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OPEN FILE 2504

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surface refraction measurements,
1989, 1990, 1991**

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1992

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by

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INTRODUCTION

The Geological Survey of Canada is conducting shear wave refraction surveying in the Fraser Delta as an aid in estimating the regional effects of earthquake shaking on thick unconsolidated sediments. Shear wave velocity structure can be utilized in estimates of liquefaction potential of deltaic sediments (Robertson and Woeller, 1992), as well as in the modelling of ground motion amplification effects (Finn and Nichols, 1988).

Various seismic methods are being used to measure shear wave velocities in sediments. These include: downhole well-lock geophone surveying, borehole-to-borehole methods, seismic cone penetrometer, spectral analysis of surface waves (SASW), as well as surface refraction methods.

Downhole surveying is being applied in the Fraser Delta when cased boreholes become available (Hunter et al., 1990). Hole-to-hole measurements have been made for specific engineering applications (Dr. Al Brown, BC Dept. of Highways, pers. comm., 1991). Seismic cone penetrometer studies are being carried out (Robertson et al., 1986; Finn et al., 1989), and wherever possible comparative studies have been made (Hunter et al., 1991). Recently, the SASW technique has been tested in the Fraser Delta (Robertson and Addo, 1991), and future tests are planned (D. Woeller, Conetec Ltd, Vancouver, 1992, pers. comm.).

The surface seismic refraction method used here should be considered as a reconnaissance technique only, since, as with any refraction method, it is limited by the requirement that velocity must increase with depth for accurate interpretation. Hence, the refraction method cannot be applied where substantial velocity reversals occur at depth. Also, even with cases of velocity increasing with depth, there may be a possibility of velocity masking as a result of the well-known "hidden-layer" effect. Despite these limitations, surface refraction methods have been in use for over 50 years in engineering geophysical applications. In comparison with other methods, surface refraction can be relatively inexpensive and rapidly executed.

In the context of the Fraser Delta, the shear wave refraction method is being used in a reconnaissance manner with over one kilometer spacing between adjacent sites. The results of this survey should serve only as a guide in the identification of velocity depth structure as well as in the delineation of large-scale anomalous zones; the data given herein should not be utilized directly in any geotechnical site investigation.

THE SURVEY AREA

The study area, shown in Figure 1, is bounded on the north by the south-sloping Pleistocene highlands immediately north of the North Arm of the Fraser River; on the south by the Tsawwassen Pleistocene uplands and Boundary Bay; on the west by the Strait of Georgia; and on the east by the Surrey uplands (Pleistocene) and the N.E. end of Annacis Island. To date, 70 sites have been completed; it is expected that up to 200 sites may be required to complete the coverage.

THE SURVEY TECHNIQUE

The refraction method was conducted in the transverse shear mode, where the orientation of the horizontal geophones is perpendicular to the line of profile. This mode was selected to minimize the effect of "converted" refracted wave interference. "True" reversed refraction procedures were followed, wherein geophones were located at source positions of forward and reversed geophone spreads. Intervals between geophones were maintained at 3 meters, and geophone spread lengths were designed to be in excess of 200 meters in order to obtain velocity-depth structure to at least 30 meters depth. In some locations, due to logistics constraints, such lengths were not possible.

The geophones used throughout the survey were 8 Hz horizontal geophones manufactured by Oyo-Geospace.

Various types of sources were used during the survey. In 1989, the source used was a horizontal firing modification of the "Buffalo Gun" (Pullan and MacAulay, 1987), where a 12-gauge blank shotgun shell was vented sideways into the ground at a depth of 1 meter below surface to produce polarized SH energy.

In 1990, several similar types of surface plate sources were used with a 16 lb sledge hammer to produce horizontally polarized energy. Such sources are generally of low energy requiring "stacking" or summing of individual records to increase the signal-to-noise ratio. This type of source was used during this field season since many of the sites were located in public parks in an urban environment where it was necessary to keep ground disturbance to a minimum.

In 1991, an 8-gauge blank shotgun shell was used in the standard "Buffalo Gun" configuration with the shot located at 1.5 meters depth. Despite the fact that the source was not polarized, it was found that there was minimal interference of compressional and "converted" waves. In general, the signal-to-noise with this source was superior to those previously used, resulting in generally good quality records.

An example of composite seismic records for site #7 is shown in Figure 2. Dominant frequencies of SH energy are in the range of 20 to 80 Hz. Since cultural noise was often in the same frequency range, the operators were sometimes required to reshoot a record to maintain

an acceptable signal-to-noise ratio.

Seismic data were recorded using a variety of different engineering seismographs including: EG&G NIMBUS 1210F, Scintrex Echo-2, Bison 9000 and EG&G 2401. Records were usually 1 second in length with time delays to start-of-record where necessary. The digital sampling rate was maintained at 1 millisecond giving a possible seismic pass-band of 0 to 250 Hz.

DATA INTERPRETATION

All composite seismic records were re-played on wide computer paper in variable area format for picking of first arrival events. This mode was used instead of the usual computer-interactive screen display to allow the interpreter maximum latitude in aspect ratio. Travel times were picked to 1 millisecond accuracy from the print-outs. Large scale travel time vs distance plots were computer-generated for both forward and reverse record suites at each site, and conventional layered-case line-segment interpretation was performed graphically by one of us (Hunter). Additionally, in order to remove operator bias, the travel-time distance data were analysed using a computer program VELDEP (Hunter, 1971). This routine fits a smoothed curve to the travel-time-distance data where velocity gradients are evident, yet maintains abrupt velocity boundaries where they exist.

RESULTS

The results are shown in the following two sections. Section I is a compilation of travel-time distance plots for the forward and reverse data of each site. Data points shown are those picked by the interpreter; the solid line is the smoothed curve obtained from the VELDEP computer routine. The graphical layered interpretation using velocity segments is not shown, since experience has shown that different interpreters will choose different line segments, especially with data where velocity-depth gradients are apparent. The reader is encouraged to attempt his own interpretation for comparison with the layered interpretation and the VELDEP results given in Section II.

Section II shows the velocity-depth interpretations for both forward and reverse profiles at each site for both the layered-case graphical method and the computer-fitted velocity-depth function using VELDEP. The data point symbols have been suppressed on these plots for clarity. Also shown with the site number is a short description of the site location and the UTM co-ordinates of the center of the geophone spread at the site. Positioning was done from surface reference using 1:25000 topographic maps available for the Fraser Delta area. Occasional field checks of locations were carried out using a GPS receiver; observed errors were less than 50 meters.

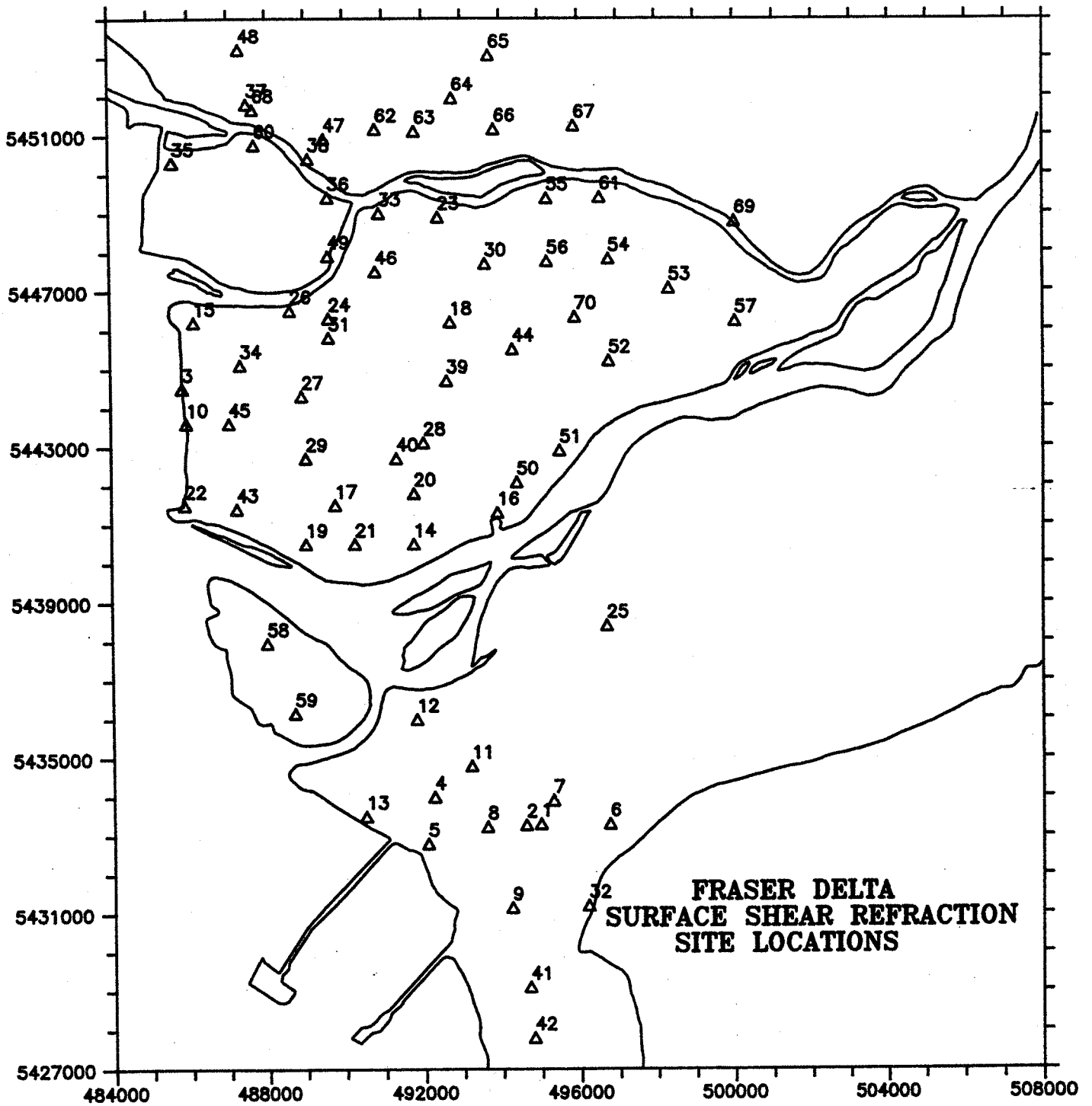


Figure 1. Fraser Delta shallow surface shear refraction site locations for 1989, 1990, and 1991.

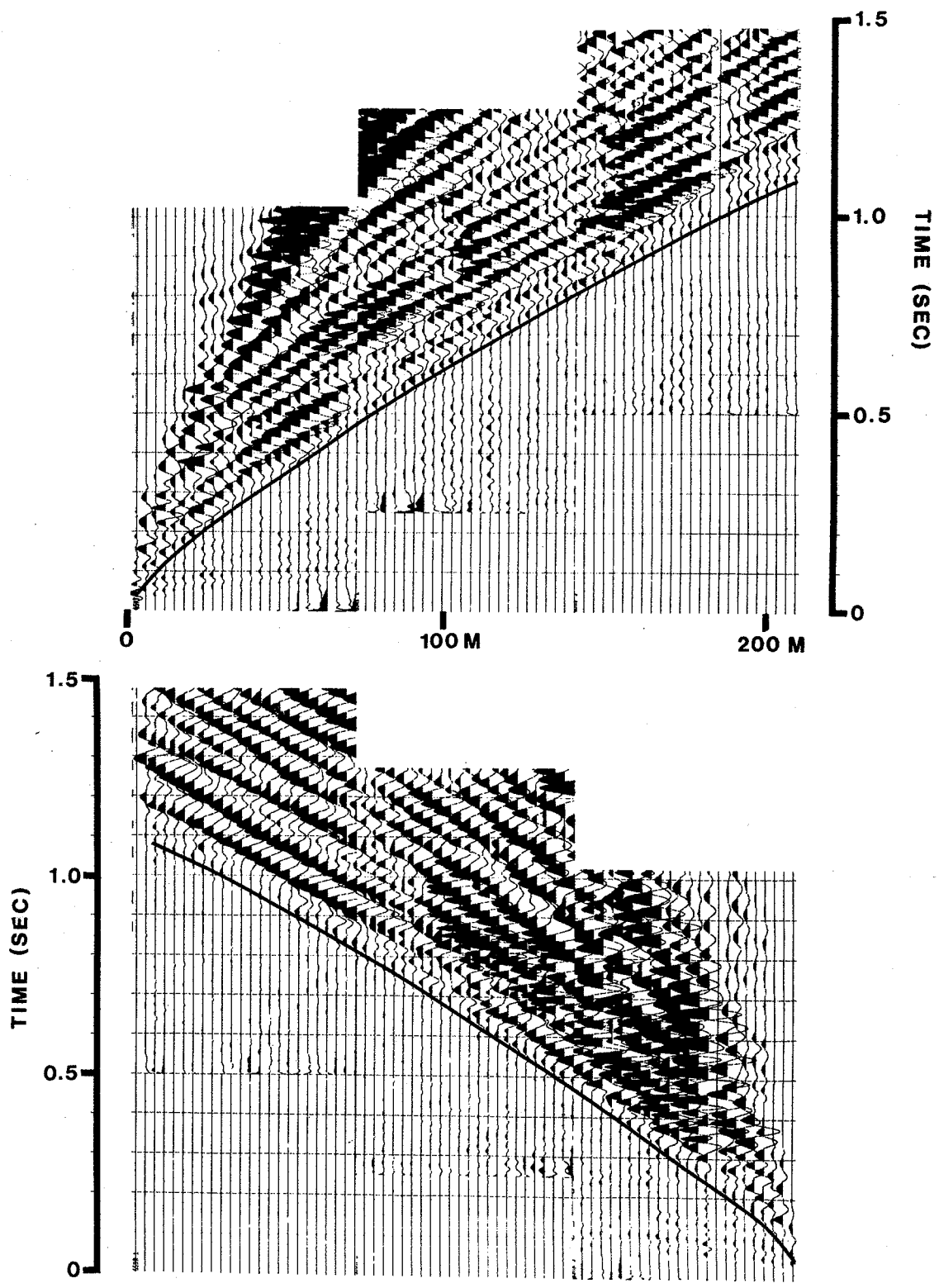


Figure 2. Example composite shear wave refraction seismic records from site 7. The forward profile is shown in the upper portion of the figure; the reverse profile below.

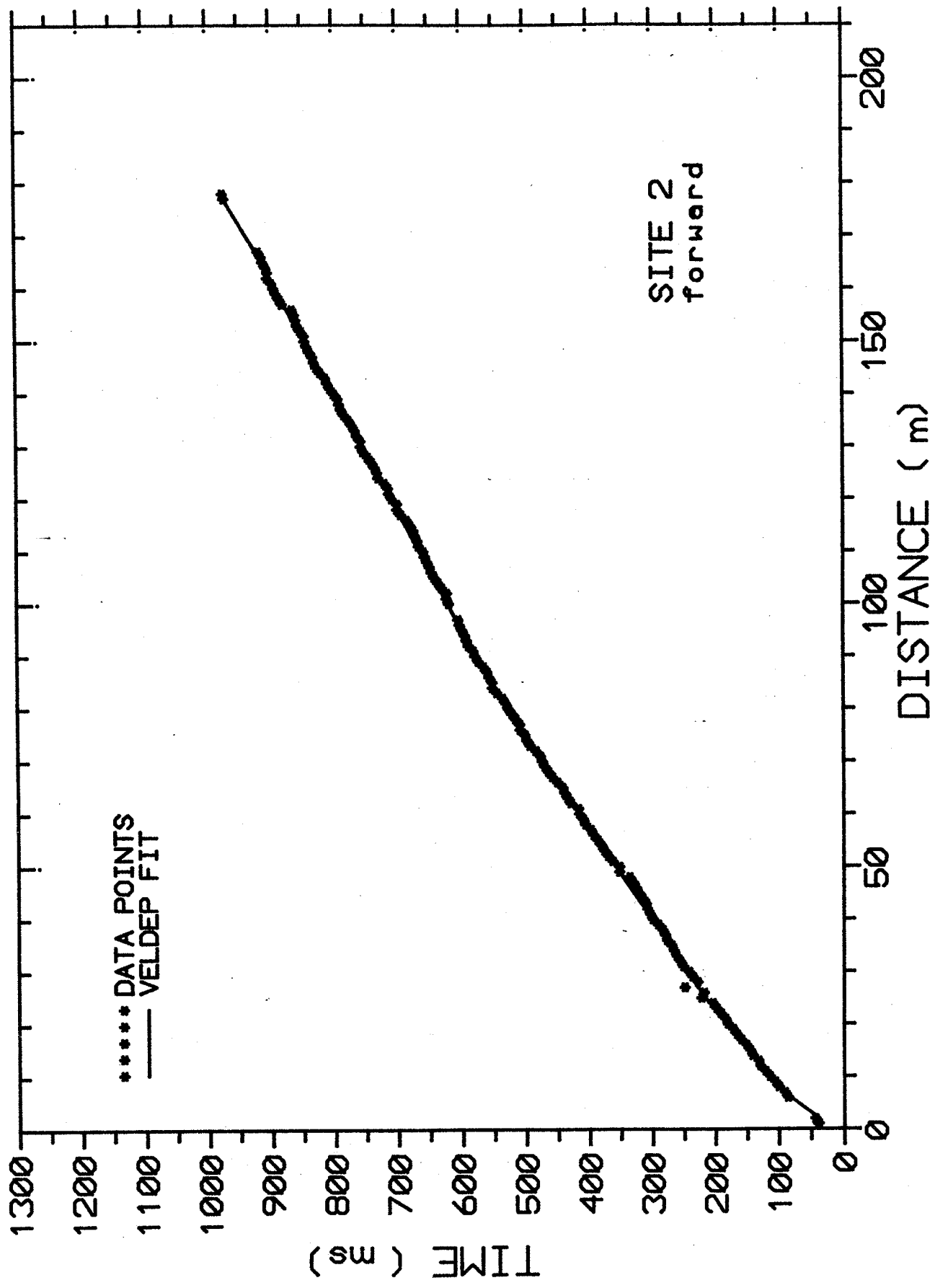
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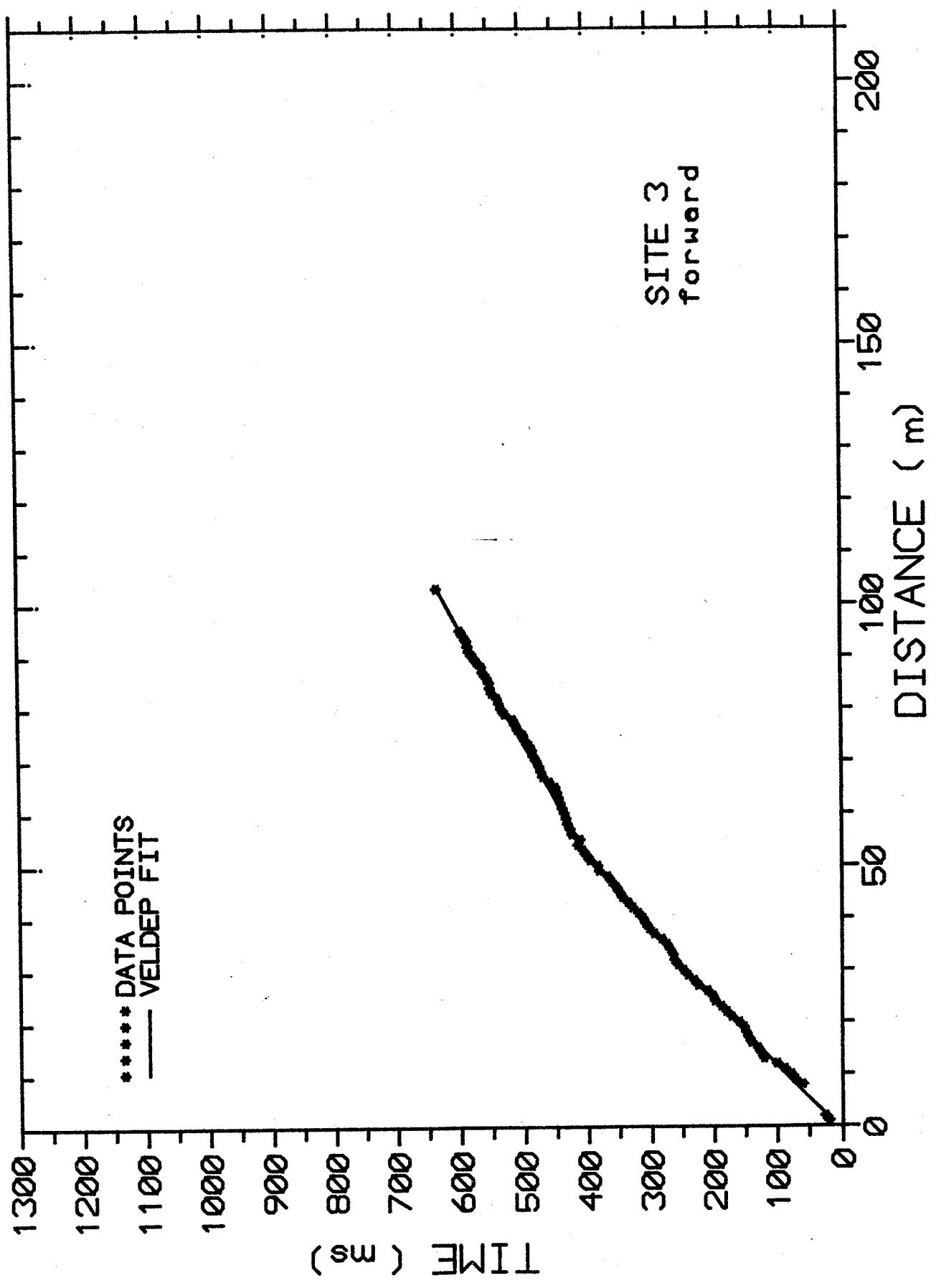
- Finn, W.D.L., and Nichols, A.M., (1988),
Seismic Response of Long-Period Sites: Lessons from the September 19, 1985 Mexican Earthquake; *Can. Geotech. J.*, v. 25, p. 128-137.
- Finn, W.D.L., Woeller, D.J., Davies, M.P., Luternauer, J.L., Hunter, J.A., and Pullan, S.E., (1989),
New Approaches for Assessing Liquefaction Potential of the Fraser River Delta, British Columbia; in *Current Research, Part E, Geol. Surv. Can.*, Paper 89-1E, p. 221-231.
- Hunter, J.A., (1971),
A Computer Method to Obtain the Velocity-Depth Function from Seismic Refraction Data; in *Report of Activities, Part B, Geol. Surv. Can.*, Paper 71-1B, p. 40-48.
- Hunter, J.A., Burns, R.A., and Good, R.L., (1990),
Borehole Shear Wave Velocity Measurements, Fraser Delta, 1989; *Geol. Surv. Can.*, Open File 2229.
- Hunter, J.A., Woeller, D.J., and Luternauer, J.L., (1991),
Comparison of Surface, Borehole and Seismic Cone Penetrometer Methods of Determining the Shallow Shear Wave Velocity Structure in the Fraser River Delta, British Columbia; in *Current Research, Part A, Geol. Surv. Can.*, Paper 91-1A, p. 23-26.
- Pullan, S.E., and MacAulay, H.A., (1987)
An In-Hole Shotgun Source for Engineering Seismic Surveys; *Geophysics*, v. 52, p.985-996.
- Robertson, P.K., Campanella, R.G., Gillespie, D., and Rice, A., (1986),
Seismic CPT to Measure In Situ Shear Wave Velocity; *J. Geotech. Engineering Div., ASCE*, v. 112, p. 791-803.
- Robertson, P.K., and Addo, K.O., (1991),
Recent In-Situ Methods to Determine Seismic Velocity Profiles; in *Geotechnical News, Can. Geotech. Soc.*, September 1991, p. 26-30.
- Robertson, P.K., and Woeller, D.J., (1992),
Seismic Cone Penetration Test for Evaluating Liquefaction Potential; *Can. Geotech. J.*, in press.

SECTION I

TRAVEL TIME - DISTANCE PLOTS

SITES 1 TO 70



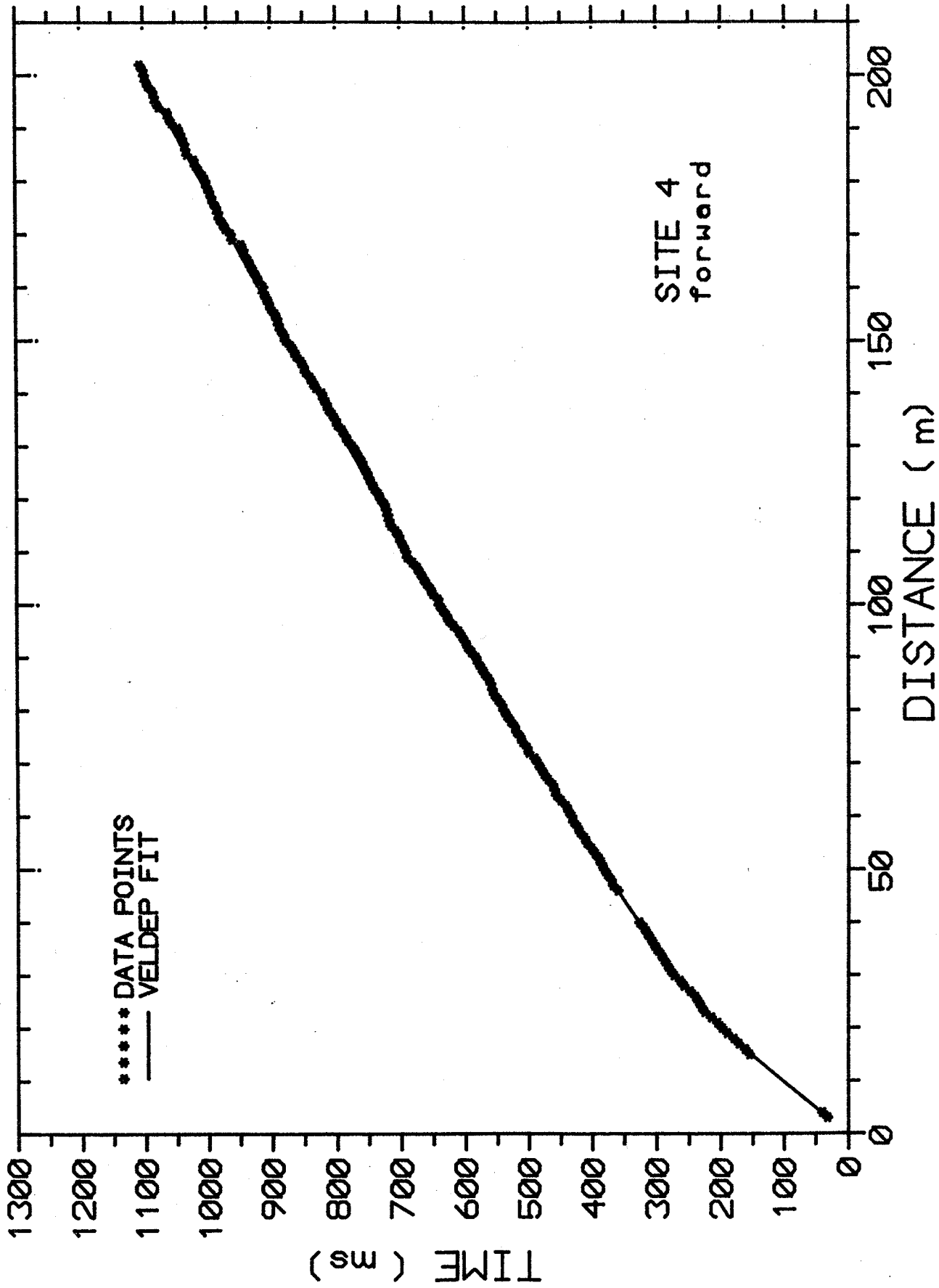


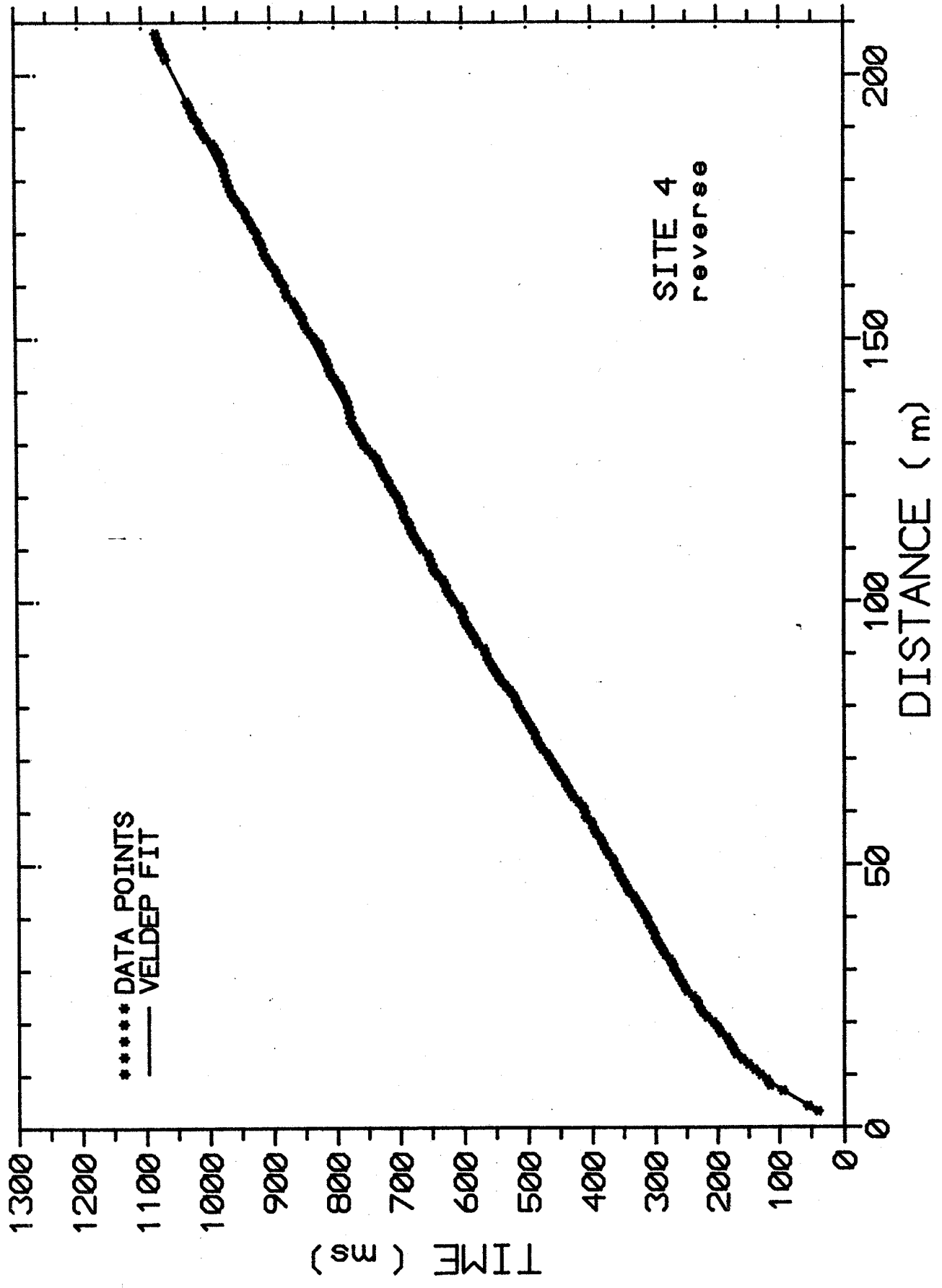
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forward

