convention used is the Virginia Tech convention used in FOCMEC:
\$ <: SH first motion to left (back to event) impulsive \$ >: SH first motion to right (back to event) impulsive \$ Preliminary Focmec computed by ML.

| Sta | Pha | Dist <br> $(\mathrm{km})$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | ---: | :---: | :---: |
| A61 | PG | 7 | 269 | -45 | C |
| A61 | SG | 7 | 269 | -45 | $<$ |
| PASQ | PG | 8 | 25 | -47 | C |
| A64 | PG | 17 | 27 | -66 | D |
| A64 | SG | 17 | 27 | -66 | $>$ |
| A76P | PG | 20 | 253 | -70 | D |
| A76P | SG | 20 | 253 | -70 | $>$ |
| A21 | PG | 23 | 87 | -72 | D |
| A21 | SG | 23 | 87 | -72 | $>$ |
| A16 | PG | 25 | 182 | -74 | C |
| A16 | SG | 25 | 182 | -74 | $>$ |
| A58P | PG | 25 | 222 | -74 | D |
| A58P | SG | 25 | 222 | -74 | $>$ |
| LMQ | PG | 30 | 237 | -76 | D |
| A82P | PG | 31 | 252 | -77 | D |
| SHQ | PG | 32 | 252 | -77 | D |


| A54 | PG | 41 | 230 | -80 | D |
| :--- | ---: | ---: | ---: | ---: | ---: |
| A80P | PG | 42 | 250 | -80 | D |
| A11 | PG | 53 | 197 | -82 | D |
| RSFQ | PG | 61 | 226 | -83 | D |
| SLQ | PG | 74 | 92 | -84 | C |
| CIQ | PG | 88 | 318 | -85 | C |
| DAQ | PG | 98 | 288 | -86 | D |
| QCQ | PG | 141 | 224 | -87 | D |

Number of P first motions: 18 Number of SH first motions: 6

2- Most Representative Solution.
A total of 75 solutions were found using a baxis increment of 1 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

| dip, strike, rake | 23.86 | 323.61 | 43.72 |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| dip, strike, rake | 73.76 | 192.43 | 107.73 | : auxiliary plane |  |  |
| lower hem. trend, plunge of $\mathrm{a}, \mathrm{n}$ | 102.43 | 16.24 | 233.61 | 66.14 |  |  |
| lower hem. trend \& plunge of b | 7.33 | 17.00 |  |  |  |  |
| lower hem. trend, plunge of $\mathrm{p}, \mathrm{t}$ | 268.49 | 26.68 | 126.13 | 57.60 |  |  |

Average $B, P$, and $T$ axes:


The solution has an $A$ rating based on the small number of $P$ and $s H$ misfits ( $5 / 100$ and $42 / 100$ respectively) and on the good constraints on the $P$, $T$ and $B$ axes (value of 0.999 ).



## Location Map



Earthquake of 199607261438 Magnitude 2.3MN

1- Earthquake information and list of first motions.

| DateTime <br> hhmm ss | Latitude | Longitude | Depth <br> $(\mathrm{km})$ | Mag | Sta/Pha |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 960726 | 1438 | 45.14 | 47.6097 | -69.9468 | 10.36 | 2.3 MN |

COMMENTS:

CHARLEVOIX SEISMIC ZONE, QUE.
\$
\$ The Sg lines of some stations include the SH FM.
\$ The convention used is the Virginia Tech convention used in FOCMEC:
\$ <: SH first motion to left (back to event) impulsive
\$ >: SH first motion to right (back to event) impulsive
\$ Preliminary Focmec computed by ML.
\$ PASQ FM is from smoker record; No T.C. available.

| Sta | Pha | Dist <br> $(\mathrm{km})$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | ---: | :---: | ---: |
| A61 | PG | 14 | 311 | -54 | C |
| A61 | SG | 14 | 311 | -54 | $>$ |
| A16 | PG | 16 | 196 | -57 | D |
| A16 | SG | 16 | 196 | -57 | $>$ |
| PASQ | PG | 16 | 360 | -58 | D |
| A21 | SG | 22 | 62 | -65 | $>$ |
| A58P | PG | 22 | 245 | -65 | C |
| A76P | PG | 22 | 280 | -65 | C |
| A64 | PG | 24 | 10 | -67 | C |
| A64 | SG | 24 | 10 | -67 | $<$ |
| LMQ | PG | 29 | 257 | -71 | C |
| A82P | PG | 33 | 270 | -73 | D |
| A82P | SG | 33 | 270 | -73 | $>$ |
| A54 | PG | 39 | 244 | -75 | C |
| A54 | SG | 39 | 244 | -75 | $>$ |
| A80P | PG | 44 | 264 | -77 | D |
| A80P | SG | 44 | 264 | -77 | $>$ |
| DAQ | PG | 105 | 293 | -84 | D |
|  |  |  |  |  |  |
|  | Number of | P first motions: | II |  |  |
|  | Number of | SH first motions: | 7 |  |  |

2- Most Representative Solution.
A total of 259 solutions were found using a b axis increment of 1 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

| dip, strike, rake | 28.76 | 310.41 | -38.86 |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| dip, strike, rake | 72.43 | 75.64 | -113.14 | : auxiliary plane |  |  |
| lower hem. trend, plunge of $\mathrm{a}, \mathrm{n}$ | 345.64 | 17.57 | 220.41 | 61.24 |  |  |
| lower hem. trend \& plunge of b | 82.99 | 22.00 |  |  |  |  |
| lower hem. trend, plunge of $\mathrm{p}, \mathrm{t}$ | 315.47 | 56.44 | 183.35 | 23.98 |  |  |

Average $B, P$, and $T$ axes:


.207



## Location Map



Lぃـ1
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Earthquake of 199608191706 Magnitude 2.1MN

1- Earthquake information and list of first motions.

| Date | Time |  | Latitude | Longitude | Depth | Mag | Sta/Pha |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | hhmm |  |  |  | (km) |  |  |
| 960819 | 1706 | 09.66 | 47.3002 | -70.2448 | 6.44 | 2.1MN | 11/022 |

COMMENTS:
CHARLEVOIX SEISMIC ZONE, QUE.
24 km SE from BAIE-SAINT-PAUL, QUE.
\$ al1 dead.
\$
\$ The Sg lines of some stations include the SH FM.
\$ The convention used is the Virginia Tech convention used in FOCMEC:
\$ <: SH first motion to left (back to event) impulsive
\$ >: SH first motion to right (back to event) impulsive
\$ Focmec computed by ML is poorly constrained.

| Sta | Pha | Dist <br> $(k m)$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | ---: | :---: | :---: |
| A84P | PG | 21 | 348 | -73 | C |
| A54 | PG | 22 | 324 | -73 | D |
| RSFQ | PG | 24 | 272 | -75 | D |
| A58P | PG | 25 | 6 | -76 | C |
| A58P | SG | 25 | 6 | -76 | < |
| A16 | PG | 26 | 43 | -76 | C |
| A16 | SG | 26 | 43 | -76 | < |
| A82P | PG | 36 | 343 | -80 | D |
| A80P | PG | 36 | 324 | -80 | D |
| A80P | SG | 36 | 324 | -80 | < |
| A76P | PG | 38 | 0 | -80 | D |
| A61 | PG | 45 | 15 | -82 | D |
| A21 | PG | 61 | 43 | -84 | C |
| DAQ | PG | 105 | 315 | -86 | D |

Number of $P$ first motions: 11
Number of SH first motions: 3

2- Most Representative Solution.
A total of 902 solutions were found using a b axis increment of 1 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

| dip,strike, rake | 21.56 | 37.35 | 76.28 |  |
| :--- | ---: | ---: | ---: | ---: |
| dip,strike, rake | 69.08 | 232.06 | 95.35 | : auxiliary plane |

```
lower hem. trend, plunge of a,n 142.06 20.92 307.35 68.44
lower hem. trend & plunge of b
50.14 5.00
lower hem. trend, plunge of p,t 
```

Average $B, P$, and $T$ axes:

|  | B | P | T |  |
| :--- | :--- | :--- | :--- | ---: |
| Mean trend: | N | 94 | N | 83 |
| Mean Plunge: | 14 | N | 209 |  |
| Vector Magnitude: | 803 | 17 | 58 |  |
| Mean length of resulting vector: | 0.890 | 261 | 860 |  |
| 3- Misfits. |  | 0.289 | 0.954 |  |

All 11 P first motions agreed with the solution.
Out of 3 SH first motions, a total of 2 did not fit the solutions (66/100).

| Station <br> Name | Number <br> of misfits | Percentage <br> of wrongs |
| :---: | :---: | :---: |
| A16 | 651 | 72 |
| A58P | 902 | 100 |
| A80P | 251 | 27 |

4- Rating of the focal mechanism.

The solution is rejected (rating $X$ ) based on the high number of $P$ and sH misfits ( $0 / 100$ and $66 / 100$ respectively) and the absence of constraints on the $P, T$ and $B$ axes (value of 0.711 ).



1- Earthquake information and list of first motions.

| Date | Time hhmm |  | Latitude | Longitude | Depth (km) | Mag | Sta/Pha |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 960913 | 2355 | 35.92 | 47.5008 | -70.2134 | 12.09 | 2. 2 MN | 11/022 |

## COMMENTS:

CHARLEVOIX SEISMIC ZONE, QUE.
\$ All down.
\$
\$ The Sg lines of some stations include the SH FM.
\$ The convention used is the Virginia Tech convention used in FOCMEC:
$\$<: S H$ first motion to left (back to event) impulsive
\$ >: SH first motion to right (back to event) impulsive
\$ Preliminary Focmec computed by ML.

| Sta | Pha | Dist <br> $(\mathrm{km})$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | ---: | :---: | :---: |
| A58P | PG | 3 | 1 | -13 | C |
| A58P | SG | 3 | 1 | -13 | $<$ |
| A84P | PG | 7 | 252 | -30 | D |
| A84P | SG | 7 | 252 | -30 | $<$ |
| LMQ | PG | 10 | 302 | -40 | D |
| LMQ | SG | 10 | 302 | -40 | $<$ |
| A54 | PG | 16 | 252 | -53 | D |
| A54 | SG | 16 | 252 | -53 | $<$ |
| A16 | PG | 16 | 102 | -53 | C |
| A16 | SG | 16 | 102 | -53 | $<$ |
| A82P | PG | 18 | 313 | -56 | D |
| A82P | SG | 18 | 313 | -56 | $<$ |
| A61 | SG | 23 | 23 | -63 | $<$ |
| A80P | PG | 24 | 287 | -64 | D |
| A80P | SG | 24 | 287 | -64 | < |
| A52P | PG | 25 | 251 | -64 | D |
| A52P | SG | 25 | 251 | -64 | $<$ |
| A21 | PG | 45 | 60 | -75 | C |

Number of P first motions: 9
Number of SH first motions: 9

2- Most Representative Solution.
A total of 843 solutions were found using a b axis increment of 2 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

| dip, strike, rake | 74.80 | 32.72 | 71.32 |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| dip, strike, rake | 23.91 | 264.92 | 139.69 | : auxiliary plane |  |  |
| lower hem. trend, plunge of $\mathrm{a}, \mathrm{n}$ | 174.92 | 66.09 | 302.72 | 15.20 |  |  |
| lower hem. trend \& plunge of b | 37.78 | 18.00 |  |  |  |  |
| lower hem. trend, plunge of $\mathrm{p}, \mathrm{t}$ | 137.50 | 27.46 | 278.64 | 56.29 |  |  |

Average $B, P$, and $T$ axes:

|  | B |  |  | P | T |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mean trend: | N | 38 | N | 143 | N | 268 |
| Mean Plunge: |  | 29 |  | 26 |  | 49 |
| Vector Magnitude: |  | 829 |  | 836 |  | 830 |
| Mean length of resulting vector: |  | 0.983 |  | 0.992 |  | 0.985 |

All 9 P first motions agreed with the solution.
Out of 9 SH first motions, a total of 2 did not fit the solutions (22/100).

| Station <br> Name | Number <br> of misfits | Percentage <br> of wrongs |
| :---: | :---: | :---: |
| A58P | 843 | 100 |
| A61 | 843 | 100 |

4- Rating of the focal mechanism.
The solution has a $C$ rating based on the high number of $P$ and $S H$ misfits ( $0 / 100$ and $22 / 100$ respectively) and on the poor constraints on the $P, T$ and $B$ axes (value of 0.987).




