

ORGANIC PETROGRAPHY AND KINETICS OF JURASSIC/CRETACEOUS SHALES AND GEOCHEMISTRY OF SELECTED LIQUID HYDROCARBONS, SCOTIAN BASIN

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1.0. SUMMARY

In this report, geochemical analysis and basin modelling using multicomponent kinetics resolved some of the intriguing problems of generation, expulsion, and entrapment of the Scotian Basin petroleums. The report establishes more understanding of the following aspects: (a) hydrocarbon potential of additional composite shale samples, (b) oil-oil and oil-source rock correlation have been reevaluated using additional analysis of aromatic biomarkers and fingerprinting the geochemical nature of additional oil asphaltenes, (c) multicomponent kinetic studies of Kerogen Type IIA-IIB and IIB for two samples using Pyromat II, and (d) amount and timing of generated and expelled hydrocarbon fractions (methane; C_2 - C_5 ; C_6 - C_{15} ; and C_{15} +) using n-component kinetics in the BasinModTM program.

Source Rock Characterization

Except for a few samples from the Merigomish C-52 and Thebaud I-93 wells, most of the analyzed rocks contain abundant terrestrial oxidized organic matter forming Kerogen Type III (Tables 1 and 2). Most analyzed source rocks are mature for petroleum generation (Table 1). Statistically, 4.8% of the analyzed rocks can generate oil and condensate (Type IIA-IIB); 28.6% are capable of generating condensate and gas (Kerogen Type IIB); 61.8% are gas-prone (Kerogen Type III) and 4.8% are nonsource for commercial petroleum.

Oil-Oil and Oil-Source Rock Correlation

Using methylphenanthrene index (MPI), the maturity of all oil and condensate samples analyzed for the last four years were reevaluated. The calculated vitrinite reflectance from most of the oil and condensate samples from Alma, Arcadia, Glenelg, S. Venture, Uniacke, and Venture fields are greater than 0.9% R_c (S. Venture oils have the highest maturity: >1.1 R_c; Fig. 2A). Most of the Cohasset, Panuke, and Balmoral oils have less than 0.9% R_c and are generally between 0.7 and 0.8% R_c.

Based on twenty-two maturity insensitive aromatic biomarkers (derived from GC/MS and Py-GC/MS), three distinctly different oil families could be recognized (Figs. 2B, 3, and 4; Tables 4a, 4b, 5, and 6). Group I represents most of the high maturity condensates from the Venture and other fields which are derived from a terrestrial source. Group 2 represents the majority of the

petroleum from the Cohasset-Panuke-Balmoral fields which are derived from an algal source. The Group 3 represents oils from the Sable Island wells (sourced from mixed organic matter). A few samples from Cohasset D-42 and Panuke J-99 do not correlate with any group possibly suggesting geochemical alteration of oil within the reservoir. According to oil-oil correlation of various reservoirs, most of the Cohasset-Panuke-Balmoral oils are genetically connected (r² >0.80) (Figs. 5a, 5b, and 5c).

N-Component Reaction Kinetics

The multicomponent (methane, ethane, and propane) kinetics suggest that the generation of ethane from both kerogen (primary cracking) and C_{15} + (secondary cracking) have the lowest activation energy distributions and T_{max} values (derived from Pyromat II) (Table 7; Figs. 6 through 6d). The generation of methane from C_{15} + required the highest activation energy distributions and T_{max} .

Amount and Timing of Methane Expulsion

Preliminary evaluation on the generation and expulsion of n-components using BasinMod and analyzed n-component kinetics showed that they differ in various stratigraphic units and are dependant on the variation of their maturity and depth. The amount of methane expulsion from sixteen stratigraphic units from wells N. Truimph G-43/B-52 and fifteen units from the well S. Desbarres O-76 has been critically reviewed. In general, N. Truimph has generated and expelled almost double the amount of various n-components compared to the S. Desbarres O-76 well. This is because N. Truimph contains abundant Kerogen Type IIB source rock intervals and the sediments were buried deeper in the geological past. The amount of methane expelled from Kerogen Type IIB varies between ~7 (at 3665m) to 70 (at 10800m) mg/g TOC in the N. Truimph well and ~8 (3670m) and ~50 (5550m) mg/gTOC in S. Desbarres. The amount of methane expulsion varied widely for various stratigraphic units in both wells when Kerogen Type III source rock intervals are compared using the measured IIB and default III kinetics.

Similarly, the timing of methane expulsion in various units are dependant on their age, depth and maturity. As an example, in unit TJ2 (Kerogen Type IIB) of the N. Truimph G-43, the expulsion started around 130 mybp and reached its peak around 20 mybp (Table 9a). At the

present time, this unit has reduced its capability for major gas expulsion. On the contrary, in well S. Desbarres O-76, the similar (Begin_Age) unit (MicMac, Kerogen Type IIB) started expelling around 90 mybp and reached its peak in the last 10 mybp (Table 9b). This suggests that the hydrocarbon system in the Scotian Basin is a highly dynamic system and the reservoirs are replenishing with hydrocarbons expelled from the younger horizons.

2.0. INTRODUCTION

2.1. Administrative Aspect

This research proposal was requested by Supply and Services Canada, Dartmouth, Nova Scotia at the initiation of the Basin Analysis Subdivision of the Geological Survey of Canada Atlantic, Bedford Institute of Oceanography. Global Geoenergy Research Ltd. of Halifax, Nova Scotia, submitted a financial and work schedule for the research proposal. The proposal was accepted and the research work was started on July 11, 1994. Canada-Nova Scotia Offshore Petroleum Board (C-NSOPB), Halifax, Nova Scotia, on our request, permitted us to collect two condensates, four core samples, and forty-two unwashed cuttings from selected Scotian Shelf wells at the C-NSOPB Repository, Dartmouth, Nova Scotia.

According to the contract, Rock-Eval pyrolysis of 40 samples was done at the Geochemistry Laboratory at GSC Calgary. This laboratory also did liquid chromatography of eleven oil samples and bitumen extractions for four source rocks. According to the contract, kerogen isolation, smear slide preparation, kerogen plug preparation, and vitrinite reflectance measurement were done at the palynology laboratory (Bernard Crilley) and coal laboratory (Mike Avery) at the GSC Atlantic.

The analytical work for gas-chromatography mass spectrometry and pyrolysis-gas chromatography/mass spectrometry of aromatic biomarkers was subcontracted to Dr. Michael Kruge of the Southern Illinois University, Carbondale, U.S.A., who successfully completed earlier subcontracts on Scotian Shelf samples (Mukhopadhyay, 1991, 1993, 1994). The use of multicomponent kinetics for oil and gas generation is at present in an experimental stage. Only two commercial laboratories (Lab Instruments [Dr. Alain Samoun] and Humble Geochemical Services [Dan Jarvie]) in North America can do those analysis. Our earlier studies indicated that oil and condensate in the Scotian Basin were generated from multiple source rocks. The use of multicomponent kinetics would be useful in partitioning the generation and expulsion of gas and condensate as normal crude oil is extremely rare in the basin. This work was subcontracted to Alain Samoun of Lab Instruments, Kenwood, California. Dr. Simoun was previously involved with this type of multicomponent kinetics studies in association with the Lawrence Livermore Group who formulated n-component reaction kinetics in the latest version of the BasinModTM (1994) Program.

2.2. Scientific Aspect

Between 1970 and 1990, significant gas and associated condensate or light oil were discovered in the Jurassic-Cretaceous reservoirs around the Sable Subbasin of the Scotian Basin. Since 1988, Basin Analysis Subdivision of Geological Survey of Canada, Atlantic at Dartmouth, Nova Scotia initiated systematic research projects to resolve problems related to the characterization of the source rocks and reservoired petroleum. Those studies (as done by Global Geoenergy Research Ltd.) characterized some of the source rocks in various stratigraphic intervals; characterized the geochemical properties of some selected oils and condensates; and determined some possible oil-oil and source rock-oil correlation (Mukhopadhyay and Birk, 1989; Mukhopadhyay, 1989; Mukhopadhyay and Wade, 1990; Mukhopadhyay, 1990a; Mukhopadhyay, 1990b; Mukhopadhyay, 1991, Mukhopadhyay, 1993; Mukhopadhyay, 1994a and b; Mukhopadhyay et al., 1995).

Mukhopadhyay (1991, 1993, 1994), from extensive organic petrographic analyses and Rock-Eval pyrolysis, established the distribution of various organic facies present in the basin and the proportion of oil-, condensate-, and gas-prone source rocks in the various stratigraphic sequences. Mukhopadhyay (1991, 1993, 1994), from the study of the aromatic biomarkers and bitumen/oil isotope analyses, characterized possible correlation of oil-oil and oil-source rock pairs which indicated that various crude oils or condensates may have been derived from three types of source rocks.

Isotopic composition of kerogen, using stable carbon isotope, may provide information on the nature of depositional environment and type of organic matter. Mukhopadhyay (1994b) studied the isotopic composition (-22.72 to -26.41°/oo) of ten kerogen samples which suggests that none of them were formed in a restricted, anoxic basin. However, some shale and limestone samples (in N. Truimph and Abenaki wells) may have some influence of marine phytoplankton as compared to the shale samples from Venture area. The isotopic composition also shows the difference in maturity among various kerogens.

Kinetic analysis is performed on known source rocks to determine the energy required to decompose organic matter to form petroleum. Application of these data in a quantitative basin modeling program permits a more accurate determination of the timing of oil generation. The *BasinMod* program utilizes those chemically derived kinetic models to accurately predict the

onset and peak oil/gas zones and timing/amount of hydrocarbon generation and migration (Platt River Associates, 1992). In our previous studies, kinetic analysis of selected source rocks showed wide variations in the distribution of activation energies and Arrhenius Factors (Mukhopadhyay, 1993, 1994a; Mukhopadhyay et al., 1995). Some Kerogen Type IIA-IIB can generate and expel hydrocarbons earlier in the maturation history of a source rock (<0.8% R_o) with about 60% of activation energies below 48 kcal/mole, whereas other Kerogen Type IIA-IIB source rocks behave similar to Kerogen Type II of Tissot and Welte (1984) having 60% activation energies between 49 and 52 kcal/mole. The reaction rate of the second form of Kerogen Type IIA-IIB is considered as medium compared to the first one (Mukhopadhyay, 1993, 1994a, 1994b). The reaction rate of some Kerogen Type IIB is slower compared to both forms of Kerogen Type IIA-IIB source rock. The kinetic analysis, acquired through various contracts, already enhanced our capability to achieve an understanding about the timing of petroleum generation and migration using the BasinMod program.

However, those studies were found to be inadequate to define precisely the generation and expulsion of various hydrocarbon fractions, and the volume of reservoired petroleum in the basin because (a) the kinetics of gas generation using primary and secondary cracking was not evaluated, (b) lack of analysis of an adequate number of composite source rock intervals, and (c) the absence of adequate oil-oil correlation within the reservoired petroleum in the Cohasset-Panuke-Balmoral area. The present work attempts to solve some of those existing problems.

2.3. Objectives

The objectives of this research are:

- (a) To define the organic facies, kerogen type, and hydrocarbon potential of additional 40 composite shale source rock intervals.
- (b) To use aromatic biomarkers and asphaltene pyrolyzates for oil-oil and possible oil-source rock correlation and differences using crude oils from the various reservoir within the Cohasset-Panuke-Balmoral and Venture fields.
- (c) To evaluate the primary and secondary cracking of kerogen and C_{15} + hydrocarbons for gas and condensate generation from some selected Kerogen Type IIB and IIA-IIB source rocks to determine the timing and an approximate amount of gas generation. Two types of gas generating

kinetics will be studied: (i) direct cracking of the kerogen macromolecule to form methane and other gases, and (ii) cracking of the generated crude oil within the organic matter which were not expelled earlier from the organic matter network.

3.0. ANALYTICAL PROCEDURES

3.1. Samples

Forty-two composite shale samples (unwashed cuttings), four core samples, and seven oil/condensate samples were analyzed (Fig. 1 and Tables 1 and 3). All rock samples were analyzed for organic petrography (organic facies and vitrinite reflectance) (Table 1). Those fortytwo composite shale samples from the Logan Canyon, Missisauga, Verrill Canyon and Mic Mac Formations were chosen from the following wells:Bluenose 2G-47 (between 4730-5797m), Citadel H-52 (5500-5620m), Eagle D-21 (10800-15900'), Intrepid L-80 (9280-12940'), Merogomish C-52 (2515-3950m), Onondaga B-96 (8100-13085'), Sable Island C-67 (9090-15100'), S. Venture O-59 (4340-6175m), Thebaud I-93 (3835-5000m), Venture D-23 (2700-2750m), Wenonah J-75 (8230-12040'). Forty rock samples were analyzed for Rock-Eval pyrolysis (Table 2). The samples used in the study for oil-oil and oil-source rock correlation are presented in Table 3. In Table 3a, the seven new samples are distinguished by the prefix "NS94" in their SIU (Southern Illinois University, Kruge, 1991, 1992, 1993) numbers. They include Balmoral M-32 (test 1), Cohasset A-52 (test 1), Cohasset D-52 (test 3), S. Venture O-59 (test 11), Venture B-13 (tests 6 and 4), and W. Venture C-62 (test 3). The asphaltenes analyzed are from the latter two samples. All four core samples (S. Desbarres O-76, 3801.88m; S. Sable B-44, 3938.3m; W. Chebucto K-20, 4043.1m; and N. Truimph B-52, 3773.5m) were analyzed for Rock-Eval pyrolysis and bitumen extraction. Based on those data, two samples (two extracted rocks and two bitumen extracts) were selected for kinetic analysis (Table 7a through 7d).

3.2. Methods

The methods adopted for organic facies, vitrinite reflectance, and Rock-Eval pyrolysis, were discussed in our earlier reports (Mukhopadhyay, 1991, 1993).

3.2.1. Aromatics Biomarkers and Pyrolysis-GC/MS of Oil Asphaltenes: Most of the analytical

and statistical methods have been described in detail previously by Kruge 1990; 1991; 1992; 1993. One difference in the current round of analyses is that asphaltenes were analyzed by pyrolysis-GC/MS, rather than py-GC-FID as was done previously. So that the data for the new samples would be compatible with the old, the five original asphaltenes were reanalyzed by py-GC/MS. The three rock extract asphaltenes were deasphaltened again by the method of Kruge (1992) in an attempt to remove contaminants previously noted. For pyrolysis-GC/MS, a CDS 120 Pyroprobe was coupled to an HP 5890A GC and an HP 5970B Mass Selective Detector. The GC was equipped with a 50 m HP-1 column (0.2 mm i.d., 0.33 µm film thickness), initially held at 40°C for 5 min., then raised to 300° at 5°/min., then held for 20 min. The mass spectrometer scanned from 50 to 450 Da, with an ionizing voltage of 70 eV. The Pyroprobe heated the sample at 610°C for 20 sec. The molecular ions of the compounds of interest were used for quantitation, except in the case of n-alkanes and n-alk-1-enes, for which the base peaks were used (m/z 57 and 55, respectively). Another difference is that the aromatic fractions were analyzed using a 50 m HP-1 column, rather than the 25 m column previously employed. The new temperature program was from 100 to 300°C at 3°/min., holding at 300° for 15 min. The aromatic data were collected in SIM mode, as described previously (Kruge, 1990; 1991; 1993), except that m/z 212 was omitted. This means that there are no data for dimethyldibenzothiophenes for the current group of samples.

Statistical processing of the quantitated, normalized and scaled aromatic GC/MS data was attempted two ways — 1) as described by Kruge (1990; 1991) and Mukhopadhyay and others (1995) and 2) by the method of Kruge (1993). The former method was found to yield results most compatible with the stratigraphic, petrologic and pyrolysis data and is presented in this report. In brief, the raw data were normalized according to compound class, scaled logarithmically, stripped of components which were sensitive to maturation and subjected to a multiple linear regression. The regression results were summarized by cluster analysis using the "single linkage" method. Refer to Kruge (1991) for a full explanation. The only difference in the method used in present report is the above-mentioned absence of dimethyldibenzothiophenes, as well as the absence of one dimethylbiphenyl peak due to a coelution problem on the 50 m column.

3.2.2. Pyrolysis-MS Kinetic Analysis: Pre-extracted rock and oil (bitumen) extract from two core samples (well: N. Truimph B-52, 3773.5m [no. 8355 in Tables 7a and 7b] and S. Desbarres O-76, 3801.88m [no. 8358 in Tables 7c and 7d]) were analyzed on a PYROMAT II MS micropyrolyzer. The temperature programme for the analysis was as follows: 10 minutes at 250°C and then pyrolyzed up to 750°C with three heating rates (50, 15, and 5°C/minute). The sample weight varies between 10 and 100 mg. In order to determine multicomponent kinetics, the following three mass fragment ions were monitored: (1) m15 - methane; (b) m29 - ethane; and (c) m43 - propane.

Hydrocarbon pyrograms are in good agreement with previous results (Burnham et al., 1987; Braun and Burnham, 1991). The two rock and two oil (bitumen) samples produced kinetic factors relatively close to each other or quite different depending on the monitored mass number.

3.2.3. Modelling of Hydrocarbon Generation Using BASINMODTM: In the BASIN-MOD program, geohistory/burial history constructs a geological model of stratigraphy versus time utilizing a wide range of parameters such as lithology, water depth, surface temperature, compaction, permeability, conductivity, subsidence, thermal history using either rifting heat flow or present day geothermal gradient. The model calculates the thermal conductivities automatically when the lithology or a mixture of lithologies is chosen. Compaction corrections have a significant impact on thermal history which, in turn, affects the timing of source rock maturity, petroleum generation and expulsion. For the modeling, the default compaction correction was used according to Sclater and Christie (Platt River Associates, 1992). The permeability factor considers the fluid flow (single phase) through porous media using Darcy's Law. For the modeling, Kozeny-Carmen/modified Kozeny Carmen default values were used.

BasinMod accepts one surface heat flow value which represents the total of all heat sources at the surface. For the modeling, Steady State Heat Flow was considered which is based on the simple relationship between heat flow and thermal conductivity. Rifting heat flow was taken as major heat source which usually decreases with time. One requirement for the calculation of rifting heat flow in BASIN-MOD is a β factor. Usually the default value for β is 2 in the BASIN-MOD Program. For this report, β was taken as 3 for the analyzed wells.

BMOD-BSM provides a n-component kinetic model which considers a parallel reaction

model and is based upon the method developed at Lawrence Livermore National Laboratory (1989, 1992, 1994). The kinetic approach considers the diversity of composition and distribution of the original kerogen. It calculates the multiple parallel reactions that occur as organic matter undergoes transformation to hydrocarbons (Burnham et al., 1987; Espitalie et al., 1987; Braun and Burnham, 1987, 1991). Each reaction has its own kinetic parameters such as percentage of kerogen with a specific activation energy and Arrhenius constant or Frequency factor (frequency with which certain reaction takes place). The kinetic approach considers the various HC potential for different kerogens. BMOD-KIM converts kerogens to oil and gas (4-component model). The oil can undergo secondary cracking to gas and residue. The expulsion efficiency in the ncomponent reaction is calculated on a "Saturation Method". In the saturation method, expulsion efficiency is controlled by a porosity saturation threshold. This suggests that hydrocarbons saturated beyond that threshold are expelled. The default saturation value is 0.20 (20% saturation). Analyzed organic facies data suggest that Kerogen Type IIB and IIA-IIB source rocks occur mostly as thin units (Mukhopadhyay, 1991, 1993, 1994a). Accordingly, the lithostratigraphic units were further subdivided into thin Kerogen Type IIB or IIA-IIB and thick Kerogen Type III units. Tables 8a and 8b illustrate the revised lithostratigraphic units for the wells N. Truimph G-43 and S. Desbarres O-76, respectively.

In the BasinMod program, three wells (S. Desbarres O-76, N. Truimph B-52, and Venture B-52) were selected to estimate the generation and migration of various hydrocarbon components (methane, C_2 - C_5 gases, C_6 - C_{15} condensates, and C_{15} +) from selected source rocks. Accordingly, the analyzed muliticomponent kinetics data were utilized within "Reaction Networks" of BasinMod. The kinetics of ethane generation (m29) is used for C_2 - C_5 hydrocarbons and the kinetics for propane (m43) generation was used for C_6 - C_{15} (condensate range).

In the "Reaction Networks", three stages of data input are required: (a) network structure; (b) reaction constants; and (c) product properties. In the *network structure*, the proportion of primary cracking (kerogen to C_{15} +, methane, C_2 - C_5 , C_6 - C_{15} and residue) and secondary cracking (C_{15} + to methane, C_2 - C_5 , C_6 - C_{15} , and residue) are arbitrarily chosen. In the *reaction constants*, the actual distribution of activation energies in relation to percentages of hydrocarbon conversion for the n-components (1. kerogen to C_{15} +, methane, C_2 - C_5 , and C_6 - C_{15} ; 2. C_{15} + to methane, C_2 - C_5 , and C_6 - C_{15}) were inserted. The third input requires the actual density and expulsion criteria of

each n-components. For those input data, three Kerogen Types (IIA-IIB, IIB, and III) were used. The n-component kinetics for Kerogen Type IIA-IIB and IIB were determined in this report. For Kerogen Type III, the default n-component kinetics of Brent coal was used (Platt River Associates, 1994). The following input data for density were used: C_{15} + = 0.81-0.84; C_6 - C_{15} = 0.73 to 0.78; C_2 - C_5 gases = 0.1; methane = 0.007 to 0.01. In this report, 1-D modelling of two wells (N. Truimph B-52/G-43 and S. Desbarres O-76) was reported to show the amount of generated and expelled n-components (methane, C_2 - C_5 , C_6 - C_{15} , and C_{15} +) through time from various source rock intervals.

4.0. RESULTS AND DISCUSSIONS

4.1. Organic Facies

Except for the Merigomish C-52 samples, the majority of the composite shale samples analyzed for this report, have abundant vitrinite and inertinite group of macerals indicating predominance of terrestrial organic matter and oxidation during tranport and at the depositional interface (Table 1). Those samples also contain oxidized liptinites such as sporinite and resinite as revealed by the transparency and fluorescence colour (example: samples from Onondaga B-96). All analyzed samples from Merigomish C-52, except one, contain algal derived organic matter (telalginite, lamalginite, exinite [algal spore], AOM 2). The sample at 3730m in Merigomish, contains more than 50% AOM 2 derived from degradation products of algal and terrestrial liptinite. Based on organic facies (having fluorescent lamalginite and AOM 2), all analyzed samples from the Logan Canyon Formation in Merigomish C-52 can be considered as Kerogen Type IIA-IIB and IIB. On the other hand, composite shale samples from the same formation, as well as underlying formations in Wenonah J-75, 18 kms to the east show abundant oxidation forming mainly Kerogen Type III and III-IV. Except for a sample from 4860m, most samples from Thebaud I-93 are contaminated with drilling mud additives (example: lignosulfonate) in spite of thoroughly cleaning and handpicking the sample.

4.2. Rock-Eval Pyrolysis

Table 2 illustrates the data of various Rock-Eval pyrolysis parameters (S_1 , S_2 , S_1+S_2 , S_3 , PI, HI, OI, T_{max} , and TOC) from the 40 composite shale samples. The total organic carbon

content of the whole rock samples varies between 0.56 (S. Venture O-59, 4475-4610m) to 5.12% (Bluenose 2G-47, 5260-5500m)).

Considering the depth and total organic carbon content of the samples, the amount of S_1 (thermal extraction below 300°C) fraction is considered as extremely high (Table 1A)(Tissot and Welte, 1984). Anomalously high S_1 content may be caused by: (a)contamination from drilling mud additives, especially hydrocarbons; (b) early generation of hydrocarbons; and (c) soaking of allochthonous bitumen or migrated petroleum. At this stage, it is difficult to predict the cause of the S_1 anomaly. Petrological evaluation of those samples (except samples from wells Thebaud I-93 and S. Venture O-59) ruled out the possibility of contamination by drilling mud additives.

Except for samples from Merigomish C-52, the S_2 fraction of most samples have <1 mg HC/g of rock suggesting extremely low potential for crude oil (Table 2). The low S_2 can also be caused by the retention of liquid hydrocarbons (derived from cracking of kerogen) within the mineral matrix (Espitalie et al., 1985; Mukhopadhyay, 1989 and references therein).

Except for the Thebaud and S. Venture wells, T_{max} (maturation parameter) values in composite shale samples increase with depth. The suppression of T_{max} in some wells may be caused by the anomalously high S_1 (free hydrocarbons) content of the samples or the presence of lignite contamination.

4.3. Maturation and Source Rock Potential

Vitrinite reflectance data (Table 1) of all samples (except one sample from Merigomish C-52) are considered as mature (between 0.5 to 1.3% R_o) to overmature (>1.4% R_o). In most cases, vitrinite reflectance values increase with the depth of the sediment. The vitrinite reflectance values in the deeper sediments, in most cases, do not correlate with the T_{max} values which are possibly caused by bitumen absorption within the whole rock matrix or due to lignite contamination. Merigomish C-52 shows a sharp increase in vitrinite reflectance between 2515m (0.48% R_o) and 3950m (0.99% R_o) possibly due to normal faulting. The presence of exhausted AOM 2 corresponds with the higher reflectance at 3950m. The lowest reflectance is observed at 2515m in Merigomish C-52 and the highest reflectance was observed at 6175m in S. Venture O-59.

Statistically, 4.8% of the 42 analyzed samples are oil- and condensate-prone Kerogen

Type IIA-IIB; 28.6% are condensate- and gas-prone Kerogen Type IIB; 61.8% are gas-prone Kerogen Type III; and 4.8% are interpreted as Kerogen Type III-IV which is considered as nonsource rock for major liquid hydrocarbons and gas. This interpretation is based mainly on organic facies analysis as Rock-Eval pyrolysis data are influenced by maturation and contamination. Most analyzed source rocks are mature for oil and gas generation.

4.4. Aromatic Biomarkers

As part of an ongoing organic petrological and geochemical study in the Scotian Basin (Mukhopadhyay et al., 1995), the aromatic fractions of 21 petroleums and 18 rock extracts had been evaluated by gas chromatography/mass spectrometry (GC/MS) (Kruge, 1990; 1991; 1993) (Tables 3a and 3b). The thermal maturity levels were determined for each sample and two statistical approaches to oil classification and oil-source rock correlation were attempted, as described in detail in the above reports. Asphaltenes from two oils and three rock extracts were analyzed by pyrolysis-gas chromatography, providing additional evidence (Kruge, 1992). This report documents the results of the analysis of 7 additional petroleum aromatic fractions and two additional petroleum asphaltenes.

4.4.1. Maturity Determination From Polyaromatic Hydrocarbon Distributions: Polyaromatic hydrocarbons (PAH) have been shown to be very sensitive to levels of thermal maturation, as was discussed previously in detail (Kruge, 1990; 1991; 1993). As was done before, the initial maturity assessment was made using the methylphenanthrene index (MPI), cast in the form "R_c", which is an estimate of the percent reflectance of vitrinite. The new samples may be seen in their maturity context in Table 4 and Figure 2A. The new Cohasset, S. Venture and Balmoral oils show maturity levels compatible with the early to early middle oil window. The Venture and W. Venture oils appear to be in the upper oil window, with Venture B-13 (test 4) being the most mature of the group.