***** DATA POINTS
—— VELDEP FIT

TIME (s)

DISTANCE (m)



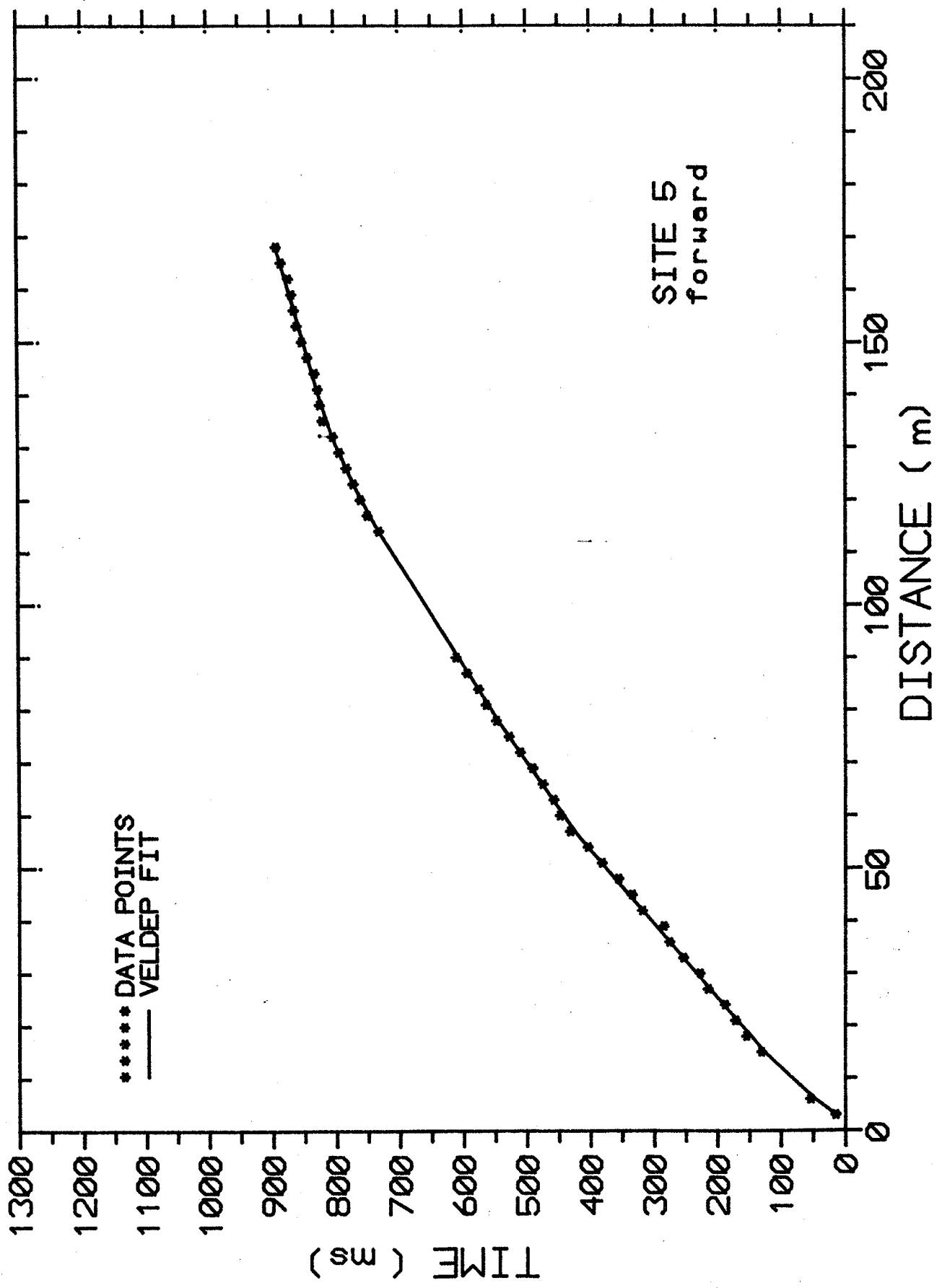


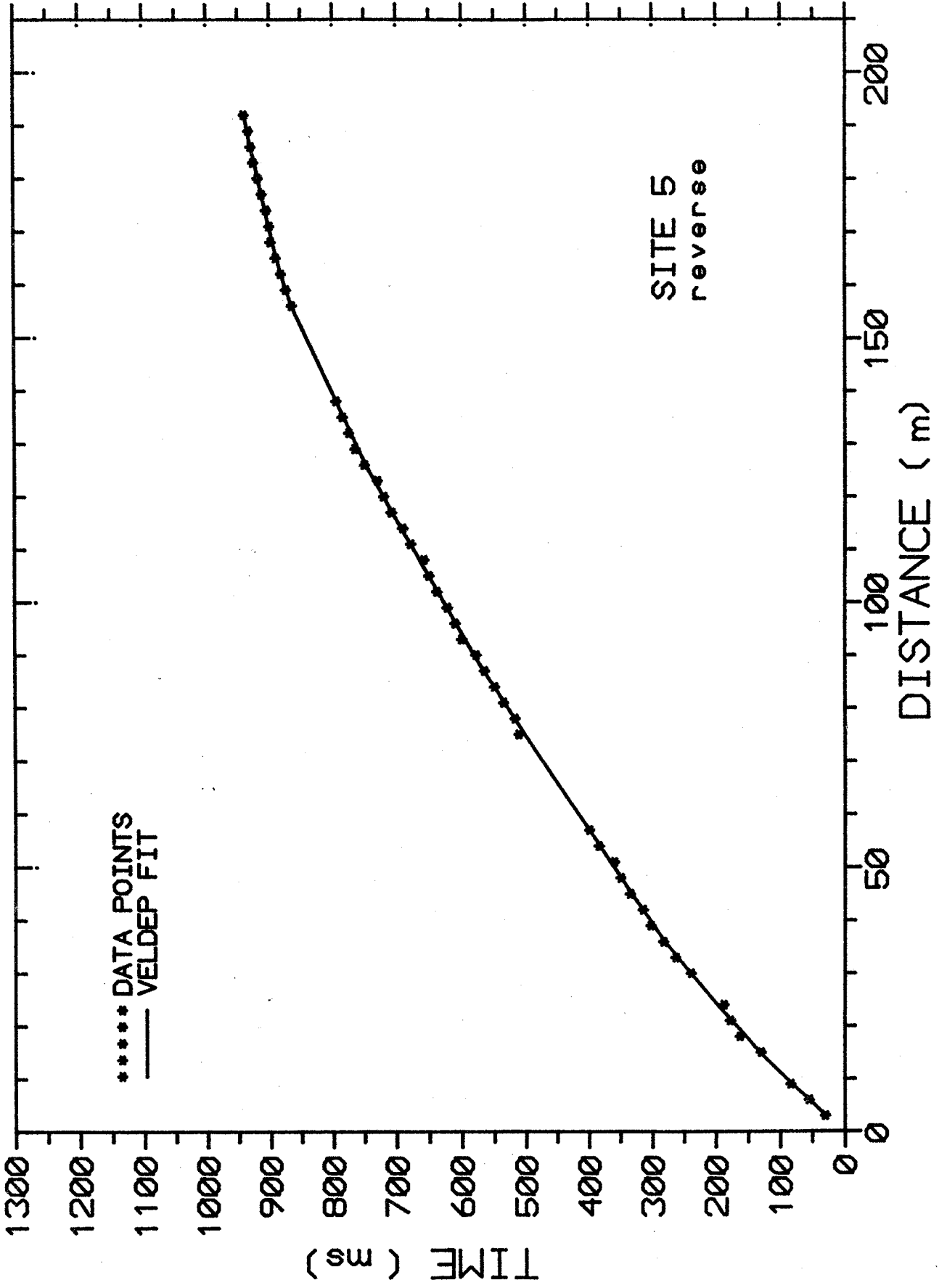
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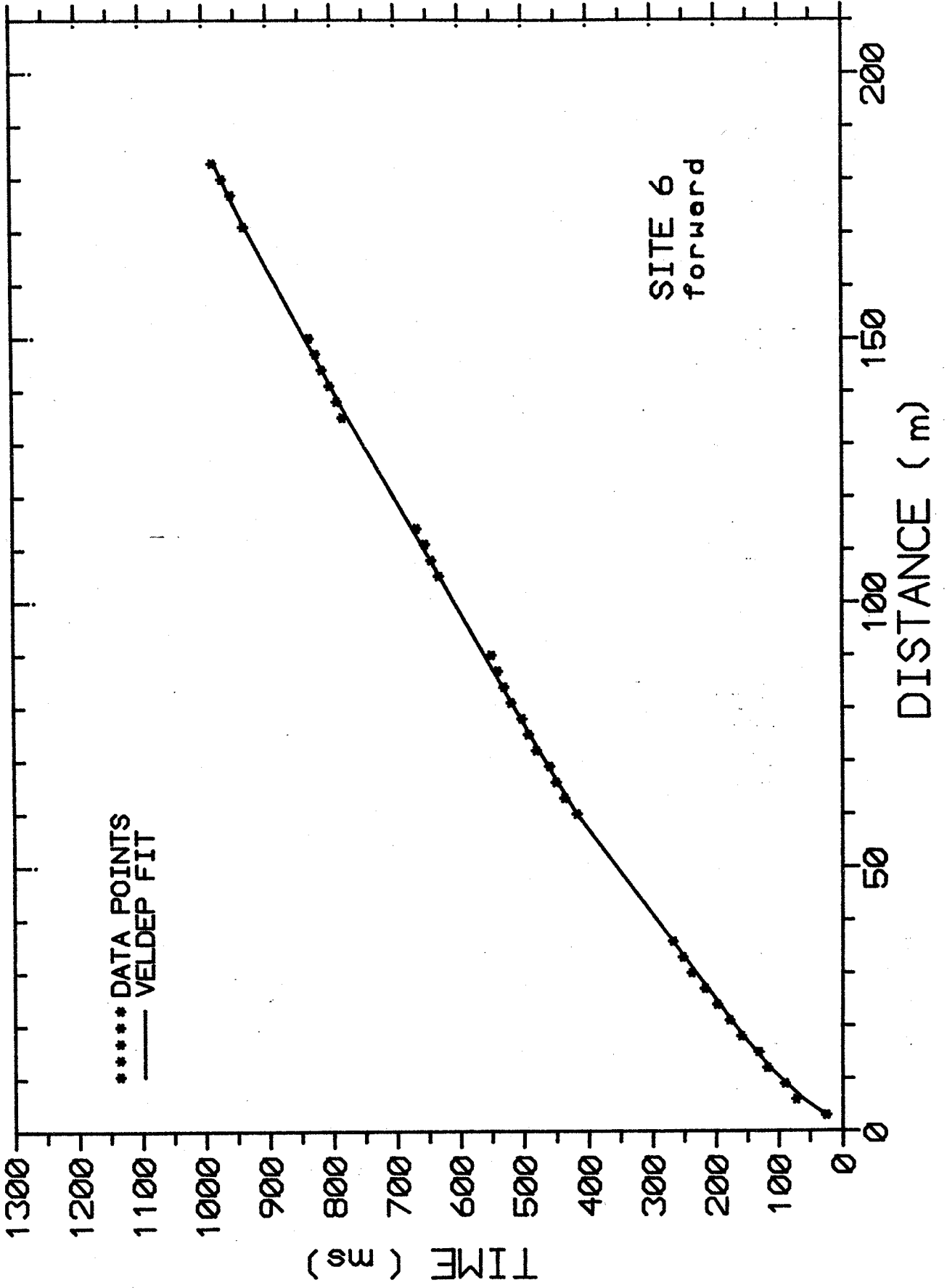
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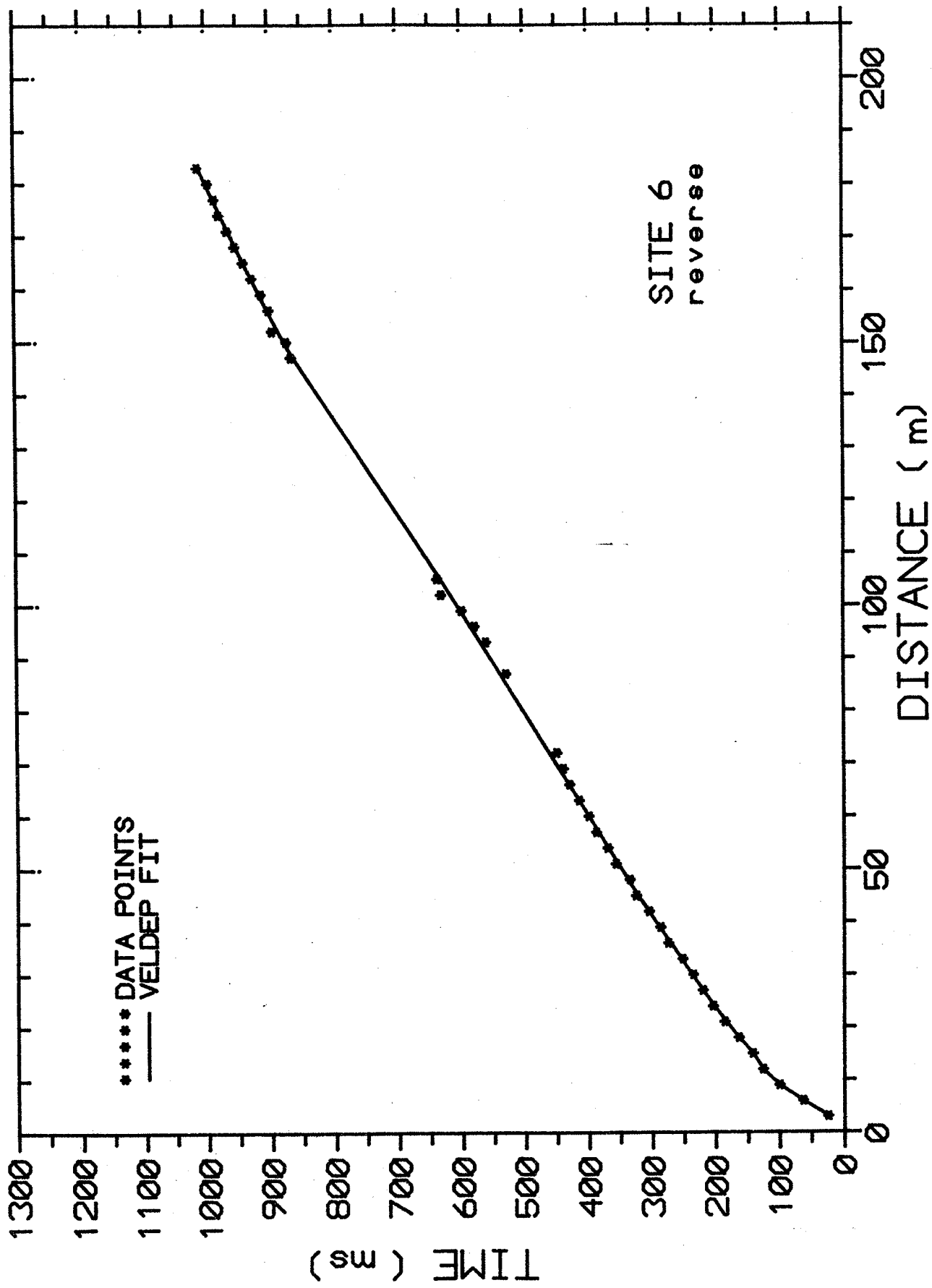
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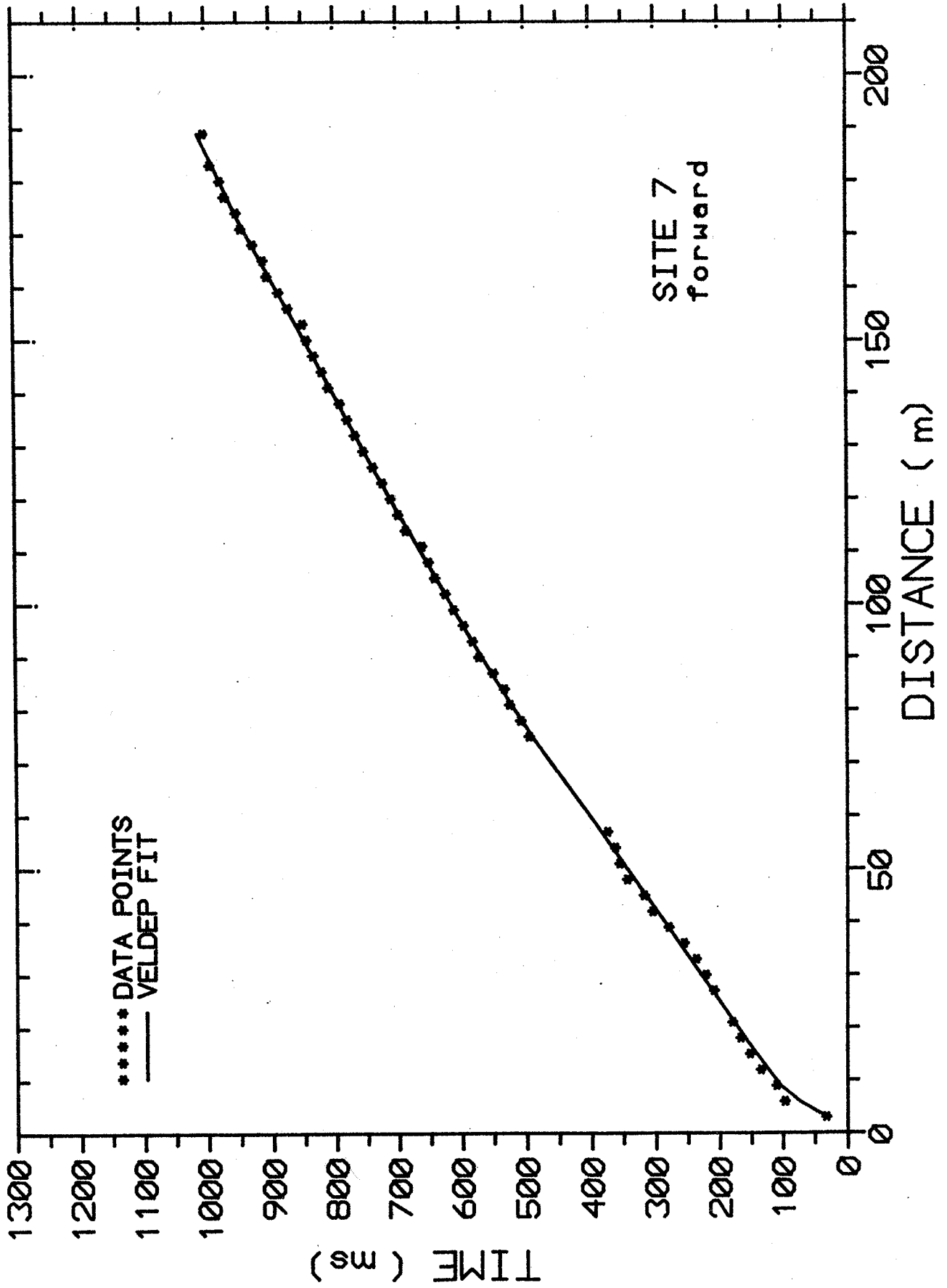
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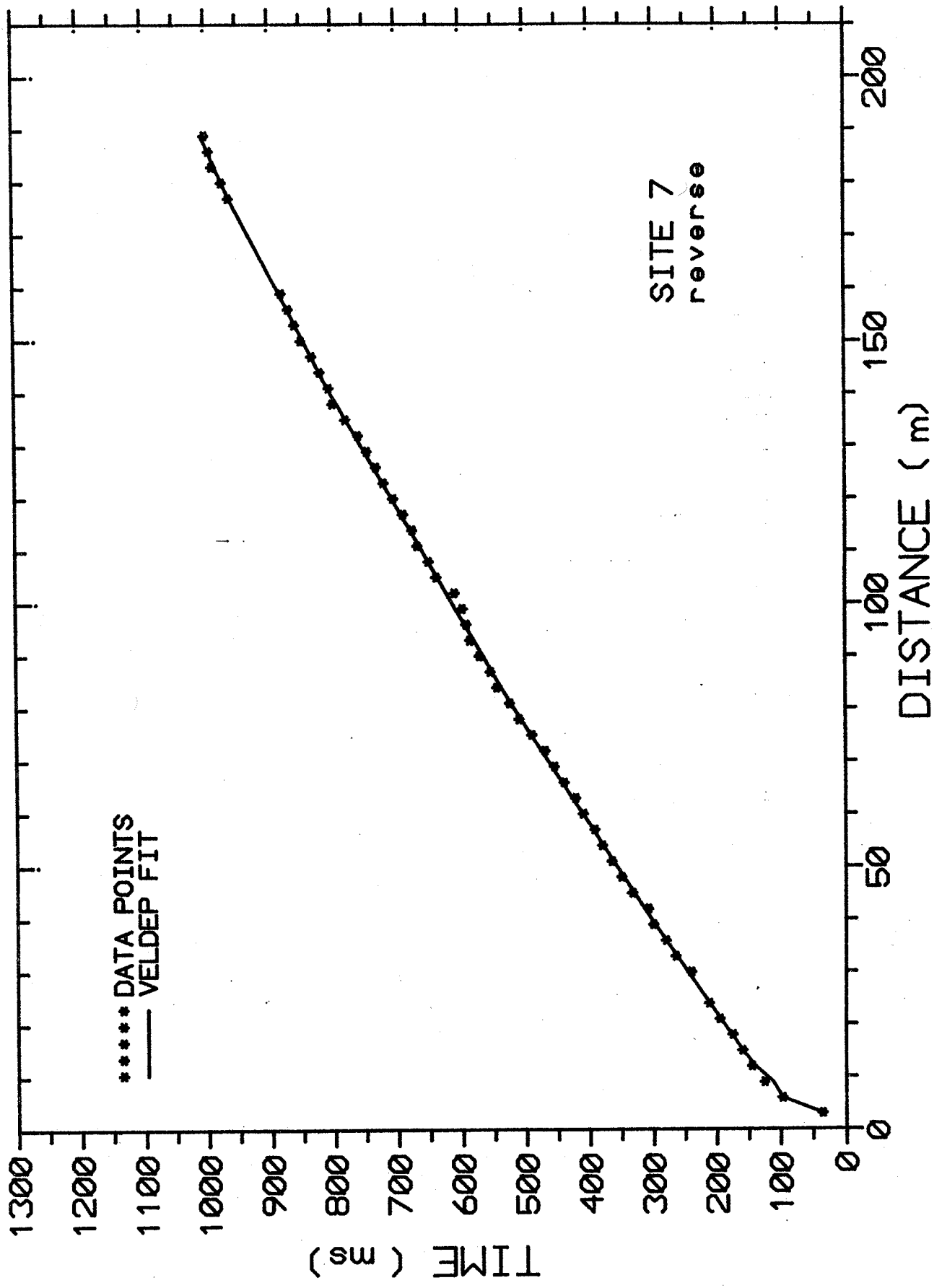