## Location Map



```
Earthquake of 19960923 0526 Magnitude 2.2MN
```

1- Earthquake information and list of first motions.

| DateTime <br> hhmm ss | Latitude | Longitude | Depth <br> $(\mathrm{km})$ | Mag | Sta/Pha |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 960923 | 0526 | 54.22 | 47.6591 | -69.8932 | 14.04 | 2.2 MN |

COMMENTS:
CHARLEVOIX SEISMIC ZONE, QUE.
$\$$
\$ The Sg lines of some stations include the SH FM.
\$ The convention used is the Virginia Tech convention used in FOCMEC:
\$ <: SH first motion to left (back to event) impulsive
\$ >: SH first motion to right (back to event) impulsive
\$ Preliminary Focmec computed by ML.

| Sta | Pha | Dist <br> $(k m)$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | ---: | :---: | :---: |
| A61 | PG | 15 | 284 | -47 | D |
| A61 | SG | 15 | 284 | -47 | $>$ |
| A21 | PG | 16 | 72 | -49 | D |
| A21 | SG | 16 | 72 | -49 | $>$ |
| A64 | PG | 19 | 0 | -53 | D |
| A64 | SG | 19 | 0 | -53 | $>$ |
| A16 | PG | 23 | 202 | -58 | C |
| A16 | SG | 23 | 202 | -58 | $<$ |
| A76P | PG | 26 | 266 | -62 | D |
| A58P | PG | 28 | 238 | -64 | D |
| LMQ | PG | 35 | 250 | -68 | D |
| A84P | PG | 37 | 237 | -69 | D |
| A82P | PG | 37 | 262 | -70 | D |
| A82P | SG | 37 | 262 | -70 | $>$ |
| A54 | PG | 45 | 240 | -73 | D |
| A80P | PG | 49 | 258 | -74 | D |
| A80P | SG | 49 | 258 | -74 | $<$ |
| A11 | PG | 52 | 206 | -75 | $D$ |
| DAQ | PG | 107 | 289 | -82 | C |
|  |  |  |  |  |  |
|  | Number of | P first motions: | 13 |  |  |
|  | Number of | SH first motions: | 6 |  |  |

2- Most Representative Solution.
A total of 592 solutions were found using a b axis increment of 2 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

| dip, strike, rake | 78.56 | 102.59 | 44.87 |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| dip, strike, rake | 46.25 | 1.42 | 164.07 | : auxiliary plane |  |
| lower hem. trend, plunge of $a, n$ | 271.42 | 43.75 | 12.59 | 11.44 |  |
| lower hem. trend \& plunge of $b$ | 113.85 | 44.00 |  |  |  |
| lower hem. trend, plunge of $p, t$ | 224.91 | 20.41 | 332.44 | 38.99 |  |

Average $B, P$, and $T$ axes:

|  | B | P | T |  |
| :--- | ---: | ---: | ---: | ---: |
| Mean trend: | N | 117 | N | 230 |
| Mean Plunge: | 53 | 15 | N | 330 |
| Vector Magnitude: | 584 | 587 | 32 |  |
| Mean length of resulting vector: | 0.986 | 0.991 | 0.98 |  |

3- Misfits.

All 13 P first motions agreed with the solution.
Out of 6 sH first motions, a total of 2 did not fit the solutions (33/100).

| Station | Number | Percentage |
| :---: | :---: | :---: |
| Name of misfits | of wrongs |  |

4- Rating of the focal mechanism.

The solution has a $B$ rating based on the number of $P$ and $S H$ misfits ( $0 / 100$ and $33 / 100$ respectively) and on the constraints on the $P, T$ and $B$ axes (value of 0.988 ).



$$
19960923 \text { 05:26 U.T. }
$$





## Location Map



Earthquake of 199609240644 Magnitude 2.0MN

1- Earthquake information and list of first motions.

| Date | Time <br> hhmm SS | Latitude | Longitude | Depth <br> $(\mathrm{km})$ | Mag | Sta/Pha |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: |
| 960924 | 0644 | 45.55 | 47.5875 | -70.1451 | 21.40 | 2.0 MN |

## COMMENTS:

CHARLEVOIX SEISMIC ZONE, QUE.
\$
\$ The Sg lines of some stations include the SH FM.
\$ The convention used is the Virginia Tech convention used in FOCMEC:
\$ <: SH first motion to left (back to event) impulsive
\$ >: SH first motion to right (back to event) impulsive
\$ Focmec computed by ML is poorly constrained.

| Sta | Pha | Dist <br> $(k m)$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | ---: | :---: | :---: |
| A58P | PG | 9 | 216 | -22 | C |
| A76P | PG | 10 | 311 | -24 | D |
| A76P | SG | 10 | 311 | -24 | $>$ |
| A61 | PG | 12 | 19 | -30 | C |
| A61 | SG | 12 | 19 | -30 | $>$ |
| LMQ | PG | 14 | 252 | -34 | D |
| A16 | PG | 17 | 141 | -38 | C |
| A16 | SG | 17 | 141 | -38 | $>$ |
| A84P | PG | 17 | 225 | -38 | D |
| A84P | SG | 17 | 225 | -38 | $>$ |
| A82P | PG | 18 | 278 | -40 | D |
| A54 | PG | 25 | 234 | -49 | D |
| A54 | SG | 25 | 234 | -49 | $<$ |
| A80P | PG | 29 | 265 | -53 | D |
| A64 | PG | 33 | 35 | -57 | C |
| A64 | SG | 33 | 35 | -57 | $>$ |
| A21 | PG | 37 | 69 | -60 | D |
| A21 | SG | 37 | 69 | -60 | $>$ |
| RSFQ | PG | 44 | 226 | -64 | D |

Number of P first motions: 12 Number of SH first motions: 7

2- Most Representative Solution.
A total of 107 solutions were found using $a b$ axis increment of 1 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

| dip, strike, rake | 33.02 | 137.47 | 19.09 |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| dip, strike, rake | 79.73 | 31.30 | 121.56 | : auxiliary plane |  |  |
| lower hem. trend, plunge of $a, n$ | 301.30 | 10.27 | 47.47 | 56.98 |  |  |
| lower hem. trend \& plunge of b | 205.05 | 31.00 |  |  |  |  |
| lower hem. trend, plunge of p,t | 96.56 | 27.83 | 333.47 | 45.96 |  |  |

Average $B, P$, and $T$ axes:

|  | B | P | T |  |
| :--- | :---: | :---: | :---: | :---: |
| Mean trend: | N | 193 | N | 90 |
| Mean Plunge: | 28 | N | 326 |  |
| Vector Magnitude: | 106 | 107 | 52 |  |
| Mean length of resulting vector: | 0.994 | 0.997 | 107 |  |
| 3- Misfits. |  |  | 0.996 |  |

All 12 P first motions agreed with the solution.
Out of 7 SH first motions, a total of 2 did not fit the solutions (28/100).

| Station | Number <br> Name | Percentage <br> of misfits |
| :---: | :---: | :---: |
|  |  |  |
| A64 | 103 | 96 |
| A84P | 107 | 100 |

4- Rating of the focal mechanism.

The solution has an $A$ rating based on the small number of $P$ and $S H$ misfits ( $0 / 100$ and $28 / 100$ respectively) and on the good constraints on the $P$, $T$ and $B$ axes (value of 0.996 ).



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arnojer

## Location Map



Earthquake of 199609242341 Magnitude 3.1MN

1- Earthquake information and list of first motions.

| DateTime <br> hhmm ss | Latitude | Longitude | Depth <br> $(\mathrm{km})$ | Mag | Sta/Pha |  |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: |
| 960924 | 2341 | 02.88 | 47.5475 | -70.2417 | 12.83 | 3.1 MN |

COMMENTS:
Felt, CHARLEVOIX SEISMIC ZONE, QUE.
Felt in St-Irenee, St-Hilarion, La Malbaie, and Clermont.
\$ Felt info from local radio station.
\$ CIQ FM from R. Du Berger, Chicoutimi.
\$ QCQ FM is unclear.
\$
\$ The Sg lines of some stations include the SH FM .
\$ The convention used is the Virginia Tech convention used in FOCMEC:
\$ <: SH first motion to left (back to event) impulsive
\$ >: SH first motion to right (back to event) impulsive
\$ Preliminary Focmec computed by ML.
\$ SH FM not picked on: A11 and A21.

| Sta | Pha | Dist <br> $(k m)$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | ---: | ---: | ---: | ---: |
| A58P | PG | 3 | 139 | -14 | C |
| A58P | SG | 3 | 139 | -14 | $<$ |
| LMQ | PG | 6 | 271 | -26 | C |
| LMQ | SG | 6 | 271 | -26 | $>$ |
| A84P | PG | 9 | 211 | -34 | C |
| A84P | SG | 9 | 211 | -34 | $>$ |
| A76P | PG | 11 | 0 | -40 | C |
| A76P | SG | 11 | 0 | -40 | $>$ |
| SHQ | PG | 14 | 298 | -46 | C |
| A54 | PG | 16 | 232 | -52 | C |
| A54 | SG | 16 | 232 | -52 | $>$ |
| A16 | PG | 20 | 116 | -57 | D |
| A16 | SG | 20 | 116 | -57 | < |
| A61 | PG | 20 | 35 | -57 | C |
| A61 | SG | 20 | 35 | -57 | < |
| A80P | PG | 21 | 275 | -59 | C |
| A80P | SG | 21 | 275 | -59 | $>$ |
| A11 | PG | 34 | 174 | -69 | D |
| RSFQ | PG | 36 | 223 | -70 | $D$ |
| A64 | PG | 41 | 40 | -72 | D |
| A64 | SG | 41 | 40 | -72 | $<$ |
| A21 | PG | 45 | 67 | -74 | C |
| DAQ | PG | 88 | 302 | -82 | D |
| CIQ | PG | 90 | 333 | -82 | D |
| SLQ | PG | 94 | 81 | -82 | D |

```
Number of P first motions: 16
```

Number of SH first motions: 9

2- Most Representative Solution.