4.4.2. Oil Classification and Oil-Source Rock Correlation: The statistical results discussed in this report represent both 1) an incorporation of the new PAH data into the preexisting matrix and 2) a revision of last year's study (Kruge, 1993). It is a return to the methods employed in the first

reports (Kruge, 1990; 1991; Mukhopadhyay et al., 1995), which appear to be more compatible with other information available (see methods section). It must be remembered that a very high coefficient of determination is required for a good match, since the single linkage method was employed in the cluster analysis. The full correlation matrix is presented in Table 5 and the dendrogram (Figure 2B) summarizes the genetic relationships between the samples.

The Venture and W. Venture petroleums match well with the previously recognized "Group 1" oils. The S. Venture and Cohasset A-52 oils have only limited similarities with this main oil group. The new Balmoral and Cohasset D-42 petroleums do not correlate well with any other samples, including the old samples from the same wells.

Although no new source rock extracts were analyzed, it is interesting to reexamine the data in light of the revised statistics. Samples from the Middle and Lower Missisauga Fm., undifferentiated Logan Canyon Fm., the Penobscot Limestone of the Mic Mac Fm. and the Baccaro Mbr. of the Abenaki Fm. are all reasonably compatible with the Group 1 oils. In contrast, the samples from the Naskapi Mbr. (Logan Canyon Fm.), Misaine Mbr. (Abenaki Fm.) and Verrill Canyon Fm. show no correlation with any of the oils. However, not all of the Missisauga and Mic Mac samples match the Group 1 oils. In particular, those labeled "undifferentiated" (Table 3b) correlate poorly. None of the rock samples seem to match the non-Group 1 oils, including the Cohasset petroleums. This does not eliminate the possibility of multiple sourcing.

4.5. Pyrolysis-GC/MS of Oil Asphaltenes and Oil-Oil/Oil-Source Rock Correlation

The samples of Venture B-13 (DST 4) and W. Venture C-62 (DST 3) received for asphaltene pyrolysis were less than satisfactory, as they were in fact polar fractions. An attempt was made to separate asphaltenes from them, but yields were less than 1 mg in both cases. Judging by the total ion current traces (Figure 3), the samples are heavily contaminated with silanes, carboxylic acids, phthalates, etc. Styrenes are also present, which may either be contaminants or true pyrolysis products of the samples. Nevertheless, the mass spectrometer permits the confident recognition and quantitation of aromatic hydrocarbons, including benzenes, naphthalenes, indenes, phenanthrenes, anthracenes, and pyrenes. Fluorenes are unusually strong in both samples. Normal alkanes and alkanes are weak; thiophenes are barely detectable. Phenols

are significant components, particularly in the W. Venture sample (Figures 3 and 4). Comparison of Figures 4A and 4B indicates that the samples are similar, confirming the correlation based on PAH (Figure 2B). A mid to late oil window maturity level is indicated by the MPR and TRMN ratios (Table 6), confirming assessments based on the aromatic fraction data (Table 4).

The presence of phenols and lack of thiophenes in the Venture and W. Venture samples indicate a strong terrestrial influence on the organic matter that formed the petroleum. Since these oils belong to the "Group 1" family (Figure 2B), it seems likely that a terrestrial kerogen type is responsible for the bulk of these petroleums. Lower Missisauga samples, such as those from S. Desbarres O-76 and Venture B-52, are candidate source rocks based on their aromatic fractions (Figure 2B). Their asphaltene pyrolyzates, although still contaminated even after repeated deasphaltening, show good correspondence with the two oils (Figure 4 and Table 4), particularly in their high aromaticity. The differences in phenol content may be ascribed to variations in maturity, as the S. Desbarres sample is less mature and the Venture B-52 sample is more mature than the two oils (Tables 4 and 6). The phenol content in terrestrially derived samples will be high initially, dropping off as peak oil generation is reached (Kruge and Bensley, 1994).

Among the other two oil asphaltenes, the Cohasset A-52 sample is very rich in aliphatic components (Figure 4 and Table 6), although the predominance of alkanes over alkenes suggests that deasphaltening was not complete (Kruge, 1992). The Naskapi rock asphaltene, from N. Truimph G-43, is extremely rich in aliphatics, suggesting a predominance of algal material, perhaps lacustrine, since the thiophene content is low. Oil from the Sable Island discovery has an intermediate aromaticity. These oils may originate from multiple source horizons containing different organic matter types in varying proportions, whereas "Group 1" oils may have been derived for the most part from terrestrial kerogens.

Using aromatic biomarkers in GCMS and pyrolysis-MS of asphaltenes of oils, an attempt was made at oil-oil correlation of various reservoirs in the Cohasset-Panuke-Balmoral fields. Figure 5a shows the reservoir stratigraphy of Cohasset, Panuke, Balmoral fields characterizing the number of tested and analyzed reservoirs as well as nonavailable reservoir samples. A comparison of all analytical data of 1991, 1993, and 1995 showed some salient variations in reservoir properties (Fig. 5b). This is possibly due to the change in the number of maturity-sensitive aromatic biomarkers used in different years. Based on this oil-oil correlation, Balmoral

M-32, DST #1 & #3, Cohasset D-42, DST #7, Panuke B-90, DST #1, Penobscot L-30, DST #5 showed strong correlation among each other (r² >0.85; Fig. 5c). Cohasset A-52, DST #5 and #11 also show fairly high correlation (r² > 0.8) with the main cluster. Only two oils (Panuke PP3 J-99, DST #1 and Cohasset D-42, DST #3) show poor correlation. This variation in correlation within various reservoirs may be related to reservoir properties such as temperature, pore pressure, water chemistry, etc., rather than type and maturity of the source rocks from which they are generated and migrated.

4.6. Multicomponent Kinetics

The multicomponent (methane, ethane, and propane) kinetics of both extracted rock (kerogen part) and bitumen extract (generated oil part) show wide variation of activation energy distribution and Arrhenius Factors (Table 7a through 7d and Figures 6a through 6d). For methane generation from Kerogen Type IIA-IIB (N. Truimph B-52/G-43) higher (between 48 and 53 kcal/mole) activation energy is required compared to Kerogen Type IIB (S. Desbarres O-76) (between 45 and 50 kcal/mole) (Tables 7a and 7c). In general, cracking of both kerogen and C_{15} + to ethane requires less energy compared to generation of methane and propane. The lowest T_{max} values (454-422-398°C) were observed on cracking of C_{15} + to ethane in Kerogen Type IIA-IIB for all temperatures of pyrolysis. Generally, the highest T_{max} value is recorded during the generation of methane cracked from both kerogen and oil. It is interesting to note that cracking of C_{15} + to methane in Kerogen Type IIB requires the highest activation energy distribution and Arrhenius Factor compared to any sample (Table 7a through 7d).

4.7. Modelling of Hydrocarbon Generation and Expulsion for N-Components

A preliminary assessment of generation and expulsion of various hydrocarbon components (methane, C_2 - C_5 , C_6 - C_{15} , and C_{15} +) was made for selected stratigraphic intervals from both the N. Truimph G-43/B-52 and S. Desbarres O-76 wells [Figs. 7a through 7r(ii) and 8a through 8q]. Because the 1-D modelling using n-component kinetics is extremely complex, more work is needed to assess the hydrocarbon mass balance in the Sable Island area. At this stage, only comparable generation and expulsion of various n-components from similar lithostratigraphic units and different kerogen types from the two wells were evaluated (all Figs 7 and 8).

Accordingly, the expulsion of methane from various stratigraphic intervals was compared (Table 9). Moreover, a comparable assessment was made on methane expulsion from selected intervals where both default Type III (Brent Coal) and analyzed IIB kinetics were used for Kerogen Type III rock intervals (Table 10).

Figues 7a and 8a showed the generation and expulsion of n-components from various Kerogen Type IIB (genetic potential 175 mg/g TOC) and Figues 7b and 8b for Kerogen Type III (genetic potential 90 mg/g TOC) stratigraphic intervals from both wells. The data implied higher generation and expulsion of various n-components for Kerogen Type IIB intervals compared to Kerogen Type III intervals and C₁₅+ hydrocarbons are cracked to methane in the deeper part of the section. The data also suggest that N. Truimph G-43/B-52 well has generated and expelled almost double the amount of various n-components, compared to the S. Desbarres O-76 well, because of the abundance of Kerogen Type IIB source rock units in the N. Truimph well.

In this report, only the expulsion of methane from various stratigraphic intervals was studied. In N. Truimph G-43/B-52, 16 intervals were evaluated (Table 9a). In intervals having Kerogen Type IIB, the methane expulsion increased from ~7 mg/g TOC (Mississauga 1 at 3665m) to 70 mg/g TOC (MM6 at 10,800m). Using the comparable kinetics (analyzed IIB and default III) for various Kerogen Type III intervals showed that (1) up to a depth of 6850 m, methane expulsion is higher for analyzed kinetics compared to the default kinetics (Units TJ1 and TJ3), and (2) beyond 6850m, default Type III kinetics expelled higher methane (Units MM1, MM3, MM5, and MM7) compared to the analyzed Type IIB kinetics.

In the S. Desbarres O-76 well, for various Kerogen Type IIB intervals, the methane expulsion varies between ~8 (unit TJ2) to 50 (unit J2a) mg/g TOC. However, the comparable kinetics between analyzed type IIB and default III showed a reverse trend compared to N. Truimph. In the younger horizon (unit TJ3), default III kinetics expelled more methane compared to measured IIB kinetics. On the other hand, the deeper interval (unit J2b) showed the reverse trend. This anomolous relationship could not be resolved by comparing the lithological variation in those units.

The timing of methane expulsion in various units differs depending on the variation of their maturity or depth. For stratigraphic unit MM5 in N. Truimph B-52 (Begin_Age: 191.5;

Kerogen Type III), the methane expulsion started around 190 mybp and reached its peak around 120 mybp. The methane expulsion in the unit MM5 of S. Desbarres (Begin Age: 174.5; Kerogen Type III) started around 115 mybp and reached its peak in the last 50 mybp. In unit Mississauga 3 of N. Truimph well (Kerogen Type IIB), migration of methane started around 105 mybp (million year before present) and reached its peak around last 5 my. In unit TJ2 (Kerogen Type IIB) of the same well, the expulsion started around 130 mybp and reached its peak around 20 mybp (Table 9a). At the present time, this unit has reduced its capability for major gas expulsion. On the contrary, in S. Desbarres O-76, the similar (Begin_Age) unit (MicMac, Kerogen Type IIB) started expelling around 90 mybp and reached its peak in the last 10 mybp (Table 9b). This suggests that expulsion of methane is active in the Scotian Shelf in the present time.

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7.0. TABLES AND FIGURES

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 - h. Unit Top Jurassic: kerogen IIB; kinetics IIB
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 - i (ii). Unit TJ1: kerogen III; kinetics III
 - j. Unit TJ2: kerogen IIB; kinetics -IIB.
 - k (i). Unit TJ3: kerogen III; kinetics IIB
 - k (ii). Unit TJ3: kerogen III; kinetics III
 - 1 (i). Unit MM1: kerogen III; kinetics IIB
 - 1 (ii). Unit MM1: kerogen III; kinetics III
 - m. Unit Mic Mac: kerogen IIB; kinetics IIB
 - n. Unit MM2: kerogen IIB; kinetics IIB
 - o (i). Unit MM3: kerogen III; kinetics IIB
 - o (ii). Unit MM3: kerogen III; kinetics -III
 - p (i). Unit MM5: kerogen III; kinetics IIB
 - p (ii). Unit MM5: kerogen III; kinetics -IIB
 - q. Unit MM6: kerogen IIB; kinetics IIB
 - r (i). Unit MM7: kerogen III; kinetics IIB
 - r (ii). Unit MM7: kerogen III; kinetics III
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- a. N-component generation and migration of all units having using IIB kinetics, well: S. Desbarres O-
- b. N-component generation and migration of all units having using IIB kinetics.
- kerogen type IIB and
- Kerogen Type III and
- N-Component generation and expulsion (in mg/g TOC)
- c. Unit Top Jurassic: kerogen IIA/IIB; kinetics IIA-IIB.
- d. Unit TJ1: kerogen III; kinetics IIB
- e. Unit TJ2: kerogen IIB; kinetics -IIB.
- f (i). Unit TJ3: kerogen III; kinetics IIB
- f (ii). Unit TJ3: kerogen III; kinetics III
- g. Unit Mic Mac: kerogen IIB; kinetics IIB
- h. Unit MM1: kerogen III; kinetics IIB
- i. Unit MM3: kerogen IIB; kinetics IIB j. Unit MM3: kerogen - III; kinetics - IIB
- k. Unit MM4: kerogen IIB; kinetics IIB
- 1 (i). Unit MM5: kerogen III; kinetics IIB
- 1 (ii). Unit MM5: kerogen III; kinetics -IIB
- m. Unit J1: kerogen IIB; kinetics IIB
- n. Unit J2: kerogen III; kinetics III
- o. Unit J2a: kerogen IIB; kinetics III

- p (i). Unit J2b: kerogen III; kinetics IIB
- p (ii). Unit J2b: kerogen III; kinetics III
- q. Unit Mohican: kerogen III; kinetics IIB

TABLE 1: Maceral Composition in volume percent (organic facies), Ro, kerogen type, and oil/gas potential of composite shale samples

Borehole No.	Depth (ft/m)	Fm/ Member	, R	Vit	Ipt	Exe	Res	Lam	Tel	PE	aom 2	aom 3	Bit	Rank	Kerogen Type	Oil/Gas Potent.
Bluenose2G-47	4730-4830m	lr.Miss	1.09	37	50	7		1						'n	目	Gas
	5050-5225m	MicMac	1.39	25	. 09	5								6	Ш	Gas
	5260-5500m	MicMac	1.38	25	8	6		11			11	1		10	IIB	Cond/Gas
	5695-5797m	MicMac	1.52	35	42	7	1	1	1		10			33	IIB	Cond/Gas
Citadel H-52	5500-5620m	MicMac	1.81	51	28	10		1		1	2			3	Ш	Gas
Eagle D-21	10800-11670'	Naskapi	0.58	45	30	18	1				3				Ш	Gas
	11800-12600'	up.Miss	0.70	51	32	14	2					1			Ħ	Gas
	13400-14400'	up.Miss	0.76	35	53	8					2			2	目	Gas
	14550-15290	lr.Miss	0.81	42	41	12			1	1	2				ш	Gas
Intrepid L-80	9280-9680	Naskapi	0.58	4	34	13	1	1	1	1	3		П		IIB	Cond/Gas
	10750-11250°	m.Miss	0.63	41	45	11					2			1	Ш	Gas
	11575-12400'	m.Miss	0.68	33	54	11					1				Ш	Gas
	12400-12940'	m.Miss	0.72	39	37	11	1	1			1		2	8	IIB	Cond/Gas
Merigomish C- 52	2515-2690m	Cree	0.48	26	36	26	2	4		1	4				EII	Cond/Gas
	2740-2895m	Cree	09:0	22	30	20	1	2	1		19	5			m m	Cond/Gas
	3000-3200m	Cree	0.69	25	35	30	П		1		3	1	2	1	IIB	Cond/Gas
	3250-3500m	Cree	0.79	78	37	15	1	5			11	1	2		IIB	Cond/Gas
	3525-3700m	Cree	0.82	23	29	5	П	33	1		30	1	1	7	IIB	Cond/Gas
	3730-3950m	Naskapi	0.99	13	28	1	1			-	56				IIA-IIB	Oil/Cond

TABLE 1 (continued): Maceral Composition in volume percent, Ro, kerogen type, and oil/gas potential of composite shale samples

Borehole No.	Depth	Fm/	R	Vit	Int	Exe	Res	Lam	Tel	Ltd	aom	aom	Bit	Rank	Kerogen	Oil/Gas
	(ft/m)	Member				1					2	3		Int	Type	Potent.
Onondaga B-96	8100-8700°	Naskapi	0.50	42	28	25	3	-	П		П				Ш	Gas
	9200-9750	up.Miss	0.50	32	30	30	9	1			-				IIB	Cond/Gas
	11890-12000*	m.Miss	0.67	27	50	17	5			1					ш	Gas
	12000-12328	m.Miss	0.71	29	47	18	4	2							ш	Gas
Sable Island C-67	9090-9700'	Naskapi up.Miss	0.51	34	36	26*	2					1			ш	Gas
	11050-11800*	m.Miss	0.61	26	43	72	2	1					1		田	Gas
	13100-13600*	lr.Miss	0.65	19	52	23	2	-					1		ш	Gas
	14000-15100*	lr.Miss	0.82	20	43	32		1	-			1	2		Ш	Gas
S. Venture O-59	4340-4475m	lr.Miss	0.78	25	40	33	1						1		ш	Gas
	4475-4610m	lr.Miss	0.84	24	37	35	П	1			1		7		Ш	Gas
	4895-5035m	lr.Miss	1.13	39	35	12					8	3	2		Ш	Gas
	5865-6175m	MicMac	1.97	31	54	2					2		2	20	IIB (over- mature)	Cond/Gas
Thebaud I-93	3835-3915m	lr.Miss	0.68	4	32	20					1				ш	Gas
	4115-4310m	lr.Miss	0.81	45	41	11	Н			:	1				III (high lignite contamina- ton	Gas (?)
	4410-4625m	lr.Miss	0.96	40	20	7					1		2		Same as above	Gas (?)
	4665-4850m	lr.Miss	1.04	46	35	13					4				III (minor contarnina- tion	Gas (?)
	4860-5000m	lr.Miss	1.49	22	28	4	4				36	4		2	Depleted IIA-IIB	Oil/Cond

TABLE 1: Maceral Composition in volume percent (organic facies), R., kerogen type, and oil/gas potential of composite shale samples

								1					-			
	Depth (ft/m)	Fm. or Member	R°	Vit	Imt	Exe	Res	Lam	Tel	Ltd	aom 2	aom 3	Bit	Rank Int	Kerogen Type	Oil/Gas Potent.
(4	2700-2750m	Cree	0.45	23	46	23	9	П			-				EIB	Cond/Gas
at any are dependent																
ω,	8230-8630	Cree	0.56	32	56	∞	2	-		-	-				VI-III	Minor Gas
(X)	8630-9060°	Cree	19.0	30	95	11	2								W-IV	Minor Gas
~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	9200-10000	Naskapi up.Miss	0.72	39	49	6	2								Ш	Gas
	10600-11400	up.Miss VerrCan	0.77	38	49	11					2				田田	Gas
— ************************************	11400-12040°	VerrCan Argo	0.82	37	51	111									目	Gas

Ltd = liptodetrinite; aom 2 = amorphous organic matter 2 (oil and condensate); aom 3 = amorphous organic matter 3 (gas); Bit = solid bitumen; Rank Int = rank inertinite or oxidized liptimite; Oil/gas potent. = oil and gas potential; * = oxidized phytoclasts; Nonsour. = nonsource rock; Cree = Cree Member, Logan Canyon Formation; up.Miss= upper member, Mississauga Formation; m.Miss= middle member Mississauga Formation; lr.Miss= lower member, Mississauga Formation; VerrCan=Verrill Canyon Formation. LEGEND:Fm = Formation; R_o = mean random vitrinite reflectance; Vit = vitrinite; Int = Inertinite; Exe = Exemite; Res = Resinite; Lam = Lamalgimite; Tel = telalgimite

Table 2: Rock-Eval pyrolysis data

```
:depth: qty:tmax: s1 : s2 : s3 : p i :s2/s3 : pc : toc : hi : oi :
: BLUENOSE 2G-47
: 4730-4830m
: 4730:100.0: 435: 0.52: 1.36: 3.64: 0.28: 0.37: 0.15: 3.45: 39: 105:
: 4730:100.3: 436: 0.50: 1.42: 3.50: 0.26: 0.40: 0.16: 3.47: 40: 100:
: 5050-5225m
: 5050:100.6: 313: 1.85: 3.71: 6.83: 0.33: 0.54: 0.46: 5.02: 73: 136:
: 5050:100.5: 314: 1.75: 3.62: 7.16: 0.33: 0.50: 0.44: 5.00: 72: 143:
: 5260:100.6: 422: 1.14: 2.81: 6.28: 0.29: 0.44: 0.32: 5.12: 54: 122:
: 5260:100.7: 422: 1.11: 2.70: 6.19: 0.29: 0.43: 0.31: 5.08:
: 5695m-TD
: 5695:100.5: 421: 0.84: 1.87: 3.26: 0.31: 0.57: 0.22: 3.32: 56: 98:
: 5695:100.8: 421: 0.85: 1.83: 3.21: 0.32: 0.57: 0.22: 3.38: 54: 94:
: CITADEL H-52
: 5500-5620m
: 5500:100.3: 418: 0.51: 0.66: 2.51: 0.44: 0.26: 0.09: 1.43: 46: 175:
: 5500:100.2: 418: 0.49: 0.56: 2.47: 0.47: 0.22: 0.08: 1.47: 38: 168:
EAGLE D-21
:10800-11670
:10800: 99.8: 435: 0.07: 0.60: 0.91: 0.11: 0.65: 0.05: 1.35: 44: 67:
:10800:100.5: 435: 0.07: 0.61: 0.88: 0.10: 0.69: 0.05: 1.35:
:11800:100.1: 436: 0.09: 0.66: 0.51: 0.12: 1.29: 0.06: 1.28:
:11800:100.6; 437: 0.09: 0.66: 0.49: 0.12: 1.34: 0.06: 1.31:
:13400-14400'
:13400:100.6: 442: 0.06: 0.43: 0.59: 0.12: 0.72: 0.04: 0.79: 54:
:13400:100.7: 442: 0.06: 0.40: 0.57: 0.13: 0.70: 0.03: 0.81: 49:
:14550-TD
:14550:100.1: 446: 0.14: 0.44: 0.51: 0.24: 0.86: 0.04: 0.83: 53: 61:
:14550; 99.9; 446; 0.16; 0.47; 0.48; 0.26; 0.97; 0.05; 0.83; 56; 57;
:14550:100.4: 445: 0.13: 0.41: 0.50: 0.24: 0.82: 0.04: 0.83: 49: 60:
INTREPID L-80
: 9280-9680'
: 9280; 99.9; 434; 0.15; 0.46; 0.87; 0.25; 0.52; 0.05; 0.99; 46; 87
: 9280:100.0: 433: 0.15: 0.41: 0.96: 0.27: 0.42: 0.04: 1.00: 41: 96
:10750-11250'
:10750:100.5: 436: 0.15: 0.73: 0.65: 0.17: 1.12: 0.07: 1.16: 62: 56
:10750:100.9; 435; 0.15; 0.79; 0.69; 0.16; 1.14; 0.07; 1.18; 66; 58
:11575-12400'
:11575:100.4: 438: 0.08: 0.56: 0.40: 0.12: 1.40: 0.05: 0.87:
:11575:100.3: 438: 0.08: 0.60: 0.37: 0.12: 1.62: 0.05: 0.88:
:12400-12940'
:12400:100.0; 442; 0.09; 0.53; 0.27; 0.15; 1.96; 0.05; 1.00; 53;
                                                               27
:12400:100.0; 442; 0.10; 0.56; 0.30; 0.15; 1.86; 0.05; 1.02;
```