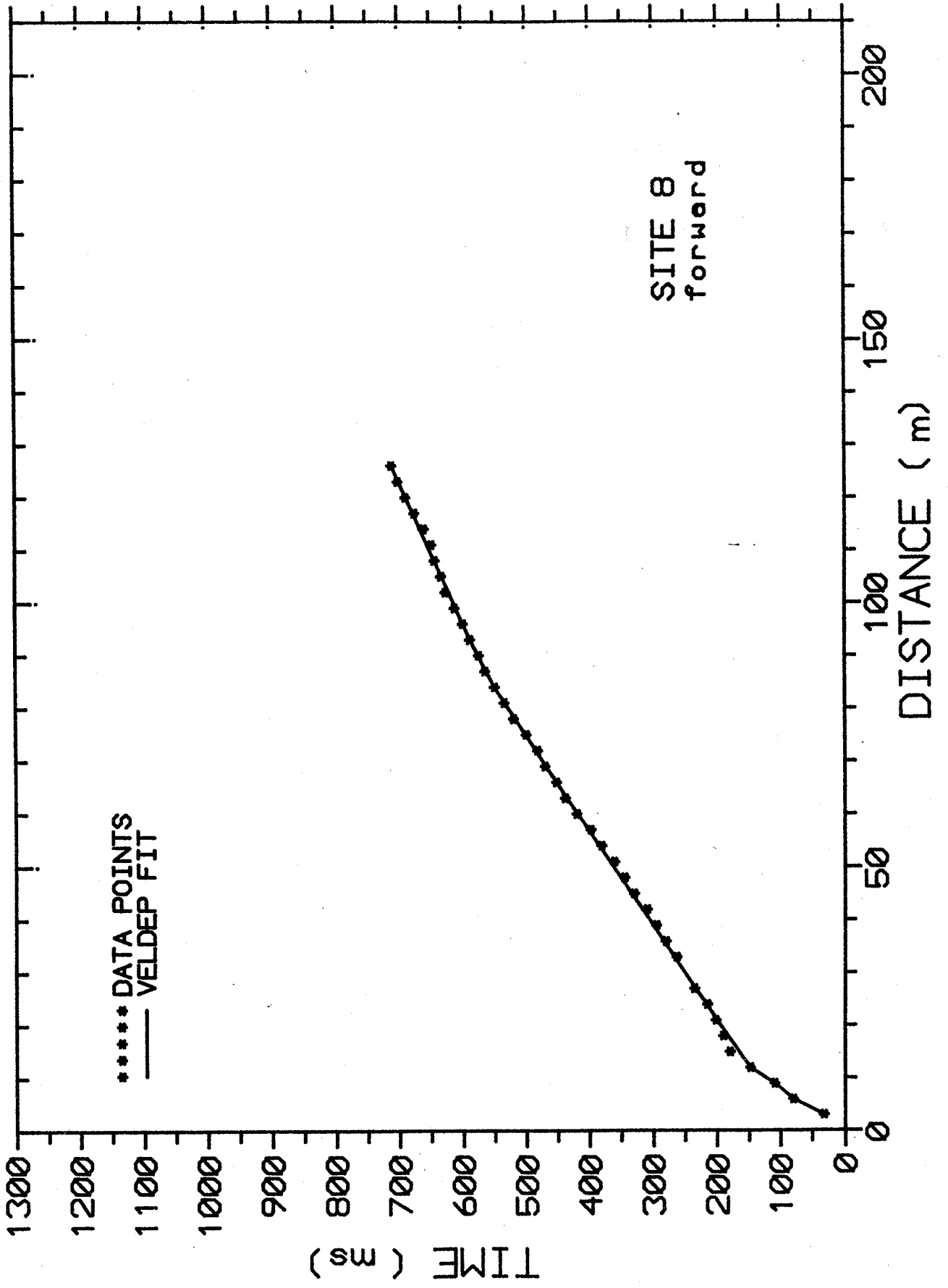
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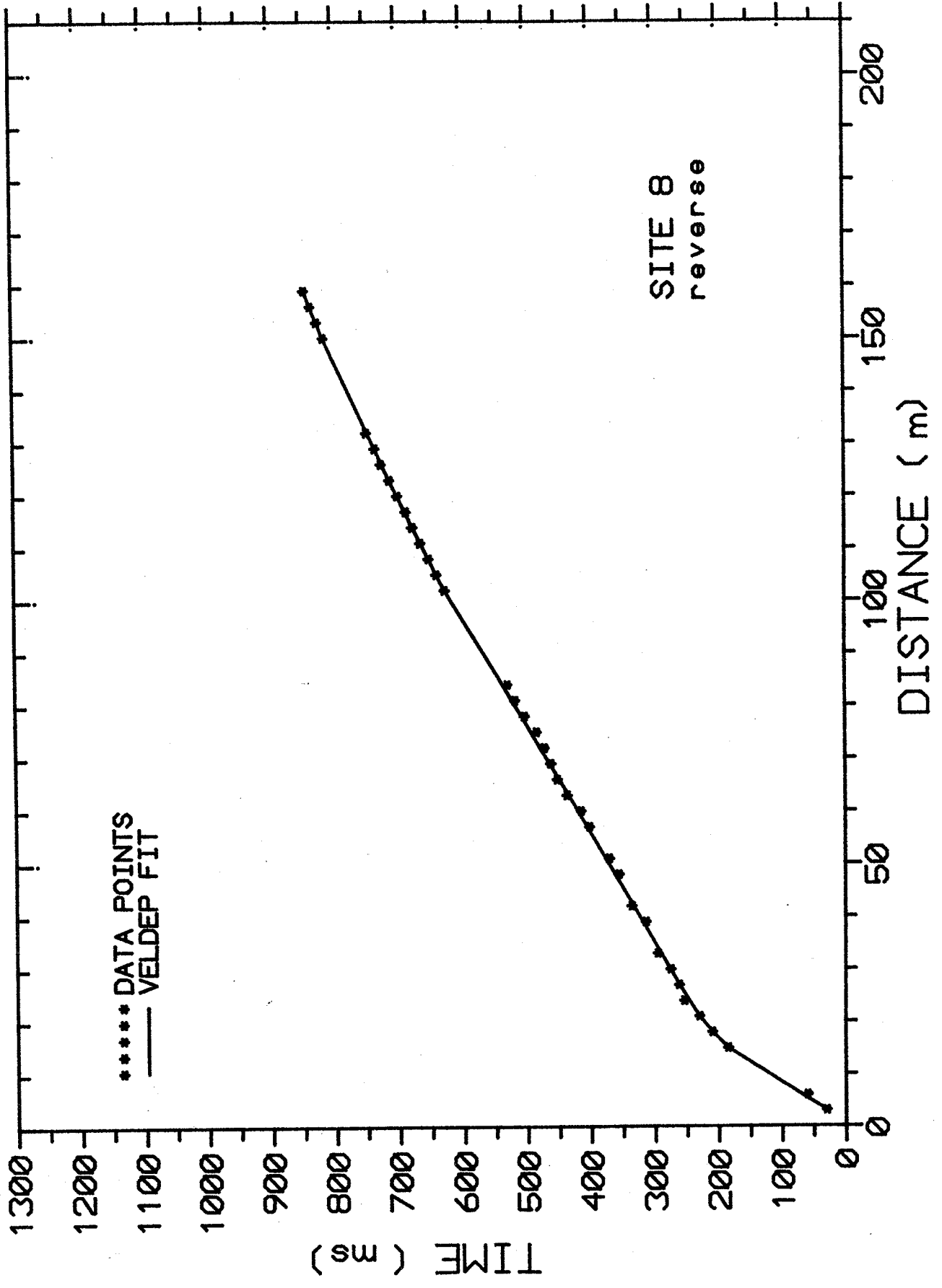
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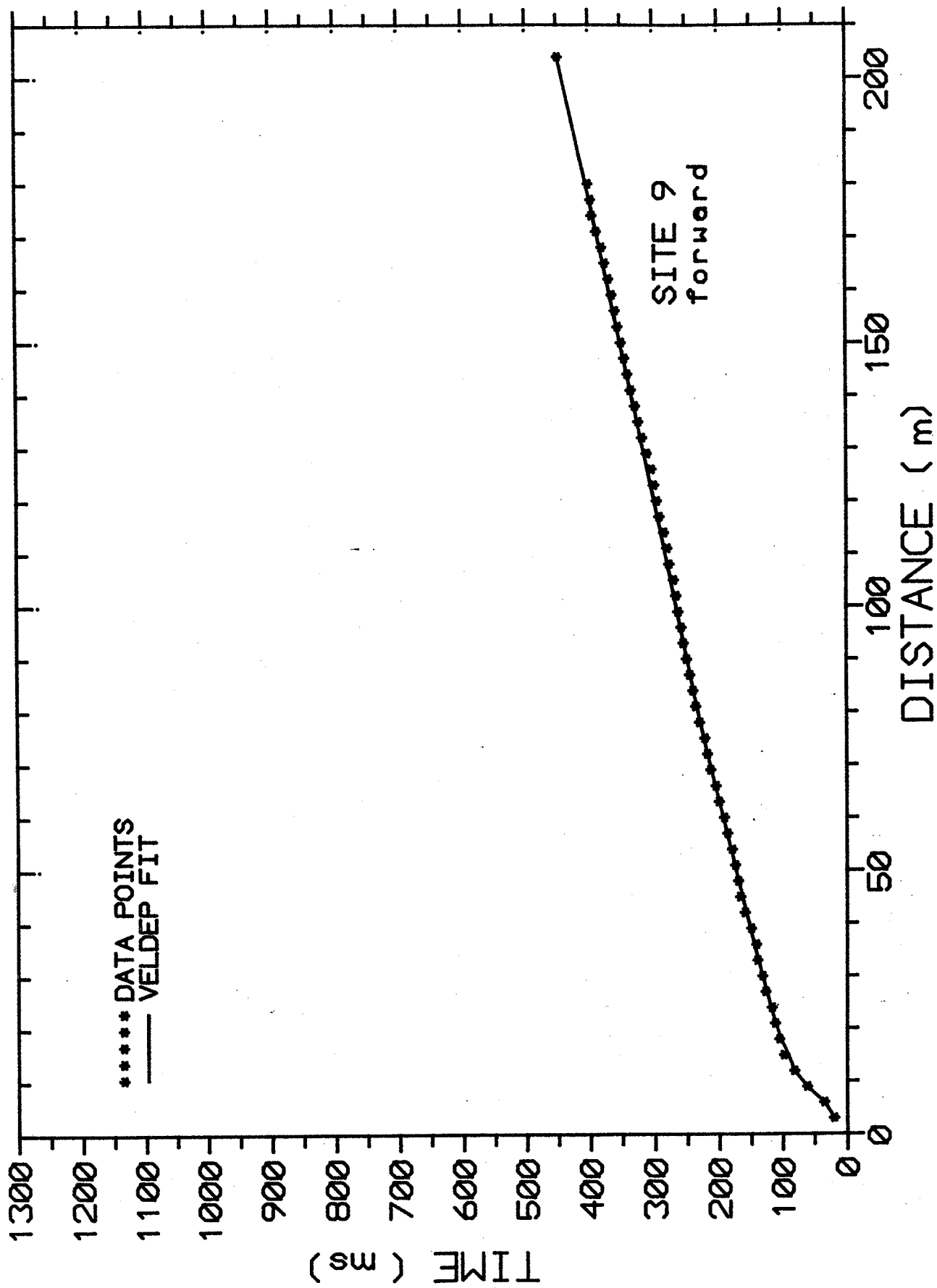


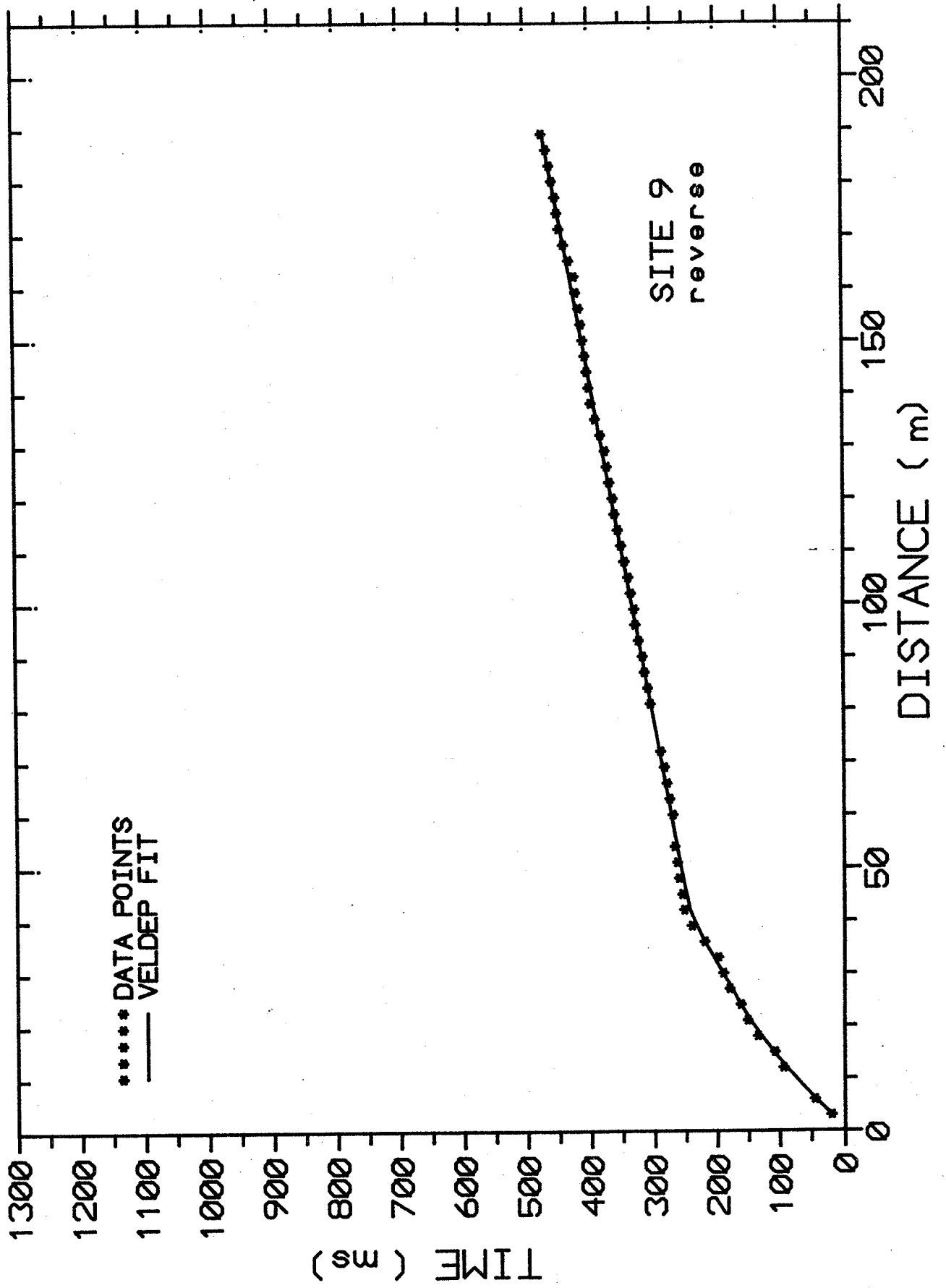
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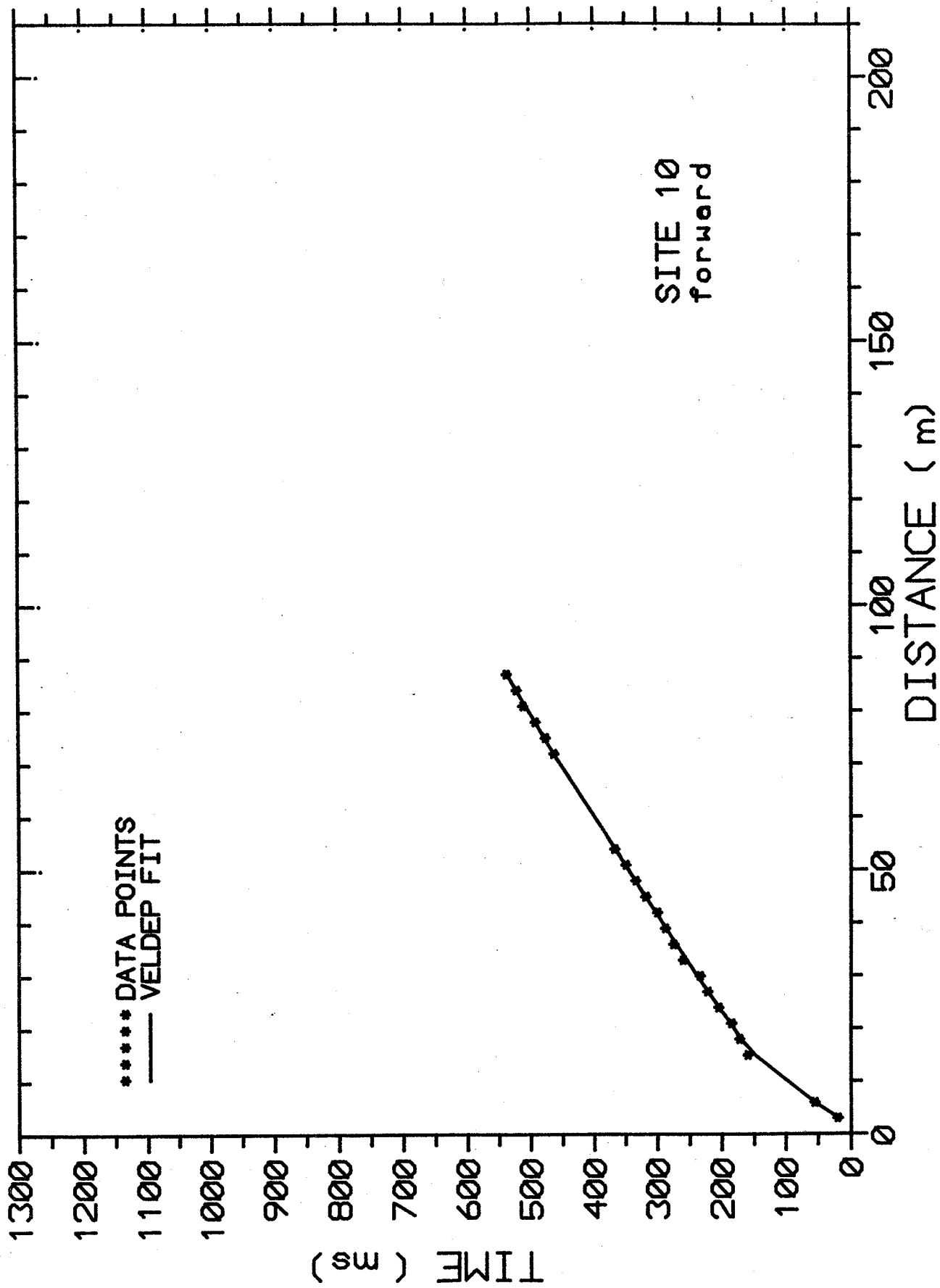