A total of 100 solutions were found using a $b$ axis increment of 1 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

| dip, strike, rake | 67.37 | 246.26 | 79.16 |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| dip, strike, rake | 24.97 | 92.73 | 114.29 | : auxiliary plane |  |  |
| lower hem. trend, plunge of $a, n$ | 2.73 | 65.03 | 156.26 | 22.63 |  |  |
| lower hem. trend \& plunge of $b$ | 250.48 | 10.00 |  |  |  |  |
| lower hem. trend, plunge of | p, $t$ | 344.49 | 21.65 | 137.22 | 65.94 |  |

Average $B, P$, and $T$ axes:

|  | B |  |  | P | T |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mean trend: | N | 250 | N | 343 | N | 142 |
| Mean Plunge: |  | 7 |  | 20 |  | 69 |
| Vector Magnitude: |  | 100 |  | 100 |  | 100 |
| Mean length of resulting vector: |  | 0.996 |  | 0.998 |  | 0.996 |

All 16 P first motions agreed with the solution.
Out of 9 SH first motions, a total of 2 did not fit the solutions (22/100).

| Station Number | Percentage |
| :---: | :--- |
| Name of misfits of wrongs |  |


| A61 | 25 | 25 |
| ---: | ---: | ---: |
| A64 | 100 | 100 |
| A76P | 75 | 75 |

4- Rating of the focal mechanism.

The solution has an $A$ rating based on the small number of $P$ and $S H$ misfits ( $0 / 100$ and $22 / 100$ respectively) and on the good constraints on the $P, T$ and $B$ axes (value of 0.996 ).




## Location Map



1- Earthquake information and list of first motions.

| Date | Time <br> hhmm ss | Latitude | Longitude | Depth <br> $(\mathrm{km})$ | Mag | Sta/Pha |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 960925 | 0834 | 24.87 | 47.8528 | -69.7504 | 22.35 | 2.2 MN |

COMMENTS:

CHARLEVOIX SEISMIC ZONE, QUE.
\$
\$ The Sg lines of some stations include the SH FM.
\$ The convention used is the Virginia Tech convention used in FOCMEC:
\$ <: SH first motion to left (back to event) impulsive
\$ >: SH first motion to right (back to event) impulsive
\$ Preliminary Focmec computed by ML.
\$ slightly outside the network.
\$ Not an aftershock of 960924.2341

| Sta | Pha | Dist <br> $(k m)$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | :---: | :---: | :---: |
| A64 | PG | 11 | 254 | -26 | C |
| A64 | SG | 11 | 254 | -26 | < |
| A21 | PG | 17 | 165 | -38 | C |
| A21 | SG | 17 | 165 | -38 | < |
| A61 | PG | 31 | 235 | -54 | C |
| A61 | SG | 31 | 235 | -54 | < |
| A16 | PG | 47 | 204 | -64 | C |
| A16 | SG | 47 | 204 | -64 | < |
| A58P | PG | 50 | 224 | -66 | C |
| LMQ | PG | 55 | 232 | -68 | C |
| A84P | PG | 59 | 225 | -69 | D |
| DAQ | PG | 112 | 277 | -79 | D |

Number of $P$ first motions: 8 Number of SH first motions: 4

2- Most Representative Solution.

A total of 589 solutions were found using a b axis increment of 1 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

| dip, strike, rake | 69.48 | 79.30 | 77.17 |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| dip, strike, rake | 24.05 | 292.30 | 120.67 | : auxiliary plane |  |  |
| lower hem. trend, plunge of | $a, n$ | 202.30 | 65.95 | 349.30 | 20.52 |  |
| lower hem. trend \& plunge of $b$ | 83.86 | 12.00 |  |  |  |  |

```
lower hem. trend, plunge of p,t 179.15 23.44 328.83 63.33
```

Average $B, P$, and $T$ axes:

|  | B | P | T |  |
| :--- | :---: | :---: | :---: | ---: |
| Mean trend: | N | 79 | N | 177 |
| Mean Plunge: | 16 | N | 321 |  |
| Vector Magnitude: | 573 | 579 | 59 |  |
| Mean length of resulting vector: | 0.973 | 0.984 | 582 |  |
| 3- Misfits. |  |  | 0.987 |  |

All 8 P first motions agreed with the solution.
All 0 SH first motions agreed with the solution.

4- Rating of the focal mechanism.

The solution has a $C$ rating based on the high number of $P$ and $S H$ misfits ( $0 / 100$ and $0 / 100$ respectively) and on the poor constraints on the $P, T$ and $B$ axes (value of 0.981 ).




## Location Map



Earthquake of 199610110228 Magnitude 1.9MN

1- Earthquake information and list of first motions.

| DateTime <br> hhmm SS | Latitude | Longitude | Depth <br> $(\mathrm{km})$ | Mag | Sta/Pha |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 961011 | 0228 | 50.34 | 47.4761 | -70.0551 | 15.56 | 1.9 MN |

COMMENTS :

CHARLEVOIX SEISMIC ZONE, QUE.
\$ S-P conversion on A21?
\$
\$ The Sg lines of some stations include the SH FM.
\$ The convention used is the Virginia Tech convention used in FOCMEC:
$\$<: S H$ first motion to left (back to event) impulsive
\$ >: SH first motion to right (back to event) impulsive
\$ Preliminary Focmec computed by ML.

| Sta | Pha | Dist <br> $(\mathrm{km})$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | ---: | :---: | :---: |
| A16 | PG | 4 | 99 | -14 | C |
| A16 | SG | 4 | 99 | -14 | $<$ |
| A58P | PG | 13 | 295 | -40 | C |
| A84P | PG | 19 | 272 | -50 | C |
| A84P | SG | 19 | 272 | -50 | $<$ |
| LMQ | PG | 22 | 292 | -55 | C |
| A76P | PG | 23 | 323 | -56 | C |
| A76P | SG | 23 | 323 | -56 | $>$ |
| A61 | PG | 24 | 354 | -57 | C |
| A54 | PG | 27 | 266 | -60 | C |
| A82P | PG | 29 | 301 | -62 | D |
| A82P | SG | 29 | 301 | -62 | $>$ |
|  |  |  |  |  |  |
|  | Number of | Pirst motions: | 8 |  |  |
|  | Number of | SH first motions: | 4 |  |  |

2- Most Representative Solution.
A total of 173 solutions were found using a b axis increment of 2 degree. The following parameters describe the most representative solution, which was derived from the average B, P, and $T$ axes listed below.

| dip, strike, rake | 28.58 | 24.98 |  | 77.38 |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| dip, strike, rake | 62.17 | 219.28 | 96.79 | : auxiliary plane |  |  |
| lower hem. trend, plunge of $\mathrm{a}, \mathrm{n}$ | 129.28 | 27.83 | 294.98 | 61.42 |  |  |
| lower hem. trend \& plunge of b | 36.10 | 6.00 |  |  |  |  |
| lower hem. trend, plunge of $p, t$ | 304.27 | 16.90 | 144.98 | 72.00 |  |  |

Average $B, P$, and $T$ axes:

|  | B |  | p |  | T |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Mean trend: N | N 30 | N | 299 | N | 135 |
| Mean Plunge: | 4 |  | 15 |  | 76 |
| Vector Magnitude: | 169 |  | 171 |  | 171 |
| Mean length of resulting vector: | 0.979 |  | 0.988 |  | 0.990 |
| 3- Misfits. |  |  |  |  |  |
| All 8 P first motions agreed with the solution. |  |  |  |  |  |
| All 4 SH first motions agreed with the solution. |  |  |  |  |  |
| 4- Rating of the focal mechanism. |  |  |  |  |  |
| The solution has a $C$ rating based on the high number of $P$ and SH misfits |  |  |  |  |  |
| ( $0 / 100$ and $0 / 100$ respectively) and on the poor constraints on the p |  |  |  |  |  |




## Location Map



Earthquake of 199610250947 Magnitude 2.2MN

1- Earthquake information and list of first motions.

| DateTime <br> hhmm SS | Latitude | Longitude | Depth <br> $(\mathrm{km})$ | Mag | Sta/Pha |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 9610250947 | 24.43 | 47.4281 | -70.3887 | 4.06 | 2.2 MN | $13 / 025$ |

COMMENTS:

CHARLEVOIX SEISMIC ZONE, QUE.
$\$ \mathrm{fm}$ unclear on A64. \$ RSFQ was taken out the previous day. \$ \$ The Sg lines of some stations include the SH FM. \$ The convention used is the virginia Tech convention used in FOCMEC: \$ <: SH first motion to left (back to event) impulsive \$ >: SH first motion to right (back to event) impulsive \$ Preliminary Focmec computed by ML.

| Sta | Pha | Dist <br> $(\mathrm{km})$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | ---: | :---: | ---: |
| A54 | PG | 4 | 331 | -42 | C |
| A54 | SG | 4 | 331 | -42 | $<$ |
| A84P | PG | 9 | 48 | -65 | D |
| A84P | SG | 9 | 48 | -65 | $>$ |
| A52P | PG | 10 | 269 | -68 | D |
| A52P | SG | 10 | 269 | -68 | $>$ |
| LMQ | PG | 14 | 19 | -74 | D |
| A58P | PG | 17 | 51 | -77 | D |
| A58P | SG | 17 | 51 | -77 | $<$ |
| A80P | PG | 18 | 326 | -78 | C |
| A80P | SG | 18 | 326 | -78 | $<$ |
| A82P | PG | 20 | 1 | -79 | C |
| A82P | SG | 20 | 1 | -79 | $>$ |
| A11 | PG | 25 | 145 | -81 | C |
| A76P | PG | 26 | 25 | -81 | D |
| A76P | SG | 26 | 25 | -81 | $<$ |
| A16 | SG | 29 | 81 | -82 | $>$ |
| A61 | PG | 37 | 37 | -84 | D |
| A64 | SG | 58 | 40 | -86 | $>$ |
| A21 | PG | 61 | 60 | -86 | D |
| DAQ | PG | 88 | 313 | -87 | C |
| SLQ | PG | 107 | 75 | -88 | C |

Number of p first motions: 13 Number of SH first motions: 9

2- Most Representative Solution.

A total of 60 solutions were found using a b axis increment of 2 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

| dip, strike, rake | 49.94 | 71.26 | -29.04 |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| dip, strike, rake | 68.19 | 180.93 | -136.11 | : auxiliary plane |  |  |
| lower hem. trend, plunge of $a, n$ | 90.93 | 21.81 | 341.26 | 40.06 |  |  |
| lower hem. trend \& plunge of b | 202.05 | 42.00 |  |  |  |  |
| lower hem. trend, plunge of $p, t$ | 43.88 | 45.88 | 302.22 | 11.09 |  |  |

Average $B, P$, and $T$ axes:
B P T

| Mean trend: | N | 205 | N |
| :--- | :---: | :---: | :---: |
| Mean plunge: | 45 | 44 | N |
| Vector Magnitude: | 60 | 43 | 9 |
| Mean length of resulting vector: | 0.996 | 60 | 60 |
|  |  | 0.998 | 0.998 |
| 3- Misfits. |  |  |  |

All 13 p first motions agreed with the solution.
Out of 9 sH first motions, a total of 3 did not fit the solutions (33/100).
Station Number Percentage
Name of misfits of wrongs

| A54 | 56 | 93 |
| ---: | ---: | ---: |
| A58P | 60 | 100 |
| A82P | 60 | 100 |

4- Rating of the focal mechanism.
The solution has an $A$ rating based on the small number of $P$ and $S H$ misfits ( $0 / 100$ and $33 / 100$ respectively) and on the good constraints on the $P, T$ and B axes (value of 0.997).