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:DEPTH: QTY:TMAX: S 1 : S 2 : S 3 : P I :S2/S3 : P C : TOC : H I : O I :
MERIGOMISH C-52
: 2515-2590m
: 2515:100.0; 431: 3.66: 2.61: 0.77: 0.58: 3.38: 0.52: 1.70: 153: 45:
: 2515:100.5: 431: 3.66: 2.74: 0.81: 0.57: 3.38: 0.53: 1.68: 163: 48:
: 3000-3200m
: 3000:100.1: 431: 2.61: 3.16: 0.89: 0.45: 3.55: 0.48: 1.91: 165: 46:
: 3000:100.2: 431: 2.60: 3.21: 0.87: 0.45: 3.68: 0.48: 1.87: 171: 46:
: 3250-3500m
: 3250: 99.8: 435: 5.12: 6.55: 1.42: 0.44: 4.61: 0.97: 3.51: 186:
: 3250:100.5; 434; 5.17; 6.68; 1.55; 0.44; 4.30; 0.98; 3.52; 189; 44;
: 3525-3700m
: 3525; 99.8; 438; 6.06; 4.92; 1.25; 0.55; 3.93; 0.91; 4.07; 120;
: 3525:100.2: 439: 5.96: 4.97: 1.22: 0.55: 4.07: 0.91: 3.99: 124: 30:
: 3730-3950m
: 3730:100.5: 438: 5.16: 5.33: 1.29: 0:49: 4.13: 0.87: 3.80: 140: 33:
: 3730:100.7: 436: 5.19: 5.11: 1.29: 0.50: 3.96: 0.85: 3.78: 135: 34:
ONONDAGA B-96
: 8100-8700'
: 8100:100.1: 430: 0.44: 1.30: 1.39: 0.25: 0.93: 0.14: 1.89: 68: 73
: 8100:100.4: 428: 0.45: 1.27: 1.43: 0.26: 0.88: 0.14: 1.88: 67:
: 9200-9750'
: 9200:100.8: 427: 0.49: 1.14: 0.63: 0.30: 1.80: 0.13: 1.08: 105:
: 9200:100.5: 426: 0.48: 1.17: 0.60: 0.29: 1.95: 0.13: 1.10: 106: 54
:11890-12000'
:11890:100.7: 438: 0.23: 0.68: 0.37: 0.26: 1.83: 0.07: 1.07: 63: 34:
:11890:100.2: 437: 0.23: 0.68: 0.39: 0.26: 1.74: 0.07: 1.05: 64: 37:
:12000:100.4: 440: 0.28: 0.61: 0.54: 0.32: 1.12: 0.07: 1.03: 59: 52:
:12000:100.6; 438: 0.28: 0.64: 0.53: 0.30: 1.20: 0.07: 1.03: 62: 51:
: SABLE ISLAND C-67
: 9090-9700'
: 9090:100.3: 429: 0.11: 0.28: 0.63: 0.29: 0.44: 0.03: 0.75: 37: 84:
: 9090:100.5: 429: 0.11: 0.32: 0.59: 0.26: 0.54: 0.03: 0.74: 43: 79:
:11050-11800'
:11050:100.1: 435: 0.11: 0.80: 0.48: 0.12: 1.66: 0.07: 1.34: 59: 35:
:11050:100.4: 438: 0.11: 0.82: 0.48: 0.12: 1.70: 0.07: 1.38: 59: 34:
:13100-13600'
:13100:100.1: 440: 0.32: 0.59: 0.25: 0.36: 2.36: 0.07: 0.62: 95: 40:
:13100:100.2: 436: 0.35: 0.61: 0.26: 0.36: 2.34: 0.08: 0.63:
:14000'-TD
:14000:100.4: 444: 0.30: 0.76: 0.38: 0.28: 2.00: 0.08: 0.87: 87: 43:
:14000: 99.8: 444: 0.31: 0.74: 0.38: 0.30: 1.94: 0.08: 0.86: 86: 44:
: SOUTH VENTURE O-59
: 4340-4475m
: 4340:100.4: 445: 0.07: 0.53: 0.56: 0.12: 0.94: 0.05: 0.80: 66: 70:
: 4340:100.0: 442: 0.09: 0.49: 0.51: 0.16: 0.96: 0.04: 0.77: 63:
: 4475-4610m
: 4475:100.2: 451: 0.10: 0.39: 0.39: 0.21: 1.00: 0.04: 0.56: 69: 69:
```

: 4475:100.7: 448: 0.09: 0.43: 0.38: 0.17: 1.13: 0.04: 0.59: 72: 64:

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:DEPTH: OTY :TMAX: S 1 : S 2 : S 3 : P I :S2/S3 : P C : TOC : H I : O I :
S. VENTURE O-59 (Continued)
: 4895-5035m
: 4895;100.0: 431: 0.53: 0.37: 1.02: 0.59: 0.36: 0.07: 0.98: 37: 104:
: 4895:100.0: 430: 0.56: 0.36: 1.03: 0.61: 0.34: 0.07: 0.96: 37: 107:
: 5865m-TD
: 5865:100.1: 426: 1.22: 1.67: 3.27: 0.42: 0.51: 0.24: 4.83: 34: 67:
: 5865: 99.7: 427: 1.27: 1.66: 3.24: 0.43: 0.51: 0.24: 5.05: 32: 64:
: THEBAUD I-93
: 3835-3915m
: 3835:100.9: 438: 0.18: 0.40: 0.59: 0.31: 0.67: 0.04: 0.61: 65:
: 3835:100.8: 438: 0.17: 0.41: 0.58: 0.29: 0.70: 0.04: 0.62: 66:
: 4115-4310m
: 4115: 99.6: 443: 0.36: 0.43: 2.26: 0.46: 0.19: 0.06: 1.11: 38: 203:
: 4115:100.4: 443: 0.35: 0.42: 2.27: 0.46: 0.18: 0.06: 1.10: 38: 206:
: 4410-4625m
: 4410:100.1: 451: 0.38: 0.39: 1.95: 0.50: 0.20: 0.06: 1.12: 34: 174:
: 4410:100.2: 448: 0.38: 0.44: 1.99: 0.46: 0.22: 0.06: 1.13: 38: 176:
: 4665–4850m
: 4665:100.4: 443: 0.61: 0.69: 2.41: 0.47: 0.28: 0.10: 1.94: 35: 124:
: 4665:100.1: 443: 0.63: 0.69: 2.35: 0.48: 0.29: 0.11: 1.94: 35: 121:
: 4860-5000m
: 4860: 99.9: 429: 0.98: 1.19: 4.88: 0.45: 0.24: 0.18: 3.73: 31: 130:
: 4860: 99.6: 428: 0.99: 1.24: 4.97: 0.45: 0.24: 0.18: 3.77: 32: 131:
: WENONAH J-75
: 8230-8630'
: 8230: 99.7: 432: 0.29: 0.67: 1.16: 0.30: 0.57: 0.08: 1.20: 55:
                                                         96:
: 8230:100.0: 431: 0.31: 0.76: 1.14: 0.29: 0.66: 0.08: 1.22: 62: 93:
: 8630: 99.8: 430: 0.25: 0.47: 0.81: 0.35: 0.58: 0.06: 0.90: 52: 90:
: 8630:100.0: 433: 0.25: 0.55: 0.81: 0.31: 0.67: 0.06: 0.94: 58:
: 9200-10000'
: 9200:100.8: 435: 0.37: 0.85: 0.72: 0.30: 1.18: 0.10: 1.50: 56: 48:
: 9200:100.9: 433: 0.35: 0.88: 0.76: 0.29: 1.15: 0.10: 1.48: 59: 51:
:10600-11400'
:10600:100.4: 439: 0.57: 1.52: 0.63: 0.27: 2.41: 0.17: 2.13:
:10600:100.8: 436: 0.60: 1.61: 0.66: 0.27: 2.43: 0.18: 2.12:
:11400'-TD
:11400:100.9: 440: 0.63: 1.41: 0.75: 0.31: 1.88: 0.17: 2.28: 61: 32:
:11400:100.8: 440: 0.63: 1.47: 0.76: 0.30: 1.93: 0.17: 2.28: 64: 33:
:DEPTH: QTY:TMAX: S 1 : S 2 : S 3 : P I :S2/S3 : P C : TOC : H I : O I :
```

# Oil samples

Code	ARCADJ-50 BALMOM-30 BALMOM-10	BANQUC-10	BLUENG-80 CHFBUK-40	CITNAI-30	COHASA-50	COHASA-10	COHASD-70	COHASD-30	GLENEJ-80	NTRIUB-40	OLYMPA-50	PANUKB-10	PANUKJ-10	PENOBL-50	SVENTO-50	SVENTO-00	SVENTO-10	SABLEH-50	THEBAC-90	UNIACG-60	VENTUB-40	VENTUB-60	VENTUH-50	VENTUH-70	WVENTC-30
Member	Lower	Lower	Unner	Lower	Cree		Cree		Upper	Upper	Lower	Upper	r I	Upper	Lower	Lower		Mamora	Lower						
Formation	Missisauga	Missisauga	Mic Mac Missisanga	Missisauga	Logan Canyon		Logan Canyon		Missisauga	Missisauga	Missisauga	Missisanga	i	Missisauga	Missisanga	Missisauga		Logan Canyon	Missisauga	Mic Mac			Mic Mac	Mic Mac	
Depth (m)	5156–5175 1954–1958	3585–3596	4577-4590 4227-4238	3777-3781	1888-1891		1861–1865		3491–3495	3771–3777	4664-4678	2293–2299	2572-2580	2642	5035-5050	4255-4267	-	1435–1436	3865-3888	5191–5199	4882-4888		5021-5025	4957-4962	4741-4743
DST/RFT	ν κ <del>-</del>	$\Box$	<b>x</b> 4	· 10	5	11	7	3	∞	4	5	1	1	S	5	10	11	5	6	9	4	9	S	7	8
SIU No.	NS9116 NS9302 NS9405	NS9113	NS9115 NS9001	NS9112	NS9004	NS9407	NS9002	NS9406	NS9010	9006SN	<b>2006SN</b>	NS9003	NS9301	NS9114	8006SN	6006SN	NS9404	NS9005	NS9118	NS9303	NS9401	NS9403	NS9117	NS9304	NS9402
Well	Arcadia J–16 Balmoral M–32 Balmoral M–32	Banquereau C-21	Bluenose 2G-4/ Chebucto K-90	Citnalta I–59	Cohasset A-52	Cohasset A-52	Cohasset D-42	Cohasset D-42	Glenelg J-48	N. Triumph B-52	Olympia A-12	Panuke B-90	Panuke PP3 J-99	Penobscot L-30	S. Venture 0-59	S. Venture 0-59	S. Venture 0-59	Sable Island 3H-58	Thebaud C-74	Uniacke G-72	Venture B-13	Venture B-13	Venture H-22	Venture H-22	W. Venture C-62

Well	SIU No.	Depth (m) Formation	Formation	Member	Code
Abenaki J-56	NS9305	3080	Missisauga	Lower	ABENAJ-3R
Alma F-67	NS9013	4500	Verrill Canyon		ALMAF-4R
Alma F-67	NS9108	5045	Verrill Canyon		ALMAF-5R
Cohasset A-52	NS9011	2036	Logan Canyon	Cree	COHASA-2R
Cohasset D-42	NS9012	4426	Abenaki	Misaine	COHASD-4R
Demascota G-43	NS9306	3615	Abenaki	Baccaro	DEMASG-3R
Migrant N-20	NS9101	3587	Missisauga	Lower	MIGRAN-3R
N. Triumph G-43	NS9103	4845	Missisanga	undif.	NTRIUG-4R
N. Triumph G-43	NS9109	3695	Logan Canyon	Naskapi	NTRIUG-3R
Penobscot L-30	NS9105	2118	Logan Canyon	undif.	PENOBL-2R
Penobscot L-30	NS9307	4214	Mic Mac	Penobscot	PENOBL-4R
S. Desberres 0-76	NS9107	3861	Missisauga	Lower	SDESBO-3R
S. Sable B-44	NS9111	3938	Missisauga	Middle	SSABLB-3R
S. Venture 0-59	NS9014	6115	Mic Mac	undif.	SVENTO-6R
Thebaud C-74	NS9110	3911	Missisauga	Lower	THEBAC-3R
Venture B-52	NS9102	5121	Missisauga	Lower	VENTUB-5R
W. Chebucto K-20	NS9104	5210	Missisauga	undif.	WCHEBK-5R
Whycocomagh N-30	NS9106	3360	Missisauga	undif.	WHYCON-3R

## Table 3b

Table 4a: Maturity parameters for Scotian Basin petroleums

Sample Code	MPI	Rc	DMP	TrMN	TeMN
ARCADJ-50	1.12	1.07	0.71	0.71	0.80
BALMOM-10	0.66	0.79	0.48	0.51	0.37
BALMOM-30	0.61	0.76	0.49	0.53	0.40
BANQUC-10	0.79	0.88	0.60	0.55	0.43
BLUENG-80	0.85	0.91	0.61	0.70	0.85
CHEBUK-40	0.76	0.86	0.60	0.68	0.62
CITNAI-30	0.62	0.77	0.53	0.45	0.27
COHASA-10	0.46	0.67	0.47	0.49	0.30
COHASA-50	0.57	0.74	0.52	0.51	0.37
COHASD-30	0.60	0.76	0.48	0.51	0.36
COHASD-70	0.76	0.86	0.50	0.54	0.38
GLENEJ-80	0.87	0.92	0.61	0.61	0.50
NTRIUB-40	0.78	0.87	0.60	0.64	0.55
OLYMPA-50	0.77	0.86	0.59	0.67	0.64
PANUKB-10	0.73	0.84	0.53	0.52	0.38
PANUKJ-10	0.63	0.78	0.48	0.54	0.37
PENOBL-50	0.69	0.82	0.57	0.57	0.38
SABLEH-50	0.80	0.88	0.64	0.44	0.42
SVENTO-00	0.76	0.85	0.48	0.63	0.57
SVENTO-10	0.62	0.77	0.46	0.54	0.43
SVENTO-50	1.25	1.15	0.75	0.74	0.71
THEBAC-90	0.85	0.91	0.59	0.63	0.56
UNIACG-60	0.96	0.98	0.72	0.71	0.67
VENTUB-40	0.93	0.96	0.64	0.74	0.71
VENTUB-60	0.76	0.85	0.63	0.68	0.62
VENTUH-50	1.00	1.00	0.71	0.71	0.81
VENTUH-70	0.90	0.94	0.65	0.74	0.73
WVENTC-30	0.77	0.86	0.65	0.69	0.60

Table 4b: Maturity parameters for Scotian Basin rock extracts

Sample Code	MPI	Rc	DMP	TrMN	TeMN
ABENAJ-3R	0.39	0.64	0.36	0.48	0.18
ALMAF-4R	0.86	0.91	0.61	0.58	0.47
ALMAF-5R	0.83	0.90	0.54	0.57	0.49
COHASA-2R	0.46	0.68	0.40	0.44	0.28
COHASD-4R	0.84	0.90	0.59	0.54	0.51
DEMASG-3R	0.57	0.74	0.45	0.66	0.49
MIGRAN-3R	0.57	0.74	0.46	0.46	0.29
NTRIUG-3R	0.75	0.85	0.58	0.57	0.47
NTRIUG-4R	0.84	0.90	0.60	0.59	0.53
PENOBL-2R	0.48	0.69	0.49	0.54	0.42
PENOBL-4R	0.55	0.73	0.48	0.68	0.53
SDESBO-3R	0.55	0.73	0.51	0.46	0.22
SSABLB-3R	0.58	0.75	0.37	0.39	0.26
SVENTO-6R	1.08	1.05	0.68	0.63	0.66
THEBAC-3R	0.74	0.85	0.50	0.63	0.56
VENTUB-5R	1.08	1.05	0.71	0.76	0.75
WCHEBK-5R	0.68	0.81	0.56	0.50	0.63
WHYCON-3R	0.61	0.76	0.48	0.47	0.31

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<u>.</u>	<b>X</b>	ė,	<u>-</u>	-Y	H-5	4	Α.	ŏ l	o l	8-13	-Y
<u> </u>	BE	IAS	<b>1</b>	IAS	E		₹	<u> </u>			- ¥
Sample	CHEBUK-40	COHASD-70	PANUKB-10	COHASA-50	SABLEH-50	NTRIUB-40	OLYMPA-50	SVENTO-50	SVENTO-00	GLENEJ-80	COHASA-2R
CHEBUK-40	1.000		14		<i>y</i>	~		- 0,	- 01		
COHASD-70	0.747	1.000									
PANUKB-10	0.836	0.927	1.000	Ý							
COHASA-5O	0.623	0.796	0.831	1.000							
SABLEH-5O	0.688	0.831	0.802	0.754	1.000						
NTRIUB-40	0.976	0.794	0.866	0.680	0.737	1.000					
OLYMPA-50	0.906	0.846	0.863	0.684	0.837	0.902	1.000				
SVENTO-50	0.937	0.786	0.843	0.693		0.933	0.910	1.000			
SVENTO-00	0.904	0.825	0.812	0.599	0.771	0.895	0.961	0.889	1.000		
GLENEJ-80	0.955	0.817	0.866	0.700	0.753	0.985	0.914	0.948	0.899	1.000	
COHASA-2R	0.805	0.537	0.621	0.543	0.583	0.766	0.627	0.698	0.645	0.713	1.000
COHASD-4R	0.558	0.416	0.515	0.481	0.571	0.560	0.474	0.488	0.466	0.499	0.736
ALMAF-4R	0.677	0.404	0.493	0.438	0.490	0.682	0.492	0.577	0.523	0.613	0.848
SVENTO-6R	0.685	0.428	0.529	0.414	0.427	0.674	0.464	0.574	0.489	0.596	0.841
MIGRAN-3R	0.923	0.648	0.731	0.562	0.658	0.923	0.797	0.823	0.822	0.883	0.847
VENTUB-5R	0.869	0.563	0.618	0.499		0.866	0.751	0.857	0.797	0.849	0.811
NTRIUG-4R	0.581	0.308	0.402	0.387		0.582	0.404	0.493	0.428	0.548	0.735
WCHEBK-5R	0.687	0.436	0.497	0.319		0.684	0.491	0.543	0.500	0.625	0.722
PENOBL-2R	0.850	0.545	0.611	0.498		0.829	0.674	0.721	0.710	0.778	0.899
WHYCON-3R	0.734	0.401	0.471	0.322	-	0.716	0.505	0.581	0.545	0.653	0.813
SDESBO-3R	0.906	0.573	0.675	0.512		0.912	0.746	0.806	0.746	0.879	0.799
ALMAF-5R	0.635	0.385	0.460	0.408		0.630	0.444	0.539	0.491	0.571	0.815
NTRIUG-3R	0.458	0.203	0.283	0.278		0.465	0.280	0.373	0.302	0.441	0.595
THEBAC-3R	0.823	0.645	0.655	0.512		0.815	0.799	0.774	0.883	0.793	0.734
SSABLB-3R	0.754	0.427	0.495	0.388	0.433	0.730	0.551	0.660	0.631	0.678	0.842
CITNAI-3O	0.848	0.754	0.867	0.573		0.837	0.824	0.789	0.772	0.822	0.574
BANQUC-10	0.856	0.693	0.847	0.582	0.621	0.826	0.784	0.782	0.748	0.803	0.657
PENOBL-50	0.849	0.881	0.856	0.685		0.888	0.925	0.854	0.869	0.918	0.606
BLUENG-80	0.945	0.835	0.865	0.686	0.807	0.953	0.967	0.930	0.943	0.954	0.717
ARCADJ-50	0.933	0.771	0.834	0.702		0.945	0.900	0.970	0.882	0.946	0.751
VENTUH-50	0.959	0.826	0.870	0,664	0.764	0.961	0.950	0.962	0.921	0.960	0.706
THEBAC-90	0.844	0.868	0.838	0.631	0.854	0.863	0.924	0.812	0.918	0.859	0.655
PANUKJ-10	0.573	0.448	0.576	0.391	0.354	0.580	0.380	0.448	0.392	0.505	0.629
BALMOM-30	0.787	0.946	0.882	0.735	0.793	0.825	0.818	0.777	0.808	0.846	0.626
UNIACG-60	0.702	0.364	0.511	0.494	0.416	0.701	0.513	0.659	0.508	0.680	0.735
VENTUH-70	0.970	0.686	0.772	0.611	0.684	0.965	0.858	0.934	0.863	0.947	0.833
ABENAJ-3R	0.852	0.512	0.615	0.487	0.559	0.847	0.660	0.709	0.680	0.791	0.897
DEMASG-3R	0.803	0.406	0.496	0.374	0.443	0.766	0.596	0.681	0.652	0.718	0.858
PENOBL-4R	0.697	0.292	0.409	0.346	0.335	0.662	0.466	0.576	0.505	0.612	0.813
VENTUB-40	0.930	0.747	0.789	0.645	0.756	0.929	0.932	0.949	0.929	0.944	0.726
WVENTC-30	0.972	0.720	0.810	0.637	0.707	0.963	0.913	0.934	0.904	0.957	0.762
VENTUB-60	0.962	0.760	0.861	0.698	- <del></del>	0.958	0.930	0.915	0.891	0.940	0.791
SVENTO-10	0.872	0.890	0.899	0.660		0.877	0.934	0.848	0.912	0.869	0.620
BALMOM-10	0.731	0.823	0.805	0.624	0.713	0.744	0.787	0.723	0.788	0.779	0.516
COHASD-3O	0.373	0.608	0.526	0.523		0.393	0.484	0.346	0.455	0.424	0.261
COHASA-10	0.862	0.742	0.782	0.599	0.787	0.859	0.894	0.786	0.864	0.846	0.680

ē.	COHASD-4R	ALMAF-4R	SVENTO-6R	MIGRAN-3R	VENTUB-5R	NTRIUG-4R	WCHEBK-5R	PENOBL-2R	WHYCON-3R	SDESBO-3R	ALMAF-5R
Sample	H	MA	E	382	Ę	RTC	異	Ş	25	ESE	¥
Sa	8	AL	SV	Ŭ	VE	E	- 8	PEI	M. I	SD	AL
CHEBUK-40											
COHASD-7O											
PANUKB-10											
COHASA-5O											
SABLEH-5O											
NTRIUB-40											
OLYMPA-5O											
SVENTO-50											
SVENTO-00											
GLENEJ-8O											
COHASA-2R											
COHASD-4R	1.000										
ALMAF-4R	0.809	1.000									
SVENTO-6R	0.727	0.912	1.000								
MIGRAN-3R	0.576	0.787	0.742	1.000							
VENTUB-5R	0.589	0.787	0.693	0.906	1.000						
NTRIUG-4R	0.614	0.800	0.679	0.705	0.715	1.000					
WCHEBK-5R	0.589	0.766	0.805	0.723	0.628	0.659	1.000				
PENOBL-2R	0.544	0.809	0.773	0.954	0.865	0.744	0.724	1.000			
WHYCON-3R	0.571	0.856	0.854	0.832	0.753	0.766	0.931	0.871	1.000		
SDESBO-3R	0.479	0.726	0.708	0.952	0.868	0.655	0.719	0.922	0.821	1.000	
ALMAF-5R	0.720	0.954	0.903	0.747	0.738	0.805	0.762	0.786	0.870	0.677	1.000
NTRIUG-3R	0.461	0.661	0.557	0.577	0.583	0.957	0.608	0.628	0.703	0.562	0.693
THEBAC-3R	0.542	0.692	0.583	0.892	0.893	0.628	0.523	0.832	0.655	0.770	0.672
SSABLB-3R	0.544	0.824	0.738	0.873	0.888	0.793	0.640	0.918	0.813	0.818	0.789
CITNAI-3O	0.354	0.435	0.503	0.778	0.596	0.360	0.542	0.655	0.536	0.764	0.398
BANQUC-10	0.439	0.525	0.591	0.801	0.644	0.449	0.536	0.697	0.565	0.776	0.483
PENOBL-50	0.420	0.479	0.475	0.775	0.701	0.395	0.552	0.667	0.533	0.762	0.440
BLUENG-80	0.489	0.575	0.566	0.889	0.819	0.480	0.579	0.783	0.617	0.850	0.533
ARCADJ-50	0.517	0.648	0.621	0.892	0.897	0.563	0.569	0.798	0.633	0.863	0.603
VENTUH-50	0.493	0.573	0.586	0.857	0.818	0.473	0.620	0.751	0.630	0.841	0.530
THEBAC-90	0.492	0.519	0.519	0.809	0.706	0.401	0.553	0.696	0.553	0.731	0.479
PANUKJ-10	0.424	0.564	0.733	0.598	0.419	0.442	0.652	0.601	0.639	0.620	0.555
BALMOM-30	0.428	0.470	0.483	0.737	0.631	0.429	0.554	0.660	0.525	0.662	0.456
UNIACG-60	0.511	0.704	0.619	0.761	0.781	0.882	0.575	0.764	0.695	0.780	0.686
VENTUH-70	0.586	0.742	0.710	0.943	0.942	0.650	0.691	0.877	0.768	0.935	0.696
ABENAJ-3R	0.687	0.887	0.839	0.936	0.858	0.801	0.831	0.932	0.923	0.915	0.851
DEMASG-3R	0.553	0.831	0.764	0.914	0.899	0.801	0.701	0.941	0.876	0.883	0.814
PENOBL-4R	0.535	0.799	0.726	0.819	0.807	0.873	0.640	0.870	0.821	0.801	0.794
VENTUB-40	0.520	0.601	0.549	0.858	0.891	0.502	0.511	0.758	0.581	0.826	0.551
WVENTC-30	0.513	0.647	0.600	0.927	0.885	0.567	0.605	0.837	0.682	0.913	0.603
VENTUB-60	0.650	0.696	0.657	0.905	0.844	0.587	0.663	0.803	0.690	0.870	0.637
SVENTO-10	0.528	0.486	0.509	0.755	0.664	0.352	0.548	0.620	0.508	0.676	0.433
BALMOM-10	0.385	0.398	0.366	0.663	0.586	0.498	0.498	0.562	0.470	0.575	0.405
COHASD-30	0.164	0.146	0.118	0.370	0.220	0.139	0.188	0.323	0.186	0.308	0.141
COHASA-10	0.513	0.587	0.500	0.866	0.741	0.514	0.623	0.768	0.643	0.794	0.535

Parameter Parameter Anni Million Anni Millio		l							٧		
	X.	38	×	0	-10	20	8	20	8	8	01
<u>9</u>	NTRIUG-3R	THEBAC-3R	SSABLB-3R	CITNAI-30	BANQUC-10	PENOBL-50	BLUENG-80	ARCADJ-50	VENTUH-50	THEBAC-90	PANUKJ-10
du d		EB/	BI	Ž.	ŎZ	Q		₹	Ę	EB/	5 2
Sample	E	臣	SSĄ	CE	BA	百	BLI	AŖ	VE	H	PA
CHEBUK-40											1
COHASD-70											
PANUKB-10											
COHASA-50											
SABLEH-50											
NTRIUB-40								***************************************			
OLYMPA-50											
SVENTO-50											
SVENTO-00											
GLENEJ-8O											
COHASA-2R	-										
COHASD-4R											
ALMAF-4R	<u> </u>										
SVENTO-6R											
MIGRAN-3R				····							
VENTUB-5R											
NTRIUG-4R							* * * * * * * * * * * * * * * * * * * *				
WCHEBK-5R											
PENOBL-2R							A CONTRACTOR OF THE CONTRACTOR				
WHYCON-3R											
SDESBO-3R											
ALMAF-5R											
NTRIUG-3R	1.000										
THEBAC-3R	0.476	1.000									
SSABLB-3R	0.672	0.831	1.000								
CITNAI-3O	0.262	0.621	0.511	1.000							
BANQUC-10	0.326	0.660	0.599	0.955	1.000		ĺ				
PENOBL-50	0.292	0.704	0.505	0.820	0.747	1.000					
BLUENG-80	0.358	0.828	0.645	0.860	0.822	0.940	1.000				
ARCADJ-50	0.431	0.835	0.735	0.798	0.805	0.867	0.951	1.000			
VENTUH-50	0.361	0.774	0.634	0.857	0.811	0.925	0.978	0.953	1.000		
THEBAC-9O	0.280	0.791	0.550	0.816	0.762	0.929	0.947	0.850	0.906	1.000	
PANUKJ-10	0.373	0.386	0.530	0.622	0.676	0.426	0.480	0.491	0.501	0.468	1.000
BALMOM-3O	0.321	0.695	0.543	0.769	0.719	0.886	0.840	0.783	0.824	0.853	0.499
UNIACG-60	0.838	0.632	0.796	0.492	0.580	0.478	0.596	0.715	0.606	0.445	0.485
VENTUH-70	0.527	0.849	0.819	0.765	0.786	0.819	0.923	0.958	0.934	0.806	0.544
ABENAJ-3R	0.694	0.779	0.867	0.636	0.691	0.655	0.760	0.778	0.748	0.680	0.630
DEMASG-3R	0.695	0.822	0.951	0.561	0.641	0.552	0.699	0.756	0.679	0.588	0.522
PENOBL-4R	0.804	0.702	0.905	0.452	0.554	0.415	0.569	0.652	0.553	0.441	0.496
VENTUB-40	0.372	0.849	0.683	0.743	0.749	0.868	0.951	0.953	0.938	0.856	0.378
WVENTC-30	0.446	0.850	0.745	0.821	0.823	0.850	0.949	0.947	0.940	0.830	0.487
VENTUB-60	0.451	0.817	0.690	0.828	0.834	0.871	0.949	0.928	0.945	0.872	0.528
SVENTO-10	0.234	0.721	0.504	0.841	0.790	0.883	0.919	0.831	0.919	0.935	0.471
BALMOM-10	0.418	0.680	0.487	0.716	0.673	0.792	0.766	0.710	0.760	0.775	0.378
COHASD-3O	0.093	0.356	0.176	0.463	0.374	0.535	0.468	0.339	0.405	0.523	0.178
COHASA-10	0.390	0.811	0.630	0.809	0.759	0.859	0.899	0.820	0.860	0.870	0.426

		1									,	
	BALMOM-30	9	2	<b>~</b>	38	쏲	8	စ္က	8	2	BALMOM-10	30
o l	Ž	9-5	Ħ	1-3	ģ	7	20	일	<u>a</u>	ō	ĭ.	Ġ
du	Σ	AC	E	ž	₹	OBO	E	Ä	Ĕ	E	Ž	¥
Sample	] Y	UNIACG-60	VENTUH-70	ABENAJ-3R	DEMASG-3R	PENOBL-4R	VENTUB 40	WVENTC-30	VENTUB-60	SVENTO-10	341	COHASD-30
CHEBUK-40				_						- 0,		
COHASD-70												
PANUKB-10												
COHASA-50												
SABLEH-50												
NTRIUB-40												
OLYMPA-50												
SVENTO-50												
SVENTO-00												
GLENEJ-80												
COHASA-2R												
COHASD-4R												
ALMAF-4R												
SVENTO-6R												
MIGRAN-3R												
VENTUB-5R												
NTRIUG-4R												
WCHEBK-5R												
PENOBL-2R												
WHYCON-3R												
SDESBO-3R											-	
ALMAF-5R												
NTRIUG-3R												
THEBAC-3R												
SSABLB-3R												
CITNAI-3O												
BANQUC-10												
PENOBL-50												
BLUENG-80												
ARCADJ-50 VENTUH-50												
THEBAC-90												
PANUKJ-10	1.000									·		
BALMOM-3O	1.000	1.000										
UNIACG-60	0.461	1.000	1 000									
VENTUH-70	0.739		1.000	1 000								
ABENAJ-3R	0.618	0.802	0.894	1.000	1 000							
DEMASG-3R	0.523		0.865	0.937	1.000	1.000						
PENOBL-4R	0.408		0.768	0.887	0.954	1.000	1.000					
VENTUB-40	0.747		0.940	0.750	0.729	0.609	1.000	1.000				
WVENTC-30	0.757	0.719	0.969	0.831	0.800	0.695	0.960	1.000	1.000			
VENTUB-60	0.777	0.694	0.948	0.847	0.754	0.656	0.931	0.962	1.000	1.000		
SVENTO-10	0.857	0.425	0.802	0.643	0.533	0.403	0.844	0.831	0.887	1.000	1.000	
BALMOM-10	0.869	0.508	0.668	0.548	0.479	0.400	0.694	0.713	0.735	0.774	1.000	
COHASD-3O	0.609		0.305	0.259	0.179	0.116	0.370	0.401	0.421	0.482	0.570	1.000
COHASA-10	0.798	0.558	0.829	0.755	0.677	0.551	0.831	0.891	0.908	0.839	0.787	0.570

Ratios computed from py-GC/MS quantitation results.