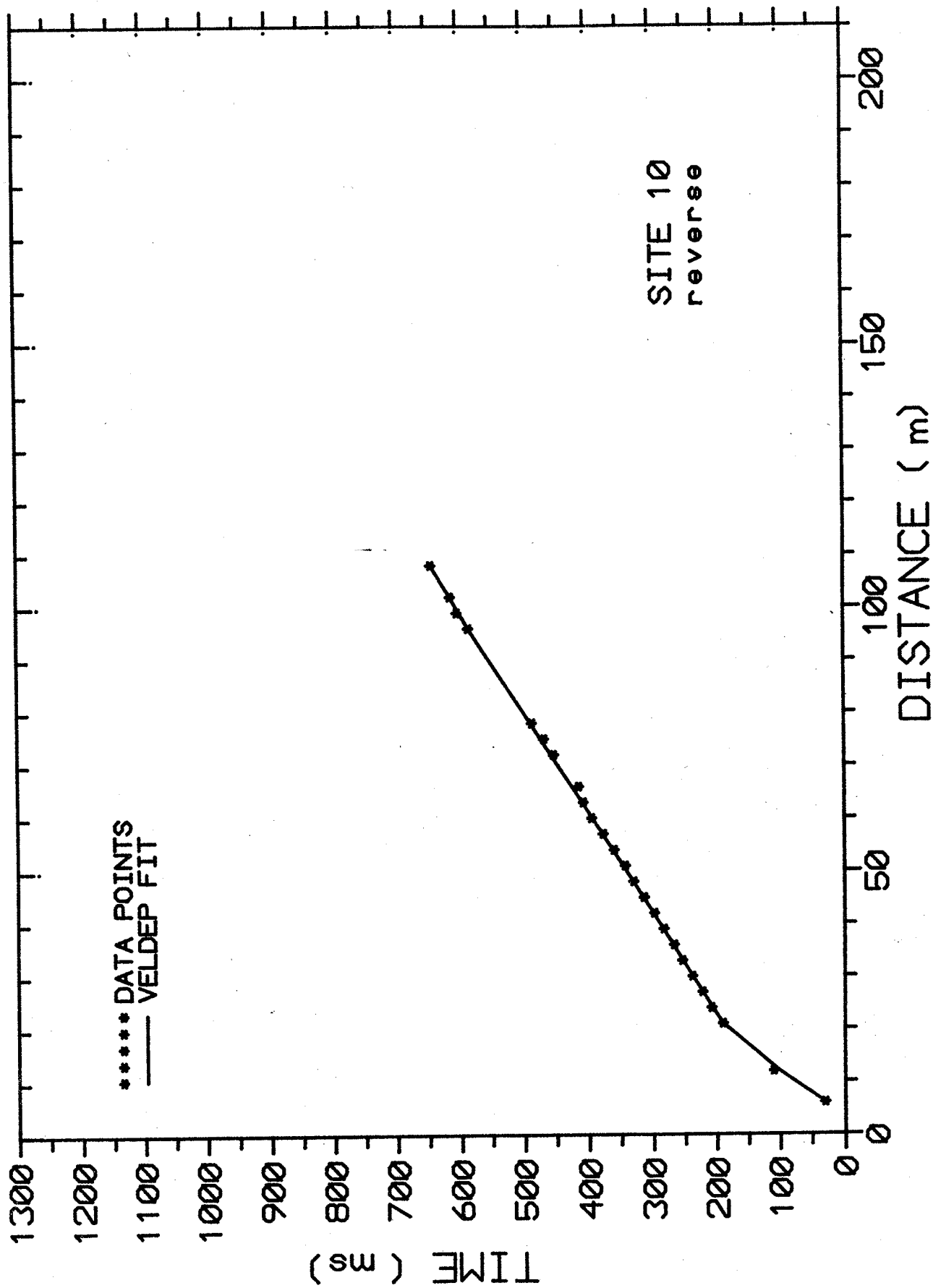


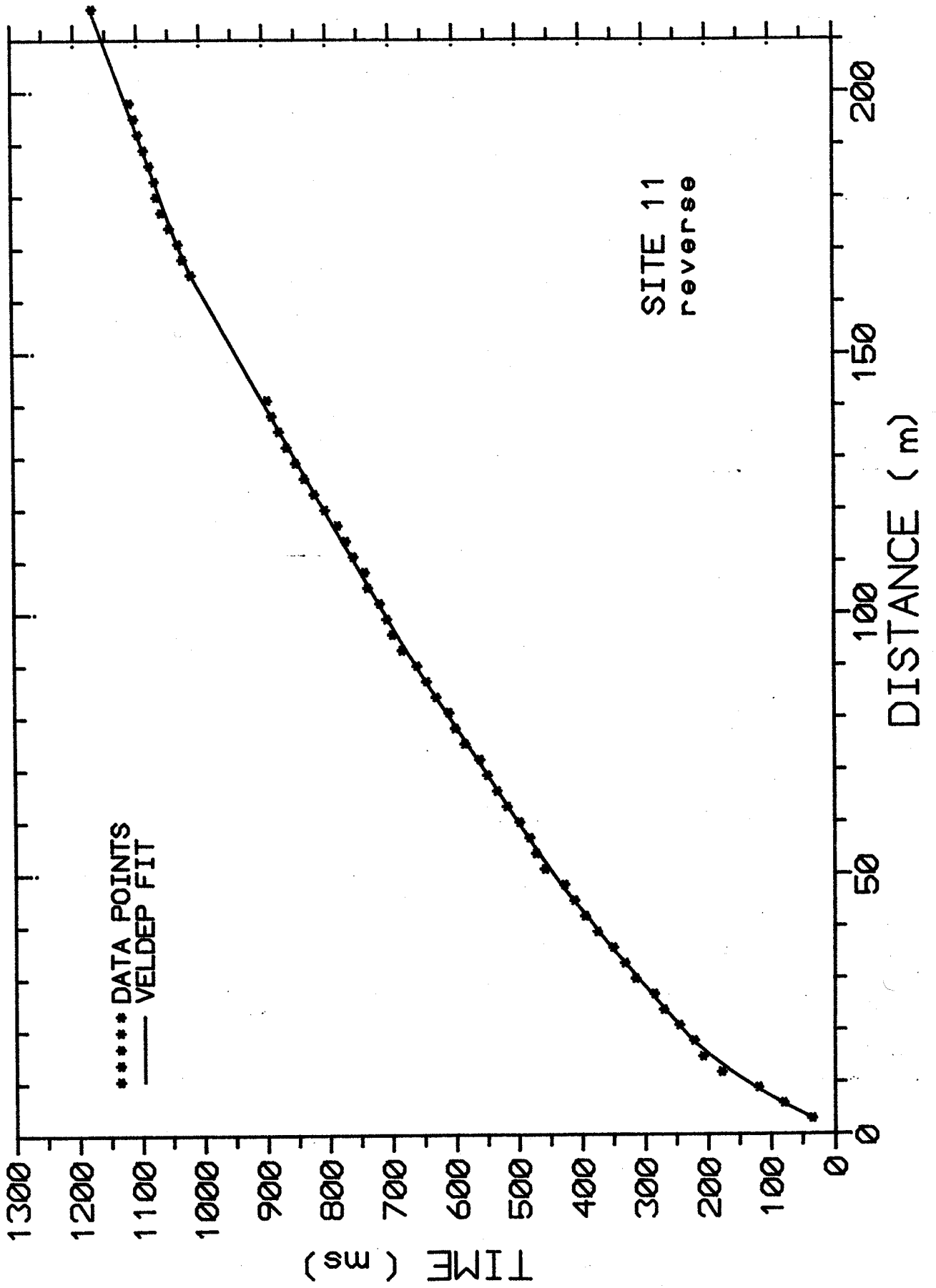


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SITE 9
reverse





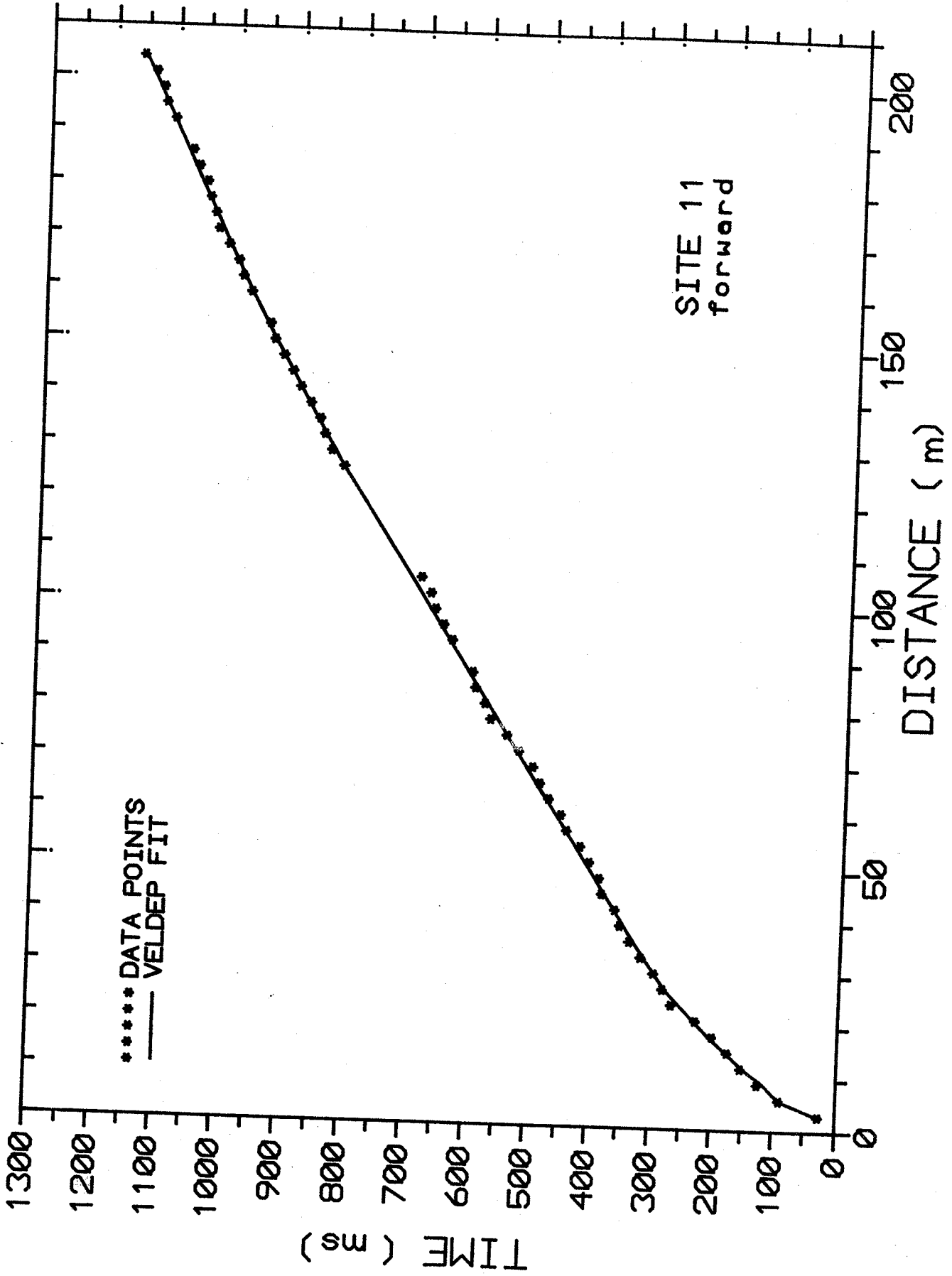


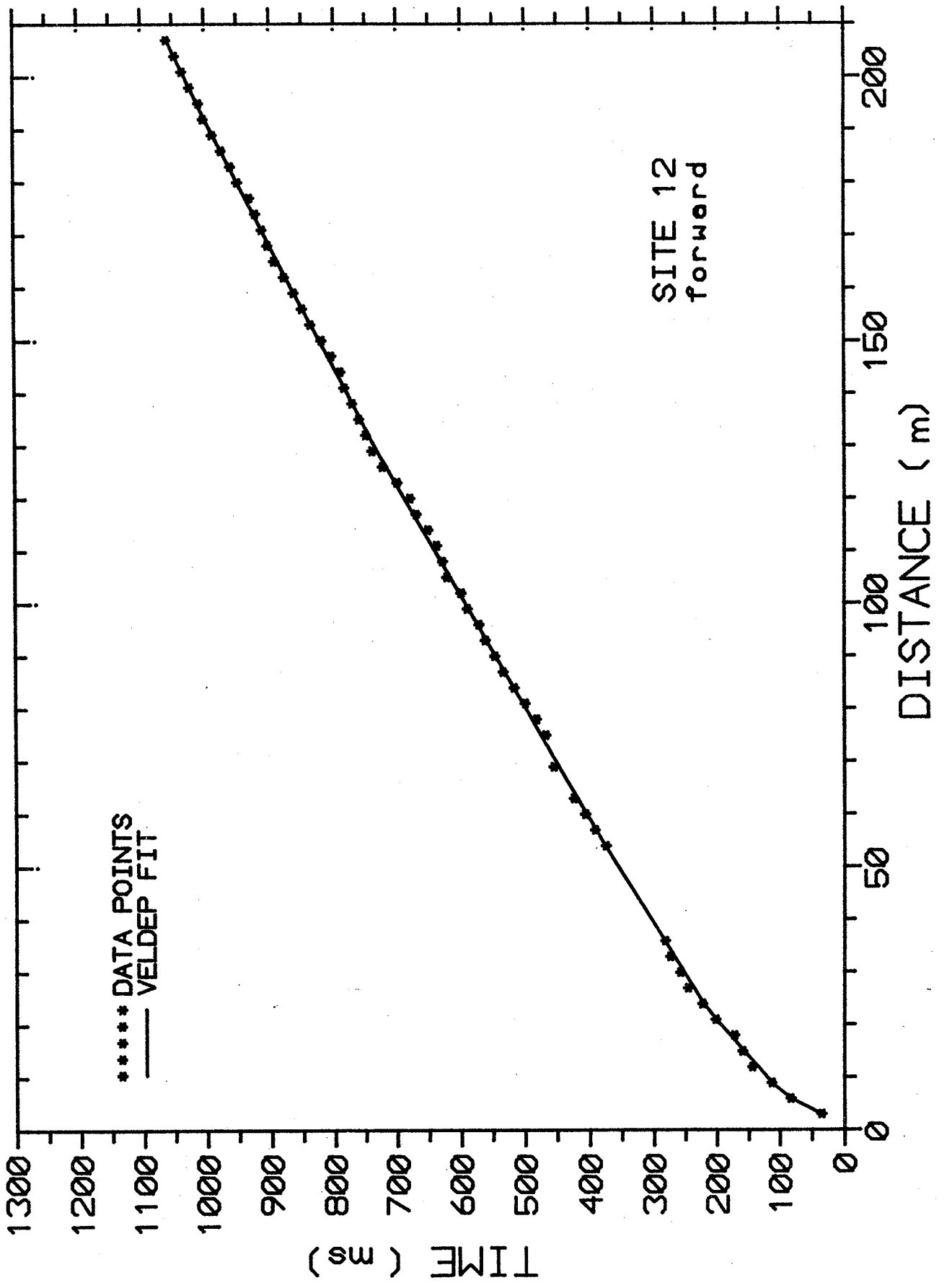
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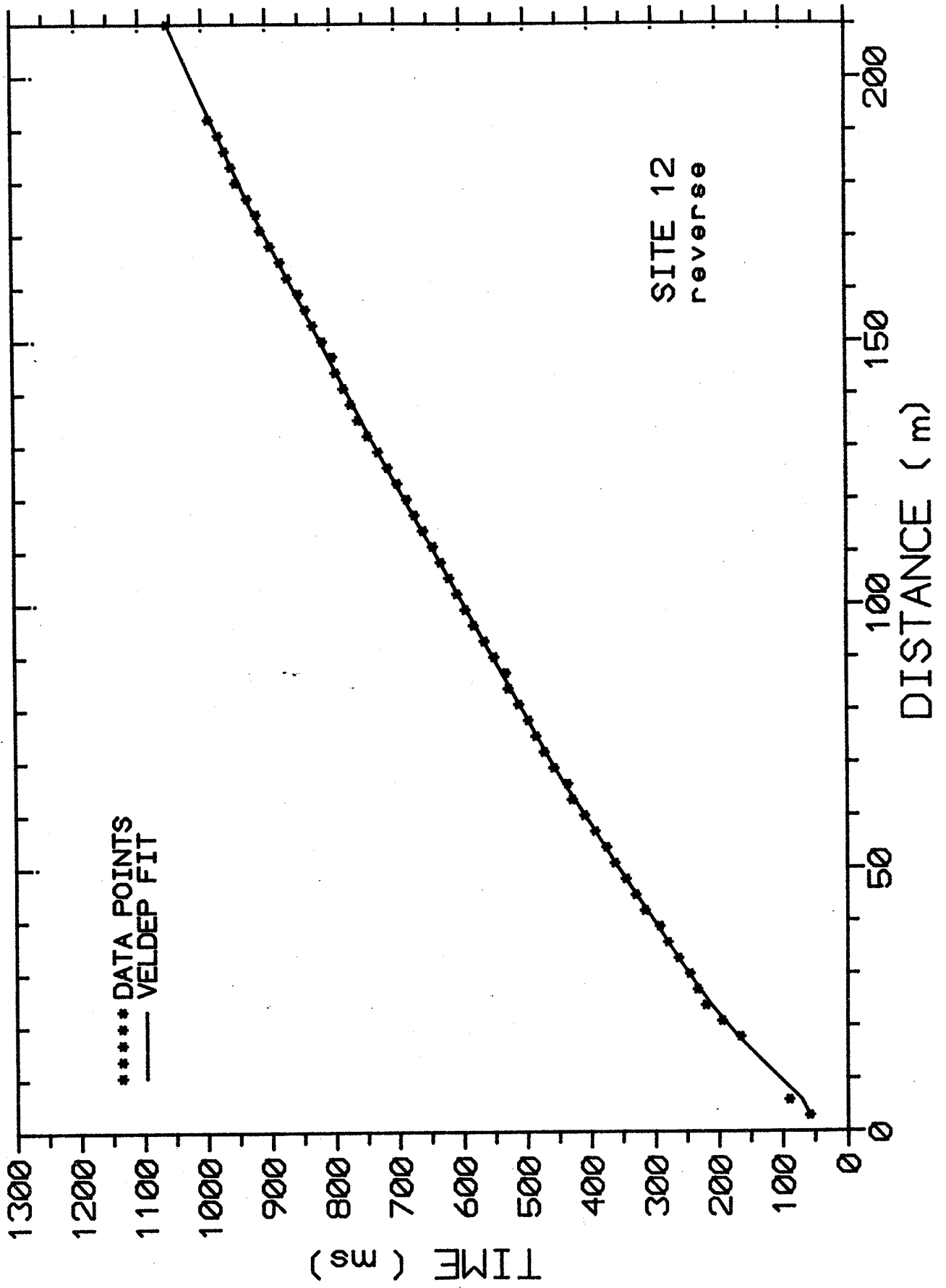
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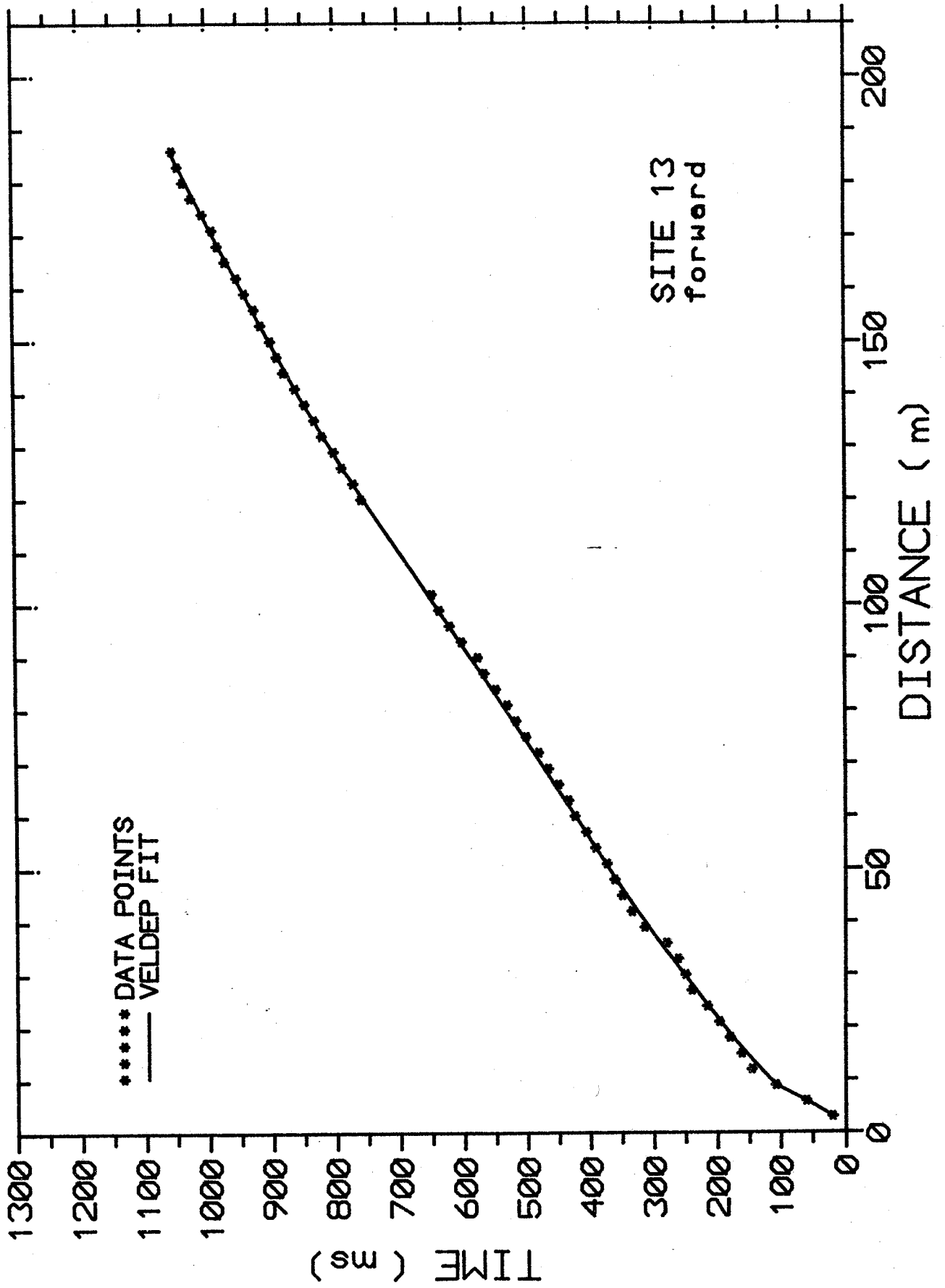
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DISTANCE (m)



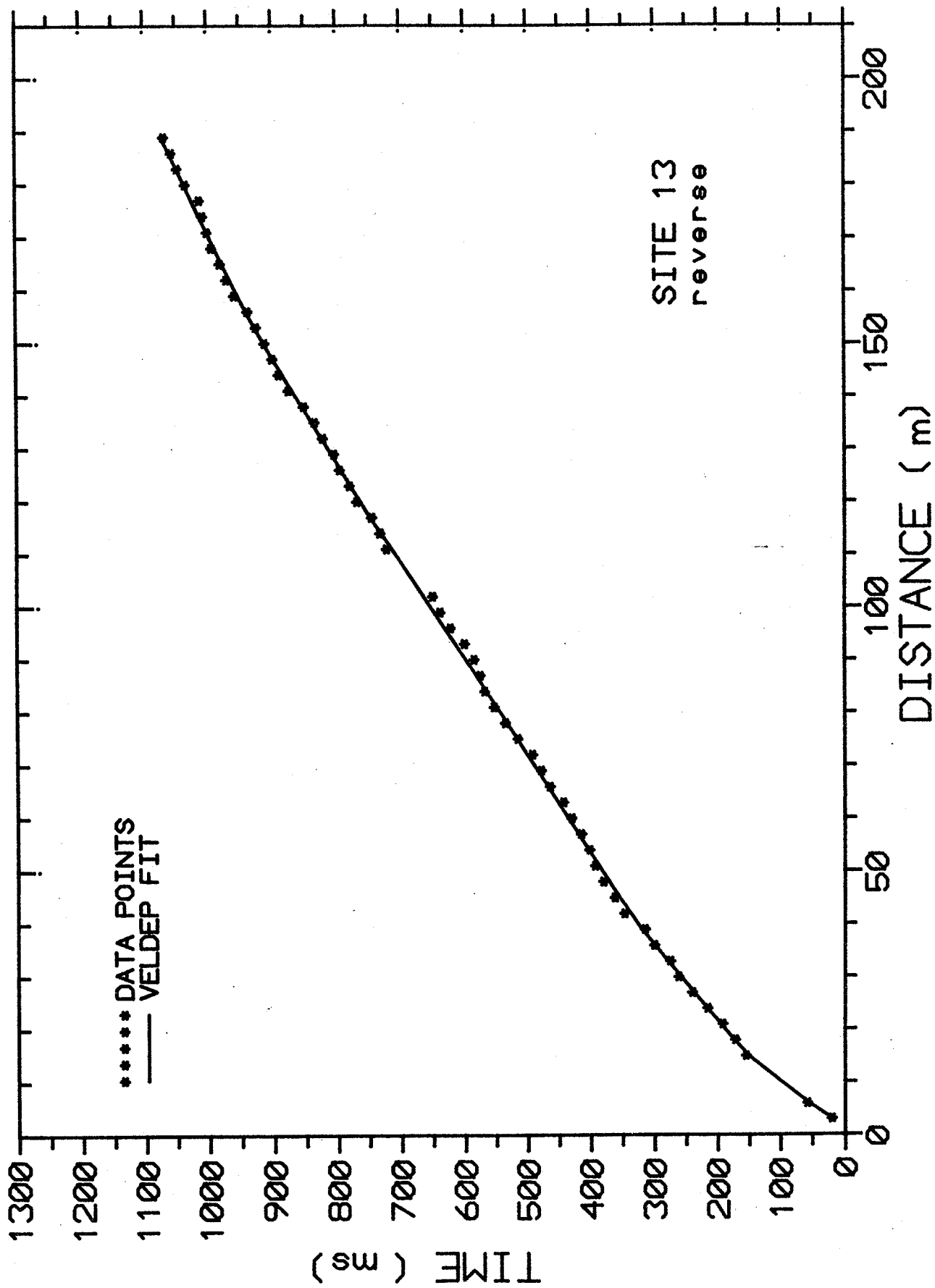


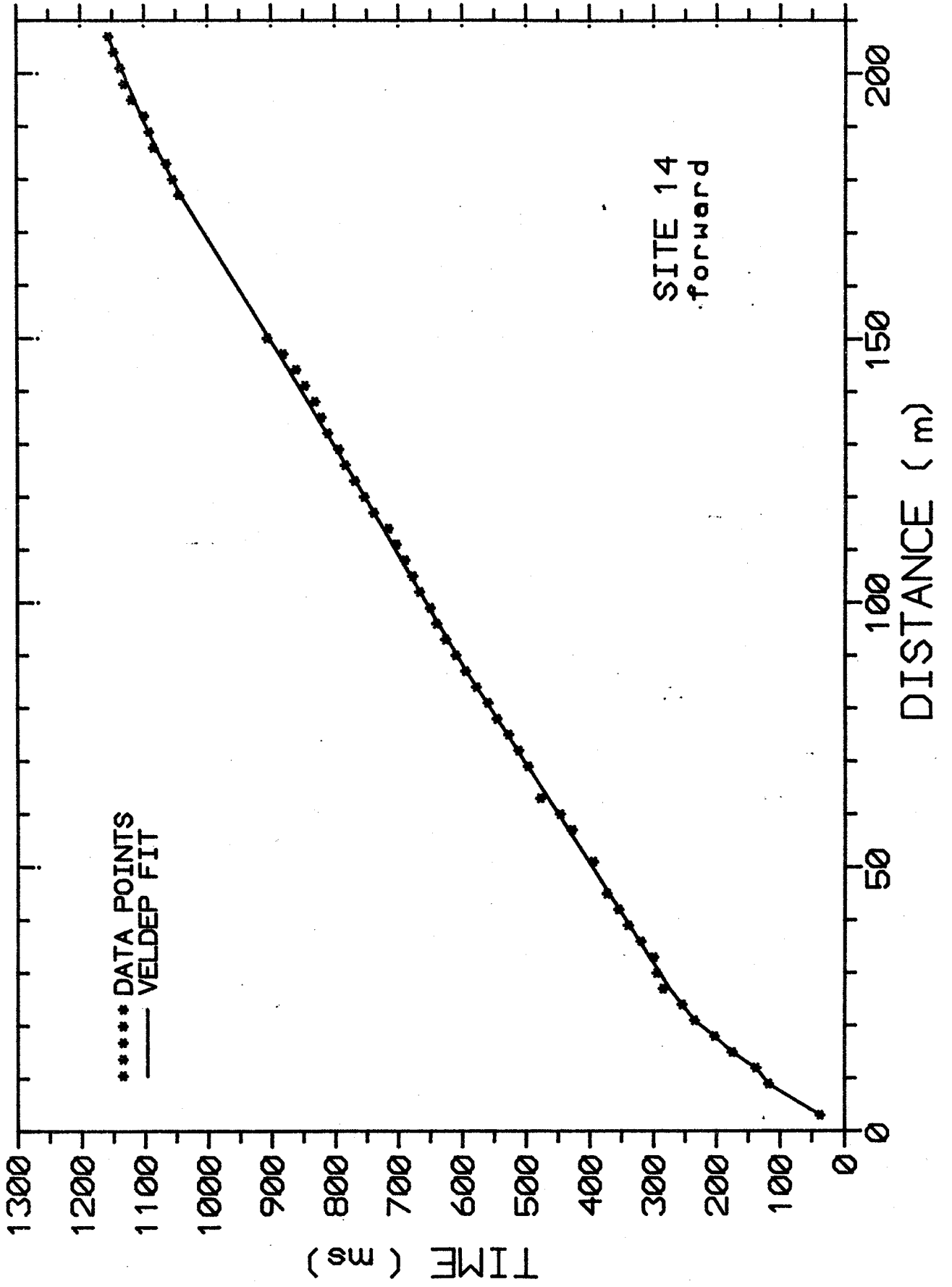


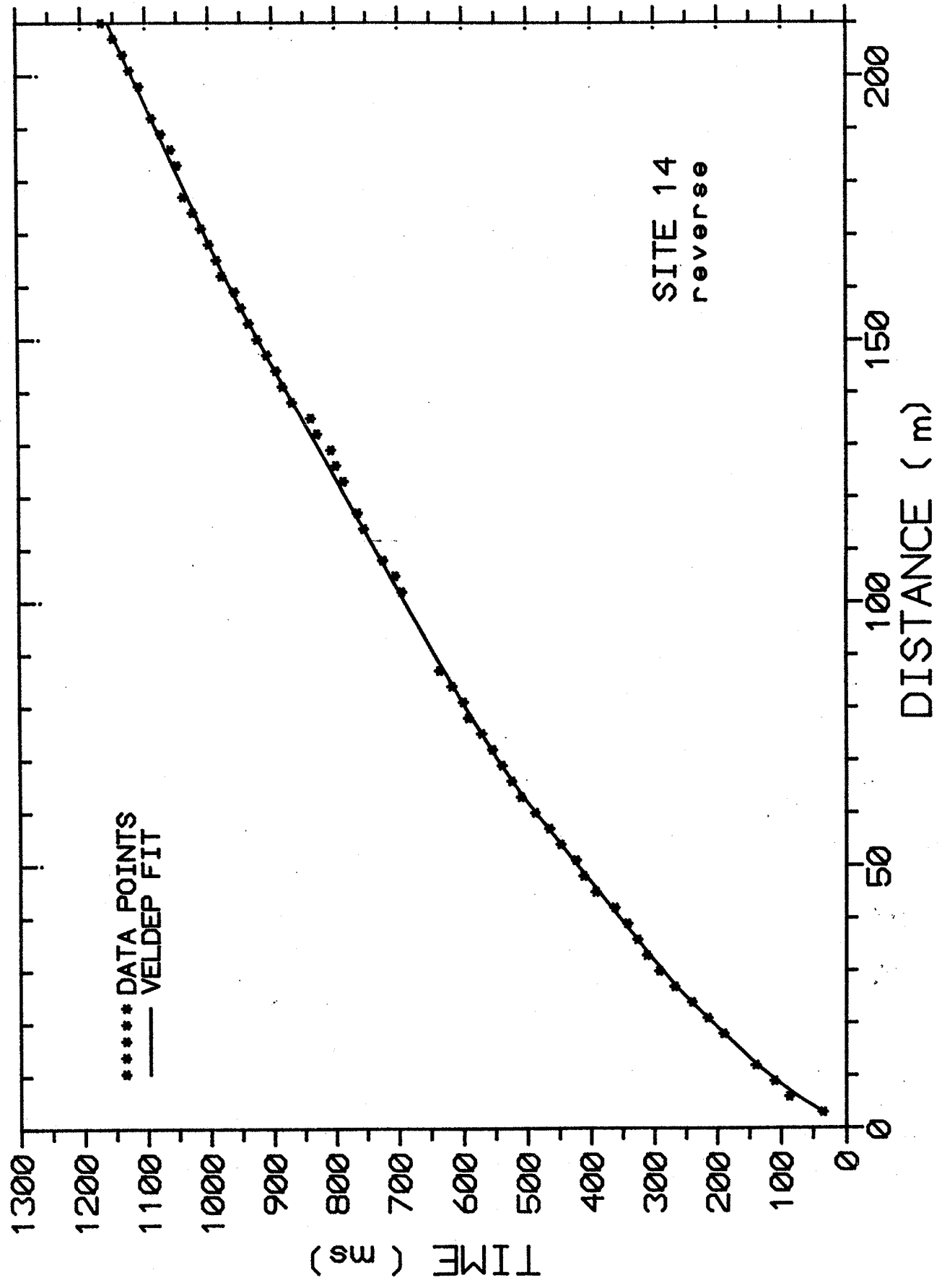


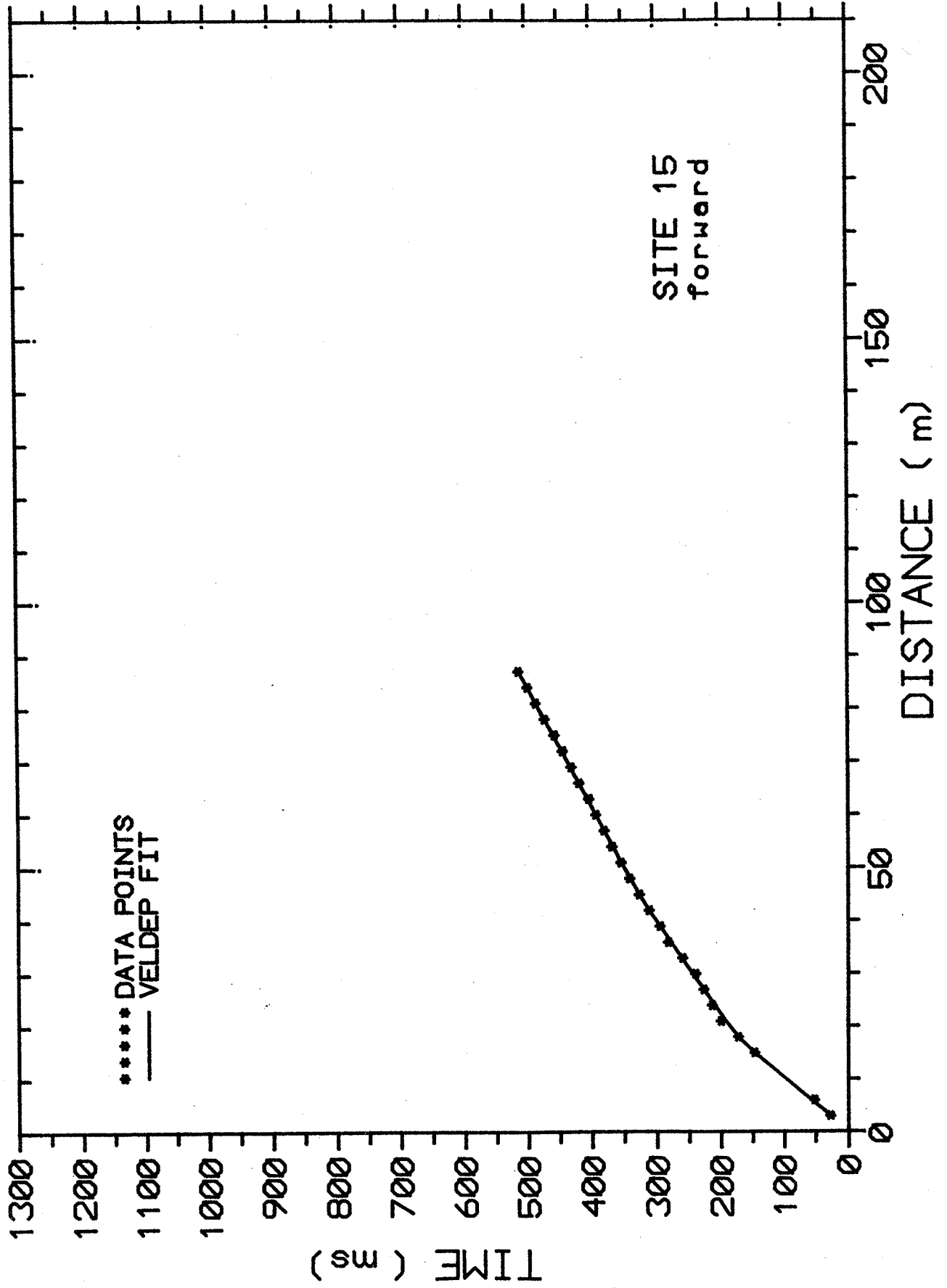
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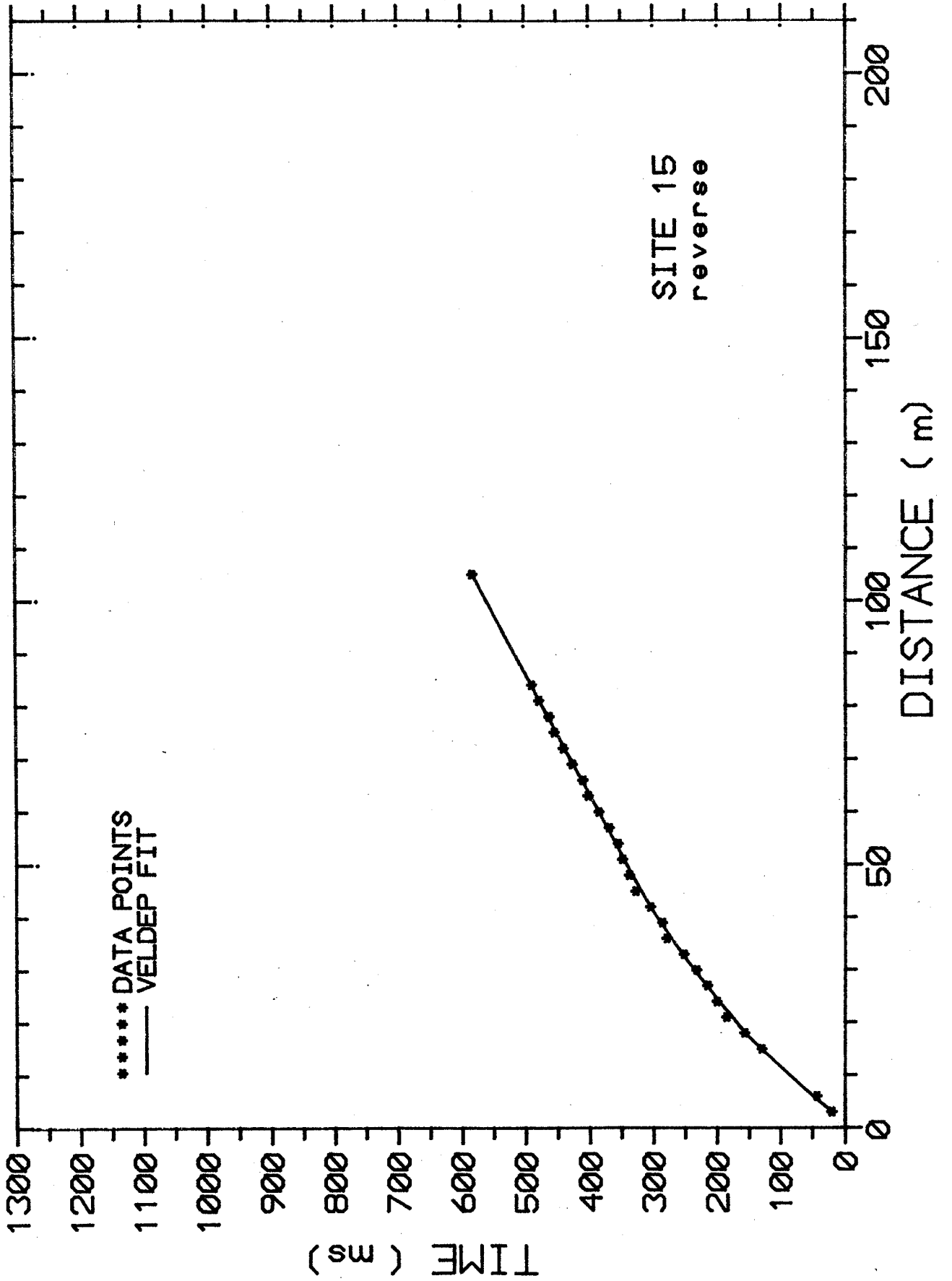
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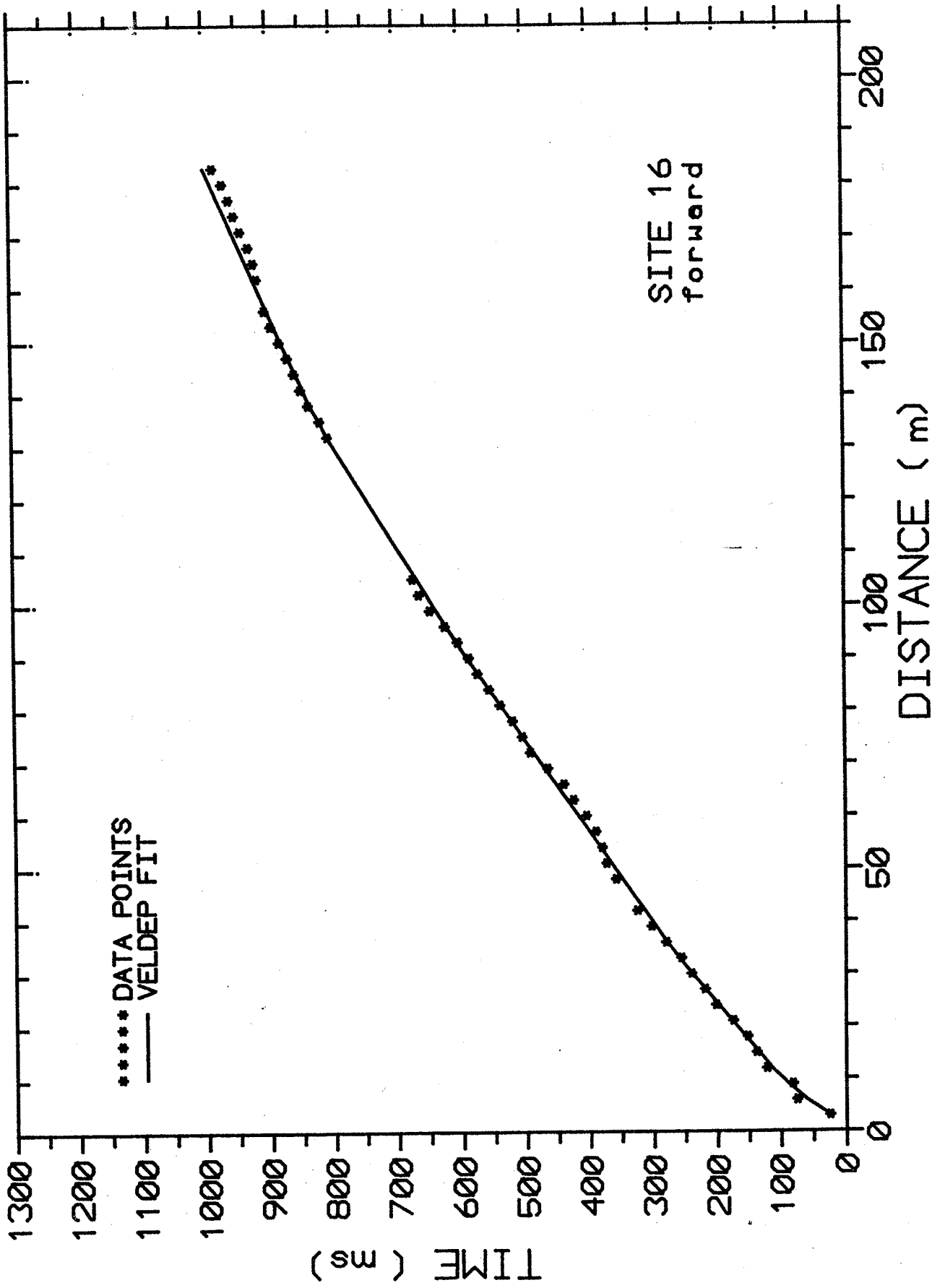