## Location Map



Earthquake of 199610280245 Magnitude 2.3MN

1- Earthquake information and list of first motions.

| Date | Time <br> hhmm | Latitude | Longitude | Depth <br> $(\mathrm{km})$ | Mag | Sta/Pha |
| :---: | :---: | :---: | :---: | ---: | :---: | ---: |
| 961028 | 0245 | 39.23 | 47.5536 | -70.0414 | 11.56 | 2.3 MN |

COMMENTS:

CHARLEVOIX SEISMIC ZONE, QUE.
\$
\$ The Sg lines of some stations include the SH FM .
\$ The convention used is the Virginia Tech convention used in FOCMEC:
\$ <: SH first motion to left (back to event) impulsive
\$ >: SH first motion to right (back to event) impulsive
\$ Preliminary Focmec computed by ML.

| Sta | Pha | Dist <br> (km) | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | ---: | :---: | ---: |
| A16 | PG | 10 | 164 | -40 | D |
| A16 | SG | 10 | 164 | -40 | $>$ |
| A58P | PG | 13 | 256 | -49 | C |
| A58P | SG | 13 | 256 | -49 | $>$ |
| A61 | PG | 16 | 347 | -54 | C |
| A61 | SG | 16 | 347 | -54 | $>$ |
| A76P | PG | 18 | 304 | -57 | C |
| A76P | SG | 18 | 304 | -57 | $>$ |
| A84P | PG | 21 | 248 | -61 | C |
| A84P | SG | 21 | 248 | -61 | $<$ |
| LMQ | PG | 22 | 268 | -62 | C |
| LMQ | SG | 22 | 268 | -62 | $>$ |
| A82P | PG | 27 | 284 | -67 | C |
| A82P | SG | 27 | 284 | -67 | $>$ |
| A54 | PG | 30 | 249 | -69 | C |
| A54 | SG | 30 | 249 | -69 | $>$ |
| A21 | PG | 31 | 58 | -70 | C |
| A64 | PG | 32 | 20 | -70 | C |
| A80P | PG | 36 | 272 | -72 | D |
| A80P | SG | 36 | 272 | -72 | $<$ |
| A11 | PG | 37 | 199 | -72 | D |
|  |  |  |  |  |  |
|  | Number of | Pirst motions: | 12 |  |  |
|  | Number of | SH first motions: | 9 |  |  |

2- Most Representative Solution.

A total of 96 solutions were found using a b axis increment of 2 degree. The
following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

| dip, strike, rake | 23.20 | 9.81 | 29.74 |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| dip, strike, rake | 78.73 | 252.11 | 110.41 | : auxiliary plane |  |
| lower hem. trend, plunge of $\mathrm{a}, \mathrm{n}$ | 162.11 | 11.27 | 279.81 | 66.80 |  |
| lower hem. trend \& plunge of b | 67.95 | 20.00 |  |  |  |
| lower hem. trend, plunge of $\mathrm{p}, \mathrm{t}$ | 325.43 | 30.78 | 185.73 | 52.01 |  |

Average $B, P$, and $T$ axes:
B P T

| Mean trend: | N | 61 | N |
| :--- | :---: | :---: | :---: |
| Mean Plunge: |  | 321 | N |
| Vector Magnitude: | 95 | 32 | 54 |
| Mean length of resulting vector: | 0.995 | 96 | 96 |
|  |  | 0.997 | 0.996 |
| 3- Misfits. |  |  |  |

All 12 p first motions agreed with the solution.
Out of 9 SH first motions, a total of 1 did not fit the solutions (11/100).

| Station <br> Name | Number <br> of misfits | Percentage <br> of wrongs |
| :---: | :---: | :---: |
| A84P | 96 | 100 |

4- Rating of the focal mechanism.

The solution has an $A$ rating based on the small number of $P$ and $S H$ misfits ( $0 / 100$ and $11 / 100$ respectively) and on the good constraints on the $P$, $T$ and $B$ axes (value of 0.996 ).



## Location Map



Appendix 3: Additional information on the 1974 and 1979 mechanisms.

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Earthquake of 197406092324 Magnitude 0.6ML

1- Earthquake information and list of first motions.

| Date | Time <br> hhmm ss | Latitude | Longitude | Depth <br> $(\mathrm{km})$ | Mag | Sta/Pha |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 740609 | 2324 | 30.82 | 47.3431 | -70.2393 | 10.12 | 0.6 ML |

COMMENTS:

CHARLEVOIX SEISMIC ZONE, QUE.
Data from the 1974 Charlevoix Field experiment.
See paper: Leblanc and Buchbinder (1977) for details.
\$Leblanc and Buchbinder (1977): Second Micro-earthquake survey of the
$\$ S t$. Lawrence Valley near La Malbaie, Quebec. C.J.E.S. 14, no. 2, 2778-2789.
\$Note: Time in Leblanc and Buchbinder (1977) is in Eastern Standard Time.
SSolution of Leblanc and Buchbinder (1977):
$\$ 197406091824 \quad 30.800 \mathrm{~L} \quad 47.342 \quad-70.240 \quad 10.00 \mathrm{~km} 0.6 \mathrm{ML} \quad \mathrm{Z}$
\$Focal mechanism computed; published in Leblanc and Buchbiner (1977) and
\$redone in Adams, Vonk, Pittman, and Vatcher (1988).
\$No Phase data for $P$ A68 SZ .
\$Entered in dbase in February 1996 by Maurice Lamontagne.

| Sta | Pha | Dist <br> $(k m)$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | ---: | :---: | :---: |
| A12 | PG | 9 | 106 | -43 | D |
| A10 | PG | 11 | 162 | -48 | C |
| A14 | PG | 15 | 81 | -56 | D |
| A54 | PG | 18 | 314 | -61 | D |
| A58 | PG | 20 | 6 | -64 | C |
| A30 | PG | 23 | 92 | -66 | D |
| A16 | PG | 23 | 51 | -66 | D |
| A56 | PG | 24 | 344 | -67 | C |
| A76 | PG | 33 | 360 | -73 | C |
| A60 | PG | 40 | 16 | -76 | C |
| A62 | PG | 49 | 21 | -78 | D |
| A66 | PG | 81 | 23 | -83 | C |
|  |  |  |  |  |  |
|  | Number of | Pirst motions: | 12 |  |  |
|  | Number of | SH first motions: | 0 |  |  |

2- Most Representative Solution.

A total of 29 solutions were found using a b axis increment of 2 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

$$
\text { dip,strike,rake } \quad 67.59 \quad 137.60 \quad 41.29
$$

| dip, strike, rake | 52.41 | 29.09 | 151.24 | : auxiliary plane |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | ---: |
| lower hem. trend, plunge of $a, n$ | 299.09 | 37.59 | 47.60 | 22.41 |  |  |
| lower hem. trend \& plunge of b | 161.06 | 44.00 |  |  |  |  |
| lower hem. trend, plunge of $p, t$ | 260.17 | 9.31 | 359.45 | 44.50 |  |  |

Average $B, P$, and $T$ axes:

|  | B | P | T |  |
| :--- | :---: | :---: | :---: | :---: |
| Mean trend: | N | 159 | N | 259 |
| Mean Plunge: | 47 | N | 356 |  |
| Vector Magnitude: | 29 | 10 | 41 |  |
| Mean length of resulting vector: | 0.991 | 0.996 | 27 |  |
| 3- Misfits. |  |  | 0.924 |  |

All 12 P first motions agreed with the solution. 4- Rating of the focal mechanism.

The solution is rejected (rating $X$ ) based on the high number of $P$ misfits ( $0 / 100$ ) and the absence of constraints on the $P, T$ and $B$ axes (value of 0.970).

Earthquake of 197406201836 Magnitude 1.5ML

1- Earthquake information and list of first motions.

| Date | Time hhmm | ss | Latitude | Longitude | Depth <br> (km) | Mag | Sta/Pha |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 740620 | 1836 | 57.48 | 47.4041 | -70.1802 | 17.30 | 1.5ML | 18/022 |

COMMENTS:

CHARLEVOIX SEISMIC ZONE, QUE.
Data from the 1974 Charlevoix Field experiment.
See paper: Leblanc and Buchbinder (1977) for details.
\$Leblanc and Buchbinder (1977): Second Micro-earthquake survey of the \$St. Lawrence Valley near La Malbaie, Quebec. C.J.E.S. 14, no. 2, 2778-2789. \$Note: Time in Leblanc and Buchbinder (1977) is in Eastern Standard Time. \$Solution of Leblanc and Buchbinder (1977):
$\$ 19740620133656.500 \mathrm{~L} \quad 47.4050-70.180016 .90 \mathrm{~km} 1.70 \mathrm{ML}$
\$Focal mechanism computed; published in Leblanc and Buchbiner (1977). \$Entered in dbase in February 1996 by Maurice Lamontagne.


| Sta | Pha | Dist <br> $(\mathrm{km})$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | ---: | :---: | :---: |
| A12 | PG | 10 | 154 | -31 | C |
| A14 | PG | 11 | 113 | -33 | C |
| A58 | PG | 14 | 350 | -38 | D |
| A16 | PG | 15 | 60 | -41 | D |
| A10 | PG | 18 | 183 | -46 | C |
| A54 | PG | 18 | 288 | -47 | D |
| A30 | PG | 20 | 113 | -49 | D |
| A56 | PG | 20 | 326 | -49 | D |
| A52 | PG | 26 | 276 | -56 | D |
| A76 | PG | 27 | 350 | -57 | D |
| A18 | PG | 27 | 62 | -57 | D |
| A60 | PG | 33 | 12 | -62 | D |
| A74 | PG | 33 | 320 | -62 | C |
| A62 | PG | 41 | 18 | -67 | D |
| A20 | PG | 50 | 48 | -71 | D |
| A64 | PG | 52 | 25 | -72 | D |
| A66 | PG | 73 | 22 | -77 | C |
| A22 | PG | 86 | 41 | -79 | D |
| A68 | PG | 98 | 22 | -80 | C |

Number of P first motions: 19 Number of SH first motions: 0

2- Most Representative Solution.

A total of 230 solutions were found using $a b$ axis increment of 2 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

| dip, strike, rake | 67.53 | 277.85 | -68.28 |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| dip, strike, rake | 30.86 | 51.66 | -131.82 | : auxiliary plane |  |  |
| lower hem. trend, plunge of $a, n$ | 321.66 | 59.14 | 187.85 | 22.47 |  |  |
| lower hem. trend \& plunge of b | 89.19 | 20.00 |  |  |  |  |
| lower hem. trend, plunge of p,t | 220.89 | 61.32 | 351.71 | 19.68 |  |  |

Average $B, P$, and $T$ axes:
B P T

| Mean trend: | N | 83 | N | 220 |
| :--- | :---: | :---: | :---: | :---: |
| Mean Plunge: | 20 | 64 | N | 346 |
| Vector Magnitude: | 220 | 224 | 19 |  |
| Mean length of resulting vector: | 0.955 | 0.972 | 216 |  |

3- Misfits.