	Aromatics/	Aromatics/ Benzenes/		Naphths/ ?henan+Antl	Phenols/	Thiophenes/	Thiophenes/ Anthracene	MPR	TRMN
	Aliphatics	<b>\( \text{Aromatics} \)</b>	<b>\( \Sigma \)</b> Aromatics	Aliphatics  \( \subseteq \text{Aromatics} \) \( \subseteq \text{Aromatics} \)	Benzenes	Benzenes	Benzenes Phenanthrene		
Oils									
Venture B-13 DST 4	4.46	0.27	0.36	0.23	0.31	0.01	0.32	0.43	0.65
W. Venture C-62 DST 3	3.24	0.35	0.35	0.22	0.71	0.01	0.34	0.41	0.61
Sable Is 3H-58 PT4		0.43	0.33	0.17	0.40	0.05	1.67	0.23	0.47
Cohasset A-52, DST5	0.52	0.49	0.30	0.10	0.49	0.04	1.26	0.28	0.44
Rock Extracts									
S. Desbarres 0-76	2.09	0.43	0.32	0.15	0.78	0.01	0.62	0.42	0.49
(L. Missisauga)									
Venture B-52	3.29	0.53	0.27	0.15	0.13	0.01	0.20	09.0	0.71
(L. Missisauga)									
N. Triumph G-43	0.23	09.0	0.22	0.08	0.23	0.05	0.42	0.41	0.50
(Naskapi)									
	Benzenes: (	30-C3 (m/z 7	Benzenes: C0-C3 (m/z 78, 92, 106, 120)	50)					
	Naphthalen	es: C0-C3 (m	Naphthalenes: C0-C3 (m/z 128, 142, 156, 170)	156, 170)					
	Phenanthren	nes and Anth	racenes: C0-0	Phenanthrenes and Anthracenes: C0-C2 (m/z 178, 192, 206)	192, 206)				
	Indenes: C0	Indenes: C0-C2 (m/z 116, 130, 144)	5, 130, 144)						
	Phenols: C0	Phenols: C0-C2 (m/z 94, 108, 122)	, 108, 122)						
	Thiophenes	: C0-C3 (m/z	Thiophenes: C0-C3 (m/z 84, 98, 112, 136)	136)					
	Aliphatics:	C5-C13 n-Al	kanes (m/z 5	Aliphatics: C5-C13 n-Alkanes (m/z 57) and n-Alk-1-enes (m/z 55)	1-enes (m/z	:55)			
	MPR: (2-M	P + 3-MP)/(1	I-MP + 9-MF	+2-MP + 3-	MP), where	MP=methy	MPR: (2-MP + 3-MP)/(1-MP + 9-MP + 2-MP + 3-MP), where MP=methylphenanthrene		
	TRMN: (1,	3,6-TMN + 2	)/(NIMI-9,E,	1,4,6-TMN+	1,3,5-TMN	+1,2,5-TM	IRMN: (1,3,6-TMN + 2,3,6-TMN)/(1,4,6-TMN + 1,3,5-TMN + 1,2,5-TMN + 1,3,6-TMN + 2,3,6-TMN)	1 + 2,3,6-1	JMN)
		where TMN	where TMN = trimethylnaphthalene	naphthalene					

Table 7a: Multicomponent kinetics data

Sample: N. Truimph B-52, 3773.5m

Extracted Rock, No. 8355

Methane(m15)			Ethane(m29)			Propane(m43)			
Activation	%	Arrhenies	Activation	%	Arrhenius	Activation	%	Arrhenius	
Energy	Q,	Constant	Energy	of,	Constant	Energy	of ·	Constant	
Distribution	Conv.		Distribution	Conv.		Distribution	Conv.		
35	0.67	3.5455e+11/sec	35	0.00	4.2118e+11/sec	35		6.4073e+11/sec	
36	0.00	Q	36	0.00	or	36		Q <b>r</b>	
37	0.73	0.1118e+26/my	37	1.28	0.1328e+26/my	37		0.2021e+26/my	
38	0.31		38	0.12		38	3.49	,	
39	0.91		39	3.92		39	0.00		
40	0.13		40	1.12		40	1.65		
41	1.33		41	5.92		41	1.60		
42	0.34		42	4.03		42	0.91		
43	0.00		43	0.00		43	1.16		
4	1.10		4	0.00		4	1.69		
45	0.00		45	5.56		45	0.00		
46	6.82		46	12.72		46	7.47		
47	3.69		47	30.97		47	19.66		
48	13.08		48	6.54		48	17.42		
49	7.98		49	14.83		49	8.63		
50	6.08		50	2.05		50	0.00		
51	12.30		51	0.00		51	0.78		
32	1.04		52	3.80		52	2.02		
<u> </u>	13.54		53	1.51		S3	0.00		
6 4	9.50		¥ ;	0.00		*	10.03		
<b>8</b> 8	9.90		ર છ	0.00		55	6.06		
3 8	20.7		36	5.65		56	1.73		
5 /	0.00		57			57	0.00		
5 %	0.00		58			58	0.00		
39	13.04		59			60	15.69	II a	Table 7a
8			8			8			
			SAMPLE	PLE	TMAX OF MASS	15	TMAX	TMAX OF MASS 29	TMAX O
					50 -	50 - 15 - 5	50	50 - 15 - 5	50 -
					Deg.	Deg.C./Min	Deg	Deg.C./Min	Deg.
			8355 Rock	Rock	549 - 5	549 - 521 - 496	511.5	1.5 - 481 - 459	508 - 4
			8355 Oil	Oil	551 - 52	551 - 528 - 500.6	454 -	454 - 422 - 398	482.6 -
			8358 Rock	Rock	552 - 51	552 - 516.8 497.6	491 -	491 - 469 - 460	510 - 48
			8258	2	<b>ググ1 4 グ</b> 2	48 - 501 65	101	160 160	<b>5</b> 01
			8358 UII	S	331.4 - 32	551.4 - 524.8 - 501.65	491 -	491 - 469 - 460	501 - 4

SAMPLE	<b>TMAX OF MASS 15</b>	TMAX OF MASS 15 TMAX OF MASS 29 TMAX OF MASS 43	TMAX OF MASS 43
	50 - 15 - 5	50 - 15 - 5	50 - 15 - 5
	Deg.C./Min	Deg.C./Min	Deg.C./Min
8355 Rock	549 - 521 - 496	511.5 - 481 - 459	508 - 478 - 457
8355 Oil	551 - 528 - 500.6	454 - 422 - 398	482.6 - 461 - 460
8358 Rock	552 - 516.8 497.6	491 - 469 - 460	510 - 480.5 -458.6
8358 Oil	551.4 - 524.8 - 501.65	491 - 469 - 460	501 - 471 - 458

Table 7b: Multicomponent kinetics data

Sample: N. Truimph B-52, 3773.5m

Total Bitumen (Oil) Extract, No. 8355

Methane(m15)			Ethane(m29)			Propane(m43)		
Activation Energy Distribution	% of Conv.	Arrhenies Constant	Activation Energy Distribution	% of Conv.	Arrhenius Constant	Activation Energy Distribution	% of Conv.	Arrhenius Constant
35 37 38		1.4447e+12/sec or 0.4556e+26/my	35 36 37 38	0.65 0.20 0.77	1.7200e+12/sec or 0.5424e+26/my	35 36 37	0.00	1.7200e+12/sec or 0.5424e+26/my
39	1.25		39 40	1.02		39 40	0.00	
41 42 43	0.71 0.00 0.99		41 42 43	2.47 0.00 0.61		41 42 43	1.91 0.00 0.00	
45 45	7.97 0.00		45	21.32 3.88		44 45 46	13.11 6.51	
47 48 49	4.36 4.16 3.158 6.62		48 49 49	10.76 6.12 9.02 10.07		46 48 49	8.04 8.64 9.42 14.58	
50 52 53 54 55 54	6.84 8.92 5.43 11.01		5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	13.40 1.71 4.39 2.48		52 52 53 53 54 54 55	15.02 0.88 5.62 0.50	
55 57 58	7.47 4.97 6.08 1.39		55 57 58	3.49 0.30 0.00		5 55 55 55 8 55 55 55 55 55 55 55 55 55 55 55 55 55	3.40 0.31 1.72 3.10 0.00	
59 60 62 63	5.30 3.67 0.00 0.00 5.65		59 60 61	4.98		59 60 61	0.00	

Table 7c: Multicomponent kinetics data

Sample: S. Desbarres O-76, 3801.88m

8358
Š.
ample,
Rock s
rtracted

Methane(m15)			Ethane(m29)			Propane(m43)		
Activation Energy Distribution	% of Conv.	Arrhenies Constant	Activation Energy Distribution	% of Conv.	Arrhenius Constant	Activation Energy Distribution	% of Conv.	Arrhenius Constant
35 35 36	0.24	8.9683e+10/sec	34 35 36	0.96	4.8407e+10/sec	35		8.0902e+11/sec
37 38	0.41 0.44	0.2828e+25/my	37 37 38	2.15 2.98	o. 0.1527e+25/my	37 38	0.00	or 0.2555e+26/my
39 40	0.44		39 40	2.20		39 40	0.00	
41	0.00		41	0.00		: 14	0.75	
42 43	3.79		42 43	10.61 13.58		42 43	0.00	
4 4	2.13		44	31.99		4 ;	1.78	
45 46	11.16 4.32		45 46	9.28 14.89		45 46	1.01 6.89	
47 48	19.38 2.78		47	0.00		47	8.34	
49	9.45		49	1.90		49	0.00	
50	9.65		50	0.00		50	14.68	
52	9.11		52	3.01		52	0.00	
£ 52	5.21		53	2.48		53	3.92	
55	7.41		55	3.49		55	2.03	
56	0.00		56	0.30		56	6.90	
S8	7.45		58	0.00		28	0.00	
S9 S9			59	4.98		59	0.00	
61			61			61	17,35	
62	0.00							
	)							

Table 7d: Multicomponent kinetics data

Sample: S. Desbarres O-76, 3801.88m

Total Bitumen (Oil) Extract, No. 8358

	Arrhenius Constant	2.0744e+11/sec or 0.6542e+25/my	Table 7
	% of Conv.	0.19 0.00 0.34 0.72 0.26 2.71 0.00 0.00 0.00 17.06 1.48 21.92 11.69 5.32 2.05 5.36 0.00 0.00 0.72 2.00 0.00 0.00 0.00 0.00	
Propane(m43)	Activation Energy Distribution	£ \$ £ £ £ £ 8 6 6 6 6 6 6 7 6 8 6 7 6 8 6 8 7 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	
	Arrhenius Constant	2.0770e+11/sec or 0.6550e+25/my	
	% of Conv.	0.81 0.76 0.65 1.37 2.58 0.00 0.00 0.00 17.85 0.00 21.40 9.27 8.02 2.60 3.69 0.72 2.27 1.51 1.51 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00	
Ethane(m29)	Activation Energy Distribution	4       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       6       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5       5	
	Arrhenies Constant	4.3261e+12/sec or 0.1364e+27/my	
	% of Conv.	1.48 0.00 0.00 0.00 0.00 6.14 0.85 7.81 4.74 11.63 4.74 11.63 2.80 11.41 2.35 7.97 7.97 7.97 7.97 7.97 7.97	00.0
Methane(m15)	Activation Energy Distribution	8888844444444486888888888888888	3

Table 8a: Lithostratigraphy data of North Truimph G-43 well in BasinMod

Table 8a: Lithostratigraphy data of North Truimph G-43 well in BasinMod	atigraphy data o	f North Truim	oh G-43 well	in BasinMod		
FM_NAME	BEGIN_AGE	TOP_DEPTH	THICKNESS	LITHOLOGY	KEROGEN_NAME TOC	10C
Quaternary Unconformity1 3	1.6	-74	-176	Sandstone		
Pliocene	5.0	-250	7500	30/70/0		
Unconformity2	10.5					
L. Miocene	20	750	-265	Shale		
Uncontormaty3	30	1	1			
L. Oligocene	49.5 50.5	1015	-415	10/80/10		
U. Paleocene		-1/30	1	0,000		
Unconformity5	70	7430	7/0	0/30/10		
E. Maastrichtian	74.5	-1600	-28	0/60/40		
Wyandot	85	-1628	08-	0/90/10	Tyne II	10
Dawson Canyon	26	1708	-154	40/60/0		1.5
Logan Canyon	5.86	-1862	-524	60/40/0	H	1.5
Sable	101	-2386	7135	20/20/0	田	2.0
Cree	117	-2521	-880	60/40/0	IB	2.7
Naskapi	120	-3401	-259	30/10/0	田	3.0
Naskapi A	120.2	.3660	75	30/70/0	IIA-IIB	3.0
Missisauga1	120.8	-3665	-100	70/30/0	田	3.0
Missisauga2	129.3	-3765	71000	20/20/0	EB	3.0
Missisauga3	131	-4765	-200	30/70/0	田田	3.0
Missisauga4	144	74965	71535	20/20/0	田	3.0
Top Jurassic	152	.6500	7100	20/80/0	留	2.0
T1 1	157	0099_	-200	20/80/0	日	1.5
TJ 2	167	0089_	-20	20/80/0	留	2.0
TI 3	170	.2850	150	20/80/0	日	1.5
Mic Mac	181	-2000	100	20/70/10	EB	1.5
MM 1	182	7100	.200	20/70/10	日	1.5
MM 2	185	0092	100	20/70/10	自	1.5
MM 3	185.5	-2700	1000	20/70/10	田	1.5
MM 4	191	-8700	7100	20/70/10	E	1.5
MM 5	191.5	-8800	-2000	20/70/10	H	1.5
MM 6	198	_10800	-100	20/70/10	曾	1.5
MM 7	198.5	_10900	-700	20/70/10	日	1.5
Mohican	200	11600	-3000	20/70/10	Ш	1.0
Breakup Unc.	201					
Argo	204	714600	72000	0/10/90	日	0.2
Eurydice	235	716600	1500	30/60/10	Ш	0.2

Table 8b: Lithostratigraphy data of S. Desbarres O-76 well in BasinMod

FM_NAME	BEGIN_AGE	TOP_DEPTH	THICKNESS	LITHOLOGY	KEROGEN_NAME	TOC
Quaternary	1.6	⁻ 50	⁻ 50	45/55/0		
up. Banquereau	15.0	<b>~100</b>	~573	70/30/0	Ш	1.0
Unconformity	55					
E. Eocene	60	673	⁻ 215	90/10/0	$\mathbf{III}$	1.5
Unconformity2	64					
E. Paleocene	66.4	888	<b>-</b> 90	Shale	III	1.0
Maastrichtian	75.0	978	⁻ 130	Shale	IIB	1.5
Wyandot	87.5	1108	⁻ 42	0/30/70	IIA-IIB	2.0
Coniacian	88.5	1150	⁻ 14	10/80/10		
Dawson Canyon	91	1164	"107	Shale		
Cenomanian	94	1271	~117	10/80/10		
Logan Canyon	97.5	1388	⁻ 157	50/50/0		
Albian	99.2	1545	~75	30/70/0		
Sable	101.3	1620	<b>-</b> 93	30/70/0		
Cree	113	1713	⁻ 427	60/40/0		
Aptian	116	2140	⁻ 245	60/40/0		
Naskapi	119	2385	~123	40/60/0		
Missisauga	124	2508	⁻ 323	70/20/10		
O Marker	144	2831	~839	80/20/0		
Top Jurassic	152	3670	~10	20/70/10	IIA-IIB	2.5
ТЈ 1	153	⁻ 3680	⁻ 50	70/20/10	Ш	1.5
TJ 2	154	⁻ 3730	~10	20/70/10	$\Pi B$	2.0
ТЈ 3	155	⁻ 3740	~120	70/20/10	III	1.5
Mic Mac	163	3860	~10	20/70/10	ПВ	2.0
MM1	164	~3870	⁻ 500	20/40/40	Ш	1.5
MM2	169	⁻ 4370	<b>-10</b>	20/70/10	IIB	2.0
MM3	169.5	~4380	⁻ 500	20/40/40	III	1.5
MM4	174	⁻ 4880	<b>-10</b>	20/70/10	IIB	2.0
MM5	174.5	⁻ 4890	~210	20/40/40	III	1.5
J1	176	<b>~5100</b>	⁻ 150	20/80/0	ПВ	1.6
Ј2	177	⁻ 5250	-300	20/70/10	III	1.5
J2a	179	~5550	-30	20/80/0	IIB	2.5
Ј2Ь	179.5	~5580	⁻ 520	20/70/10	Ш	2.0
Ј3	181	<b>~6100</b>	<b>-</b> 960	20/70/10	III	1.5
Mohican	200	7060	⁻ 3740	45/40/15	Ш	0.5
Breakup Unc.	201					
Argo	204	10800	~1000	0/10/90	III	0.2
Eurydice	225	11800	~1000	40/50/5/5	III	0.2

Table 9a

Table 9a. Methane expulsion (mg/g TOC) in various stratigraphic units in N. Truimph B-52/G-43 well using multicomponent kinetics

N. Truimph G-43/B-52

Fm_Name	Top_Depth (m)	Thickness (m)	Kerogen Type	TOC (mg/g_TC	Kinetic Type DC)	Methane Expulsion (mg/g_TOC)
Naskapi Mississauga1 Mississauga2 Mississauga3 Mississauga4 Top Jurassic T11 * T12 * T13 * T13 * T13 * MicMac MM1 * MM2 * MM3 * MM3 * MM5 * MM5 * MM5 * MM5 * MM5 * MM6 * MM6 * MM6 * MM6 * MM7 *	3401 3665 3765 4765 4965 6500 6600 Same 6800 6850 6850 5800 7700 7700 7700 Same 10800	259 1000 10000 2000 2000 2000 Same 50 153 1000 Same 1000 Same 1000 Same 1000 Same 1000		3.0 3.0 3.0 3.0 3.0 2.0 1.5 Same 1.5 Same 1.5 Same 1.5 1.5 Same 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5		2
MM7*	Same	Same	Ħ	Same	∄	-63

Table 9b. Mthane expulsion (mg/g TOC) in various stratigraphic units in S. Desbarres O-76 using multicomponent kinetics

	Methane Expulsion (mg/g_TOC)		8	% S	φ.	-35	751	71	9_	-21	-13	-35	717	2	-42	-24	-20	-29	-23		-38
S. Desbarres O-76	Kinetic Type		IIA-IIB	田	留	目	日	图	留	目	91	图	图	目	田	911	田	自	Ħ		留
	TOC (mg/g_TOC)		2.5	1.5	2.0	1.5	same	2.0	1.5	2.0	1.5	2.0	1.5	same	1.6	1.5	2.0	2.0	same		0.5
	Kerogen Type		IIA-IIB	П	EB	Ш	same	留	Ħ	<b>E</b>	Ħ	留	Ħ	same	曾	日	曾	Ш	same		Ш
	Thickness (m)	123	10	20	10	120	same	10	200	10	200	10	210	same	150	300	30	520	same	096	3740
	Top_Depth (m)	2385	3670	3680	3730	3740	same	3860	3870	4370	4380	4880	4890	same	5100	5250	5550	5580	same	6100	7060
وبين وول الموادية والمادية الموادية والموادية والموادية والموادية والموادية والموادية والموادية والموادية والم	Em_Name	Naskapi Mississauga1 Mississauga2 Mississauga3 Mississauga4	Top Jurassic	T11*	TJZ	T13*	T13*	MicMac	MM1*	MM2	MM3*	MM4	MM5*	MM5*	Л	12	JZa	126*	J2b*	13	Mohican

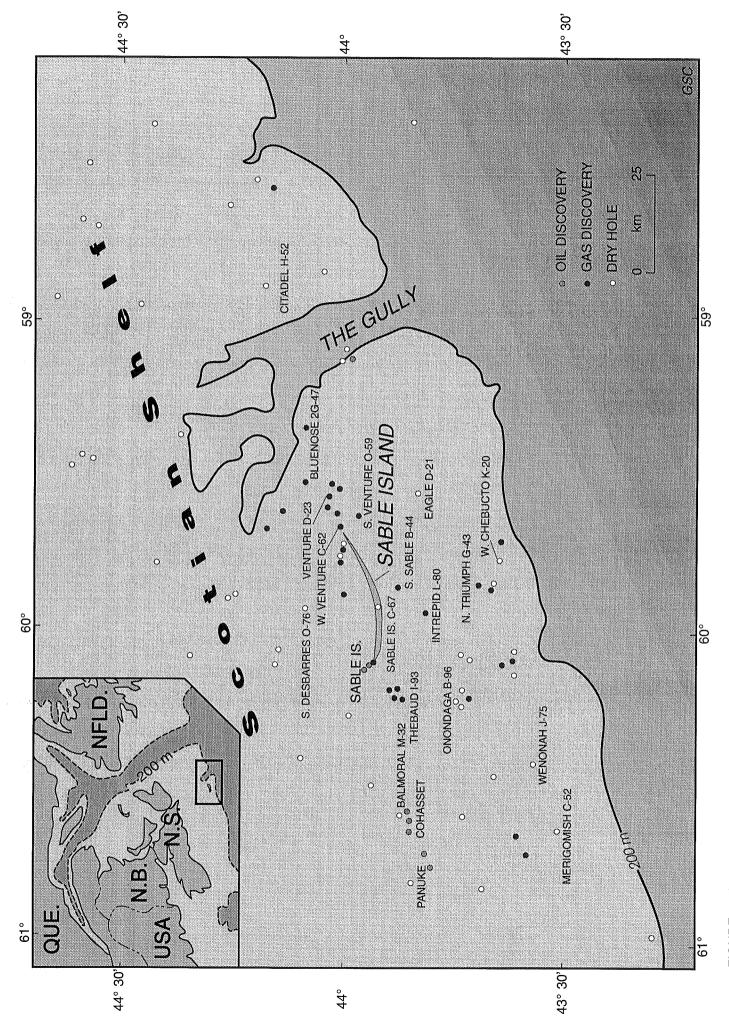
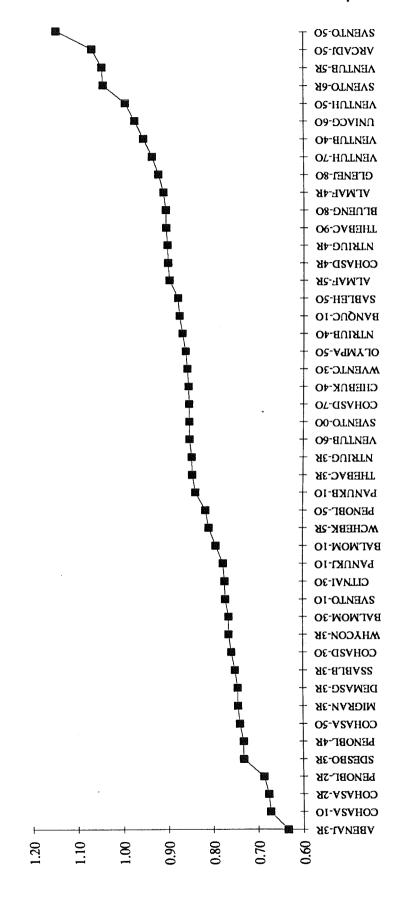
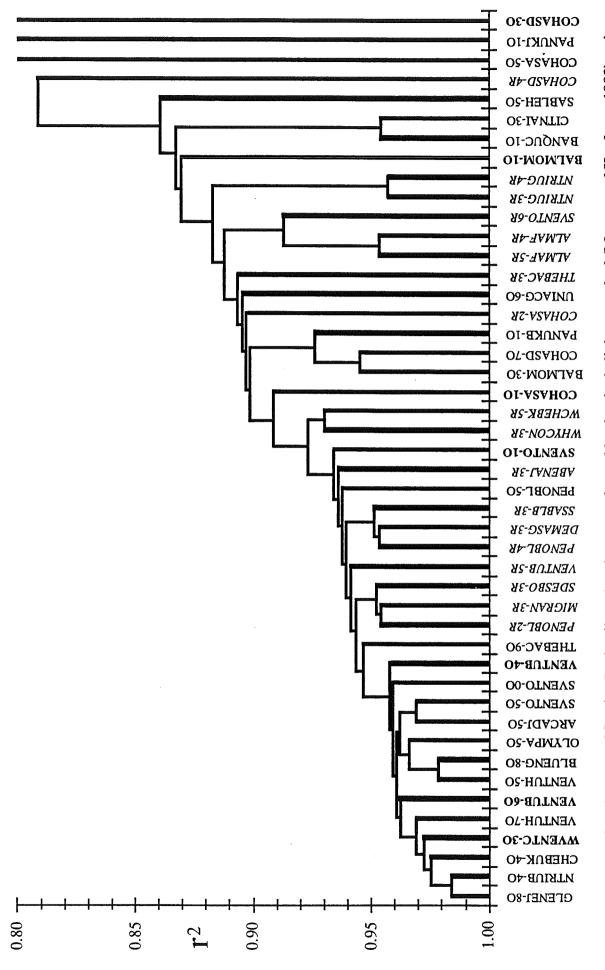


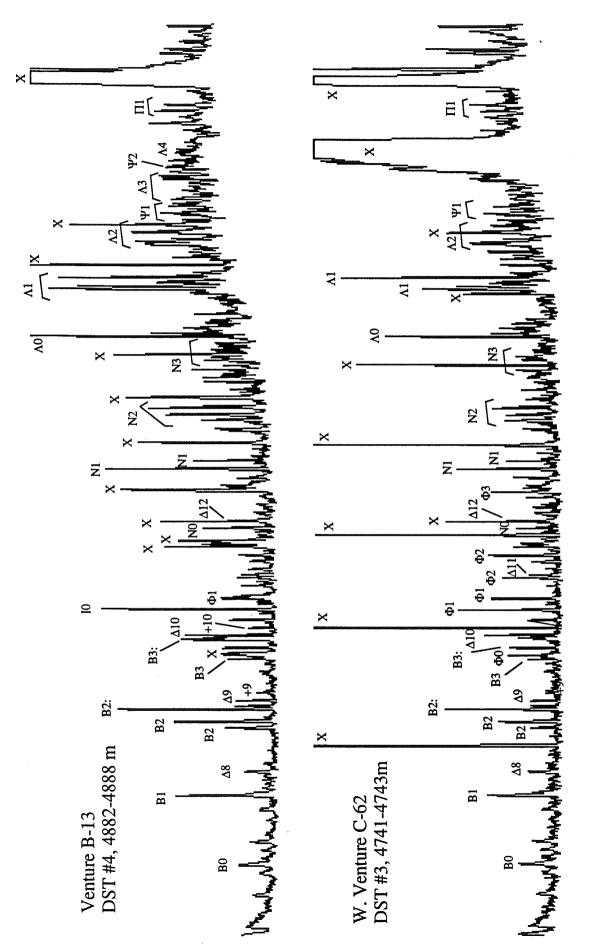
FIGURE 1. Index map of wells analysed in this report.