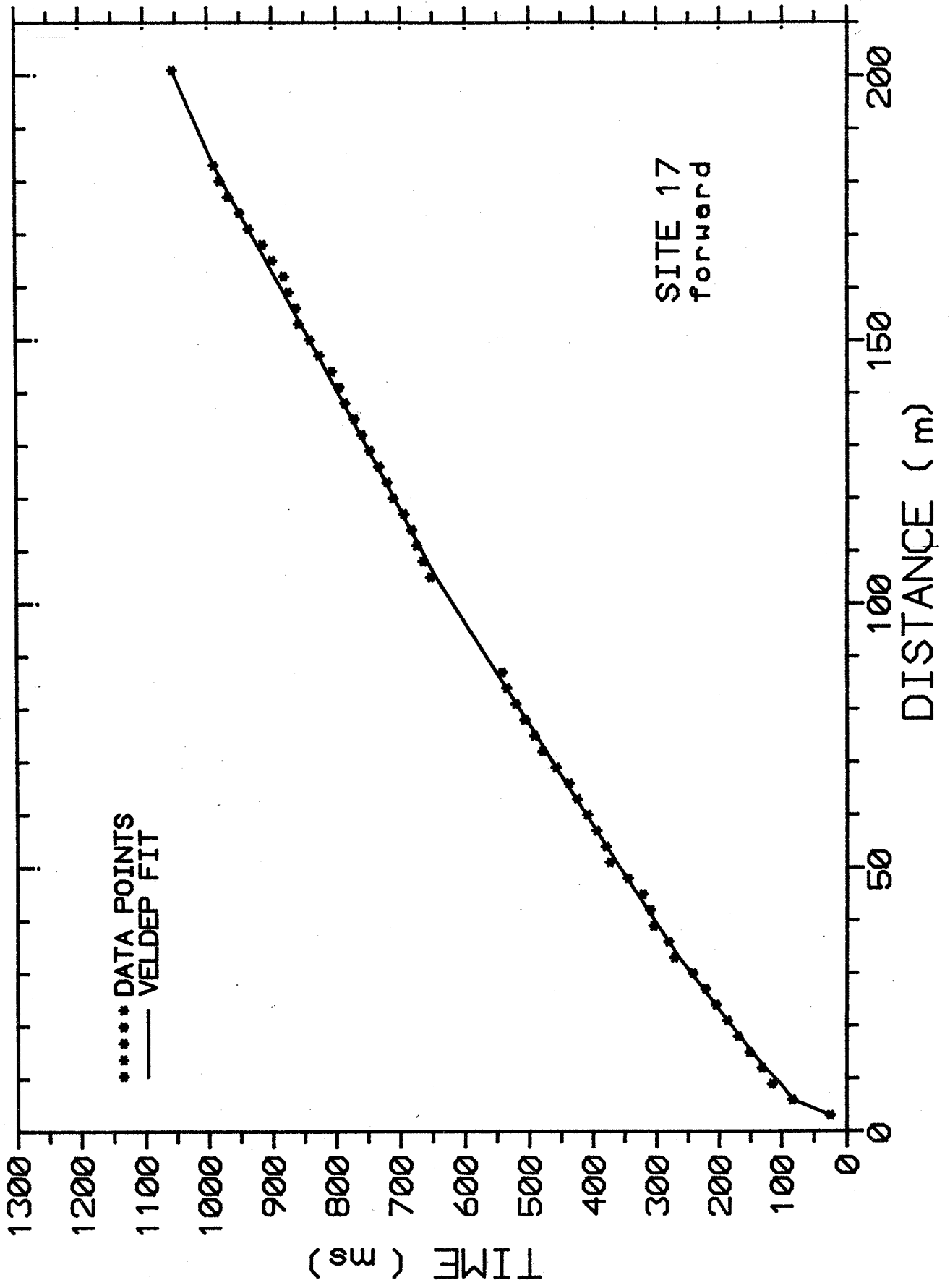


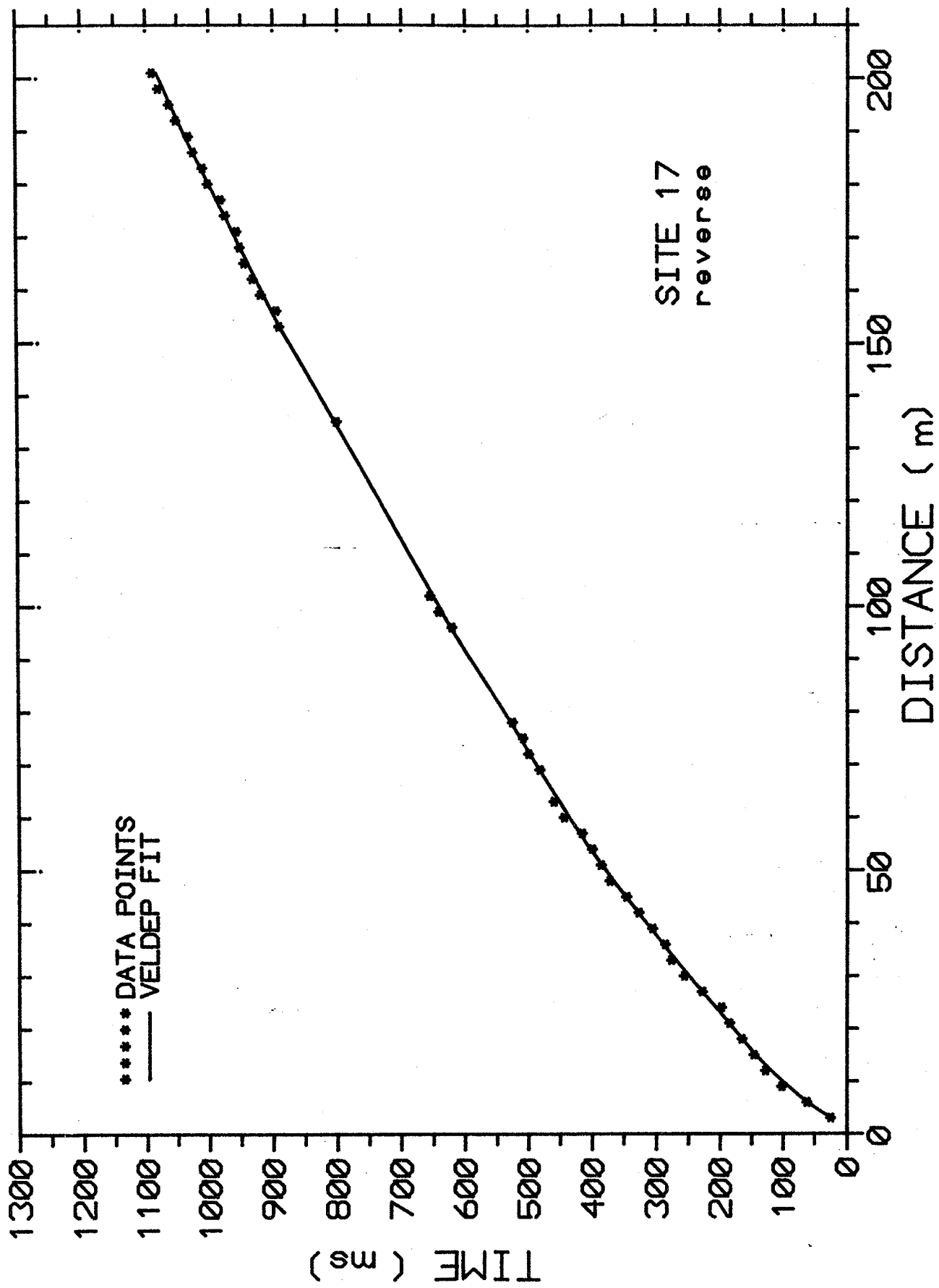


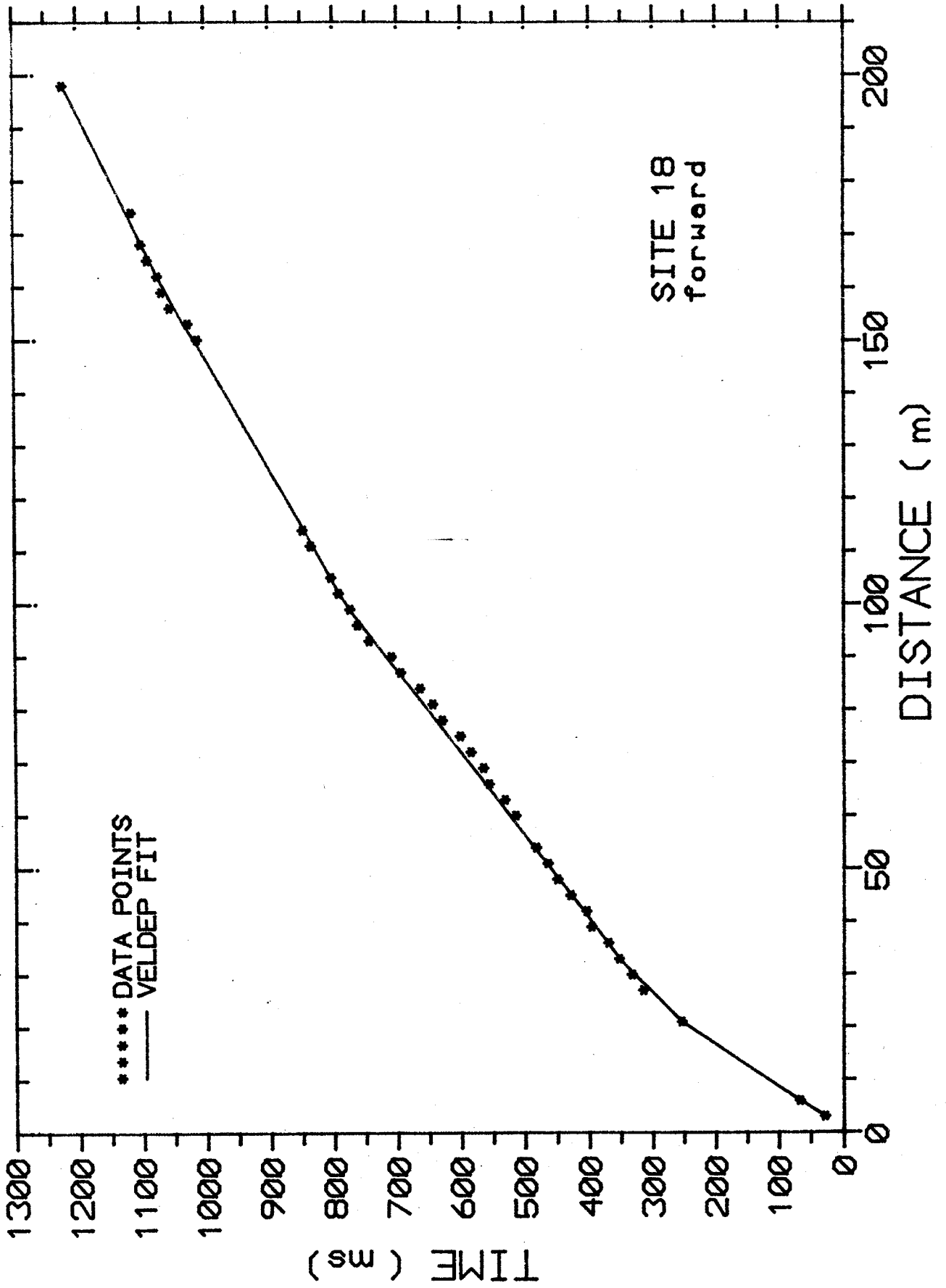


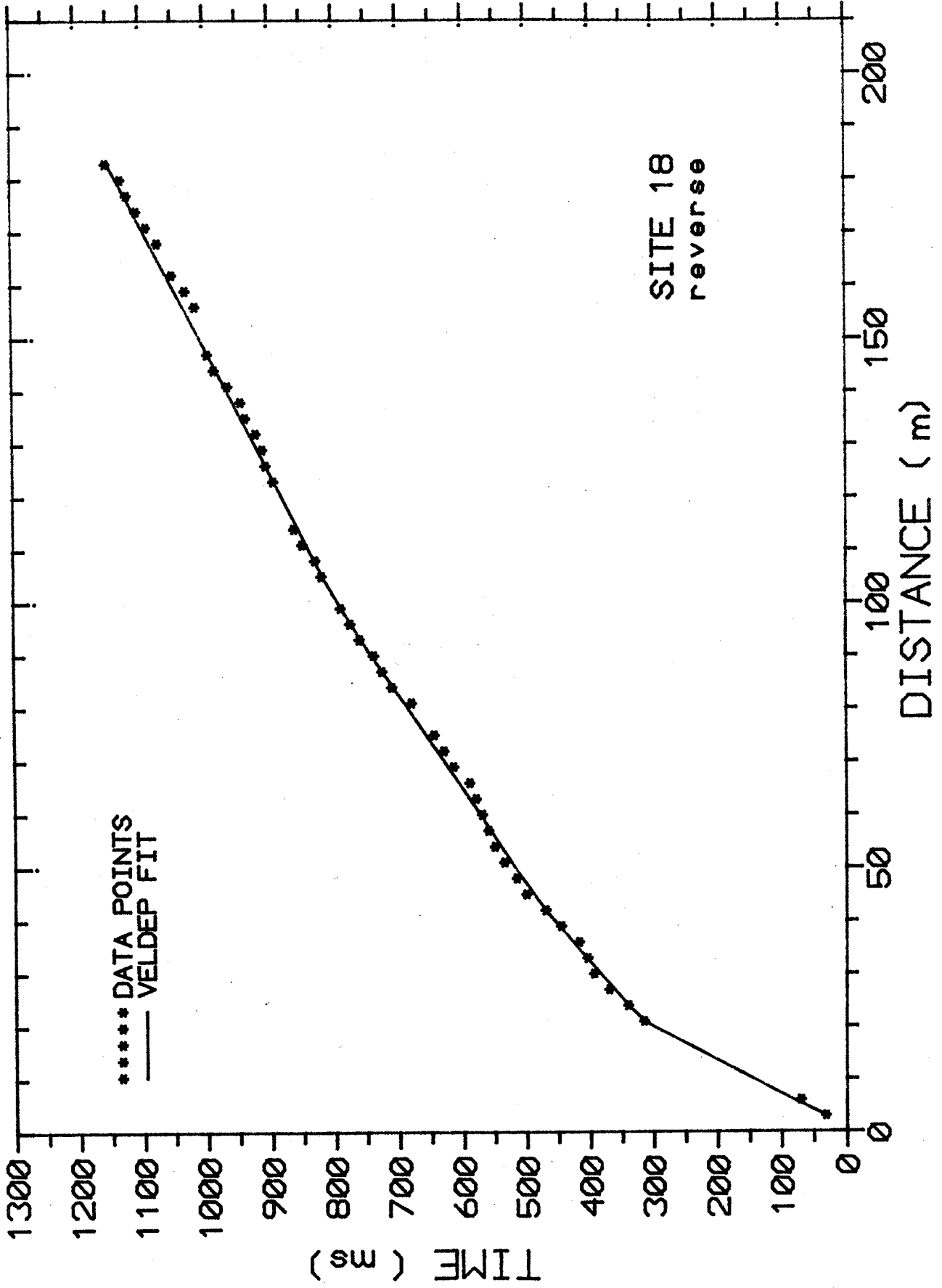










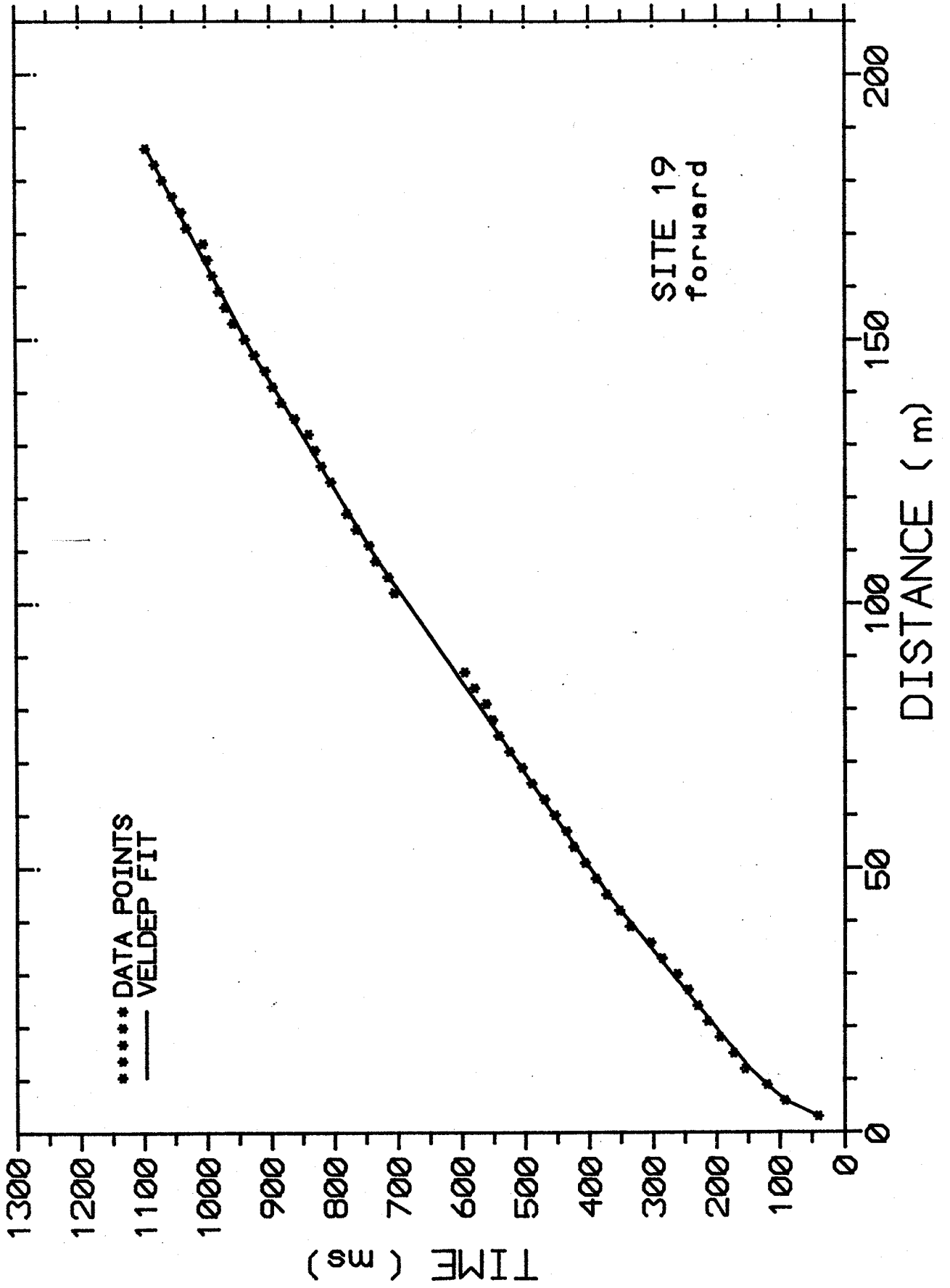


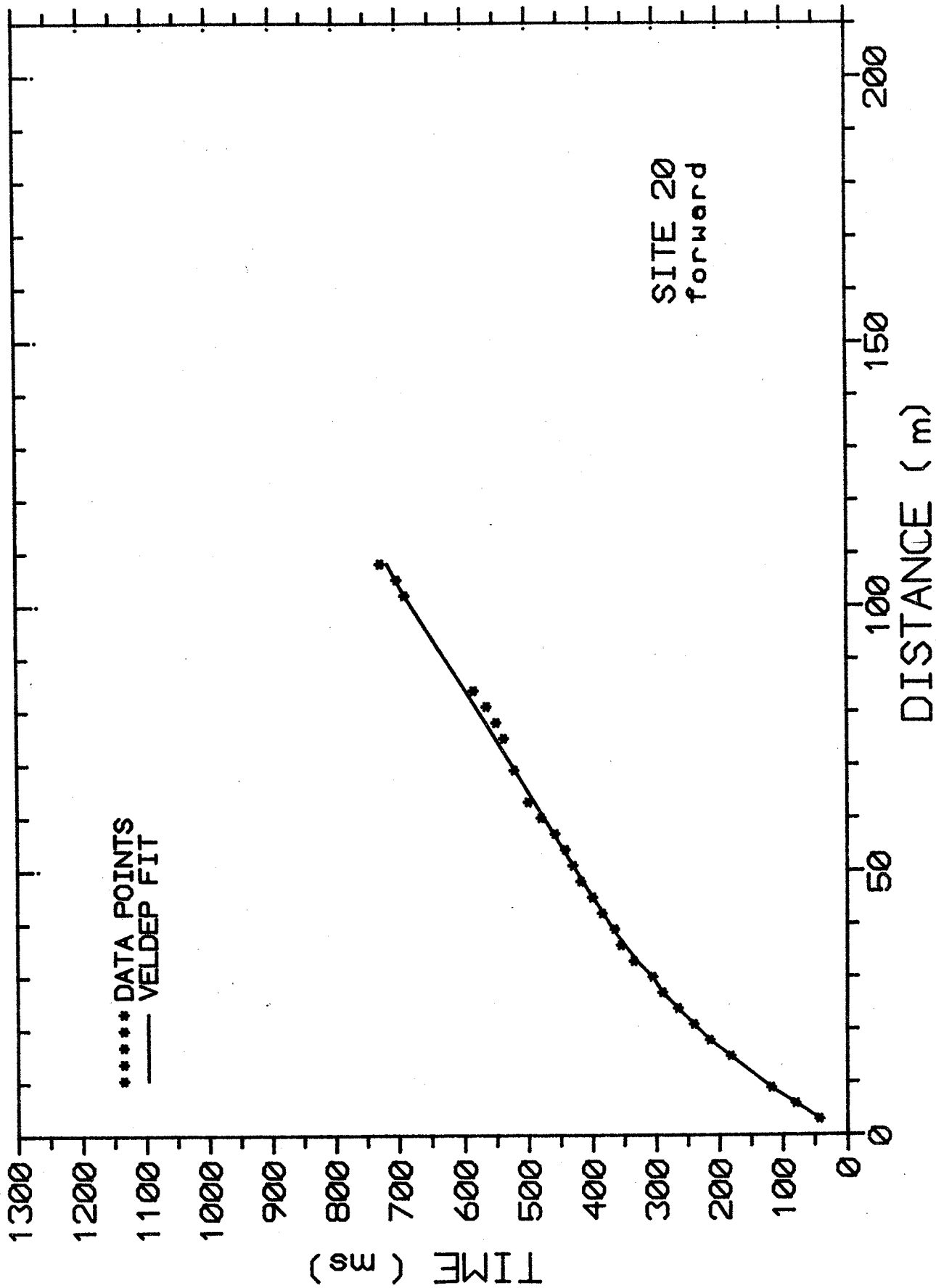
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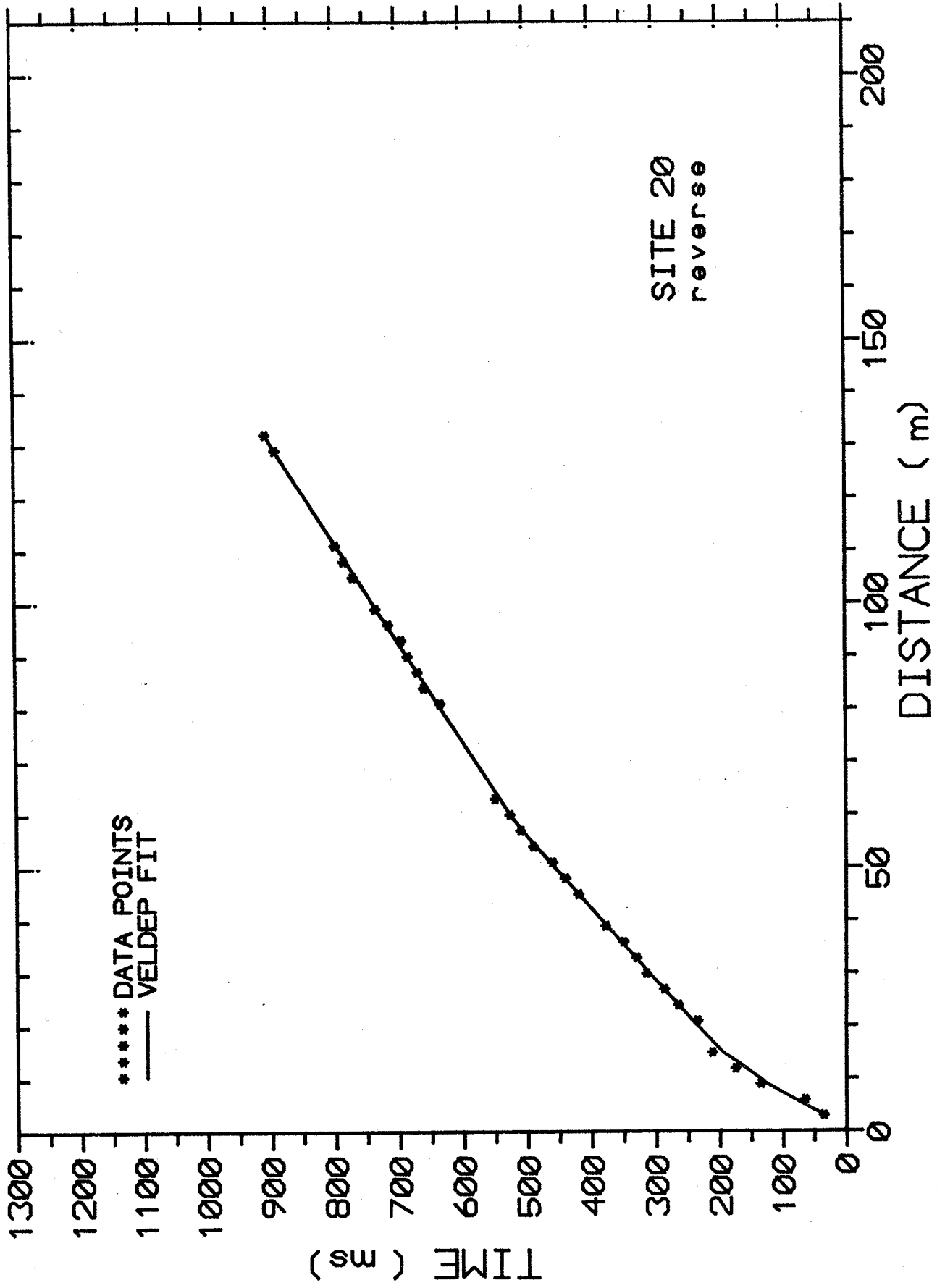
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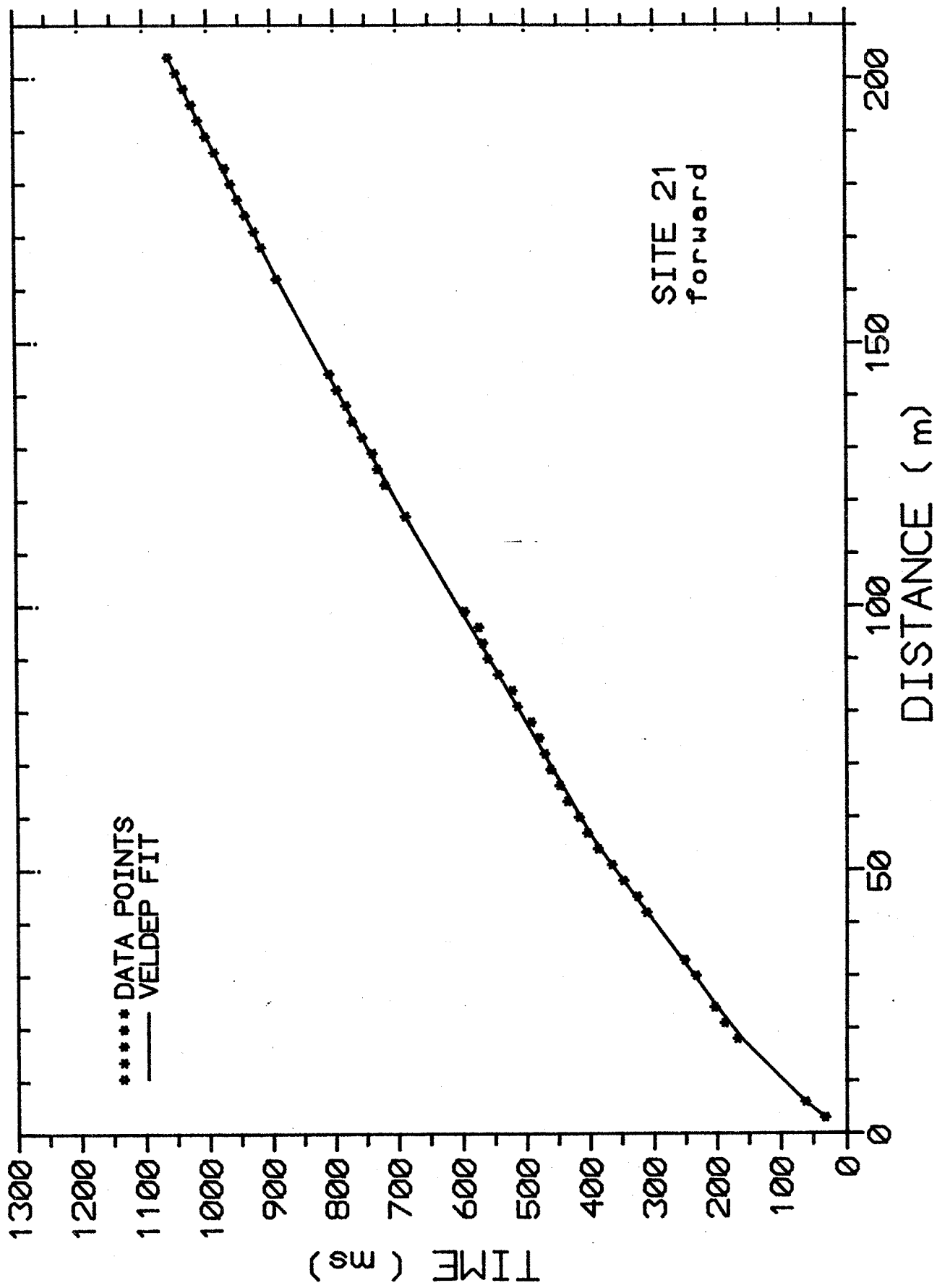
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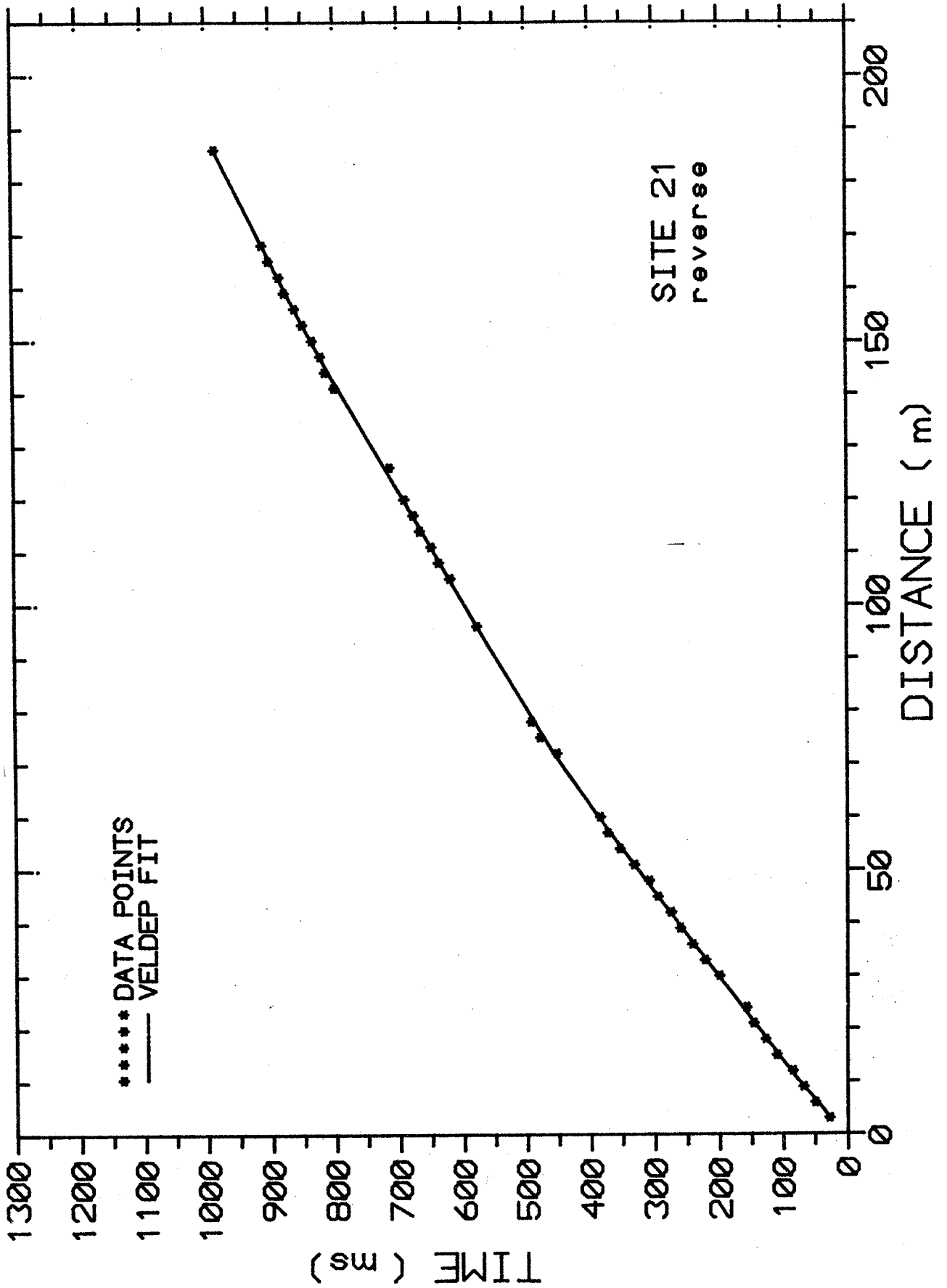
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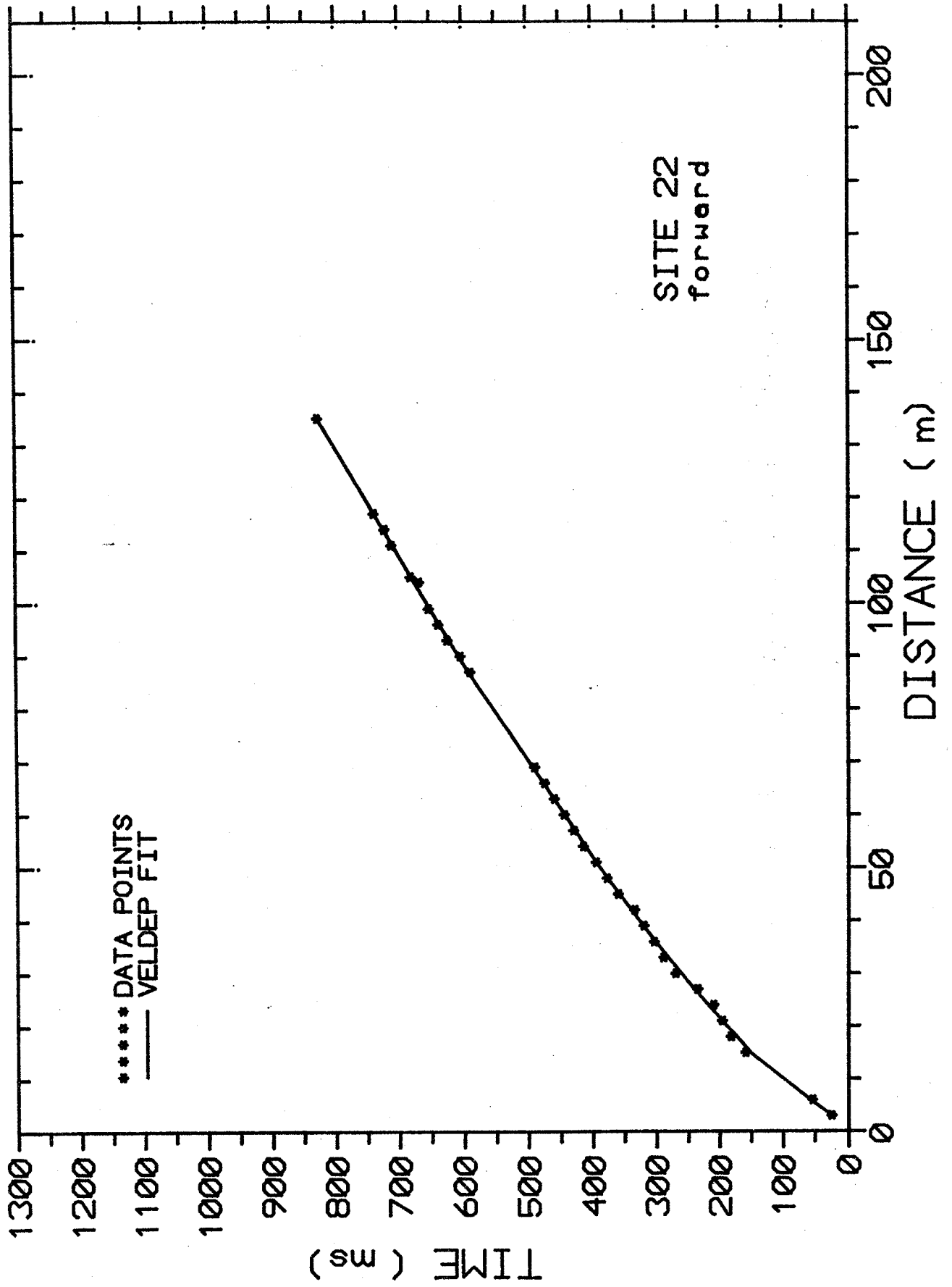