Out of 19 P first motions, one did not fit the solutions (5/100)
Station Number Percentage
Name of misfits of wrongs

| A14 | 196 | 85 |
| ---: | ---: | ---: |
| A30 | 33 | 14 |
| A76 | 1 | 0 |

4- Rating of the focal mechanism.
The solution is rejected (rating $X$ ) based on the high number of P misfits ( $5 / 100$ ) and the absence of constraints on the $P, T$ and $B$ axes (value of 0.956 ).

Earthquake of 197406231406 Magnitude 0.4 ML

1- Earthquake information and list of first motions.

| DateTime <br> hhmm ss | Latitude | Longitude | Depth <br> $(\mathrm{km})$ | Mag | Sta/Pha |  |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: |
| 740623 | 1406 | 57.40 | 47.5127 | -70.2144 | 14.95 | 0.4 ML |

## COMMENTS:

CHARLEVOIX SEISMIC ZONE, QUE.
Data from the 1974 Charlevoix Field experiment.
See paper: Leblanc and Buchbinder (1977) for details.
\$Leblanc and Buchbinder (1977): Second Micro-earthquake survey of the
$\$$ St. Lawrence Valley near La Malbaie, Quebec. C.J.E.S. 14, no. 2, 2778-2789.
\$Note: Time in Leblanc and Buchbinder (1977) is in Eastern Standard Time.
SSolution of Leblanc and Buchbinder (1977):
$\$ 19740623090657.400 \mathrm{~L} \quad 47.5133-70.215014 .80 \mathrm{~km} 0.50 \mathrm{ML}$
\$Focal mechanism computed; published in Leblanc and Buchbinder (1977), \$ redone in Adams, Vonk, Pittman, and Vatcher (1988).
\$Entered in dbase in February 1996 by Maurice Lamontagne.

| Sta | Pha | Dist <br> $(k m)$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | ---: | :---: | :---: |
| A58 | PG | 1 | 4 | -5 | C |
| A56 | PG | 9 | 296 | -32 | C |
| A76 | PG | 15 | 352 | -44 | C |
| A54 | PG | 16 | 247 | -47 | C |
| A16 | PG | 16 | 107 | -48 | C |
| A14 | PG | 21 | 142 | -55 | D |
| A52 | PG | 25 | 248 | -59 | C |
| A18 | PG | 26 | 88 | -60 | D |
| A30 | PG | 29 | 134 | -62 | D |
| A62 | PG | 31 | 30 | -64 | C |
| A66 | PG | 63 | 28 | -77 | D |
| A22 | PG | 79 | 48 | -79 | C |

Number of P first motions: 12 Number of $S H$ first motions: 0

2- Most Representative Solution.
A total of 125 solutions were found using a b axis increment of 2 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

```
dip,strike,rake 44.14 222.50 84.25
dip,strike,rake 46.13 50.48 95.55 :auxiliary plane
```

| lower hem. trend, plunge of $a, n$ | 320.48 | 43.87 | 132.50 | 45.86 |
| :--- | :--- | :---: | :---: | :---: | :---: |
| lower hem. trend \& plunge of $b$ | 226.63 | 4.00 |  |  |
| lower hem. trend, plunge of $p, t$ | 136.56 | 1.00 | 32.58 | 85.88 |

Average $B, P$, and $T$ axes:

|  | B |  |  | P | T |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mean trend: | N | 228 | N | 138 | N | 352 |
| Mean Plunge: |  | 1 |  | 1 |  | 89 |
| Vector Magnitude: |  | 124 |  | 124 |  | 125 |
| Mean length of resulting vector: |  | 0.994 |  | 0.994 |  | 0.997 |

3- Misfits.

All 12 P first motions agreed with the solution.
4- Rating of the focal mechanism.
The solution has an $A$ rating based on the small number of $p$ misfits ( $0 / 100$ ) and on the good constraints on the $P, T$ and $B$ axes (value of 0.995).

Earthquake of 197406301655 Magnitude 2.0ML

1- Earthquake information and list of first motions.

| Date | Time | Latitude | Longitude | Depth <br> hhmm ss |  | Mag |
| :---: | :--- | ---: | ---: | ---: | ---: | ---: |$\quad$ Sta/Pha

COMMENTS:

CHARLEVOIX SEISMIC ZONE, QUE.
Data from the 1974 Charlevoix Field experiment. See paper: Leblanc and Buchbinder (1977) for details. \$Leblanc and Buchbinder (1977): Second Micro-earthquake survey of the \$St. Lawrence Valley near La Malbaie, Quebec. C.J.E.S. 14, no. 2, 2778-2789. SSolution of Leblanc and Buchbinder (1977): \$Note: Time in Leblanc and Buchbinder (1977) is in Eastern Standard Time. Earthquake of $\$ \mathrm{~S} 19740630$ Magnitude 15.20 km

1- Earthquake information and list of first motions.

| Date | Time <br> hhmm ss | Latitude | Longitude | Depth <br> $(\mathrm{km})$ | Mag | Sta/Pha |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 19740 | 30155.11 | 47.7 | $150-69.8$ | 00150 km 2.0 M | $5 / 197$ |  |

\$Focal mechanism computed; published in Leblanc and Buchbinder (1977) and \$Entered in dbase in February 1996 by Maurice Lamontagne.

| Sta | Pha | Dist <br> $(k m)$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | ---: | :---: | :---: |
| A20 | PG | 11 | 95 | -36 | C |
| A64 | PG | 13 | 343 | -40 | C |
| A62 | PG | 13 | 288 | -40 | D |
| A60 | PG | 19 | 262 | -51 | D |
| A18 | PG | 22 | 184 | -55 | C |
| A16 | PG | 30 | 205 | -63 | C |
| A76 | PG | 31 | 255 | -64 | D |
| A66 | PG | 33 | 3 | -65 | C |
| A58 | PG | 35 | 233 | -66 | D |
| A56 | PG | 41 | 243 | -69 | D |
| A14 | PG | 42 | 201 | -70 | C |
| A30 | PG | 43 | 190 | -70 | C |
| A22 | PG | 43 | 46 | -70 | D |
| A12 | PG | 49 | 206 | -72 | D |
| A54 | PG | 52 | 236 | -73 | D |
| A68 | PG | 57 | 12 | -75 | C |
| A10 | PG | 59 | 207 | -75 | D |

$\begin{array}{llllll}\text { A52 } & \text { PG } & 60 & 238 & -76 & D\end{array}$

Number of P first motions: 18 Number of SH first motions: 0

2- Most Representative Solution.

A total of 18 solutions were found using a b axis increment of 5 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.


Average $B, P$, and $T$ axes:

B P T

| Mean trend: | N | 185 | N | 82 |
| :--- | :---: | :---: | :---: | :---: |
| Mean Plunge: | 39 | 10 | N | 331 |
| Vector Magnitude: | 15 | 17 | 48 |  |
| Mean length of resulting vector: | 0.849 | 0.969 | 16 |  |

3- Misfits.

All 18 p first motions agreed with the solution.
4- Rating of the focal mechanism.
The solution is rejected (rating $X$ ) based on the high number of $P$ misfits ( $0 / 100$ ) and the absence of constraints on the $P, T$ and $B$ axes (value of 0.894).

Earthquake of 197407020730 Magnitude 0.2 ML

1- Earthquake information and list of first motions.

| DateTime <br> hhmm ss | Latitude | Longitude | Depth <br> $(\mathrm{km})$ | Mag | Sta/Pha |  |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: |
| 740702 | 0730 | 18.62 | 47.5641 | -70.2271 | 4.43 | 0.2 ML |

COMMENTS:

CHARLEVOIX SEISMIC ZONE, QUE.
Data from the 1974 Charlevoix Field experiment.
See paper: Leblanc and Buchbinder (1977) for details.
\$Leblanc and Buchbinder (1977): Second Micro-earthquake survey of the \$St. Lawrence Valley near La Malbaie, Quebec. C.J.E.S. 14, no. 2, 2778-2789. \$Note: Time in Leblanc and Buchbinder (1977) is in Eastern Standard Time. \$Solution of Leblanc and Buchbinder (1977): $\$ 19740702023018.6 \mathrm{~L} \quad 47.5633-70.2283 \quad 4.4 \mathrm{~km} 0.3 \mathrm{ML}$ \$Focal mechanism computed; published in Leblanc and Buchbinder (1977). \$Entered in dbase in February 1996 by Maurice Lamontagne.

| Sta | Pha | Dist <br> $(k m)$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | ---: | :---: | ---: |
| A58 | PG | 4 | 166 | -45 | C |
| A56 | PG | 8 | 258 | -60 | D |
| A76 | PG | 9 | 353 | -63 | C |
| A60 | PG | 17 | 35 | -76 | C |
| A54 | PG | 18 | 229 | -76 | D |
| A16 | PG | 20 | 122 | -77 | D |
| A62 | PG | 27 | 38 | -80 | C |
| A52 | PG | 27 | 236 | -81 | D |
| A18 | PG | 28 | 100 | -81 | D |
| A20 | PG | 43 | 68 | -84 | D |
| A66 | PG | 59 | 31 | -86 | C |
| A22 | PG | 76 | 52 | -87 | C |
|  |  |  |  |  |  |
|  | Number of | Prirst motions: | 12 |  |  |
|  | Number of | SH first motions: | 0 |  |  |

2- Most Representative Solution.

A total of 125 solutions were found using a b axis increment of 5 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

| dip, strike, rake | 69.30 | 133.89 | -22.21 |  |  |
| :--- | ---: | :--- | ---: | :--- | :--- | :--- |
| dip, strike, rake | 69.30 | 232.11 | -157.79 | : auxiliary plane |  |
| lower hem. trend, plunge of | a, $n$ | 142.11 | 20.70 | 43.89 | 20.70 |

```
lower hem. trend & plunge of b 273.00 60.00
lower hem. trend, plunge of p,t 93.00 30.00 183.00 0.00
```

Average $B, P$, and $T$ axes:

|  | B | P | T |  |
| :--- | :---: | :---: | :---: | ---: |
| Mean trend: | N | 303 | N | 98 |
| Mean Plunge: | 55 | N | 202 |  |
| Vector Magnitude: | 68 | 23 | 35 |  |
| Mean length of resulting vector: | 0.544 | 0.979 | 113 |  |
| 3- Misfits. |  |  | 0.901 |  |

All 12 P first motions agreed with the solution. 4- Rating of the focal mechanism.

The solution is rejected (rating $X$ ) based on the high number of $P$ misfits ( $0 / 100$ ) and the absence of constraints on the $P, T$ and B axes (value of 0.808 ).