Vitrinite Reflectance (%) Calculated from Methylphenanthrene Index



Dendrogram of Scotian Basin oils and rock extracts formed by the single linkage method (Massart and Kaufman, 1983), using coefficients of determination from the multiple linear regression of 22 maturation insensitive polyaromatic compounds quantitated in each sample. 1994 samples in bold face. Rock samples in italics.



Flash pyrolysis-GC/MS total ion current traces of asphaltenes isolated from two Scotian Shelf petroleum samples.

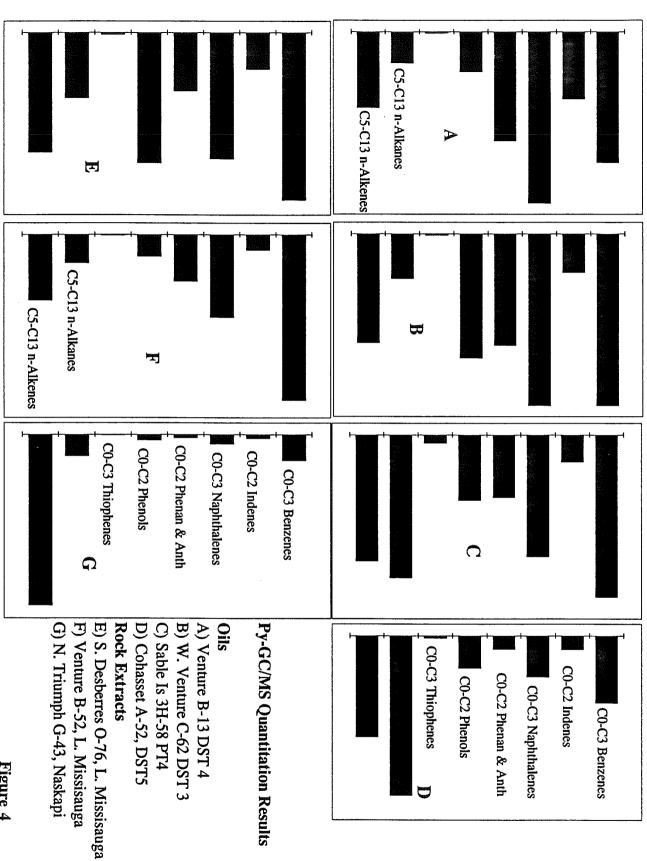


Figure 4

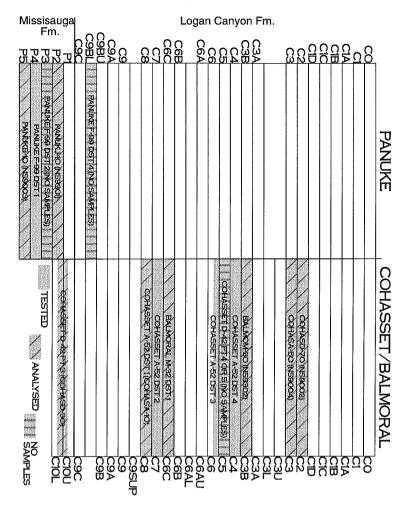
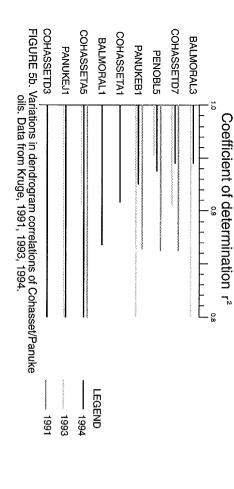


FIGURE 5a. Reservoir stratigraphy for Cohasset and Panuke fields showing location of analysed oils (Stratigraphy from C-NSOPB)



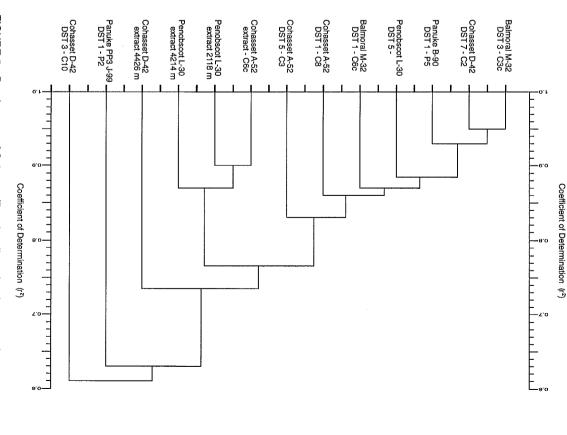
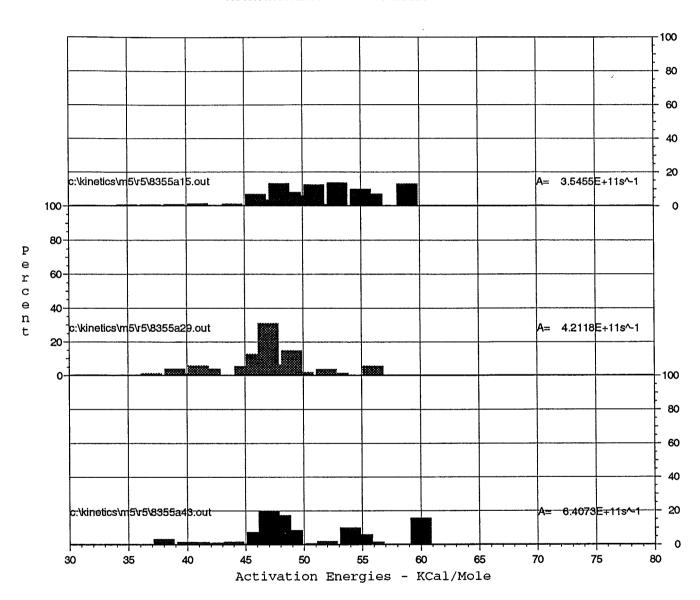


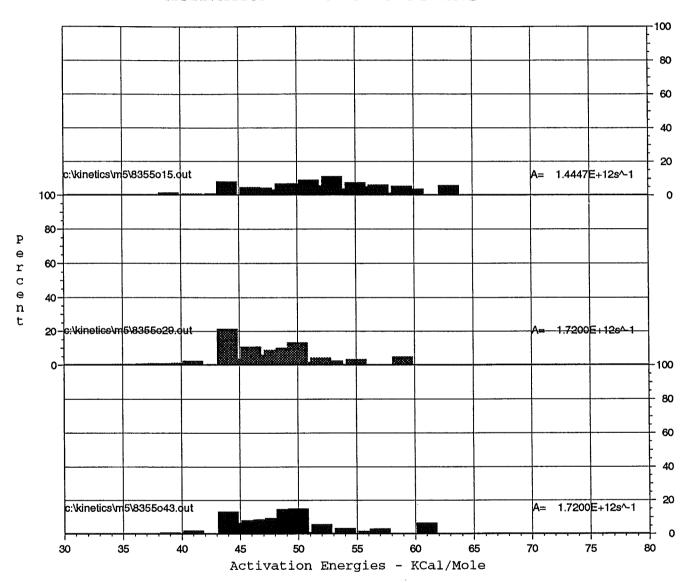
FIGURE 5c. Dendrogram of Cohasset/Panuke oils and rock extracts formed by the single linkage method (Massart and Kaufman, 1983), using coefficients of determination from the multiple linear regression of 22 maturation insensitive polyaromatic compounds quantitated in each sample.

Figures 5a, 5b, and 5c



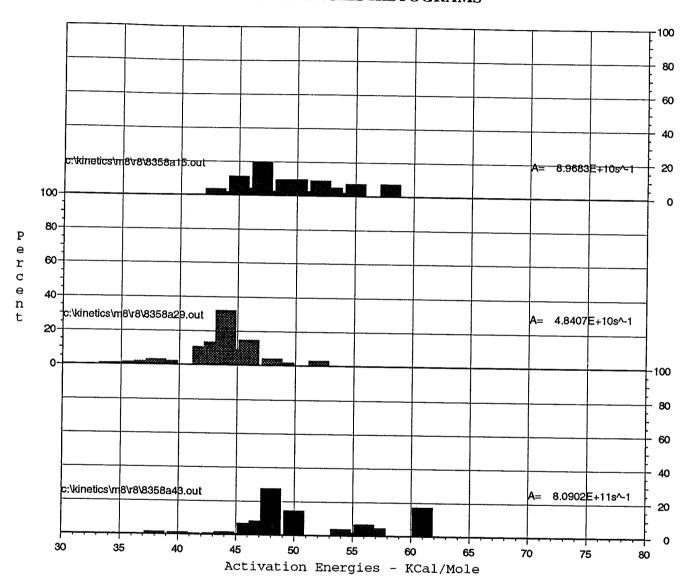
N. Truimph B-52, Extracted Whole Rock

Figure 6a



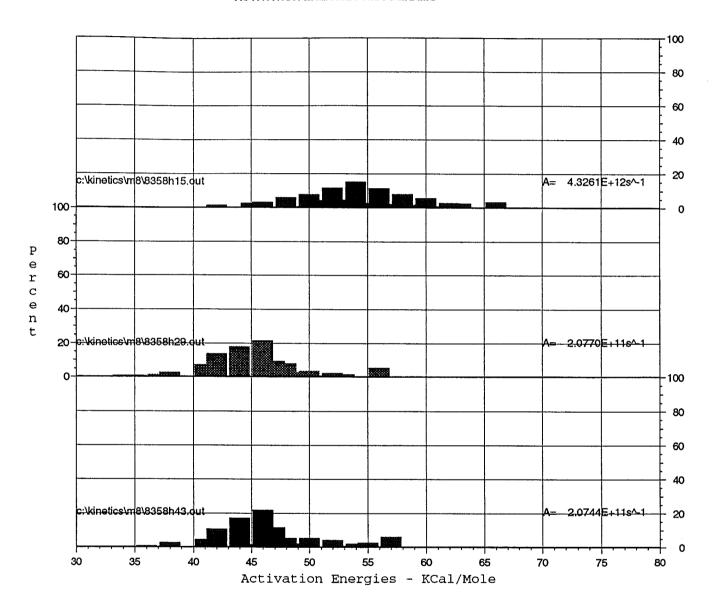
N. Truimph B-52, Bitumen (Oil)

Figure 6b



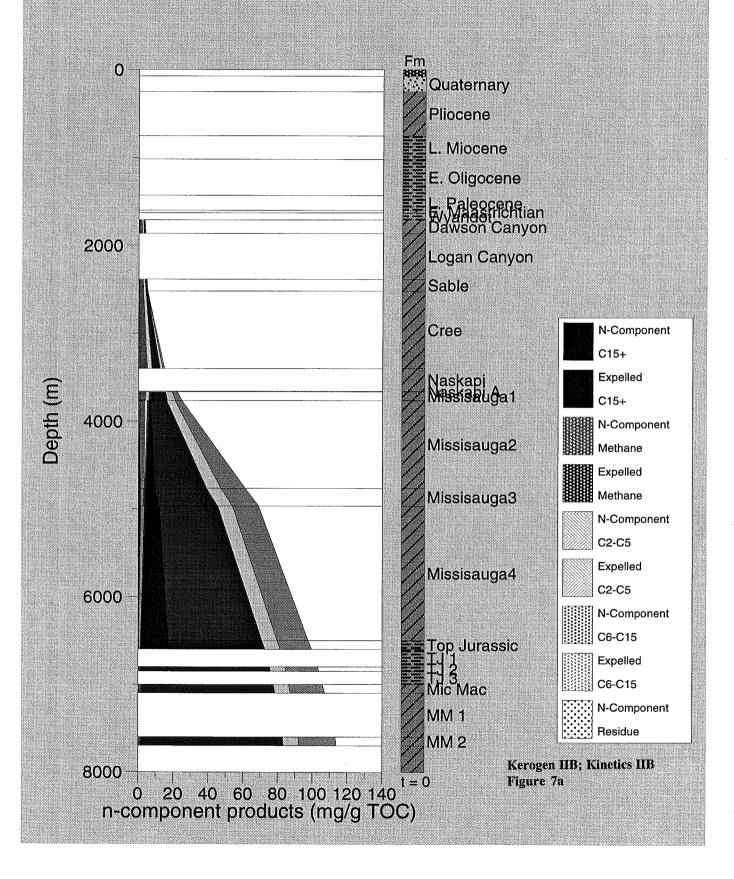
### S. Desbarres O-76, Extracted Whole Rock