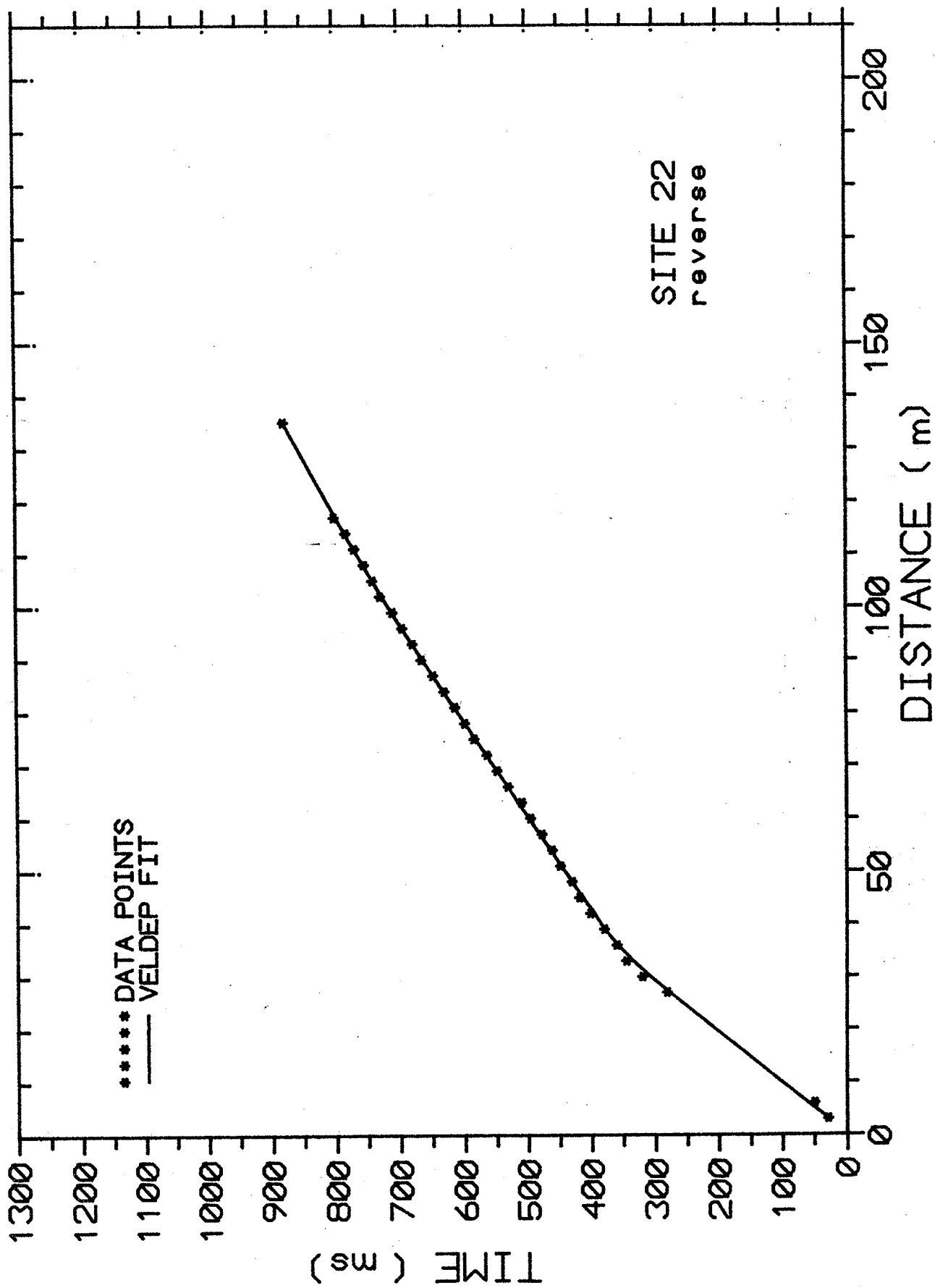


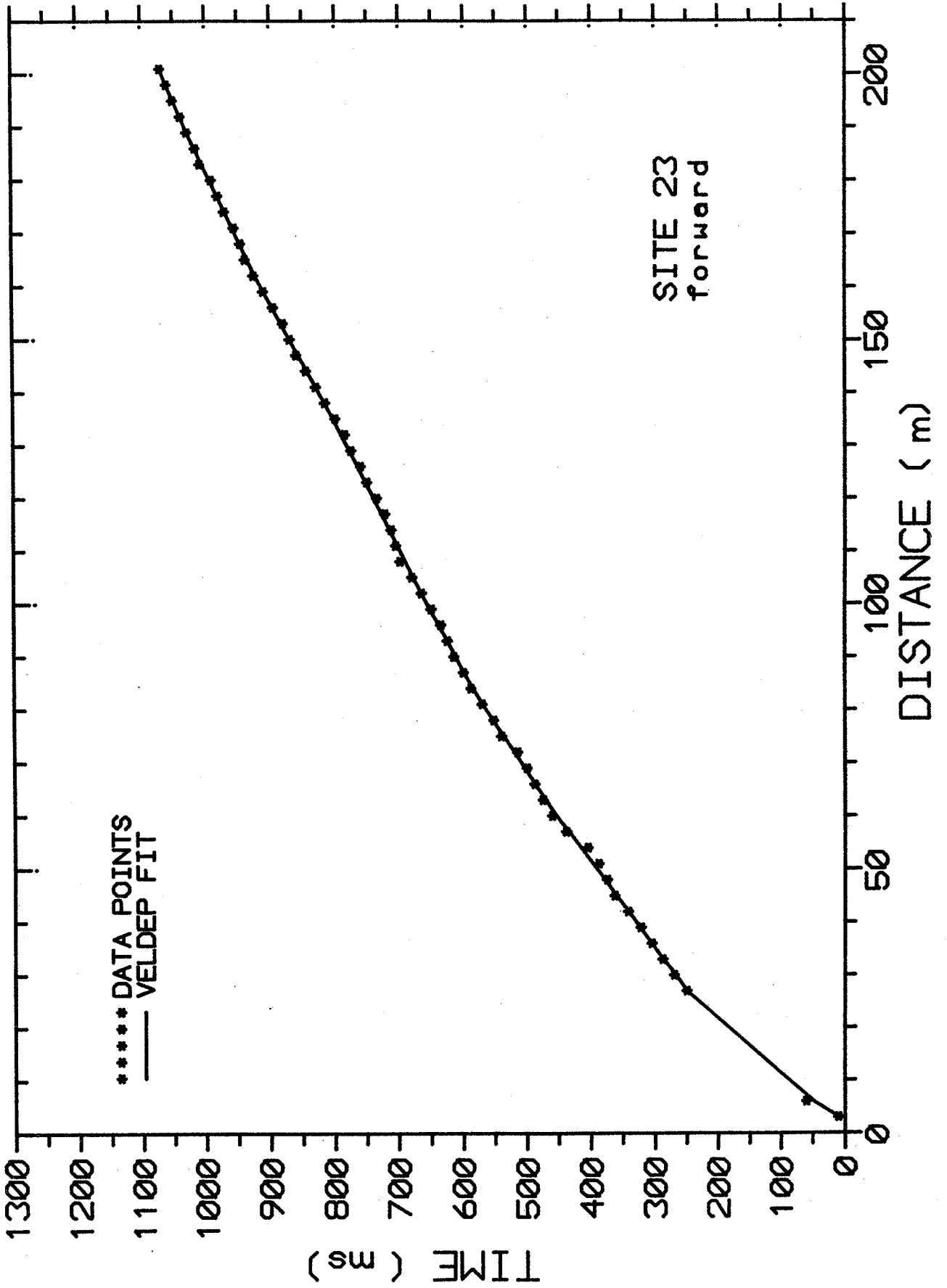


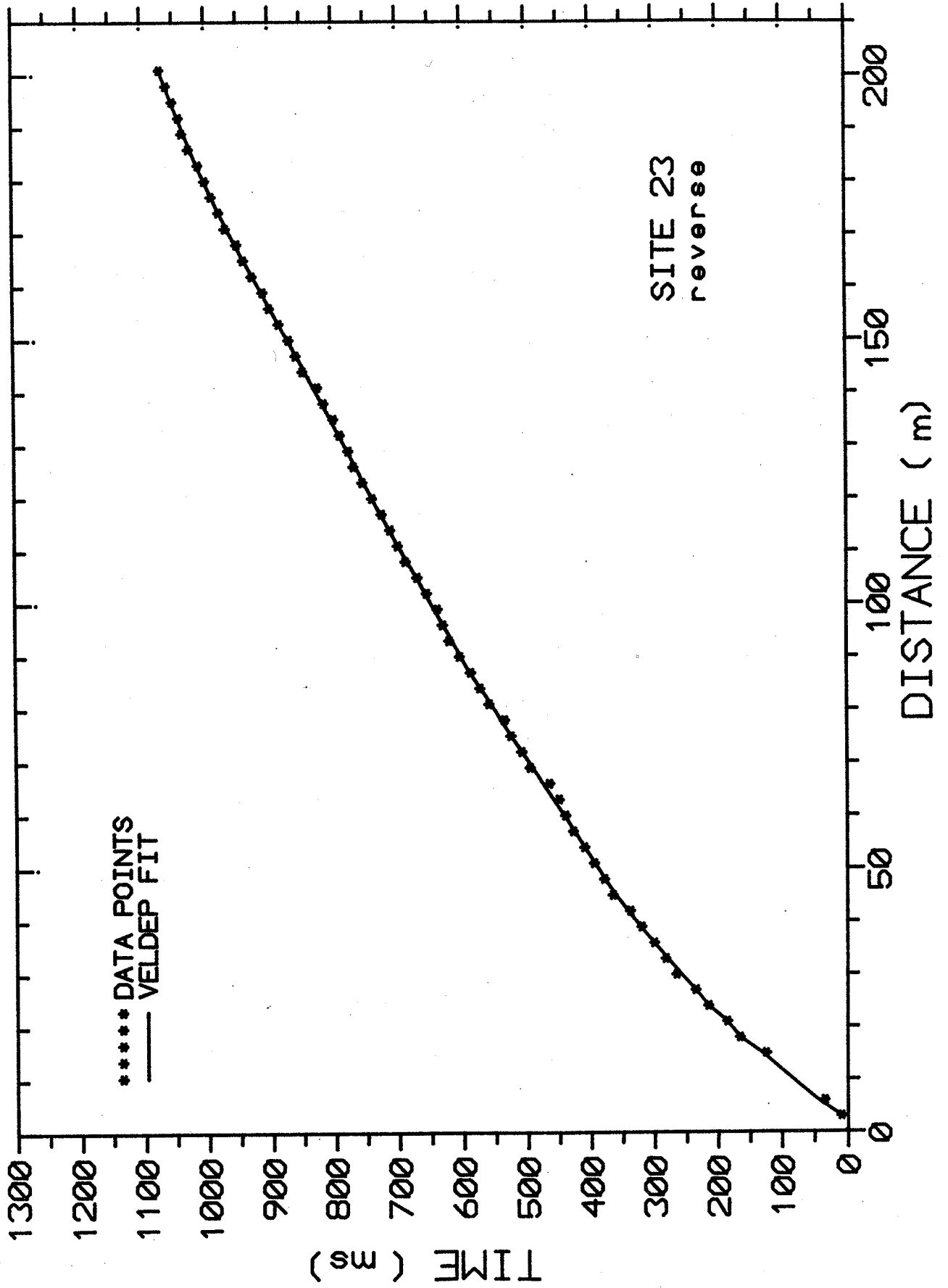


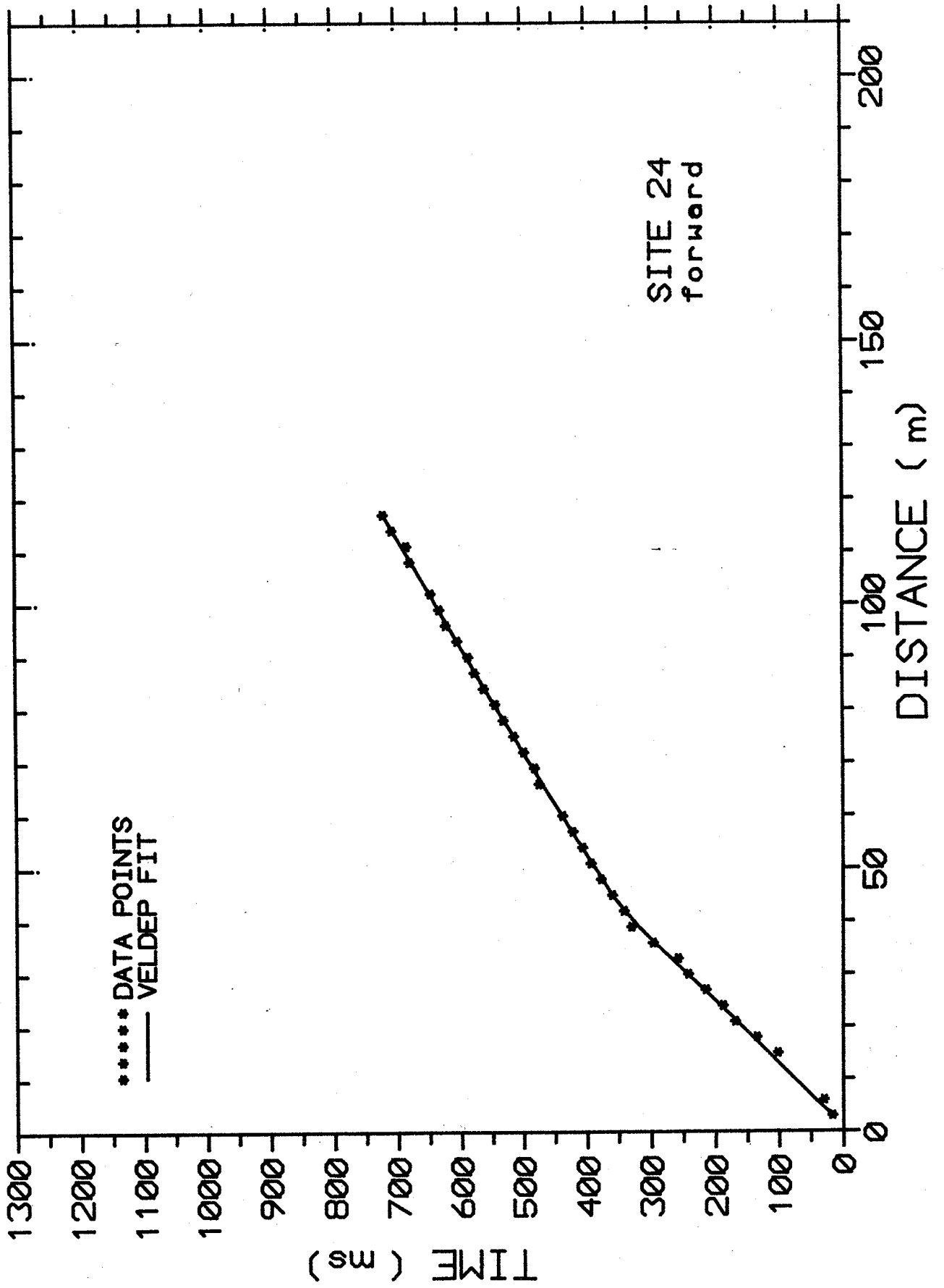






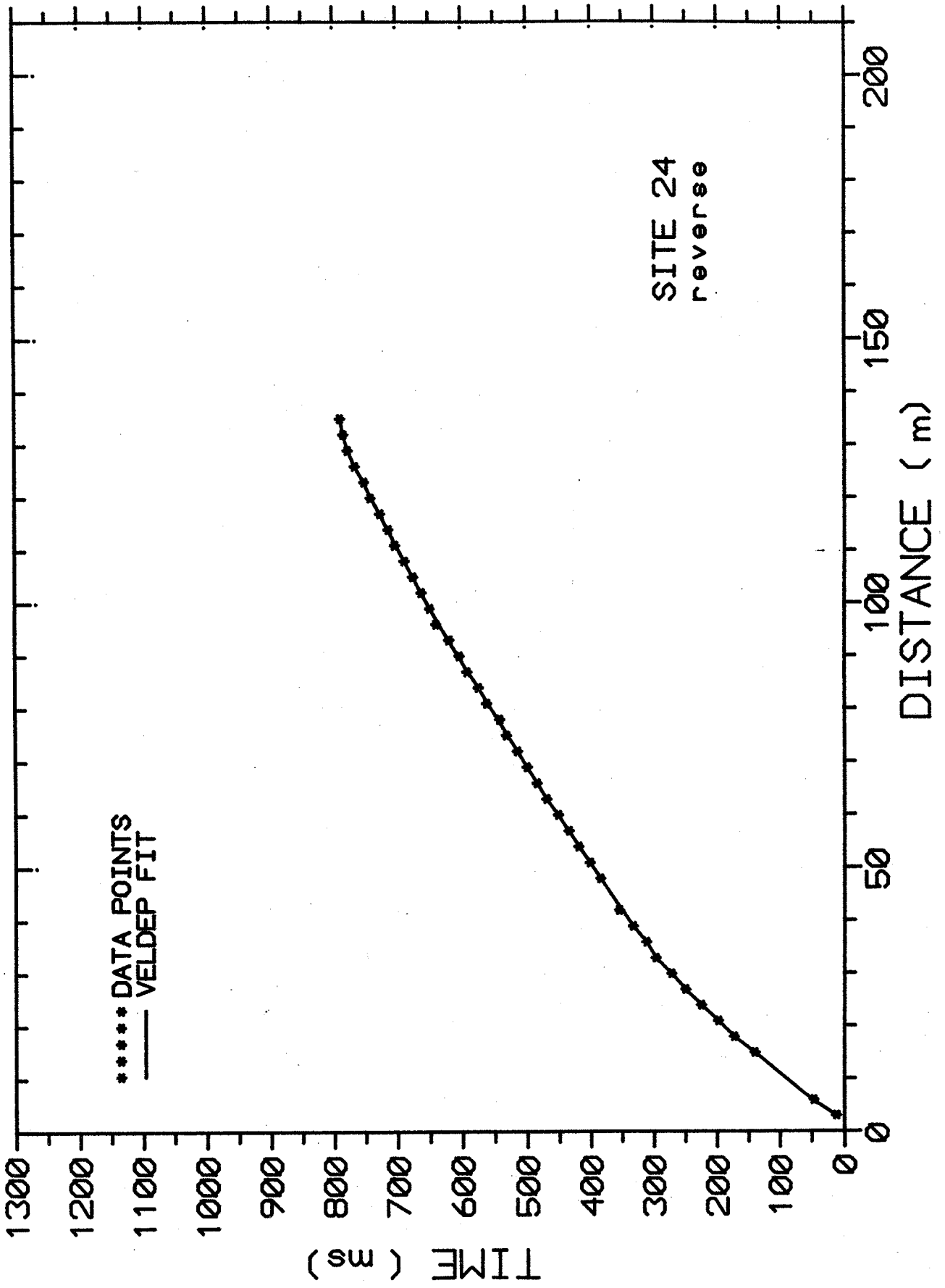






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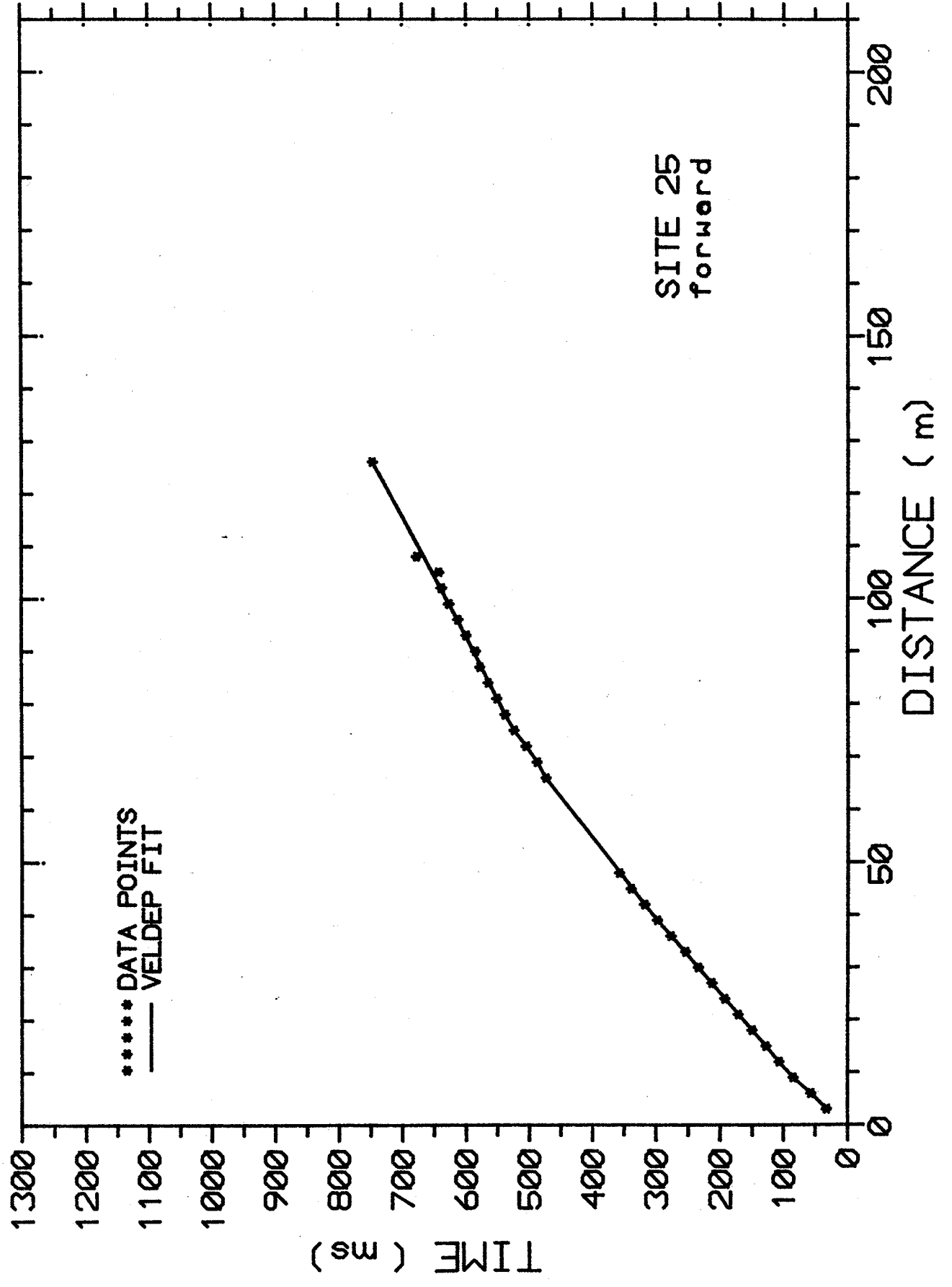