Earthquake of 197407140029 Magnitude 0.5ML

I- Earthquake information and list of first motions.

| Date | Time <br> hamm ss | Latitude | Longitude | Depth <br> $(\mathrm{km})$ | Mag | Sta/Pha |
| :---: | :--- | :--- | :--- | ---: | :--- | ---: |
| 740714 | 0029 | 56.78 | 47.4919 | -69.9720 | 12.71 | 0.5 ML |

COMMENTS:

CHARLEVOIX SEISMIC ZONE, QUE.
Data from the 1974 Charlevoix Field experiment.
See paper: Leblanc and Buchbinder (1977) for details.
\$Leblanc and Buchbinder (1977): Second Micro-earthquake survey of the \$Note: Time in Leblanc and Buchbinder (1977) is in Eastern Standard Time.
\$St. Lawrence Valley near La Malbaie, Quebec. C.J.E.S. 14, no. 2, 2778-2789.
SSolution of Leblanc and Buchbinder (1977):
$\$ 19740713192956.800 \mathrm{~L} \quad 47.4917-69.971712 .70 \mathrm{~km} 0.06 \mathrm{ML}$
\$Focal mechanism computed; published in Leblanc and Buchbinder (1977).
\$Entered in dbase in February 1996 by Maurice Lamontagne.

| Sta | Fha | Dist <br> $(\mathrm{km})$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | ---: | ---: | ---: | ---: |
| A16 | PG | 4 | 228 | -16 | C |
| A18 | PG | 9 | 70 | -34 | C |
| A14 | PG | 15 | 200 | -50 | C |
| A30 | PG | 18 | 172 | -54 | C |
| A58 | PG | 19 | 282 | -56 | D |
| A60 | PG | 24 | 338 | -62 | D |
| A76 | PG | 26 | 310 | -64 | D |
| A56 | PG | 28 | 284 | -65 | D |
| A62 | PG | 29 | 354 | -66 | D |
| A54 | PG | 33 | 263 | -69 | D |
| A64 | PG | 38 | 9 | -71 | C |
| A64 | SG | 38 | 9 | -71 | C |

Number of $p$ first motions: 12 Number of SH first motions: 0

2- Most Representative Solution.

A total of 314 solutions were found using ab axis increment of 5 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

| dip, strike, rake | 71.25 | 14.32 | 68.83 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| dip, strike, rake | 27.99 | 244.63 | 136.78 | : auxiliary plane |  |
| lower hem. trend, plunge of | a, n | 154.63 | 62.01 | 284.32 | 18.75 |

```
lower hem. trend & plunge of b 21.41 20.00
lower hem. trend, plunge of p,t 120.47 123.40 255.15 58.39
```

Average $B, P$, and $T$ axes:

|  | B | P | T |  |
| :--- | ---: | :--- | ---: | ---: |
| Mean trend: | N | 207 | N | 109 |
| Mean Plunge: | 26 | N | 282 |  |
| Vector Magnitude: | 273 | 304 | 67 |  |
| Mean length of resulting vector: | 0.870 | 0.967 | 176 |  |
| 3- Misfits. |  |  | 0.560 |  |

All 12 P first motions agreed with the solution. 4- Rating of the focal mechanism.

The solution is rejected (rating $X$ ) based on the high number of $p$ misfits ( $0 / 100$ ) and the absence of constraints on the $P, T$ and $B$ axes (value of 0.799).

Earthquake of 197908192249 Magnitude 4.98MN

1- Earthquake information and list of first motions.

| Date | Time <br> hhman |  | Latitude | Longitude | Depth <br> (km) | Mag | Sta/Pha |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 790819 | 2249 | 30.60 | 47.6720 | -69.9010 | 10.00 | 4.98MN | 5 |

## COMMENTS:

Felt; CHARLEVOIX SEISMIC ZONE, QUE.
About 8 km SE of St -Fidele, Que.
Felt in Quebec, New Brunswick and Maine.
Maximum intensity MM V. Minor damage in the epicentral region
Three damaged chimneys on the North Shore.
Followed by at least 6 aftershocks in the first 24 hours (largest is MN 3.0).
Isoseismals, aftershocks and focal mechanism are described in:
The Charlevoix earthquake of 19 August 1979 and its seismotectonic environment.
Hasegawa and Wetmiller, 1980. Earthquake notes, 51, 23-37.
SEE FIGURE 6 for isoseismals.
MAG(NEIS) 4.6 MB ON 22 stations MAG(NEIS) 4.5 MS ON 2 stations.
SIC, HAL AND IGL not operating.
$\begin{array}{llllllllllllllll} \\ \$+47.67 & -69.90 & \mathrm{~F} 1 \mathrm{MN}=0.0 & 224931 . & 19081979 & 0 & 0 & 0 & 4 & 8 & 0 & 210\end{array}$
$\$ 047.73-70.02 \mathrm{~F} 1 \mathrm{MN}=5.0 \quad 224930.1908197900 .02 \quad 0.030 .1 \quad 2247101.7$ 218LMQ 3
$\$$ Pegged at publised solution of Hasegawa and Wetmiller (1980).
\$ April 1996, Maurice Lamontagne completed the pikfile with some first motions, \$ phase readings and additional comments. All ISC phase data for canadian statio \$ and for all stations of epicentral distance < 2000 km were added.
\$
\$ FIRST MOTIONS:
Charlevoix network fm's read from analogue display.
Al0 first motion looks uncertain: very weak $C$ then D.
A54 Noisy at the time.

ECTN fm's: MNT, MNQ, GNT, MIQ, LBQ all re-checked. No fm on OTT, LDQ, LAQ: too noisy.
FHO fm (FORMERLY C) was taken out: Too noisy to pick.

New England fm's: Used file folder that contained some fm data.
Some original records were found.
BPM fm was read as $C$ but polarity is uncertain: not entered.
FLET fm is up but polarity is reversed: entered as D.
Teleseismic distances: First motions from ISC BUlletin (some might be question \$
fm on FHO; SUD; OTT; LAQ,: too weak.

Sta Pha Dist Azim Take-off FM

268

|  |  | (km) |  | Angle |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| A60 | PG | 15 | 279 | -56 | D |
| A20 | PG | 16 | 77 | - 58 | D |
| A64 | PG | 17 | 2 | -60 | C |
| A16 | PG | 24 | 200 | -67 | C |
| LMQ | PG | 35 | 247 | -74 | D |
| POC | PG | 36 | 197 | -74 | C |
| D2A | PG | 83 | 136 | -83 | D |
| CHQ | PG | 137 | 231 | -86 | D |
| QCQ | PG | 144 | 227 | -86 | D |
| CBM | PN | 158 | 121 | 49 | D |
| HNME | PN | 223 | 138 | 49 | C |
| JKM | PN | 226 | 187 | 49 | D |
| GNT | PN | 238 | 233 | 49 | D |
| UNB | PN | 314 | 126 | 49 | C |
| MNQ | PN | 329 | 14 | 49 | C |
| DVT | PN | 348 | 211 | 49 | D |
| PQ0 | PN | 353 | 147 | 49 | C |
| BNH | PN | 358 | 198 | 49 | D |
| MNT | PN | 374 | 231 | 49 | D |
| FLET | PN | 404 | 217 | 49 | D |
| PNY | PN | 423 | 223 | 49 | D |
| COV | PN | 426 | 217 | 49 | D |
| WNY | PN | 476 | 222 | 49 | D |
| HNH | PN | 479 | 204 | 49 | C |
| GAC | PN | 480 | 245 | 49 | D |
| MDV | PN | 481 | 213 | 49 | D |
| MIQ | PN | 484 | 255 | 49 | D |
| MSNY | PN | 484 | 234 | 49 | C |
| PTN | PN | 523 | 231 | 49 | D |
| APH | PN | 556 | 222 | 49 | D |
| CROG | PN | 599 | 228 | 49 | D |
| SCH | PN | 825 | 14 | 49 | D |
| LBQ | PN | 839 | 324 | 49 | D |
| LGQ | PN | 868 | 323 | 49 | D |
| PBQ | PN | 1006 | 330 | 49 | C |
| ECM | PN | 1091 | 214 | 49 | C |
| MRG | PN | 1205 | 226 | 49 | C |
| AAM | PN | 1236 | 246 | 49 | C |
| BLA | PN | 1447 | 220 | 49 | C |
| DAG | PN | 3941 | 18 | 32 | C |
| MLS | PN | 4592 | 314 | 30 | C |
| LFF | PN | 5261 | 66 | 28 | C |
| CAF | PN | 5352 | 65 | 28 | C |
| BNG | PN | 9530 | 88 | 17 | D |
| WB2 | PN | 16241 | 316 | 0 | C |

Number of P first motions: 45 Number of SH first motions: 0

A total of 32 solutions were found using a b axis increment of 1 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

| dip, strike, rake | 58.08 | 177.14 | 67.45 |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| dip, strike, rake | 38.38 | 35.29 | 121.62 | : auxiliary plane |  |  |
| lower hem. trend, plunge of | $a, n$ | 305.29 | 51.62 | 87.14 | 31.92 |  |
| lower hem. trend \& plunge of b | 189.53 | 19.00 |  |  |  |  |
| lower hem. trend, plunge of $\mathrm{p}, \mathrm{t}$ | 283.15 | 10.39 | 40.37 | 68.15 |  |  |

Average $B, P$, and $T$ axes:


Appendix 4: Photocopies of the focal mechanisms published in the National Summaries of Canadian earthquakes.

## CANADIAN EARTHQUAKES

TREMBLEMENTS DE TERRE CANADIENS

# NATIONAL SUMMARY SOMMAIRE NATIONAL 

## JANUARY-MARCH 1989 JANVIER-MARS

J.A. Drysdale<br>* R.B. Horner<br>* R. Kolinsky<br>M. Lamontagne

```
SEISMOLOGICAL SERVICE SERVICE SEISMOLOGIQUE
            GEOPHYSICS DIVISION DIVISION DE LA GEOPHYSIQUE
GEOLOGICAL SURVEY OF CANADA COMMISSION GEOLOGIQUE DU CANADA
    1 OBSERVATORY CRESCENT 1, PLACE DE L'OBSERVATOIRE
            OTTAWA, ONT. OTTAWA, ONT.
                K1A OY3 K1A OY3
    *PACIFIC GEOSCIENCE CENTRE *CENTRE GEOSCIENTIFIQUE DU PACIFIQUE
GEOLOGICAL SUIRVEY OF CANADA COMMISSION GEOLOGIQUE DU CANADA
    P.O. BOX 6000 B.P. }600
                SIDNEY, B.C. SIDNEY, C.-B.
            V8L 4B2 V8L 4B2
```