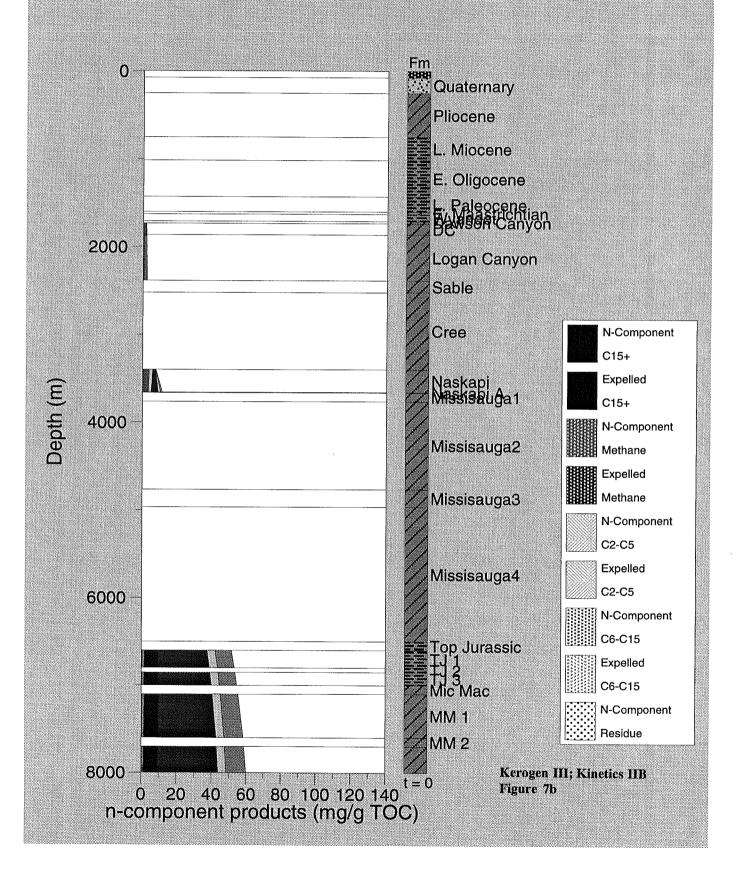
Figure 6c

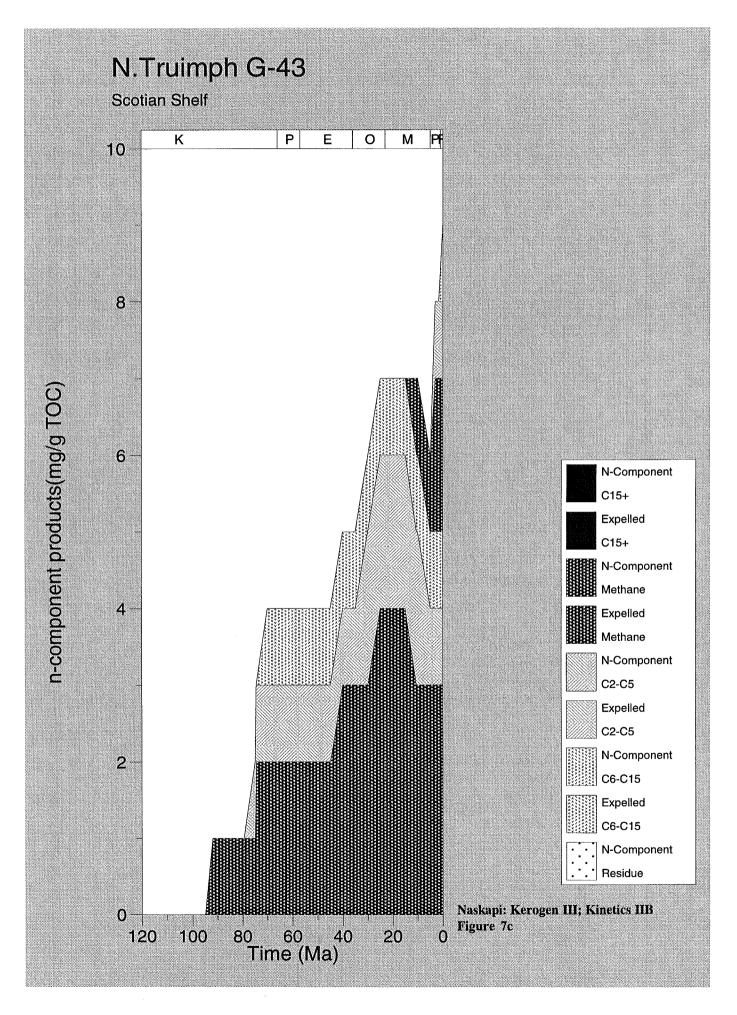


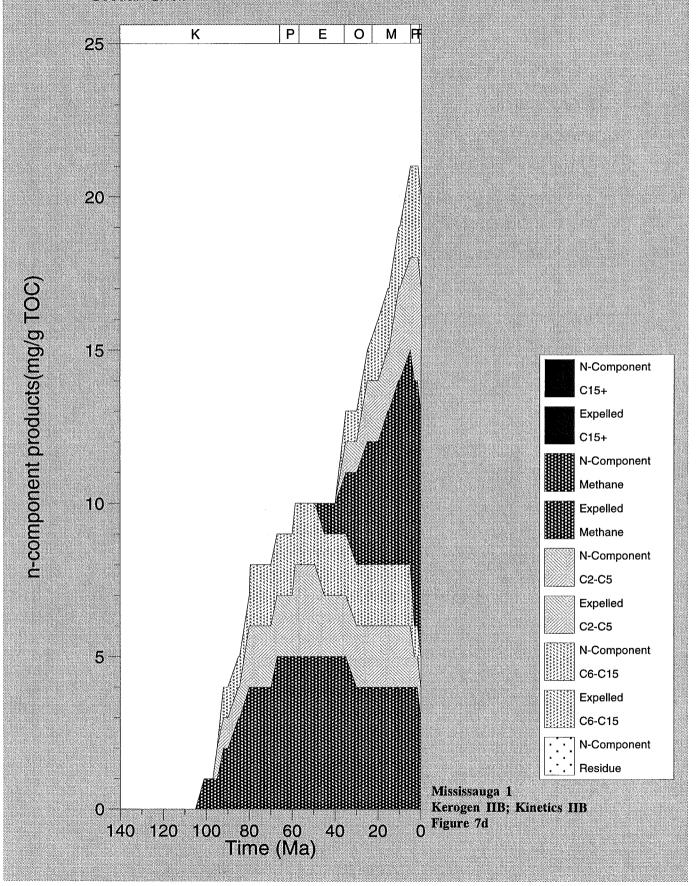
### S. Desbarres O-76, Bitumen

Figure 6d

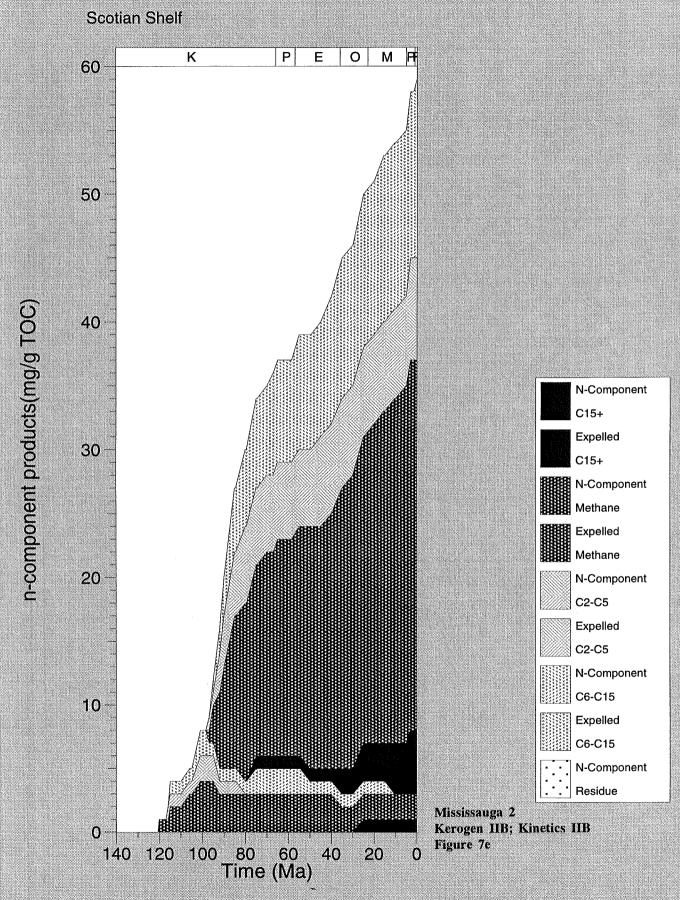


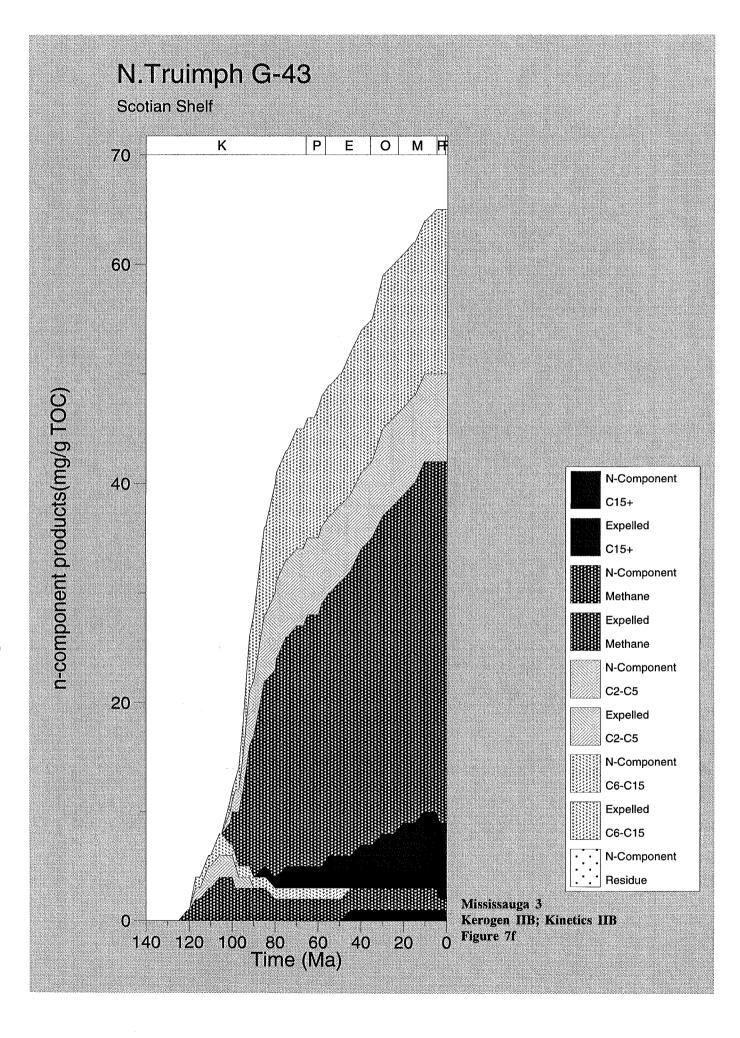


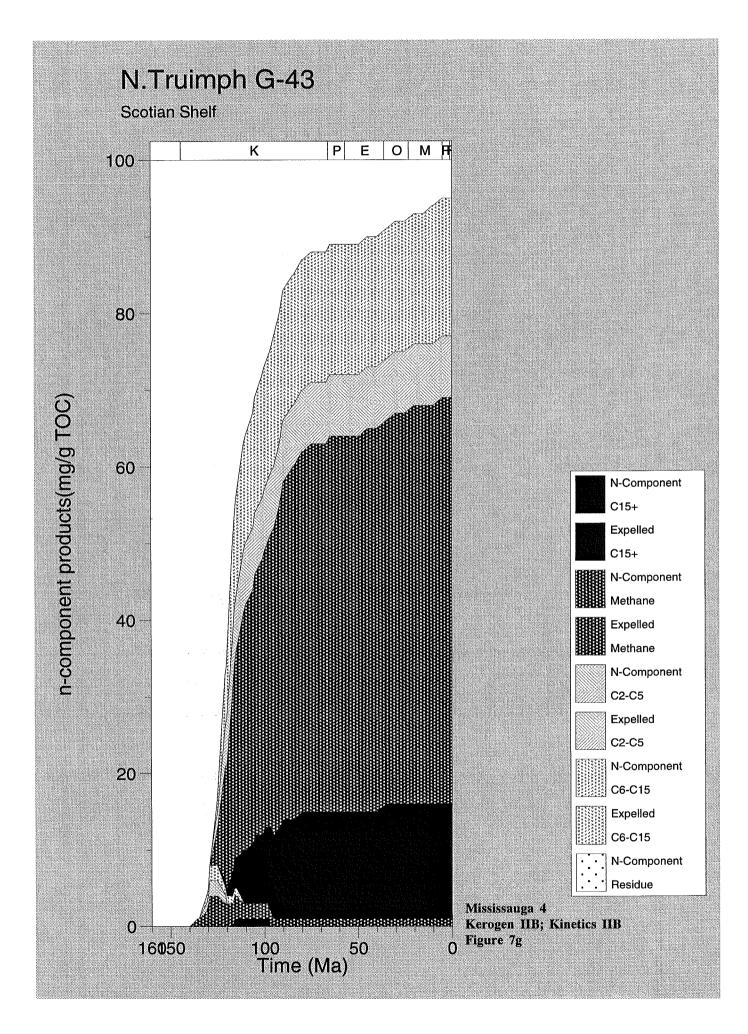


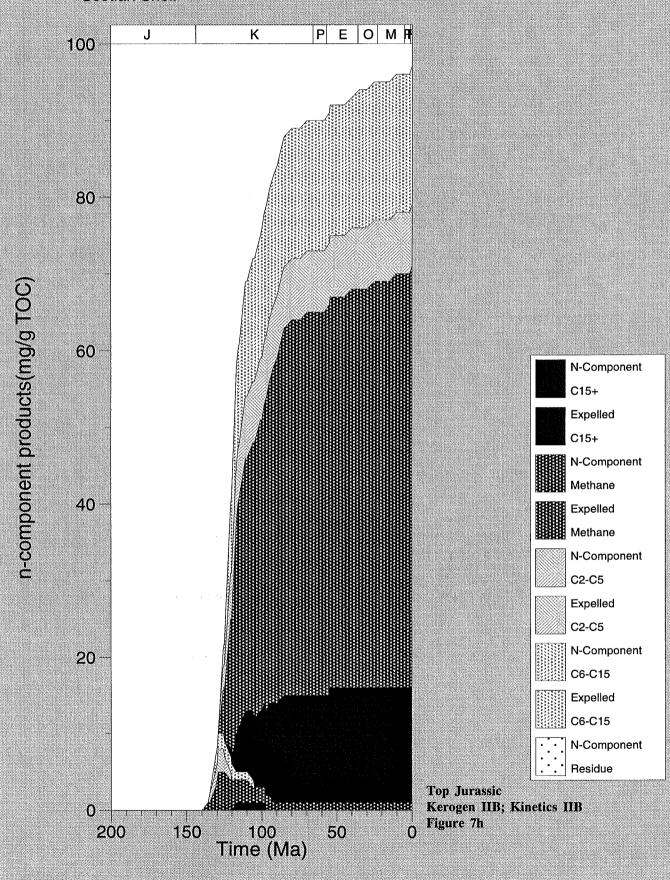


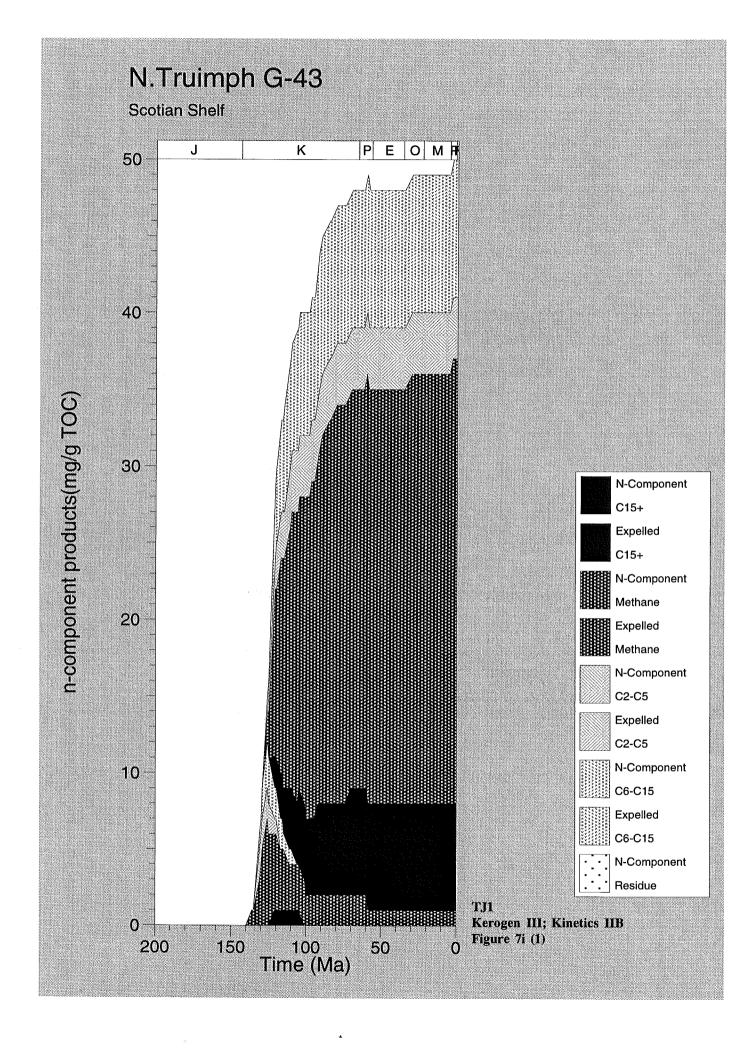


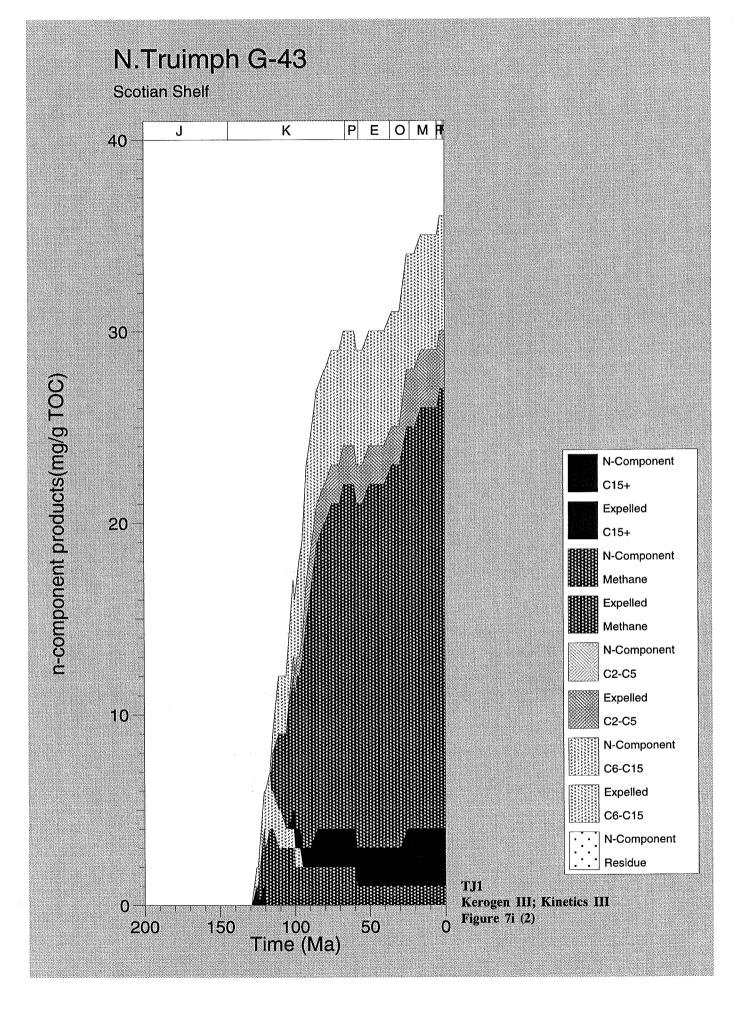




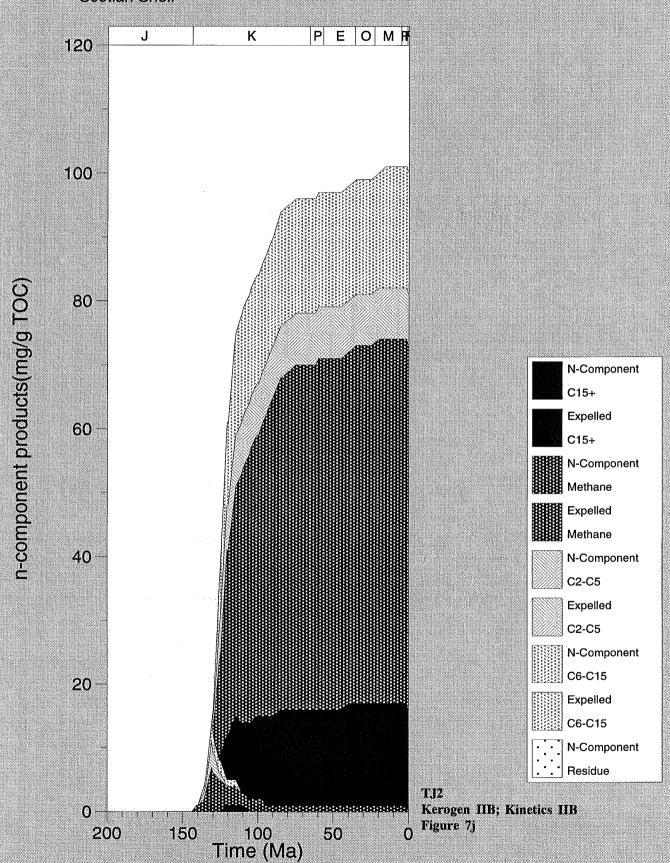


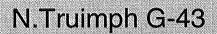




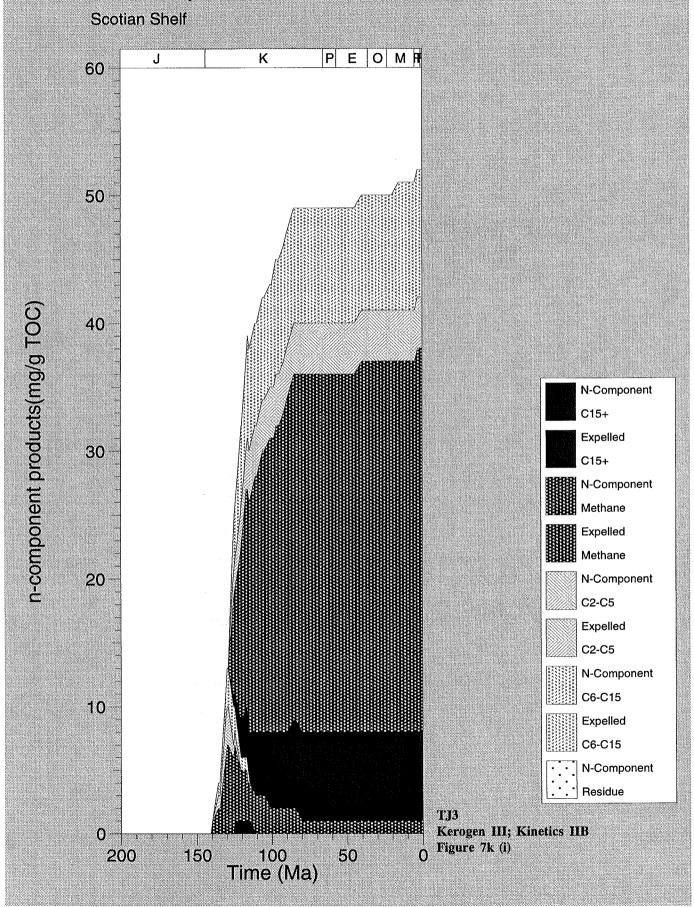


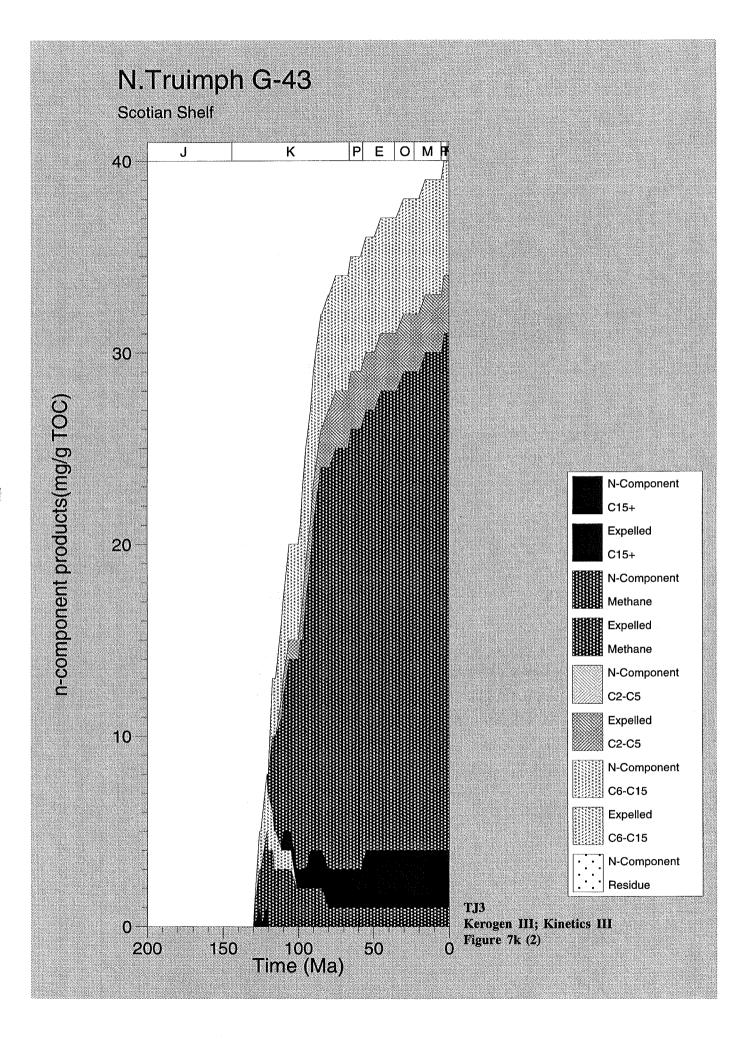


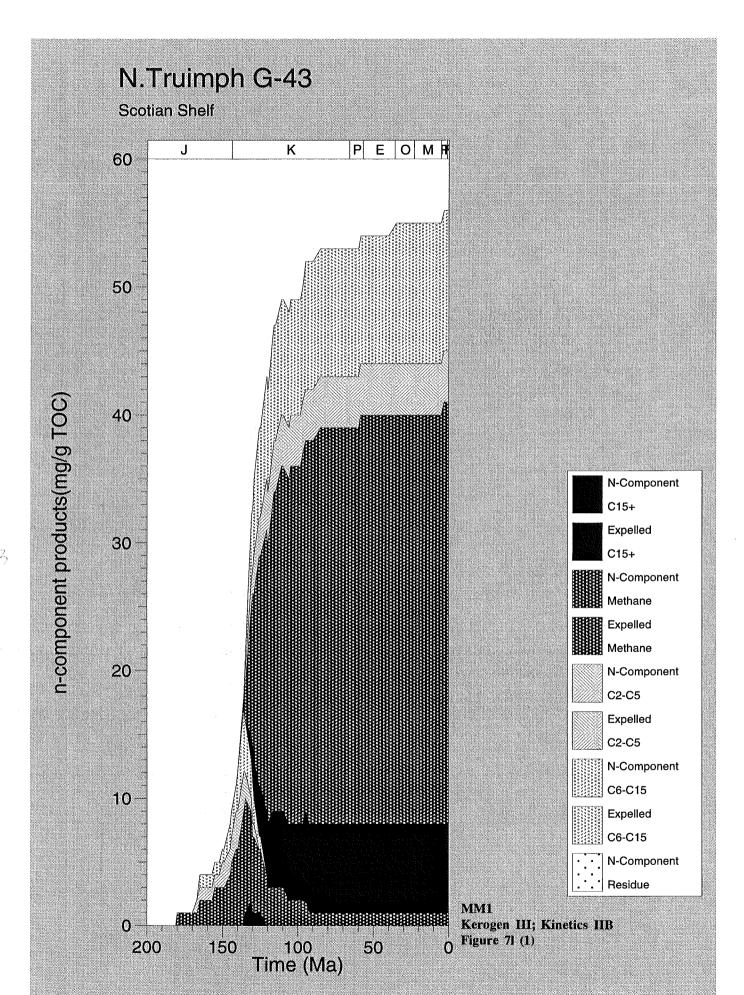


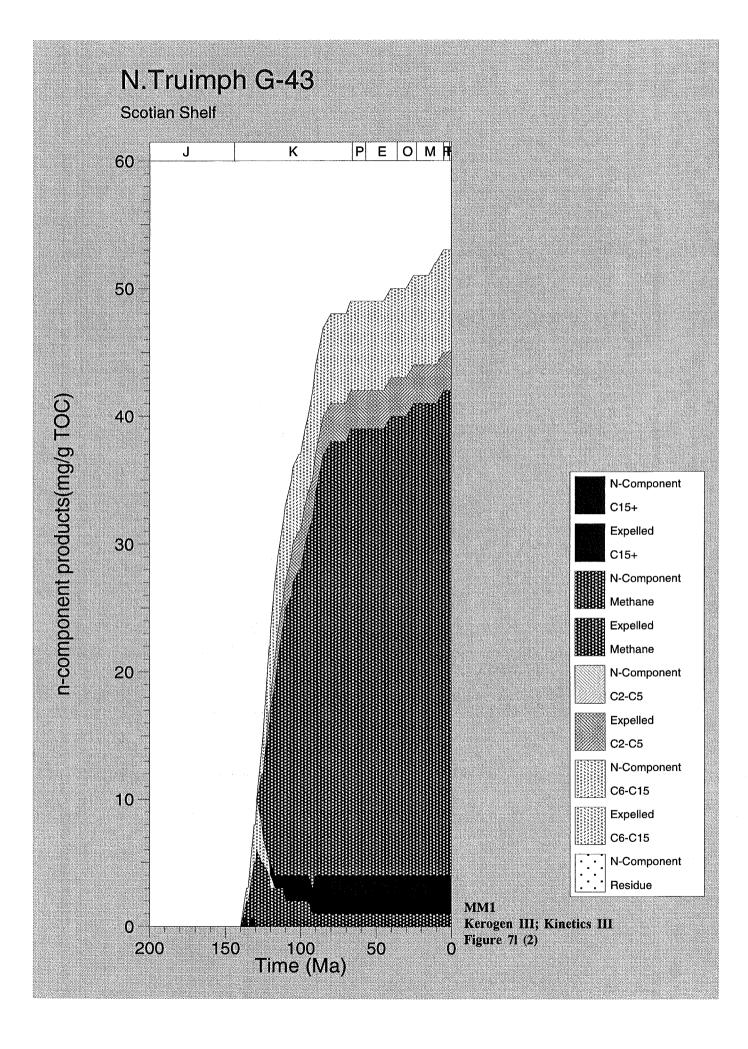


4)