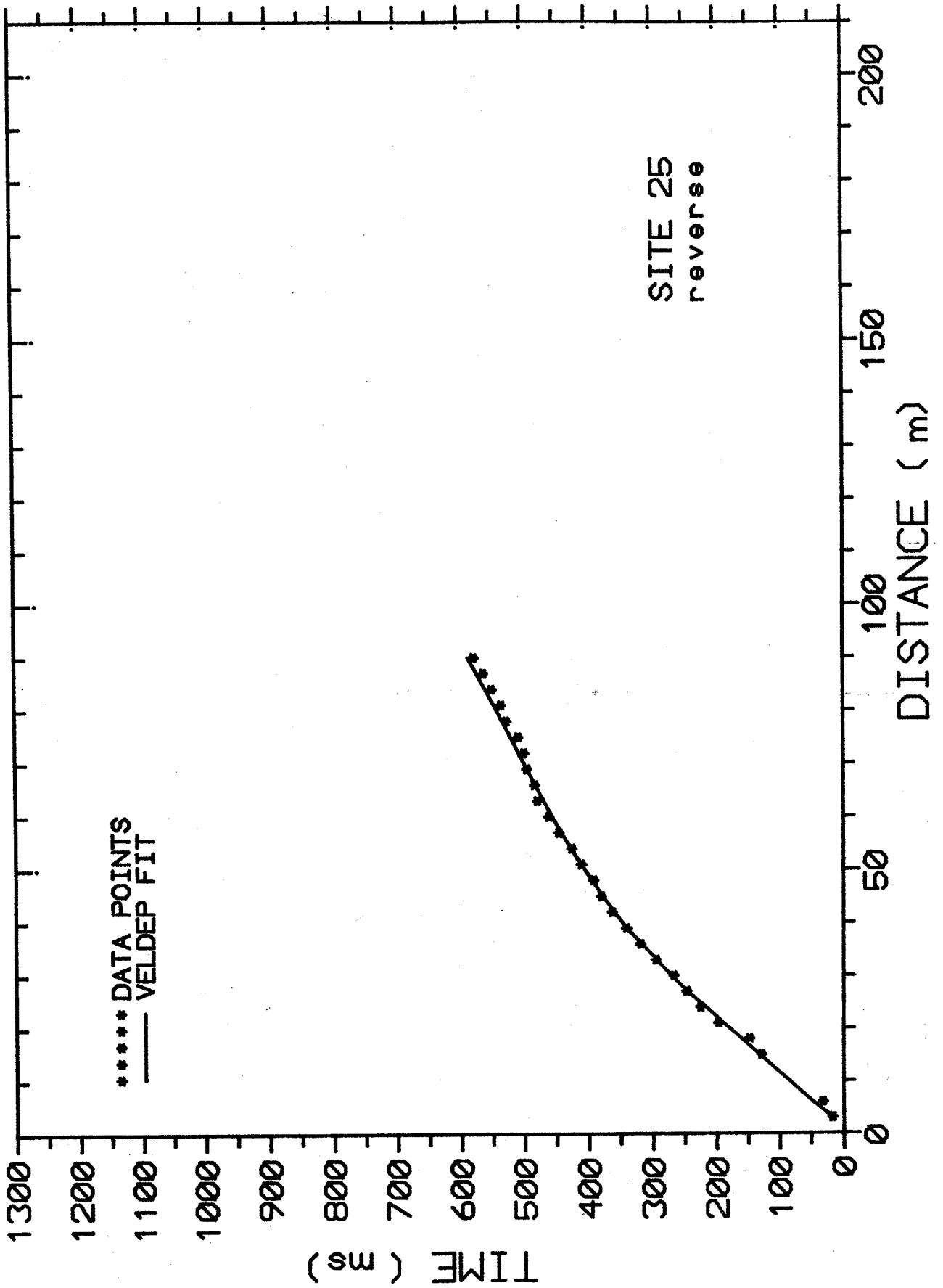
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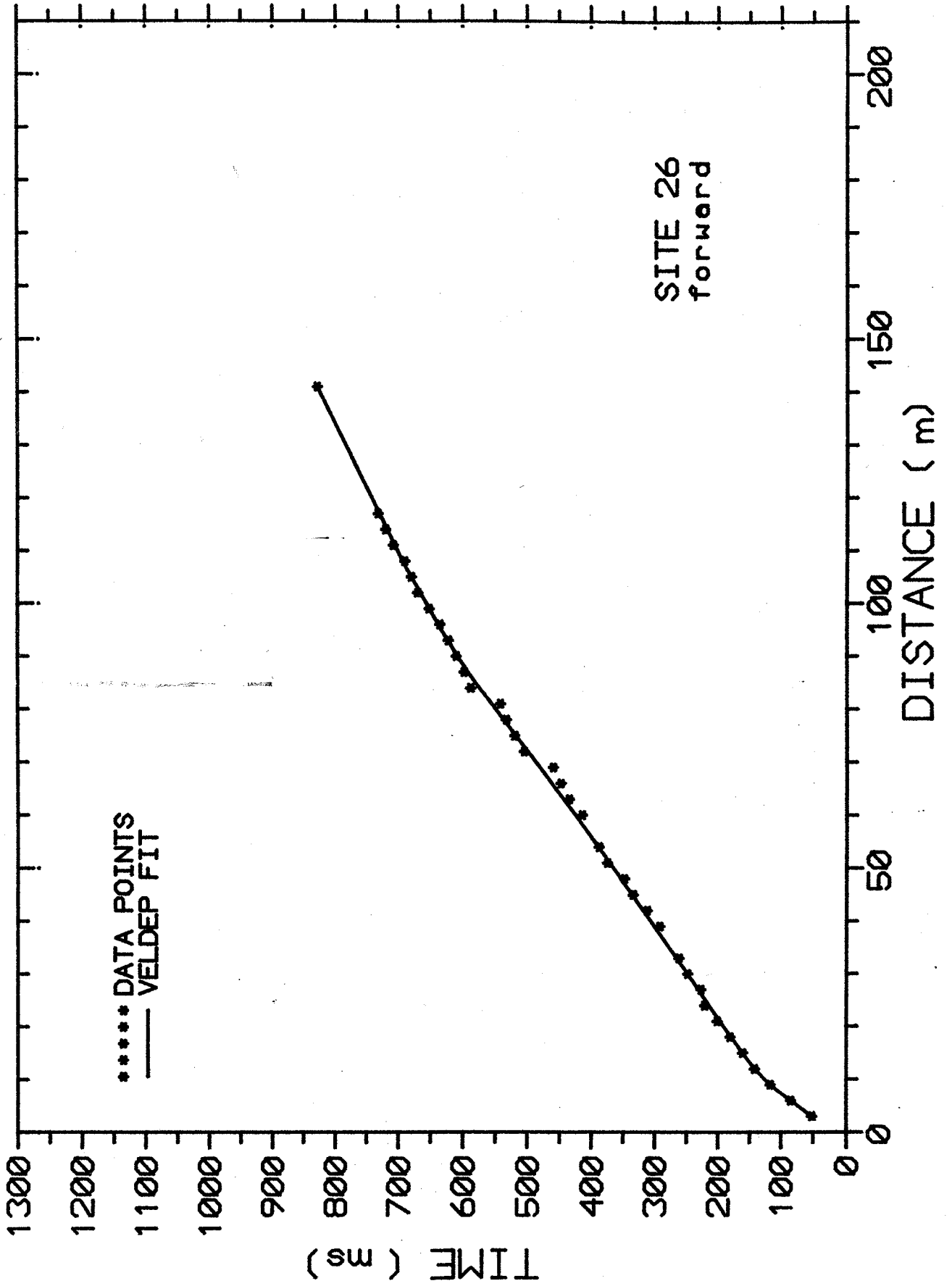
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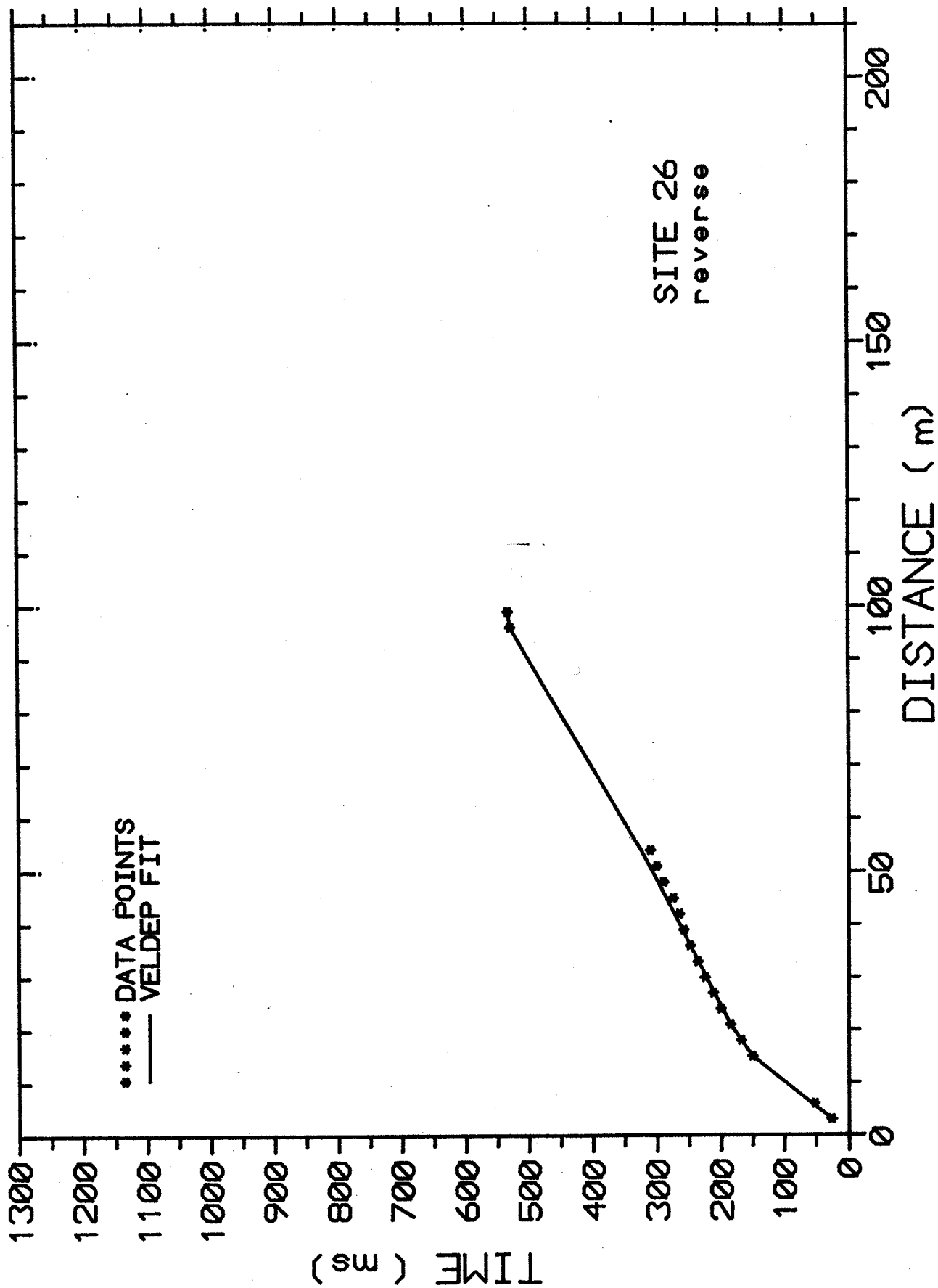
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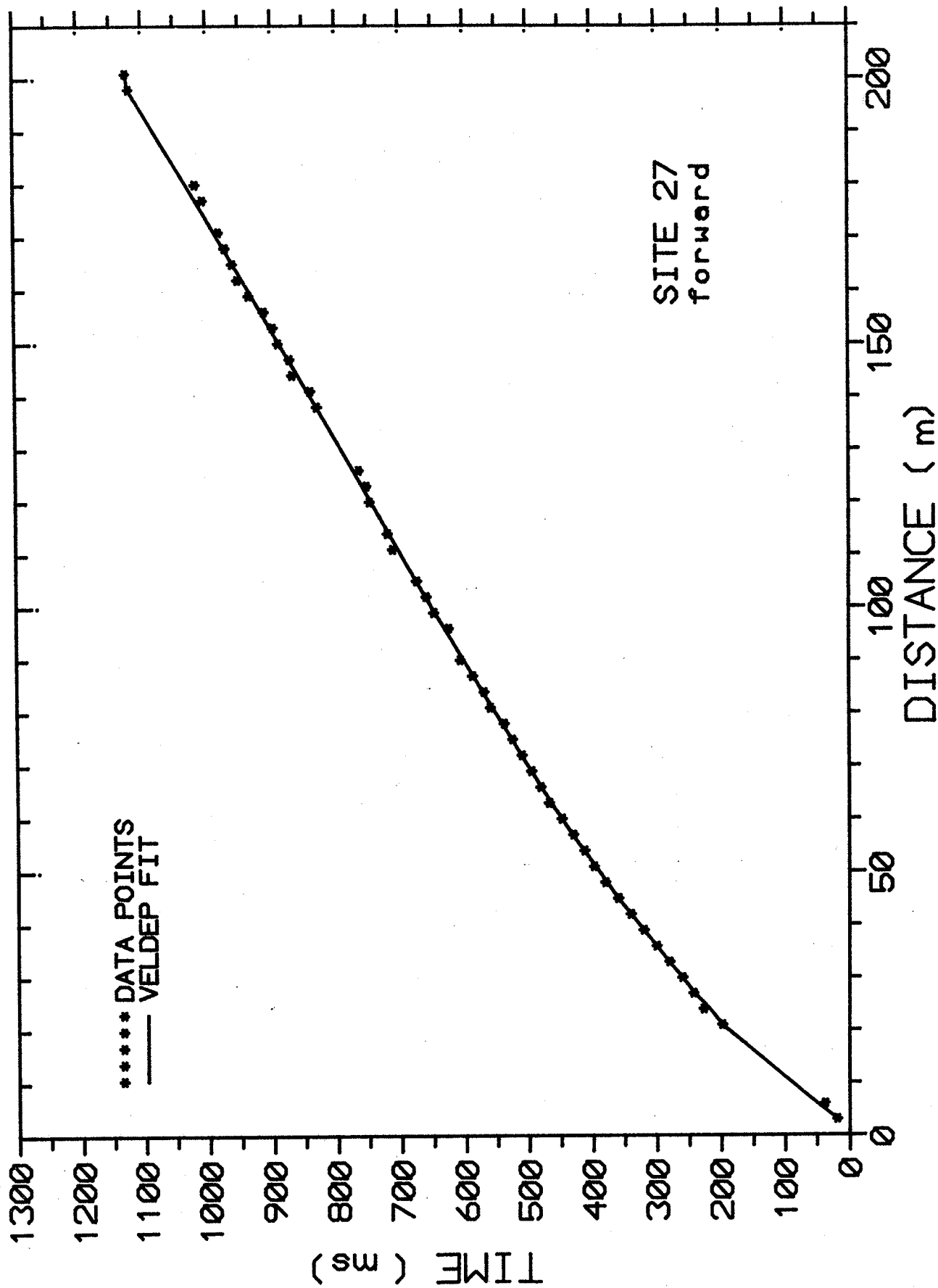
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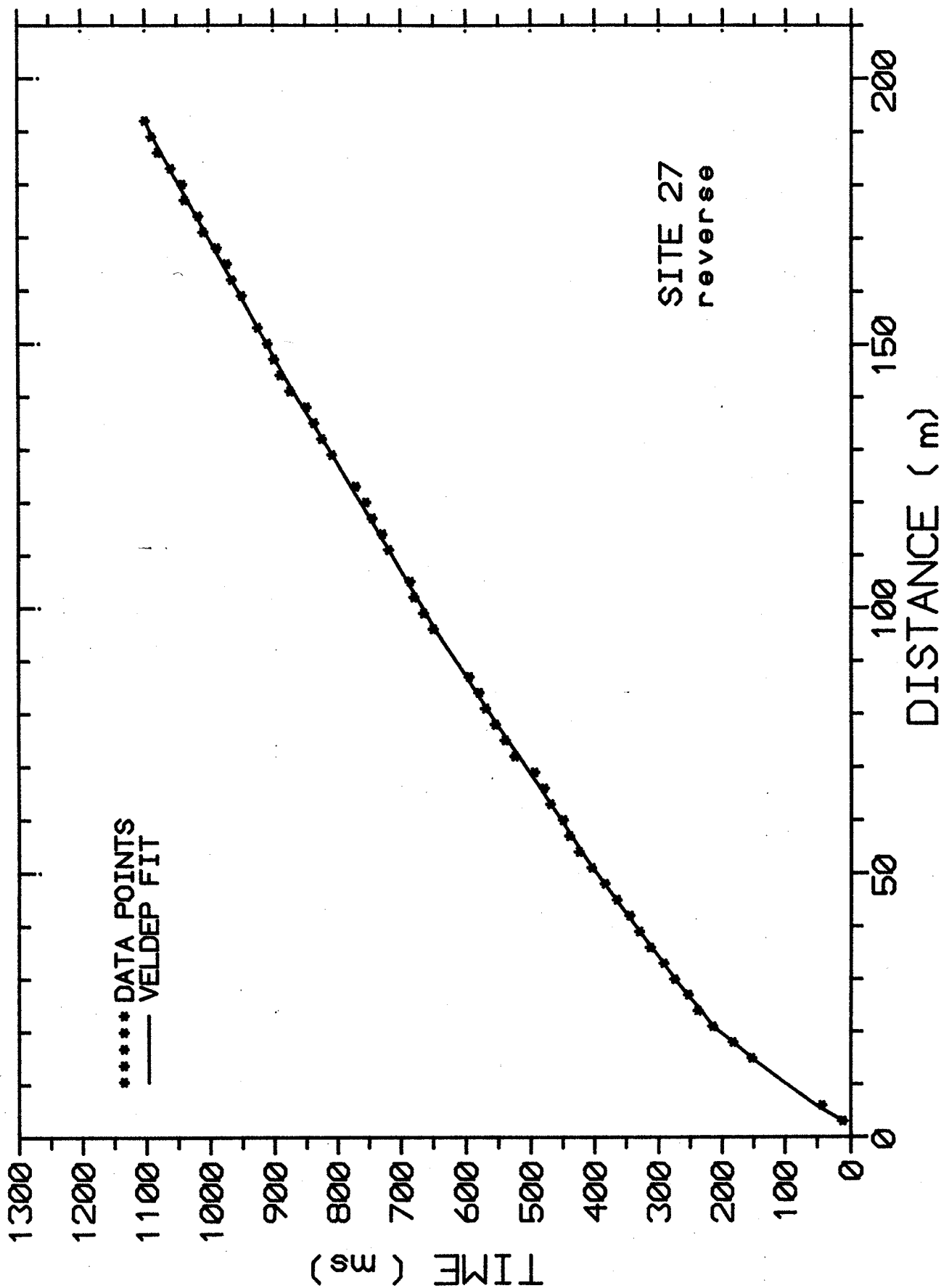