EASTERN CANADIAN FOCAL MECHANISMS JANUARY-MARCH 1989
MECANISMES AU FOYER DE L'EST DU CANADA JANVIER-MARS 1989

| Date | H M | $\begin{aligned} & \text { LAT } \\ & \left({ }^{\circ} \mathrm{N}\right) \end{aligned}$ | $\begin{aligned} & \text { LONG } \\ & \left({ }^{\circ} \mathrm{W} /{ }^{\circ} \mathrm{O}\right) \end{aligned}$ | $\begin{gathered} 2 \\ (\mathrm{~km}) \end{gathered}$ | $\begin{aligned} & \text { MAG } \\ & \mathrm{m}_{\mathrm{N}} \end{aligned}$ | NODAL PLANES-PLANS NODAUX STRIKE/DIP/RAKE DIRECTION/PENDAGE/REJET |  |  | AXESTREND/PLUNGEDIRECTION/PLONGEMENT |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  | P | T | B |
| :890309: 094147.72 (Charlevoix, Que.) |  |  | 69.86 | 11 | 4.3 | 168 | 31 | 071 | 92/15 | 308/72 | 185/10 |
|  |  |  | 011 |  |  | 60 | 102 |  |  |  |
| 890311 | 0831 | 47.72 |  | 69.87 | 10 | 4.4 | 184 | 38 | 080 | 101/07 | 322/81 | 192/06 |
| (Charle | ix, | e.) | 017 |  |  |  | 52 | 098 |  |  |  |  |
| 890316 | 0417 | 60.04 | 70.06 | 11 | 5.7 | 260 | 42 | 058 | 192/07 | 085/68 | 285/21 |  |
| (Payne | y, Qu |  |  |  |  | 120 | 55 | 116 |  |  |  |  |

These focal mechanisms have been derived using the program FOCMEC from Arthur Snoke of Virginia Tech. On the plot, strong compressive, weakly compressive, emergent, weakly dilatational and strong dilatational $P$ arrivals are $C, C, e, d$ and $D$, respectively; $P, T$, and $B$ represent the $P, T$ and $B$ axes; and the diagonal crosses are $\log \mathrm{Sv} / \mathrm{P}$ amplitude ratio data (small crosses represent large ratios)
Ces mécanismes au foyer font calculé grâce au programme FOCMEC d'Arthur Snoke du Virginia Tech. Pour les premières arrivées d'onde $P$, les symboles utilisés dans la figure sont $C$, $c$, $e, d e t D$ représentant respectivement une compression claire, une compression faible, une arrivée émergente, une dilatation faible et une dilatation claire. $P$, $T$ et $B$ représentent les axes $P, T$ et $B$. Les croix diagonales représentent les données des rapports d'amplitudes $\log S v / P$ (les petites croix correspondent à de grands rapports).


## CANADIAN EARTHQUAKES

## TREMBLEMENTS DE TERR CANADIENS

## NATIONAL SUMMARY SOMMAIRE NATIONAL

## JULY -SEPTEMBER 1989 JUILLET-SEPTEMBRE

J.A. Drysdale<br>* R.B. Horner<br>* R. Kolinsky<br>M. Lamontagne

SEISMOLOGICAL SERVICE SERVICE SEISMOLOGIQUE<br>GEOPHYSICS DIVISION DIVISION DE LA GEOPHYSIQUE<br>geological survey of canada commission geologique du canada 1 OBSERVATORY CRESCENT 1, PLACE DE L'OBSERVATOIRE OTTAWA, ONT. OTTAWA, ONT.<br>KIA OYeZ KIA OY3

*PACIFIC GEOSCIENCE CENTRE *CENTRE GEOSCIENTIFIQUE DU PACIFIQUE GEOLOGICAL SURVEY OF CANADA COMMISSION GEOLOGIQUE DU CANADA P.O. BOX 6000 B.P. 6000

SIDNEY, B.C. SIDNEY, C.-日.
VEL 4B2 VEL $4 B 2$

| Date | Time Heure | $\begin{aligned} & \text { LAT } \\ & { }^{\circ} \mathrm{N} \end{aligned}$ | $\begin{aligned} & \text { LONG } \\ & { }^{\circ} \mathrm{W} \end{aligned}$ | $\begin{aligned} & \mathrm{Z} \\ & \mathrm{~km} \end{aligned}$ | $\begin{gathered} \mathrm{MAG} \\ \mathrm{~m}_{\mathrm{N}} \end{gathered}$ | Plans Nodaux Nodal Planes str/dip/rak dir/pend/incl. | Axes des Contraintes Stress Axes az/pl |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1989/08/10 | 21:17 | 46.63 | 65.82 | 17 | 3.5 | $\begin{aligned} & \text { P: } 324 / 59 / 60 \\ & \text { A: } 191 / 42 / 129 \end{aligned}$ | P: 074/09 <br> T: 182/63 <br> B: 340/25 |
| 41989/09/13 | 14:55 | 47.57 | 70.04 | 15 | 2.9 | $\begin{aligned} & \text { P: 042/57/40 } \\ & \text { A: } 288 / 57 / 140 \end{aligned}$ | P: 345/00 <br> T: 255/50 <br> B: 075/40 |

These focal mechanisms have been derived using the program FOCMEC from Arthur Snoke of Virginia Tech.. On the plot, strong compressive, weakly compressive, emergent, weakly dilatational and strong dilatational $P$ arrivals are $C, c, e, d$ and $D$ respectively: $P, T$, and $B$ represent the $P, T$ and $B$ axex; and the diagonal crosses are $\log \mathrm{Sv} / \mathrm{P}$ amplitude ratio data (small crosses represent large ratios).
Ces mécanismes au foyer font calculé grâce au programme FOCMEC d'Arthur Snoke du Virginia Tech. Pour les premières arrivées d'onde $P$, les symboles utilisés dans la figure sont $\mathrm{C}, \mathrm{c}, \mathrm{e}, \mathrm{d}$ et D reprèsentant respectivement ane compression claire, une compression gailbe, une arrivée émergente, une dilatation faible et un dilatation claire. P, T et B reprèsentent les axes P, T, et B. Les croxi diagonales representent les donnnées des rapports d'amplitudes $\log \mathrm{Sv} / \mathrm{P}$ (les petites croix correspondent à de grands rapports).


## CANADIAN EARTHQUAKES

## TREMBLEMENTS DE TERRE CANADIENS

## JANUARY-MARCH 1990 JANVIER-MARS

J.A. Drysdale

* R.B. Horner
* R. Kolinsky
M. Lamontagne

```
SEISMOLOGICAL SERVICE SERVICE SEISMOLOGIQUE
            GEOPHYSICS DIVISION DNISION DE LA GEOPHYSIQUE
gEOLOGICAL SURVEY OF CANADA COMMISSION GEOLOGIQUE DU CANADA
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            K1A OYZ K1A OY3
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GEOLOGICAL SURVEY OF CANADA COMMISSION GEOLOGIQUE DU CANADA
    P.O. BOX }6000\mathrm{ B.P. }600
                        SIDNEY, B.C. SIDNEY, C.-B.
                            V8L 4B2 V8L 4B2
```

EASTERN CANADIAN FOCAL MECHANISMS (January 1 - March 31, 1990)
MECANISMES AU FOYER DE L’EST DU CANADA (Janvier 1 - Mars 31, 1990)
W. McNeil - J. Adams


These focal mechanisms have been derived using the program FOCMEC from Arthur Soke of Virginia Tech.. On the plot, strong compressive, weakly compressive, emergent, weakly dilatational and strong dilatational $P$ arrivals are $C, c, e, d$ and $D$ respectively: $P, T$, and $B$ represent the $P, T$ and $B$ axes; and the diagonal crosses are $\log \mathrm{Sv} / \mathrm{P}$ amplitude ratio data (small crosses represent large ratios).

Cos mécanismes au foyers fonts calculés grâce au programme FOCMEC d'Arthur Snore du Virginia Tech. Pour les premières arrivées d'onde $P$, les symboles utilisés dons la figure sons $C, c, e, d$ et $D$ représentant respectivement une compression claire, une compression faible, une arrive émergente, une dilatation faible et one dilatation claire. $\mathrm{P}, \mathrm{T}$ et B représentent les axes $\mathrm{P}, \mathrm{T}$, et B . Les croix diagonales représentent les données des rapports d'amplitudes $\log \mathrm{Sv} / \mathrm{P}$ (les petites croix correspondent à de grands rapports).

## CANADIAN EARTHQUAKES

## TREMBLEMENTS DE TERRE CANADIENS

## NATIONAL SUMMARY SOMMAIRE NATIONAL

APRIL-JUNE 1990 AVRIL-JUIN

J.A. Drysdale<br>* R.B. Horner<br>* R. Kolinsky<br>M. Lamontagne

## SEISMOLOGICAL SERVICE SERVICE SEISMOLOGIQUE

GEOPHYSICS DIVISION DIVISION DE LA GEOPHYSIQUE
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1 OBSERVATORY CRESCENT 1, PLACE DE L'OBSERVATOIRE
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K1A OY3 K1A OY3
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P.O. BOX 6000 B.P. 6000

SIDNEY, B.C. SIDNEY, C.-B.
V8L 4B2 V8L 4B2
EASTERN CANADIAN FOCAL MECHANISMS (APRIL - JUNE 30, 1990)
MECANISMES AU FOYER DE L'EST DU CANADA (AVRIL 1 - JUIN 30, 1990)

| Date | Time Heure | $\begin{aligned} & \text { LAT } \\ & \stackrel{\circ}{\mathrm{N}} \end{aligned}$ | $\begin{aligned} & \text { LONG } \\ & \circ \mathrm{W} \end{aligned}$ | $\begin{aligned} & \mathrm{Z} \\ & \mathrm{~km} \end{aligned}$ | $\begin{gathered} \mathrm{MAG} \\ \mathrm{~m}_{\mathrm{N}} \end{gathered}$ | Nodal Planes Plans Nodaux str/dip/rak dir/pend/incl. | Stress Axes <br> Axes des Contraintes az/pl |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ¿1990/04/21 | 01:23 | 47.55 | 70.07 |  | 3.1 | $\begin{aligned} & \text { P: } 297 / 51 / 77 \\ & \text { A: } 137 / 41 / 105 \end{aligned}$ | $\begin{aligned} & \text { P: } 036 / 05 \\ & \text { T: } 152 / 79 \\ & \text { B: } 305 / 10 \end{aligned}$ |
| 1990/04/23 | 00:28 | 47.41 | 70.18 |  | 3.0 | $\begin{aligned} & \text { P: } 174 / 41 / 41 \\ & \text { A: } 051 / 65 / 123 \end{aligned}$ | P: 117/13 <br> T: 007/57 <br> B: 215/30 |
| 1990/04/24 | 13:46 | 45.92 | 72.64 |  | 2.8 | $\begin{aligned} & \text { P: } 066 / 72 / 64 \\ & \text { A: } 304 / 32 / 144 \end{aligned}$ | P: $176 / 23$ <br> T: 303/55 <br> B: 075/25 |

These focal mechanisms have been derived using the program FOCMEC from Arthur Snoke of Virginia Tech.. On the plot, strong compressive, weakly compressive, emergent, weakly dilatational and strong dilatational $P$ arrivals are $C, c, e, d$ and $D$ respectively: $P, T$, and $B$ represent the $P, T$ and $B$ axes; and the diagonal crosses are $\log \mathrm{Sv} / \mathrm{P}$ amplitude ratio data (small crosses represent large ratios).
Ces mécanismes au foyers sonts calculés grâce au programme FOCMEC d'Arthur Snoke du Virginia Tech. Pour les premières arrivées d'onde $P$, les symboles utilisés dans la figure sont $C, c, e, d$ et $D$ représentant respectivement une compression claire, une compression faible, une arrivée émergente, une dilatation faible et une dilatation claire. $P, T$ et $B$ représentent les axes $P, T$, et $B$. Les croix diagonales représentent les données des rapports d'amplitudes $\log \mathrm{Sv} / \mathrm{P}$ (les petites croix correspondent à de grands rapports).

$$
\begin{aligned}
& \text { SNOILIINI.AGG }
\end{aligned}
$$



Lambert conformal geopirsicis division ghoiogical. simviy of canaida
PROJECTION DE LAMBERT


## CANADIAN EARTHQUAKES

## TREMBLEMENTS DE TERR CANADIENS

## NATIONAL SUMMARY SOMMAIRE NATIONAL

## OCTOBER-DECEMBER 1990 OCTOBRE-DÉCEMBRE

J.A. Drysdale

* R.B. Horner
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EASTERN CANADIAN FOCAL MECHANISMS (OCT. 1 - DEC. 31, 1990)
MECANISMES AU FOYER DE L'EST DU CANADA (OCT. 1 - DEC. 31, 1990)
W. McNeil


These focal mechanisms have been derived using the program FOCMEC from Arthur Snoke of Virginia Tech.. On the plot, strong compressive, weakly compressive, emergent, weakly dilatational and strong dilatational $P$ arrivals are $C, c, e, d$ and $D$ respectively: $P, T$, and $B$ represent the $P, T$ and $B$ axes; and the diagonal crosses are $\log \mathrm{Sv} / \mathrm{P}$ amplitude ratio data (small crosses represent large ratios).