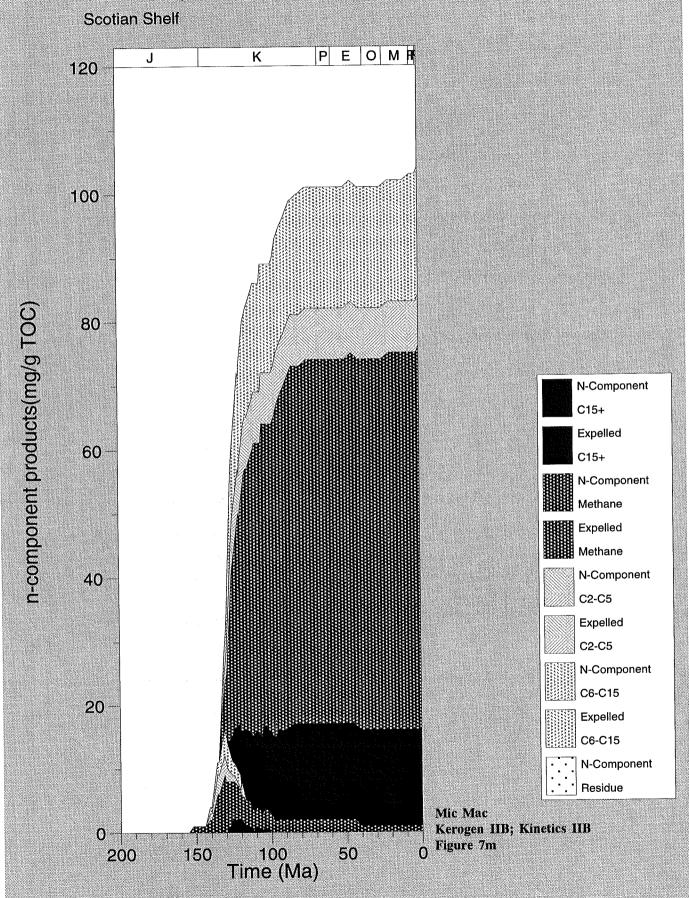




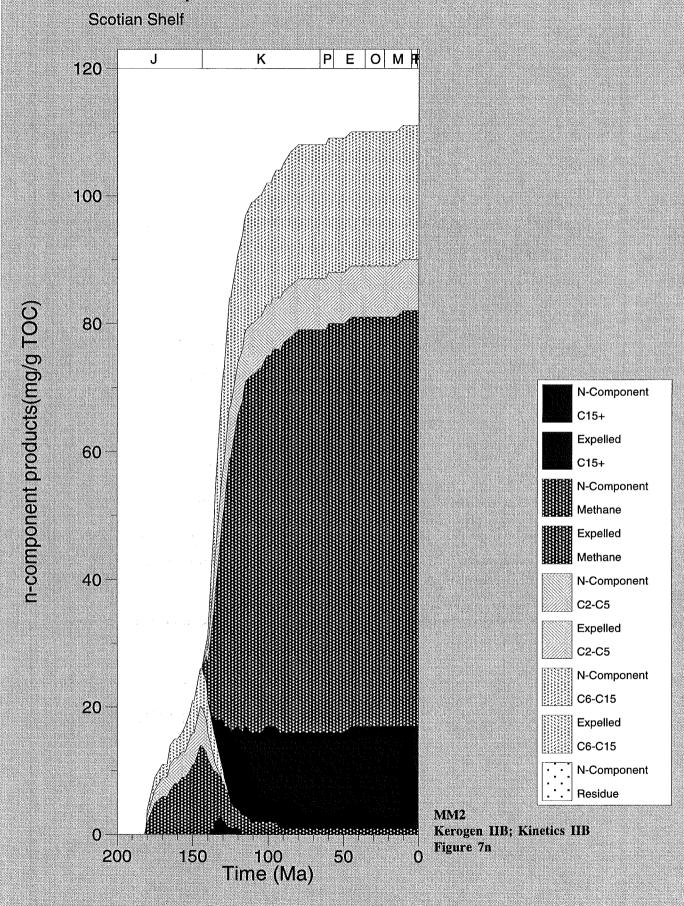


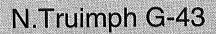


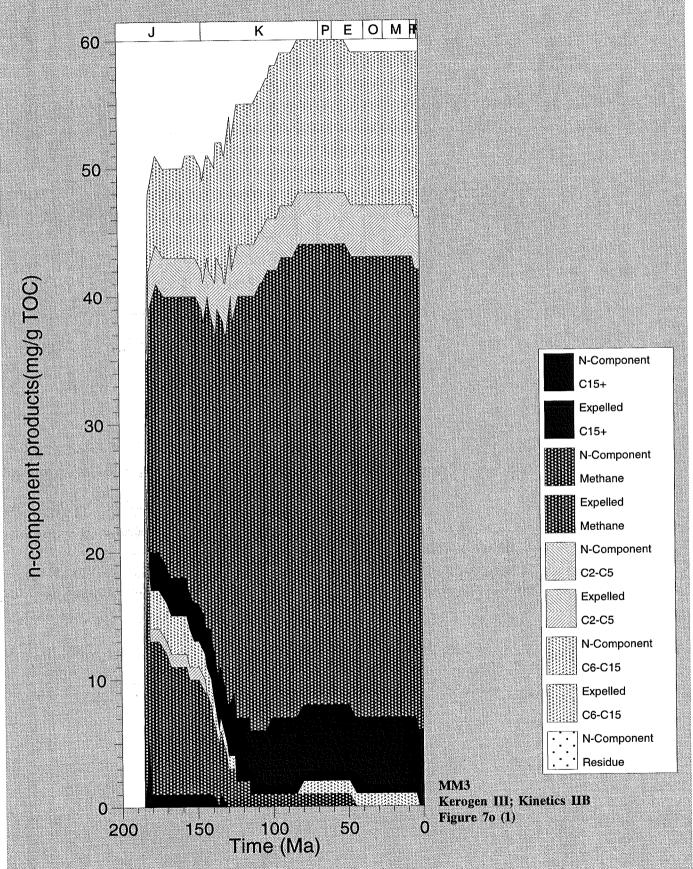


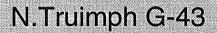


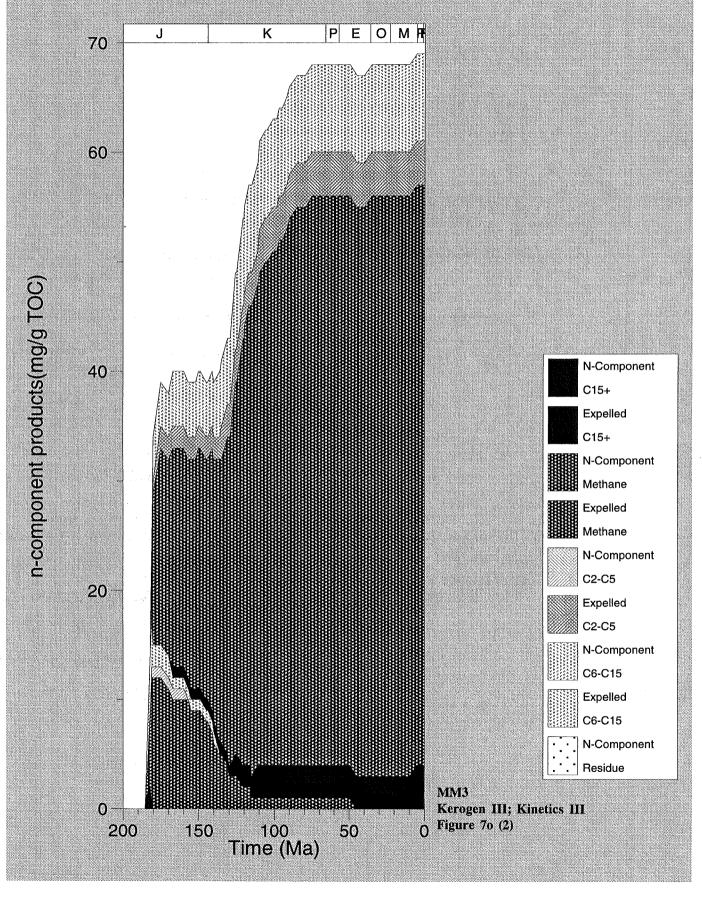


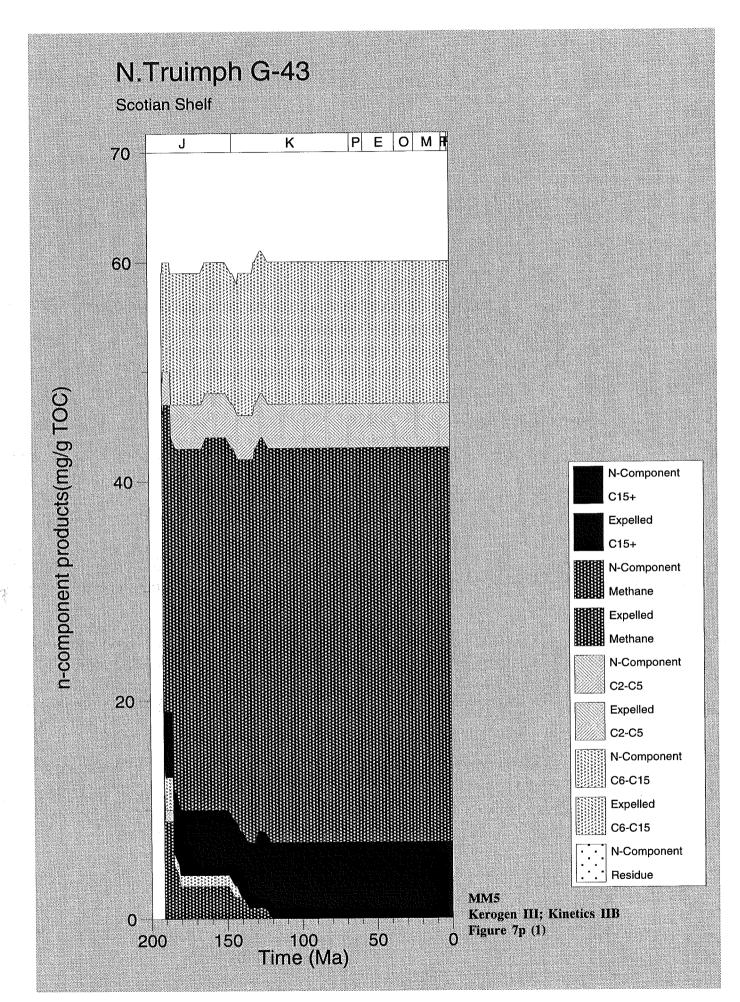


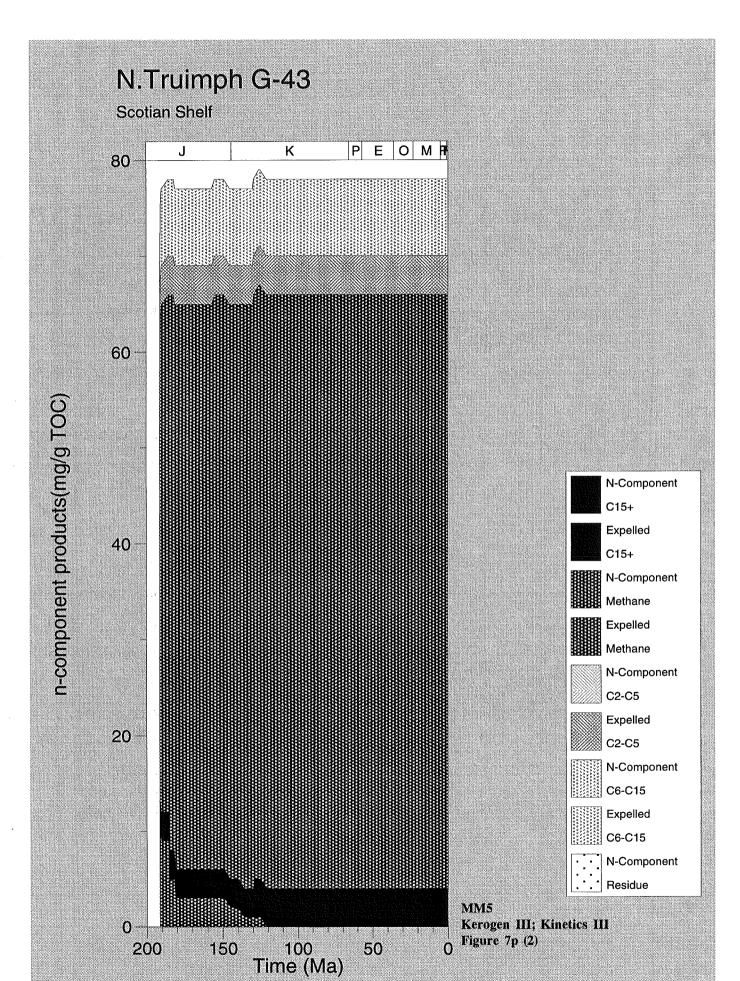


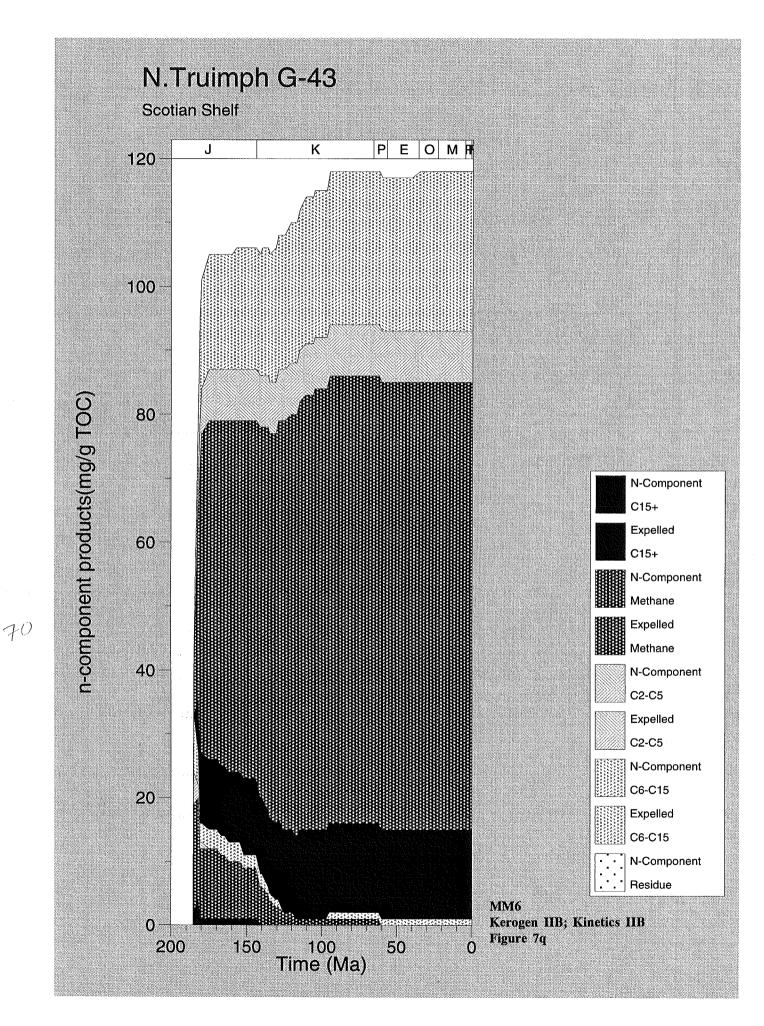


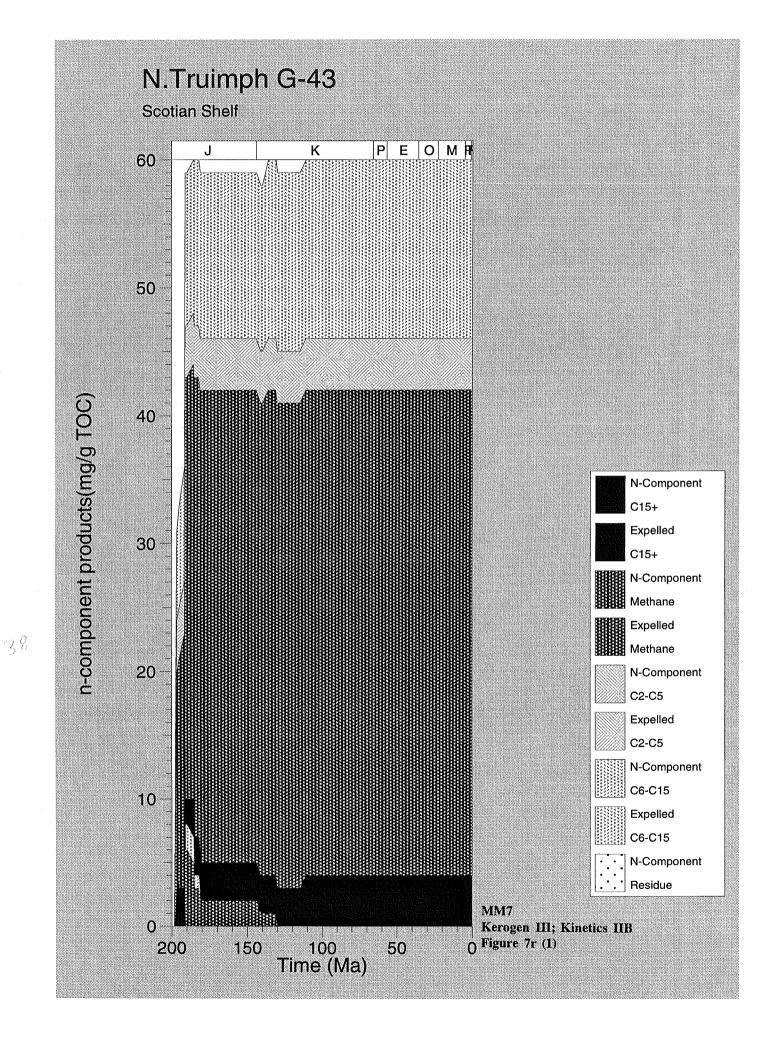


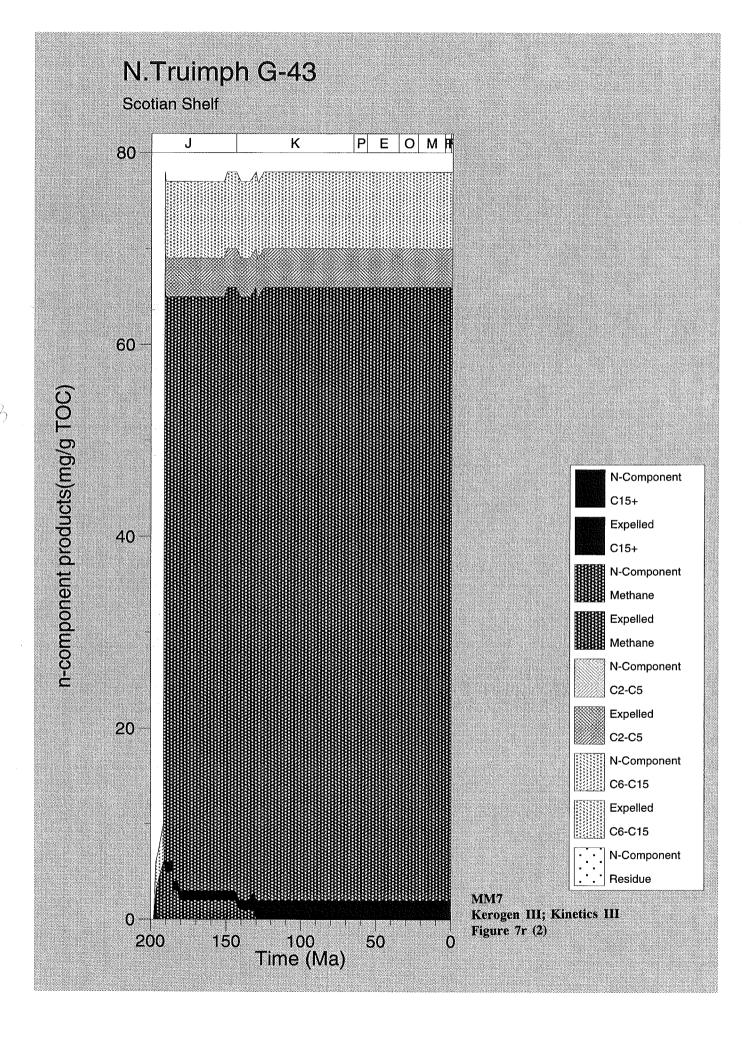




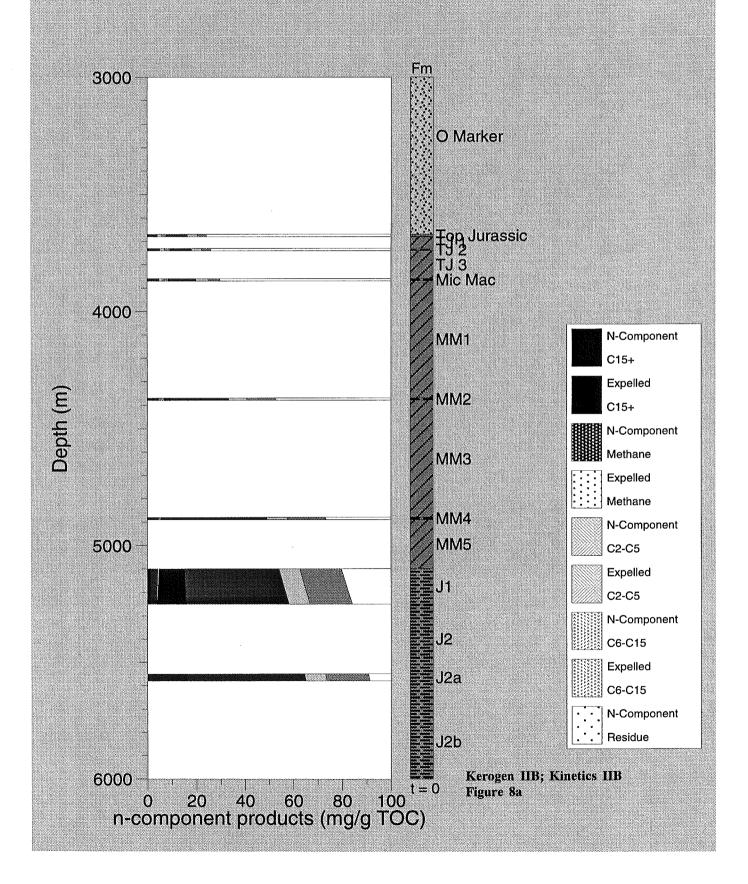


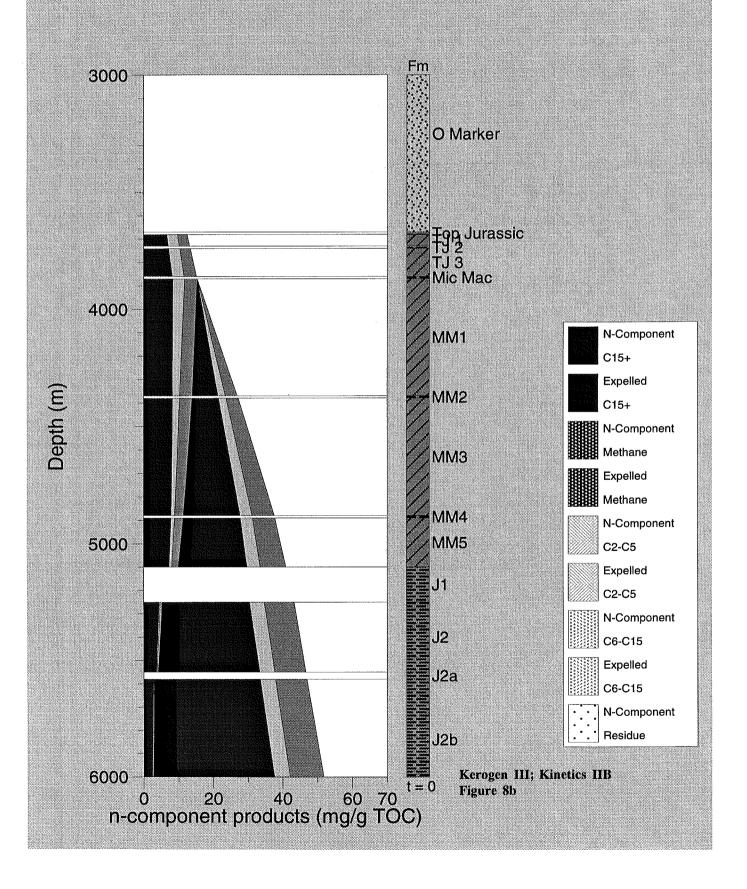


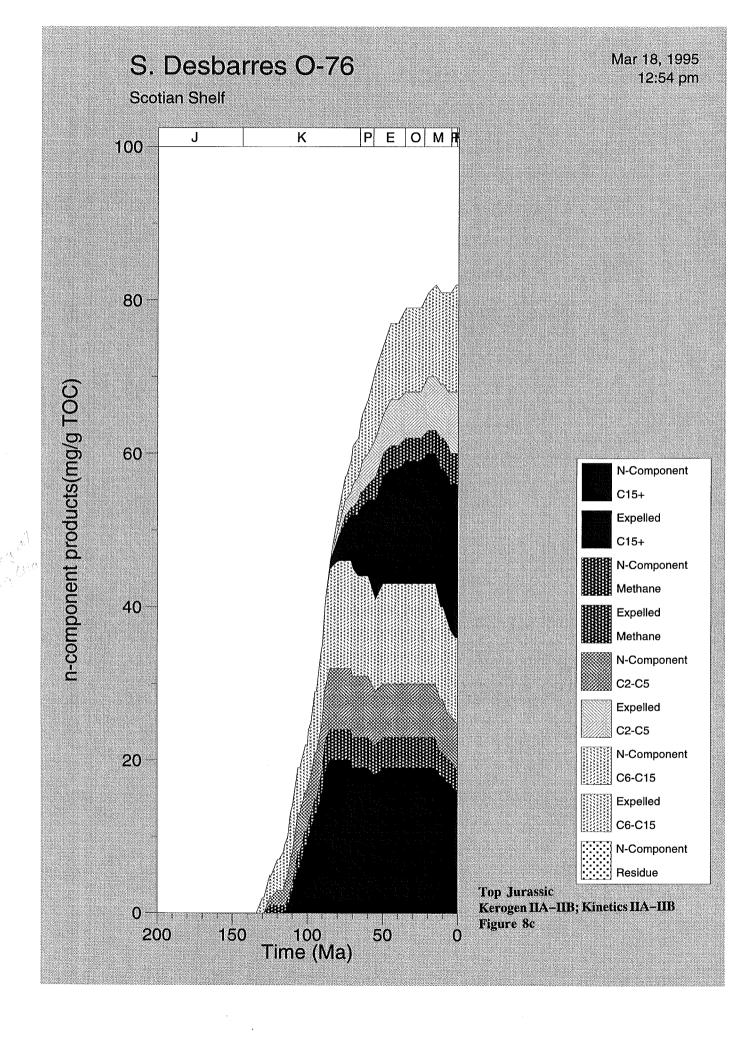


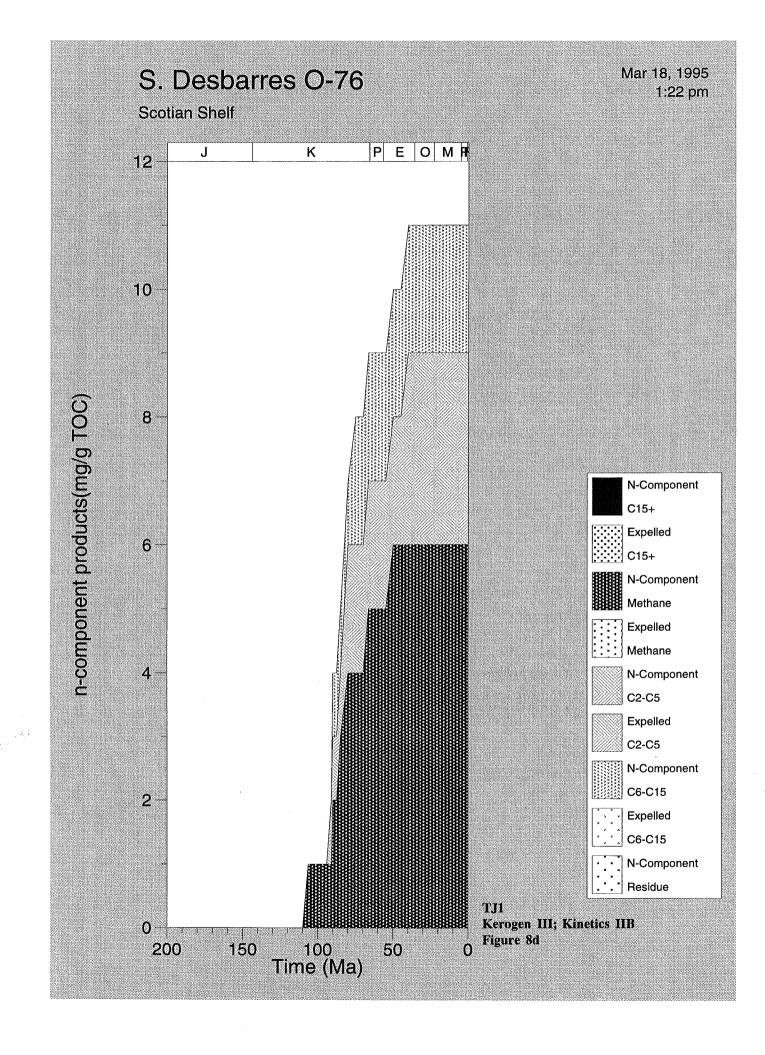


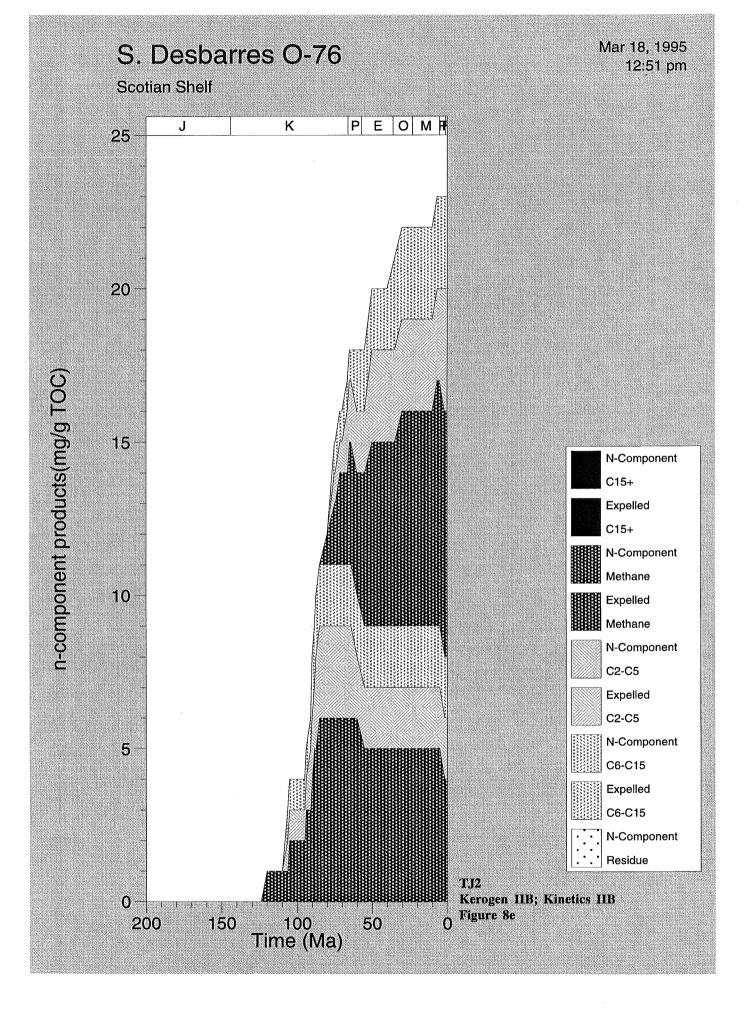
## S. Desbarres O-76

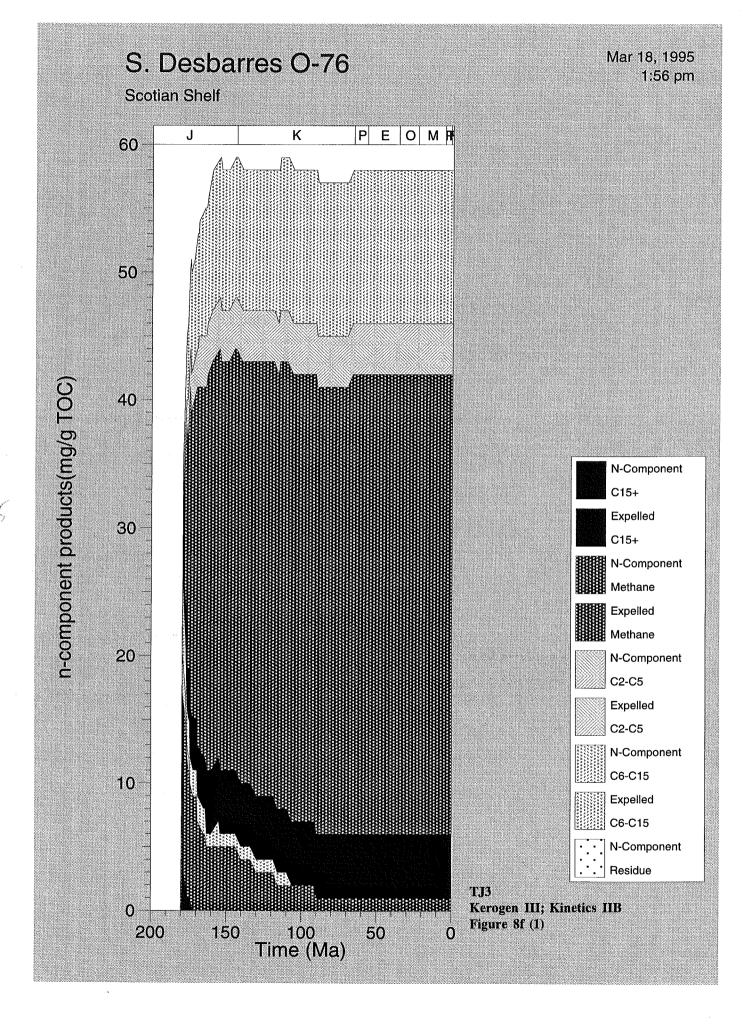


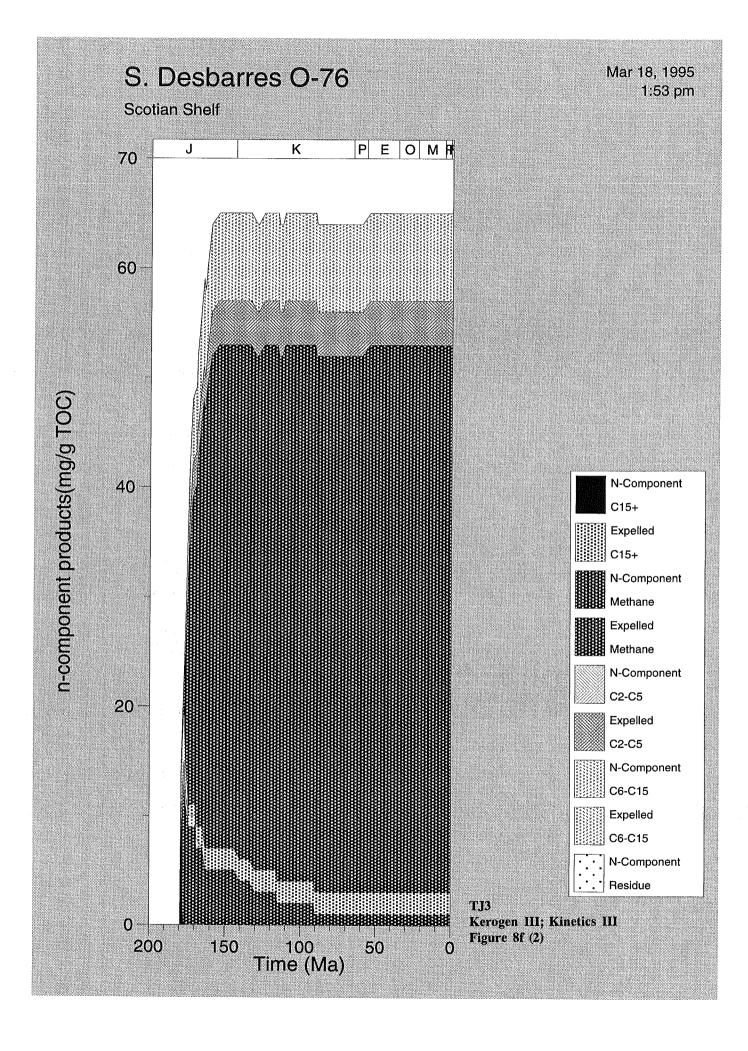


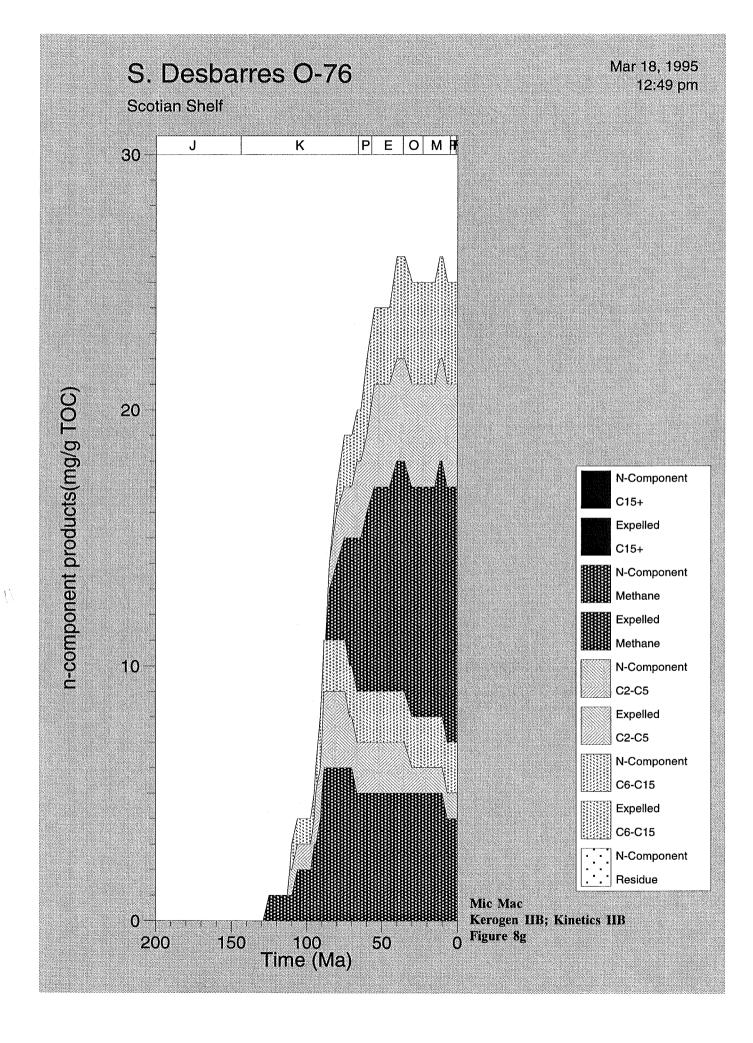


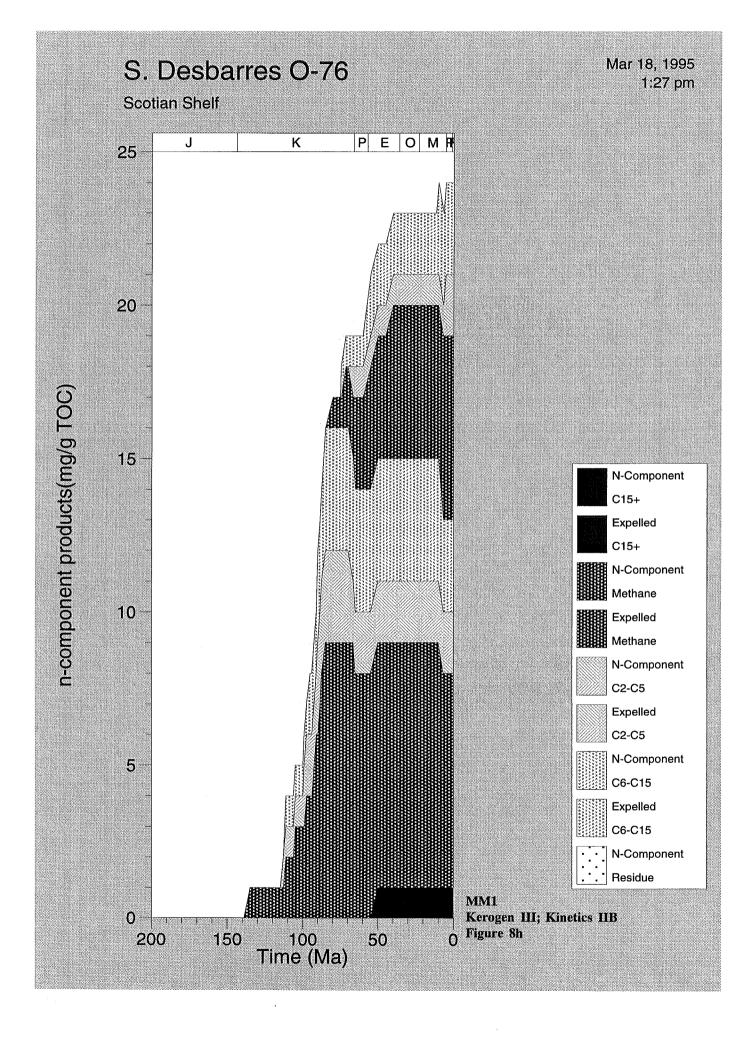


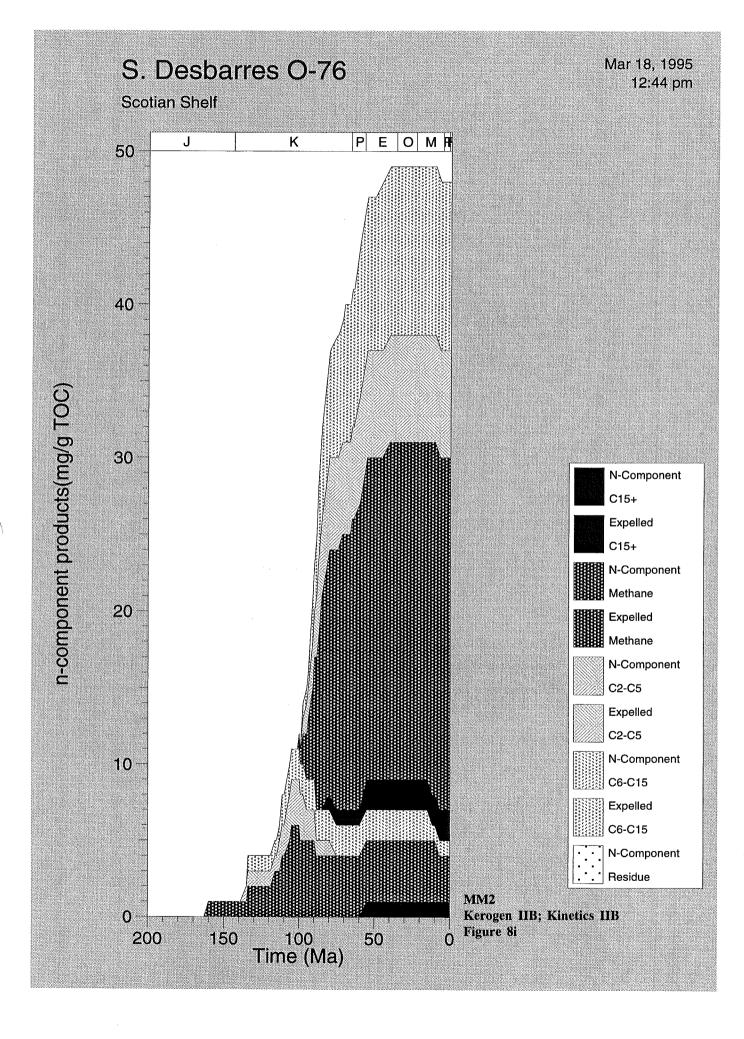


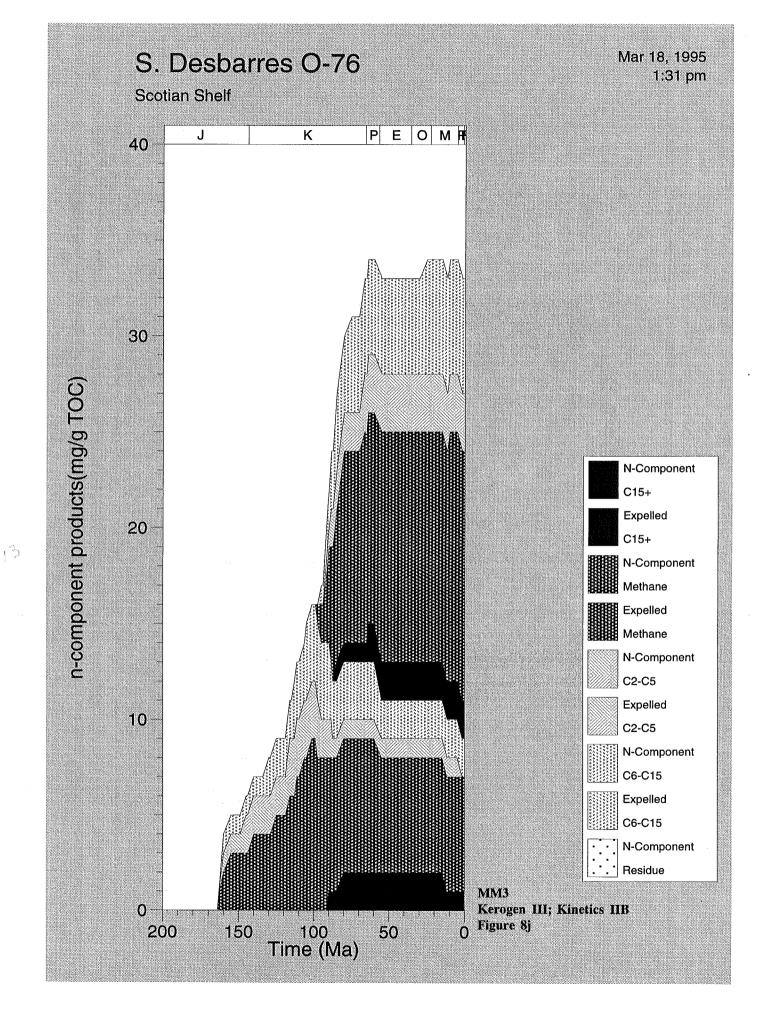


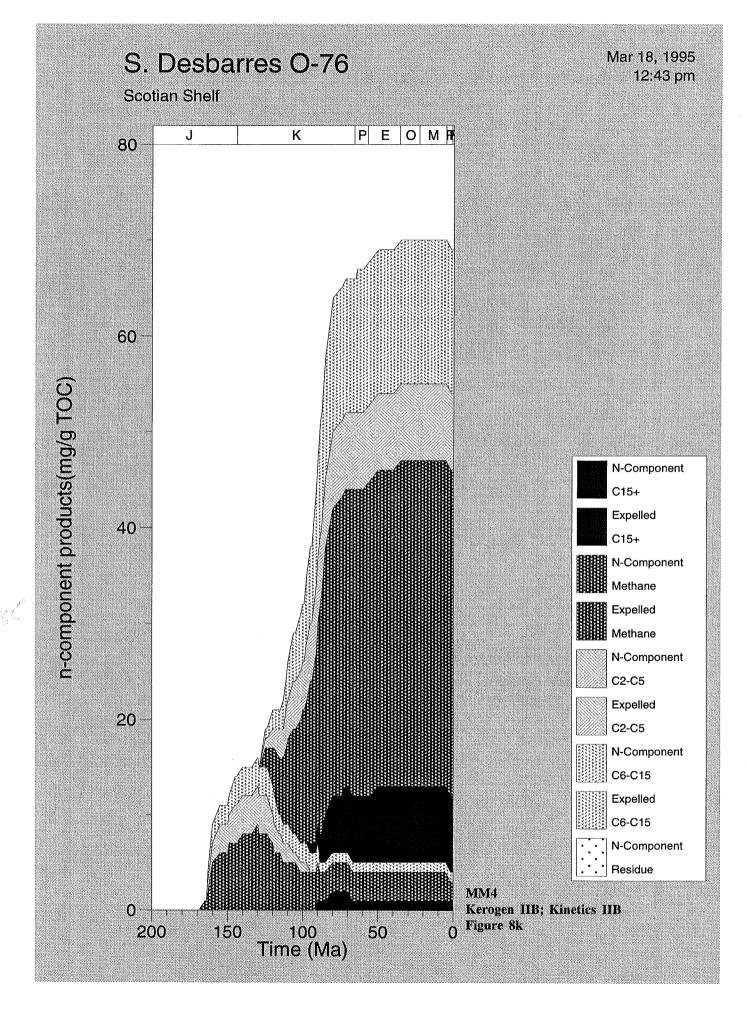


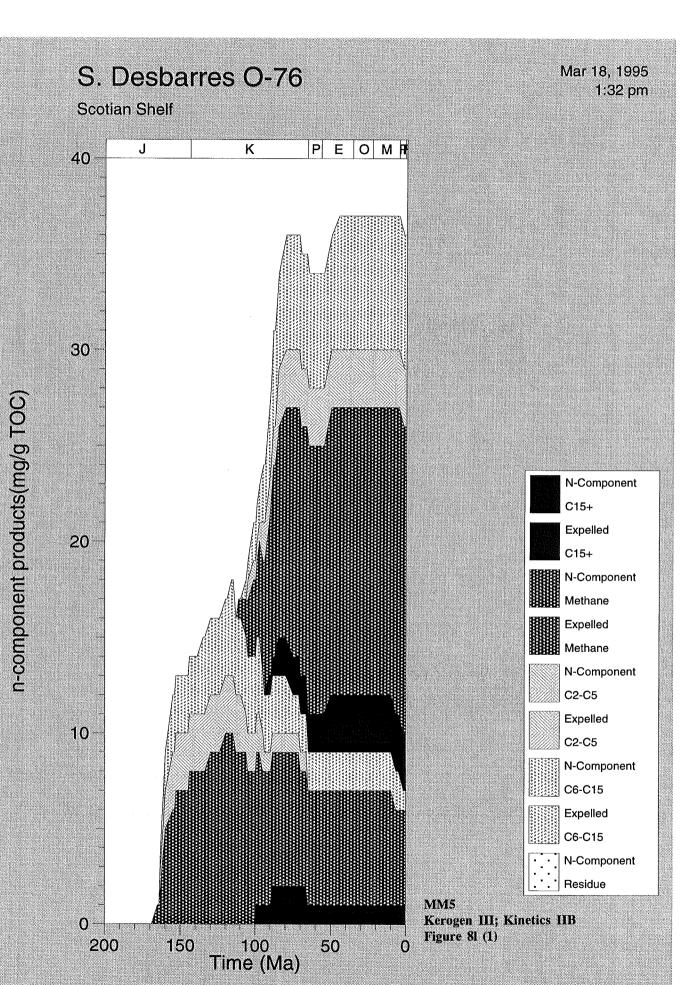


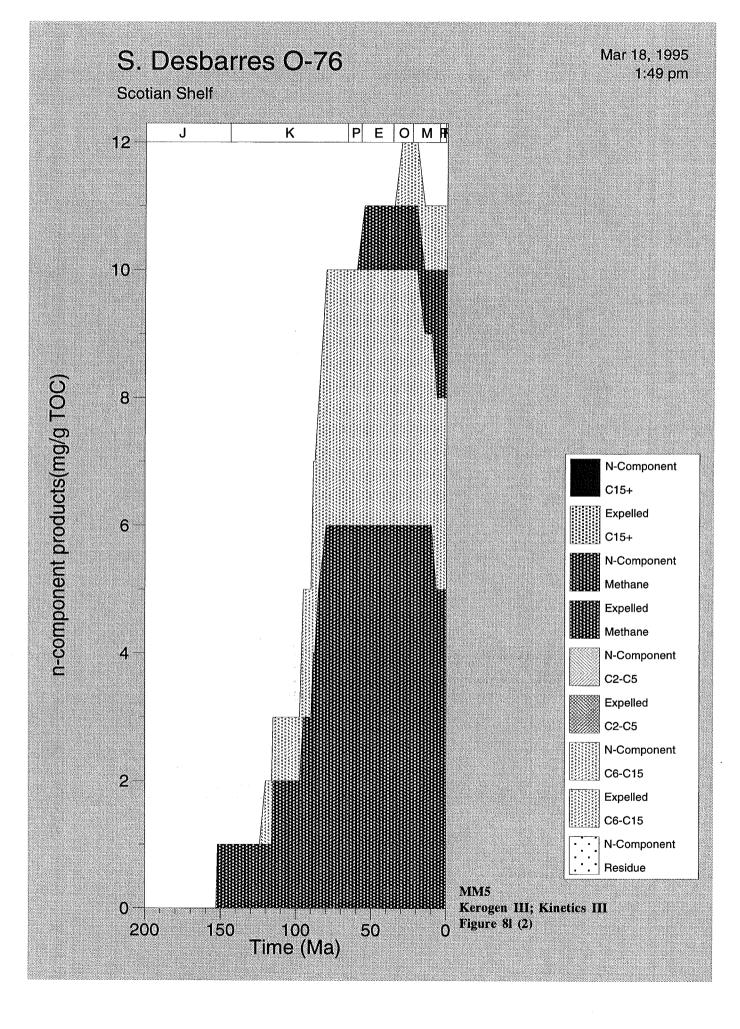


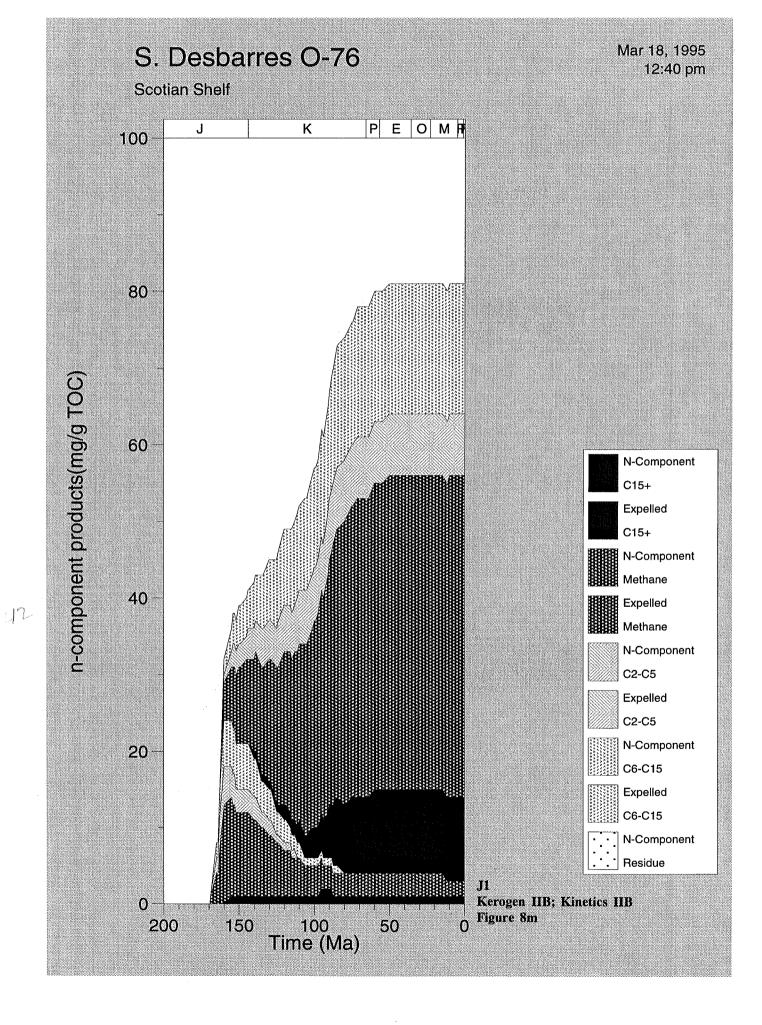


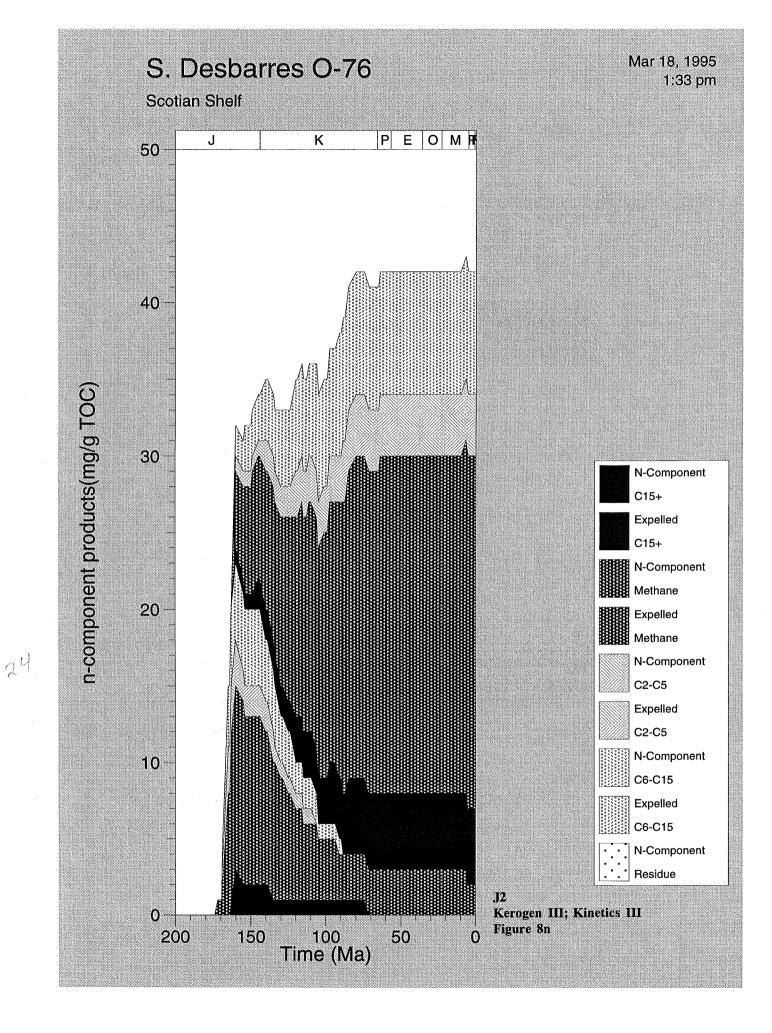


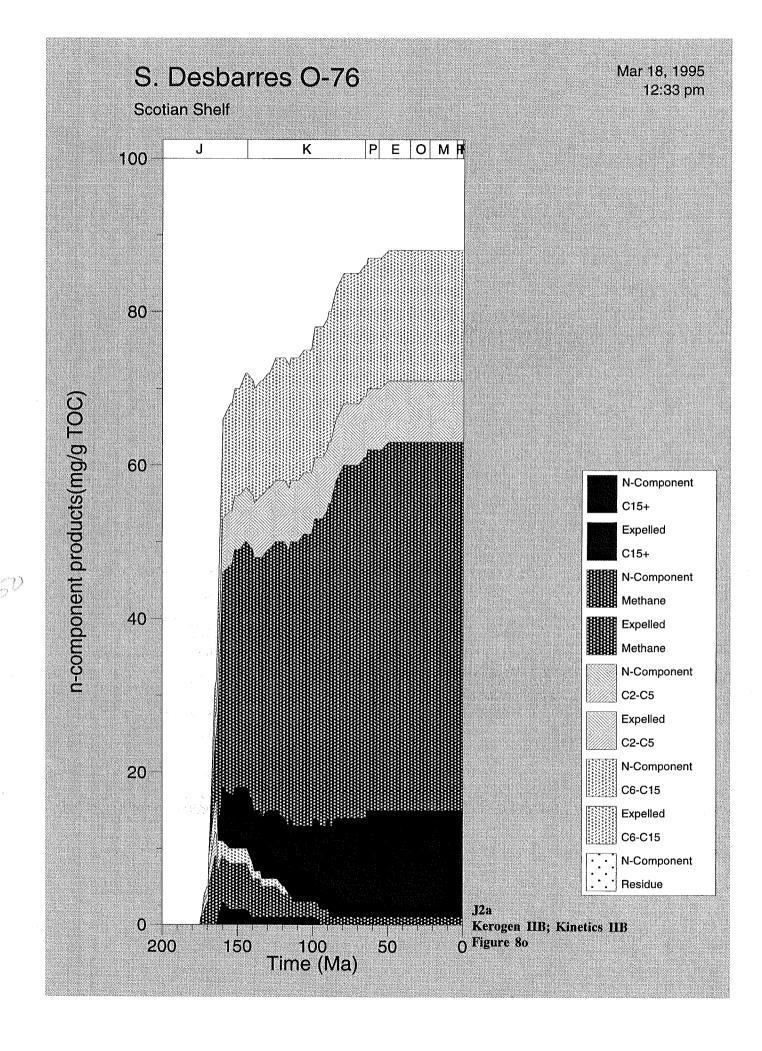












S. Desbarres O-76 Mar 18, 1995 1:36 pm Scotian Shelf Р O M R K Ε J 50 40 n-component products(mg/g TOC) 30 N-Component C15+ Expelled C15+ N-Component Methane 20 Expelled Methane N-Component C2-C5 Expelled C2-C5 N-Component 10 C6-C15 Expelled C6-C15 N-Component Residue J2b Kerogen III; Kinetics IIB Figure 8p (1) 100 Time (Ma) 200 150 50 0

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