Cos mécanismes au foyers sons calculés grâce au programme FOCMEC d'Arthur Soke du Virginia Tech. Pour les premières arrivées d'onde $P$, les symboles utilisés dan la figure sort $C, c, e, d$ et $D$ représentant respectivement une compression claire, une compression faible, une arrivée émergente, une dilatation faible et un dilatation claire. $\mathrm{P}, \mathrm{T}$ et B représentent les axes $\mathrm{P}, \mathrm{T}$, et B . Les croix diagonales représentent les données des rapports d'amplitudes $\log \mathrm{Sv} / \mathrm{P}$ (les petites croix correspondent à de grands rapports).


Appendix 5: Focal mechanisms of earthquakes published in Lamontagne and Ranalli (1997).

1- Earthquake information and list of first motions.

| Date Time | Latitude | Longitude | Depth <br> hhmm ss |  | Mag | Sta/Pha |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 891208 | 1720 | 34.44 | 47.7010 | -70.0644 | 10.41 | 2.6 MN |

COMMENTS:

CHARLEVOIX, QUEBEC
\$ The Sg lines of some stations include the SH FM.
\$ The convention used is the Virginia Tech convention used in FOCMEC:
$\$<: S H$ first motion to left (back to event) impulsive
\$ >: SH first motion to right (back to event) impulsive
\$ Preliminary Focmec computed by ML: Results to come after Nov. 1995.

| Sta | Pha | Dist <br> $(k m)$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | ---: | :---: | :---: |
| A61 | PG | 2 | 245 | -12 | C |
| A61 | SG | 2 | 245 | -12 | $<$ |
| A64 | PG | 19 | 43 | -61 | D |
| A64 | SG | 19 | 43 | -61 | < |
| A16 | PG | 26 | 170 | -68 | C |
| A16 | SG | 26 | 170 | -68 | $>$ |
| LMQ | PG | 26 | 229 | -68 | D |
| A21 | PG | 28 | 89 | -70 | D |
| A21 | SG | 28 | 89 | -70 | $>$ |
| A54 | PG | 38 | 224 | -75 | C |
| A54 | SG | 38 | 224 | -75 | < |
| LPQ | PG | 40 | 174 | -76 | C |
| A11 | PG | 52 | 191 | -79 | C |
| SLQ | PG | 79 | 92 | -82 | C |
| CIQ | PG | 84 | 320 | -83 | D |
| DAQ | PG | 93 | 289 | -84 | D |

Number of P first motions: 11 Number of SH first motions: 5

2- Most Representative Solution.
A total of 363 solutions were found using a b axis increment of 2 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

| dip, strike, rake | 43.06 | 149.20 | 25.62 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| dip, strike, rake | 72.83 | 39.89 | 130.12 | :auxiliary plane |  |
| lower hem. trend, plunge of | a, $n$ | 309.89 | 17.17 | 59.20 | 46.94 |

```
lower hem. trend & plunge of b 205.92 38.00
lower hem, trend, plunge of p,t 101.28 17.93 351.34 46.50
```

Average $B, P$, and $T$ axes:
B P T

| Mean trend: | N | 205 | N | 98 |
| :--- | :---: | :---: | :---: | :---: |
| Mean Plunge: | 47 | 15 | 354 |  |
| Vector Magnitude: | 353 | 357 | 39 |  |
| Mean length of resulting vector: | 0.973 | 0.984 | 335 |  |

3- Misfits.
Out of 11 P first motions, one did not fit the solutions ( 9/100)
Station Number Percentage
Name of misfits of wrongs
SLQ 363100
All 5 SH first motions agreed with the solution.
4- Rating of the focal mechanism.
The solution is rejected (rating $X$ ) based on the high number of $P$ and SH misfits
( $9 / 100$ and $0 / 100$ respectively) and the absence of constraints on the $P$, $T$ and
$B$ axes (value of 0.960 ).




## Location Map



Earthquake of 199107230103 Magnitude 1.9MN

1- Earthquake information and list of first motions.

| Date Time | Latitude | Longitude | Depth <br> hhmm ss |  | Mag | Sta/Pha |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: |
| 910723 | 0103 | 14.30 | 47.6860 | -70.1030 | 11.02 | 1.9 MN |

COMMENTS:

7 KM NE OF POINTE-AU-PIC, QUE. CHARLEVOIX, QUE.
\$
\$ The Sg lines of some stations include the $\mathrm{SH} F \mathrm{FM}$.
\$ The convention used is the Virginia Tech convention used in FOCMEC:
\$ <: SH first motion to left (back to event) impulsive
\$ >: SH first motion to right (back to event) impulsive
\$ Preliminary Focmec computed by ML.

| Sta | Pha | Dist <br> $(\mathrm{km})$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | ---: | ---: | ---: | ---: |
| A61 | Pg | 1 | 53 | -6 | C |
| A61 | Sg | 1 | 53 | -6 | $>$ |
| A64 | Pg | 22 | 45 | -64 | D |
| A64 | Sg | 22 | 45 | -64 | $>$ |
| LMQ | Pg | 23 | 228 | -64 | D |
| A16 | Pg | 25 | 163 | -66 | D |
| A16 | Sg | 25 | 163 | -66 | < |
| A21 | Pg | 31 | 86 | -70 | D |
| A21 | Sg | 31 | 86 | -70 | $>$ |
| A54 | Pg | 35 | 222 | -72 | D |
| A54 | Sg | 35 | 222 | -72 | $>$ |

Number of P first motions: 6 Number of SH first motions: 5

2- Most Representative Solution.
A total of 65 solutions were found using a b axis increment of 5 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.

$$
\begin{array}{llll}
\text { dip,strike,rake } \quad 55.00 \quad 114.68 \quad 90.00
\end{array}
$$

| dip, strike, rake | 35.00 | 294.68 | 90.00 | : auxiliary plane |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| lower hem. trend, plunge of $\mathrm{a}, \mathrm{n}$ | 204.68 | 55.00 | 24.68 | 35.00 |  |  |
| lower hem. trend \& plunge of b | 114.68 | 0.00 |  |  |  |  |
| lower hem. trend, plunge of p,t | 204.68 | 10.00 | 24.68 | 80.00 |  |  |

Average $B, P$, and $T$ axes:
B
P
T

| Mean trend: | N | 117 | N | 206 |
| :--- | :---: | ---: | :---: | :---: |
| Mean Plunge: |  | -0 | 5 | N |
| Vector Magnitude: | 64 | 64 | 84 |  |
| Mean length of resulting vector: | 0.982 | 0.983 | 64 |  |

3- Misfits.

All 6 P first motions agreed with the solution.
All 5 SH first motions agreed with the solution.

4- Rating of the focal mechanism.

The solution has a $C$ rating based on the high number of $P$ and $S H$ misfits ( $0 / 100$ and $0 / 100$ respectively) and on the poor constraints on the $P, T$ and $B$ axes (value of 0.984 ).

$295$



## Location Map



Earthquake of 199303300215 Magnitude 1.82MN

1- Earthquake information and list of first motions.

| DateTime <br> hhmm ss | Latitude | Longitude | Depth <br> $(\mathrm{km})$ | Mag | Sta/Pha |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 930330 | 0215 | 18.46 | 47.6849 | -70.1044 | 4.58 | 1.82 MN |

COMMENTS:

5 KM NE OF LA MALBAIE, CHARLEVOIX, QUE.
\$ 1 KM NE OF CAP-A-L'AIGLE, QUE. $1 \mathrm{KM} N E$ DE CAP-A-L'AIGLE, QUE.
\$ LPQ PHASES X'ED OUT DUE TO SUSPECTED TIMING DESCREPANCY
\$ BETWEEN CNSN AND CLTN, AND TO FIR-FILTER RINGING BEFORE PG \$ The Sg lines of some stations include the SH FM.
\$ The convention used is the Virginia Tech convention used in FOCMEC:
\$ <: SH first motion to left (back to event) impulsive
\$ >: SH first motion to right (back to event) impulsive
\$ Preliminary Focmec computed by ML: Results to come after Nov. 1995.

| Sta | Pha | Dist <br> $(k m)$ | Azim | Take-off <br> Angle | FM |
| :--- | ---: | :---: | ---: | :---: | :---: |
| A61 | PG | 1 | 50 | -17 | D |
| A61 | SG | 1 | 50 | -17 | $>$ |
| A64 | PG | 22 | 45 | -78 | C |
| A64 | SG | 22 | 45 | -78 | $<$ |
| A16 | PG | 25 | 163 | -80 | C |
| A16 | SG | 25 | 163 | -80 | $>$ |
| A21 | PG | 31 | 86 | -82 | C |
| A21 | SG | 31 | 86 | -82 | $>$ |
| A54 | PG | 34 | 222 | -82 | D |
| A54 | SG | 34 | 222 | -82 | $<$ |

Number of P first motions: 5 Number of SH first motions: 5

2- Most Representative Solution.

A total of 523 solutions were found using a b axis increment of 2 degree. The following parameters describe the most representative solution, which was derived from the average $B, P$, and $T$ axes listed below.


```
Average B, P, and T axes:
```

B P T

```
Mean trend: N 235
Mean Plunge: 18 69 10
Vector Magnitude: 519 517 517
Mean length of resulting vector: 0.992 0.988
3- Misfits.
```

All 5 P first motions agreed with the solution.
Out of 5 SH first motions, a total of 1 did not fit the solutions (20/100).
Station Number Percentage
Name of misfits of wrongs
A16 $523 \quad 100$
4- Rating of the focal mechanism.
The solution has a $B$ rating based on the number of $P$ and $S H$ misfits
( $0 / 100$ and $20 / 100$ respectively) and on the constraints on the $P, T$ and
$B$ axes (value of 0.990 ).




## Location Map




[^0]:    i
    Ligure