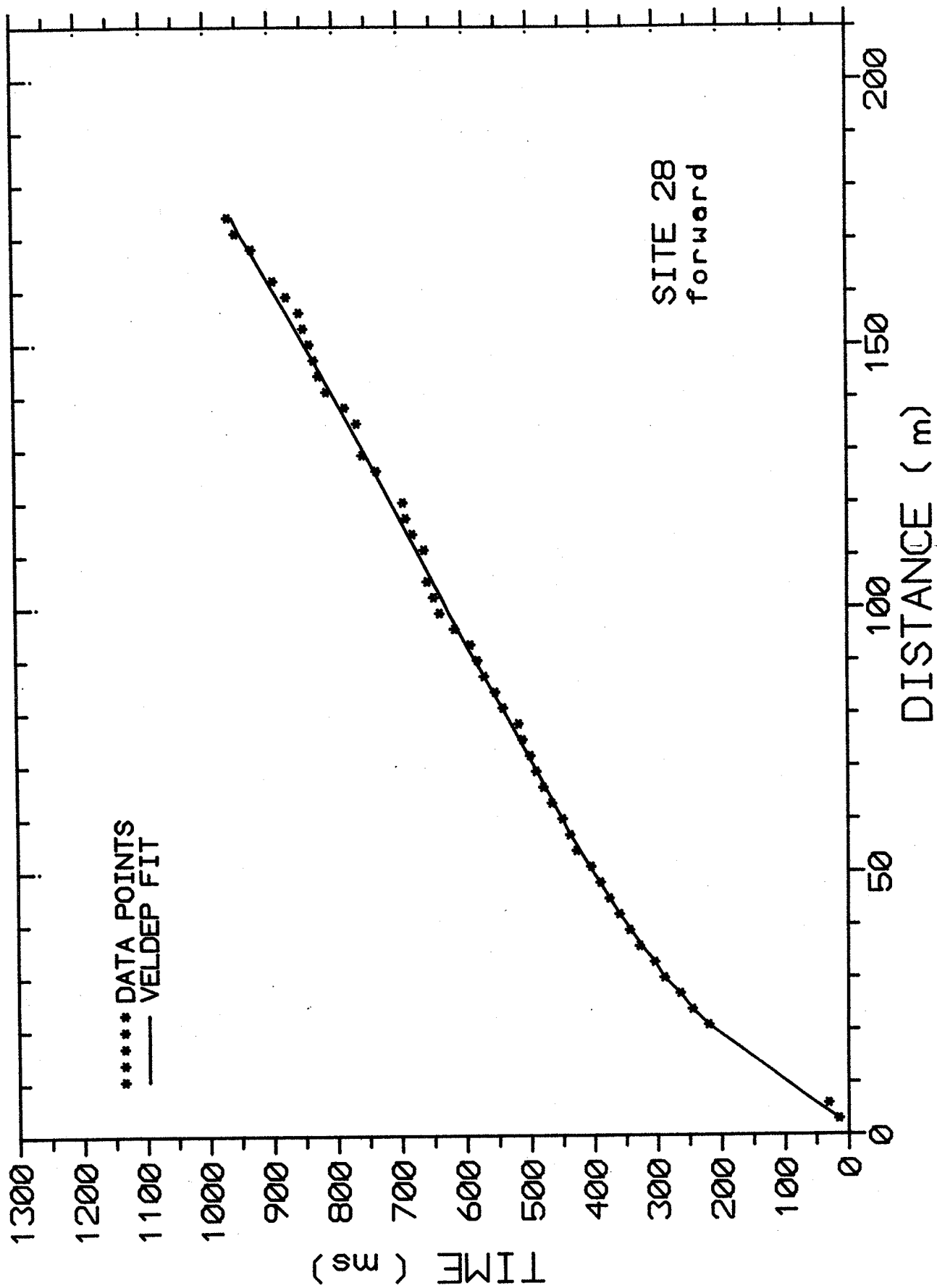
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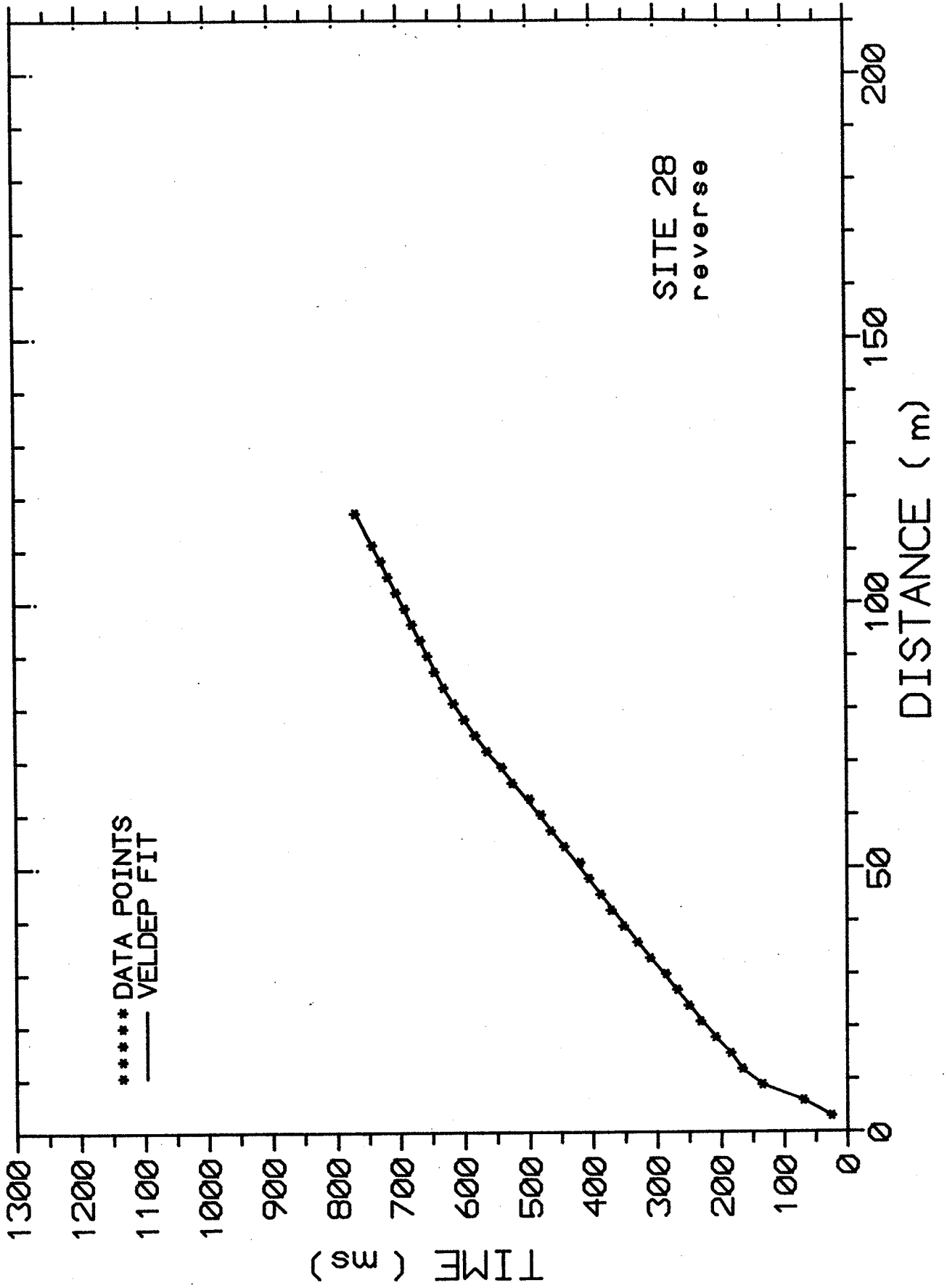
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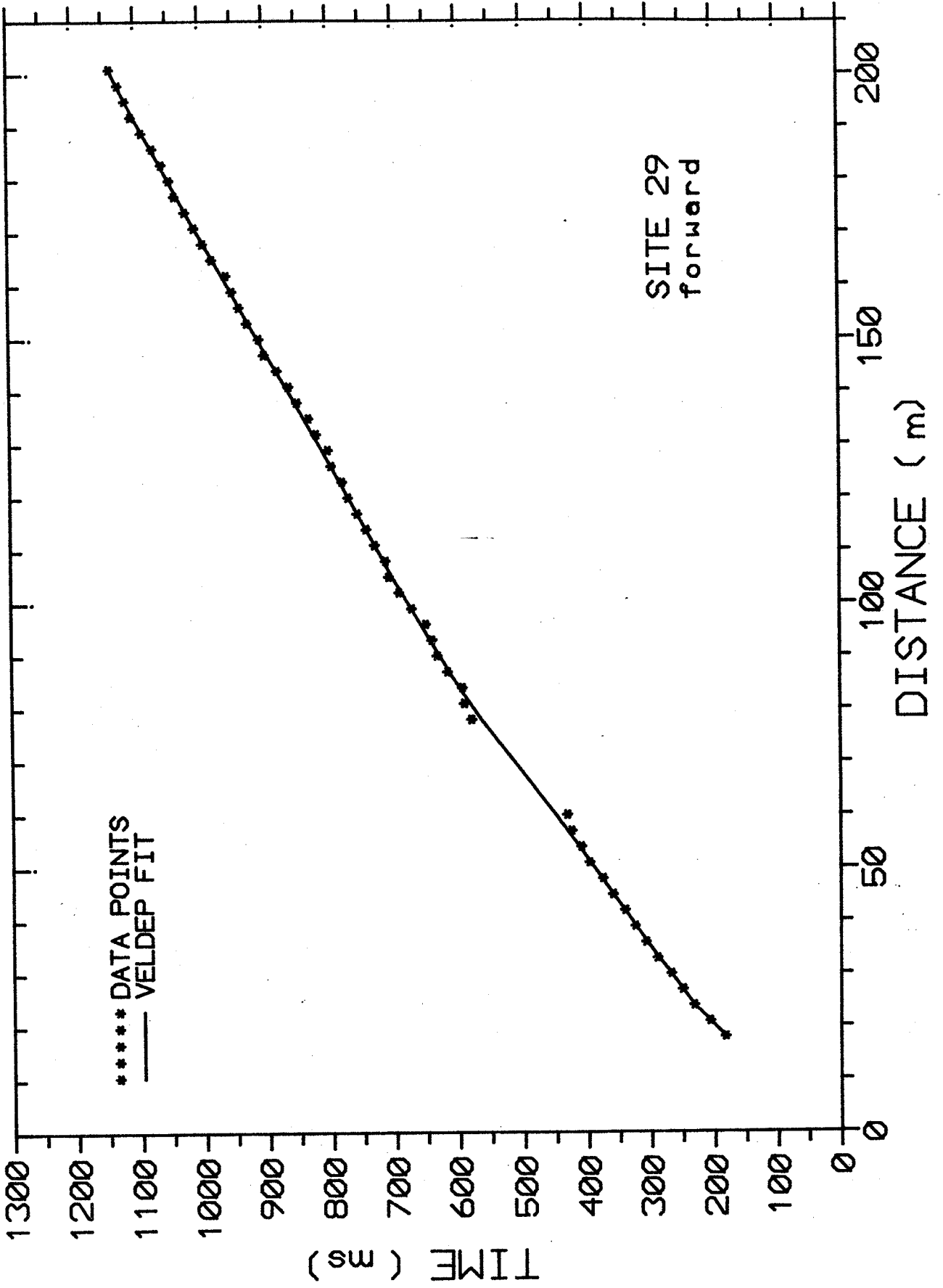
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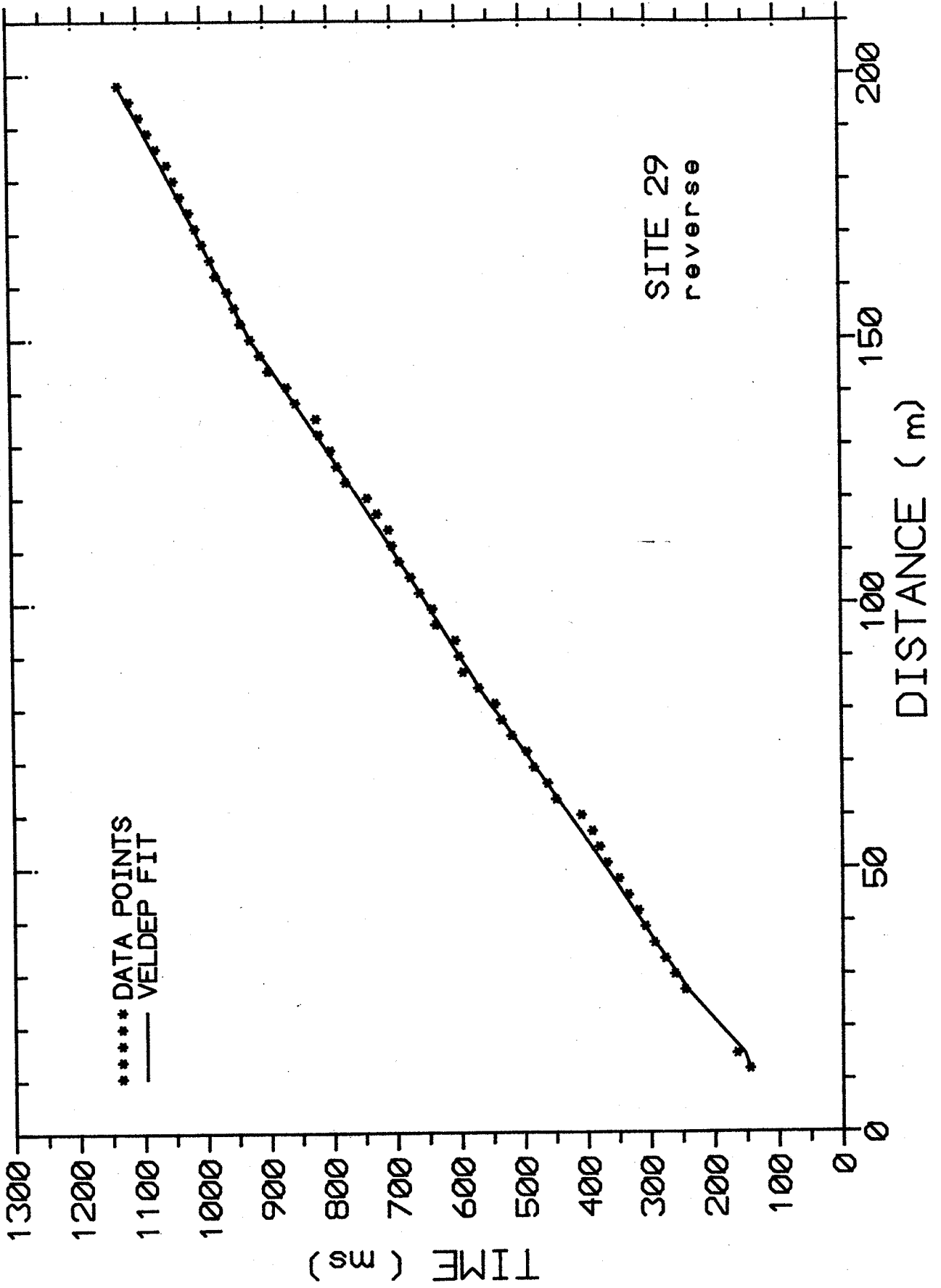
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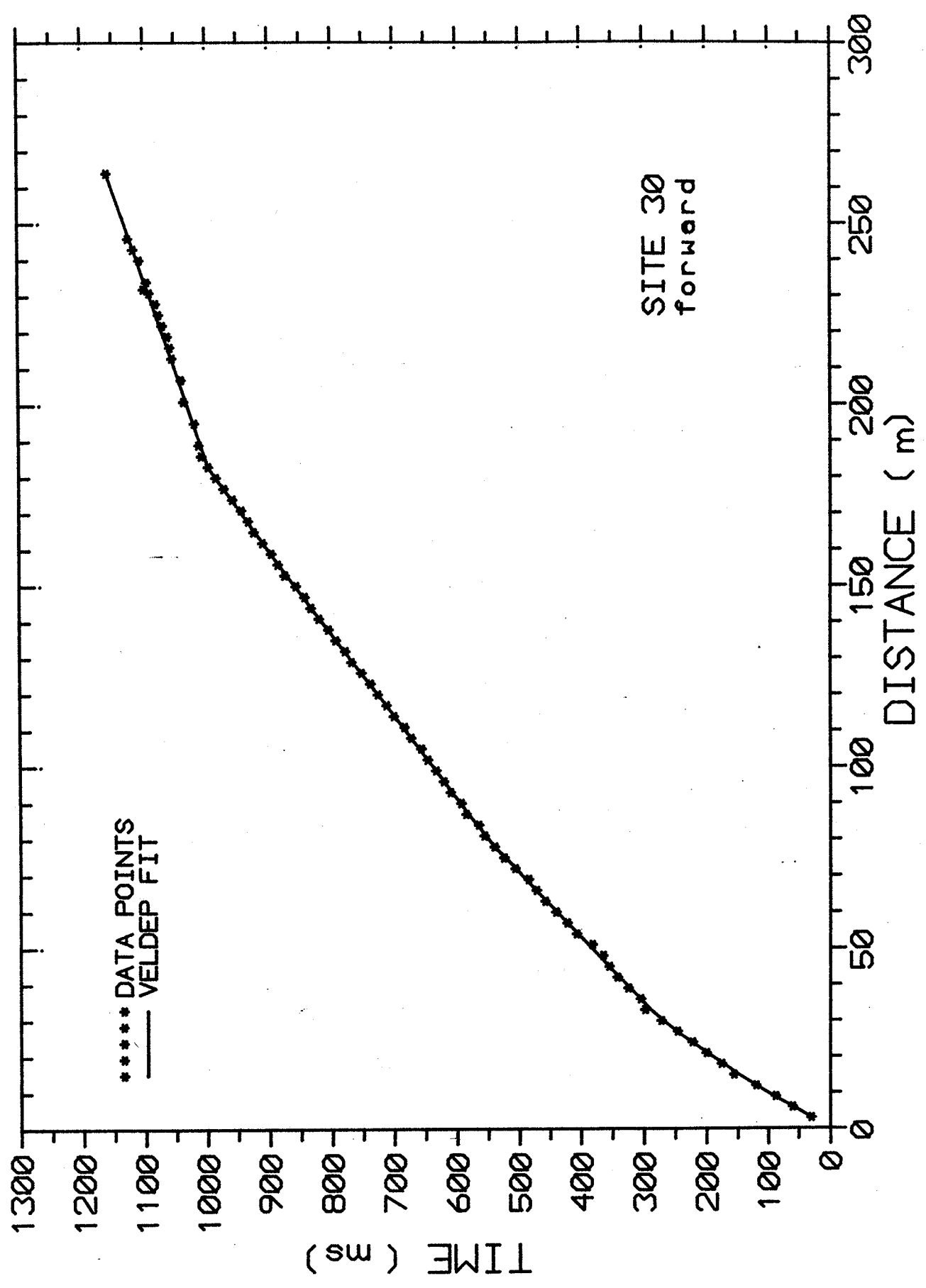


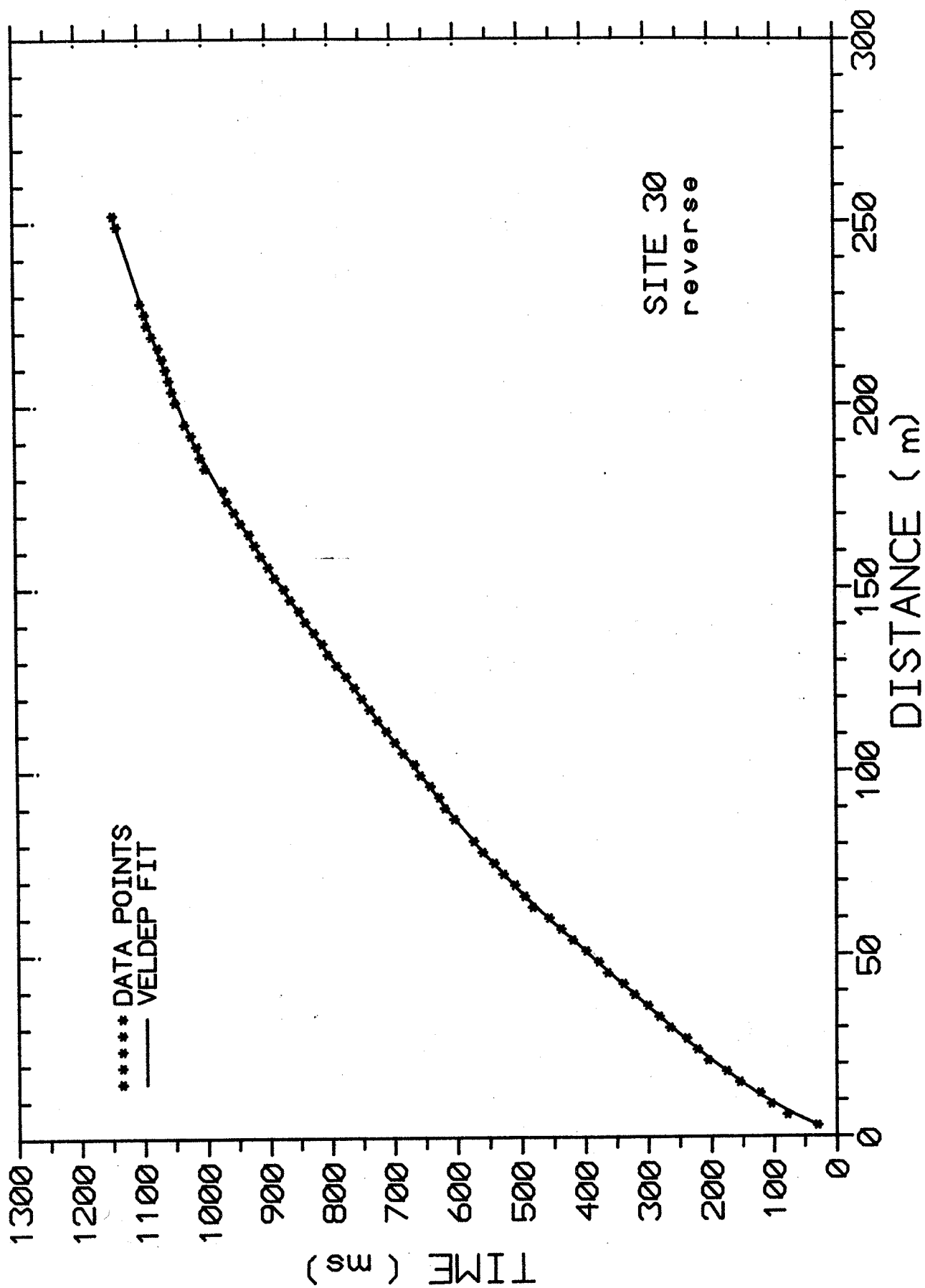


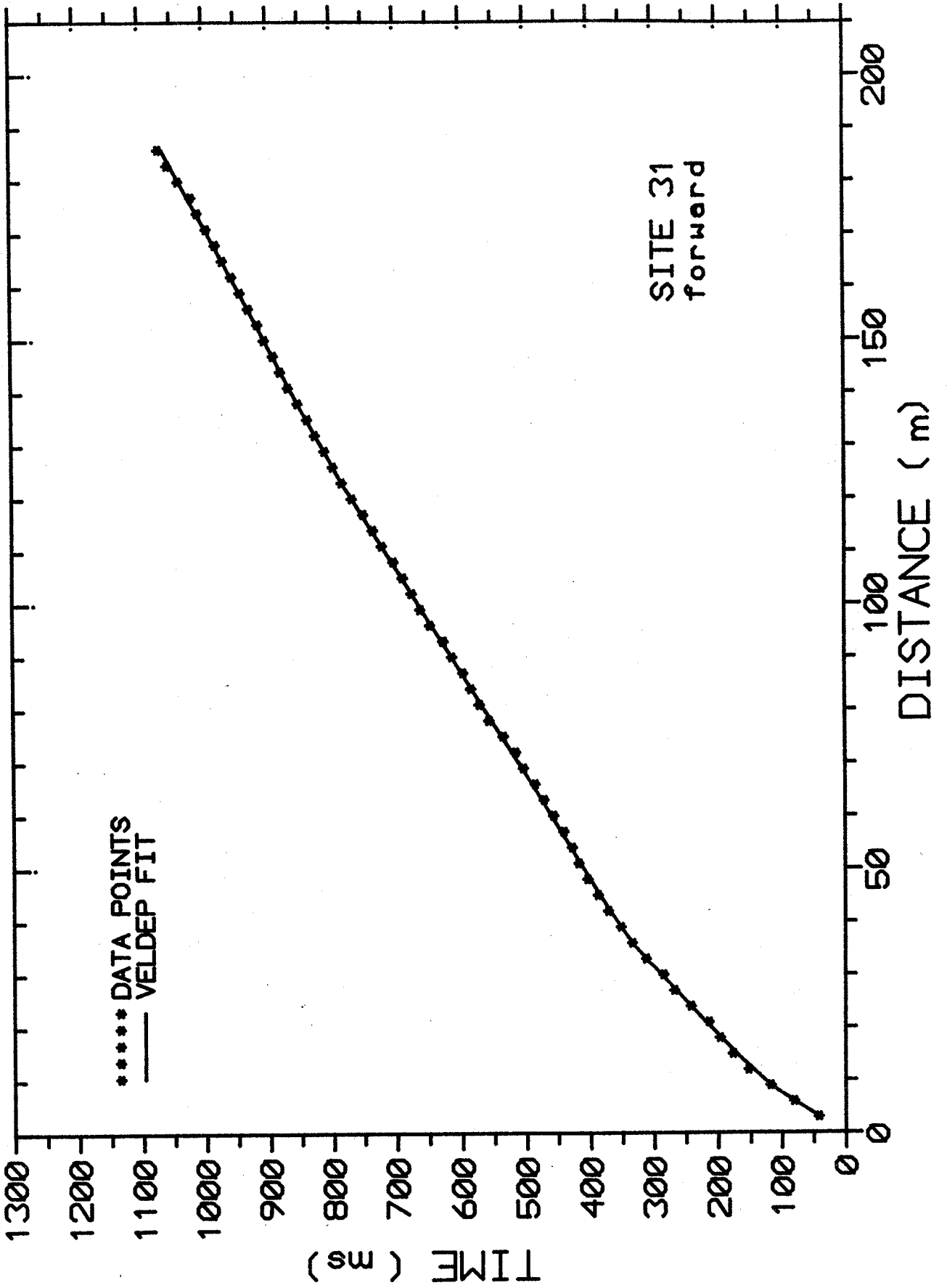


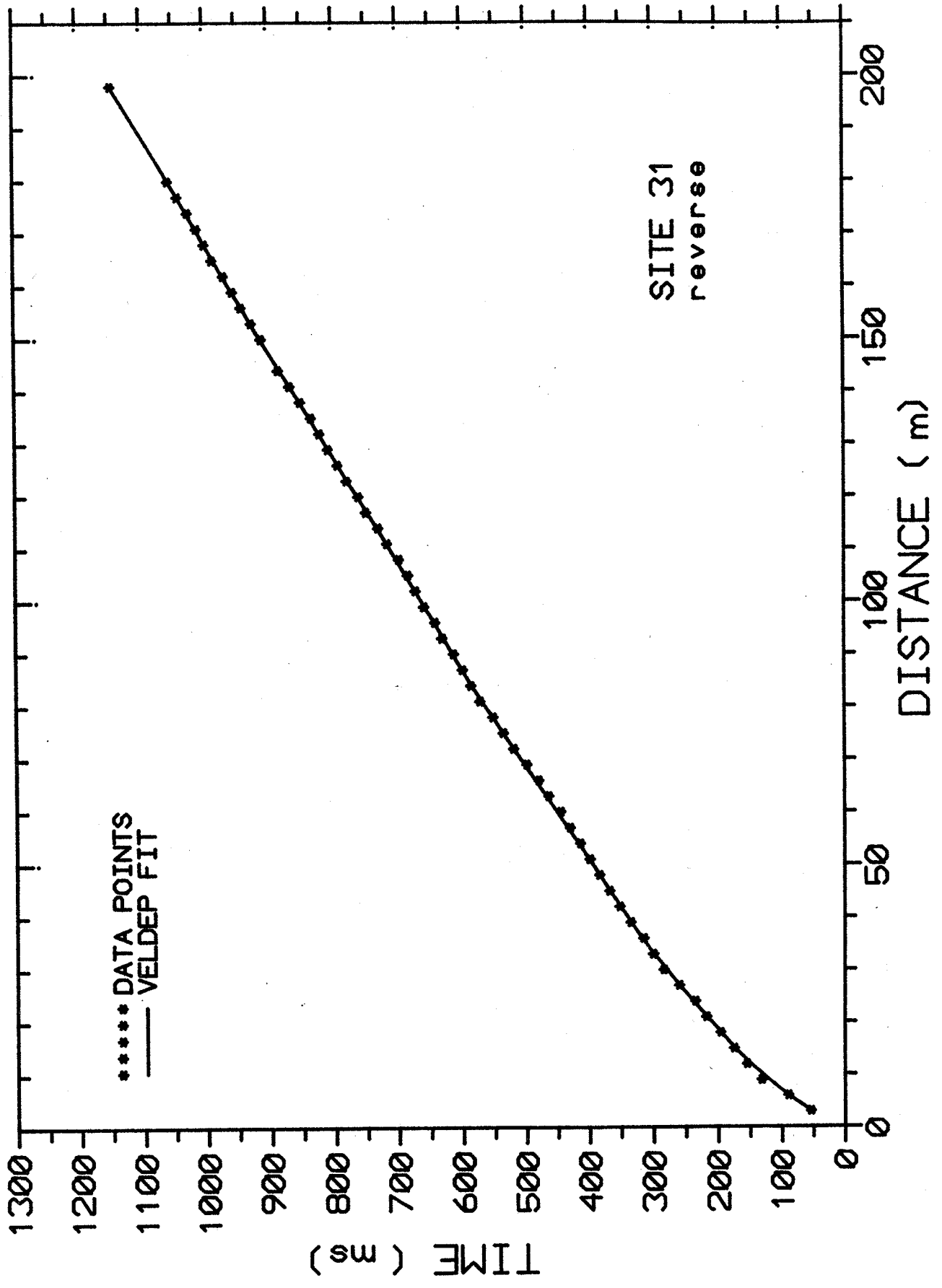


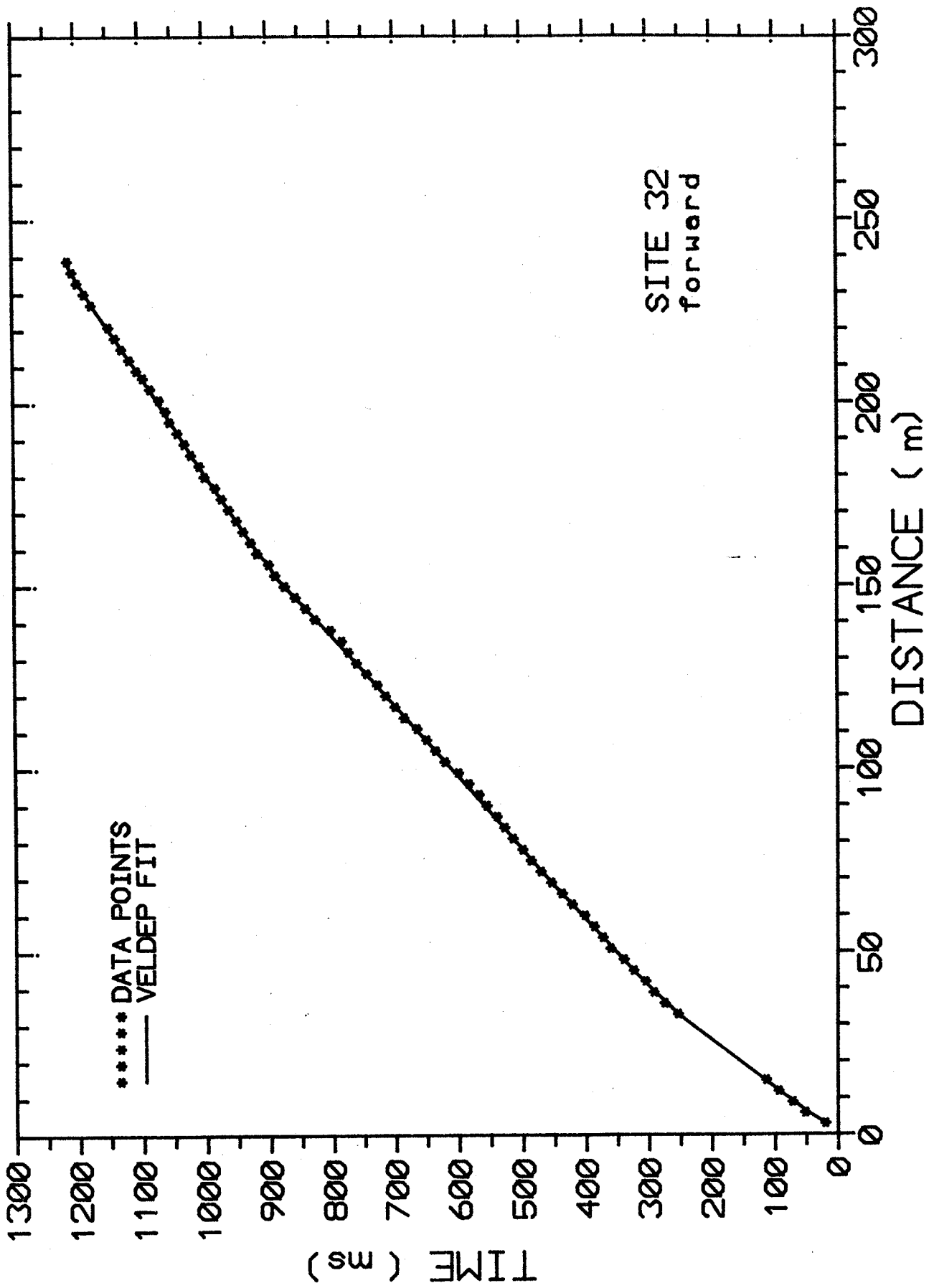


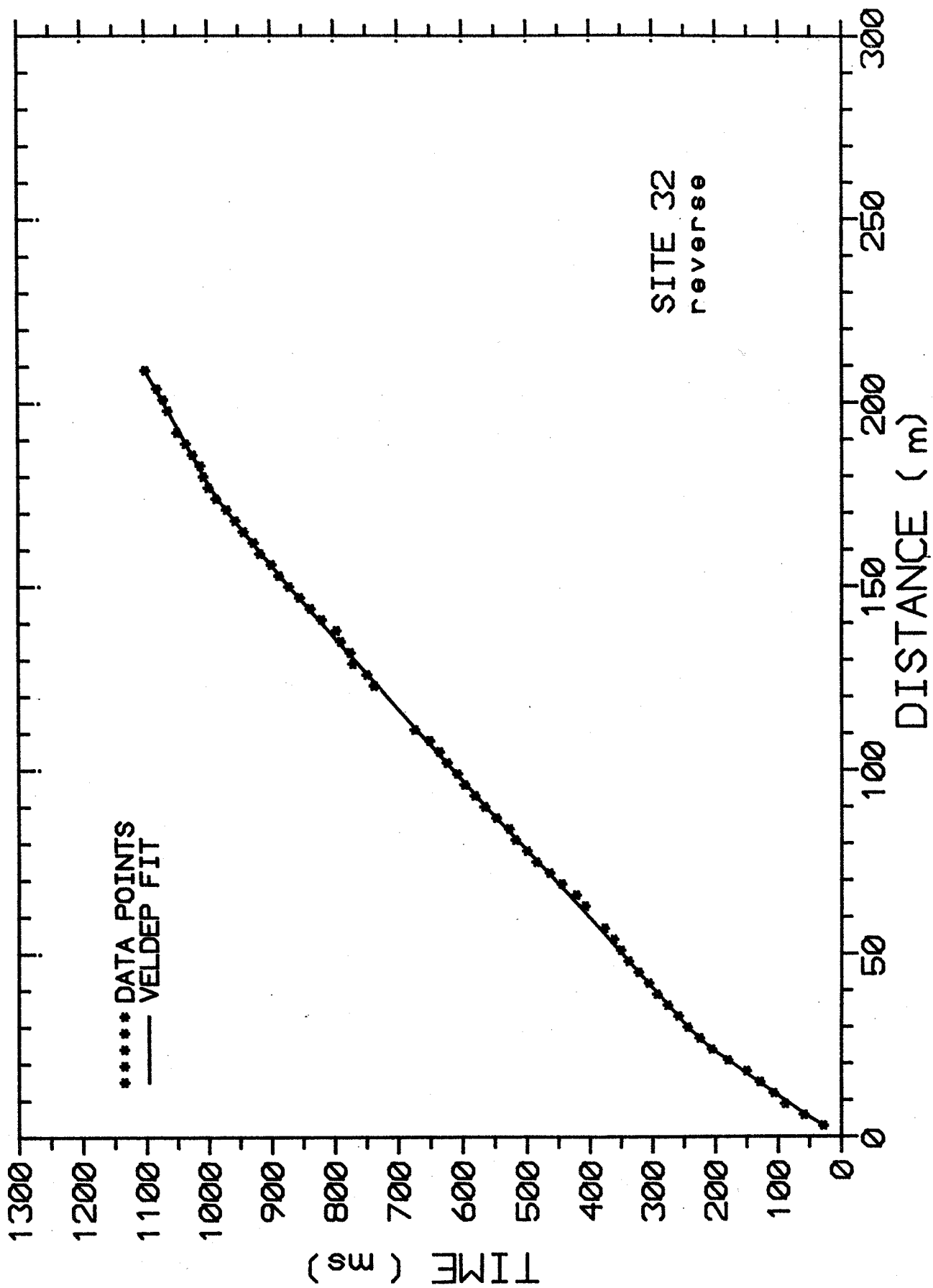


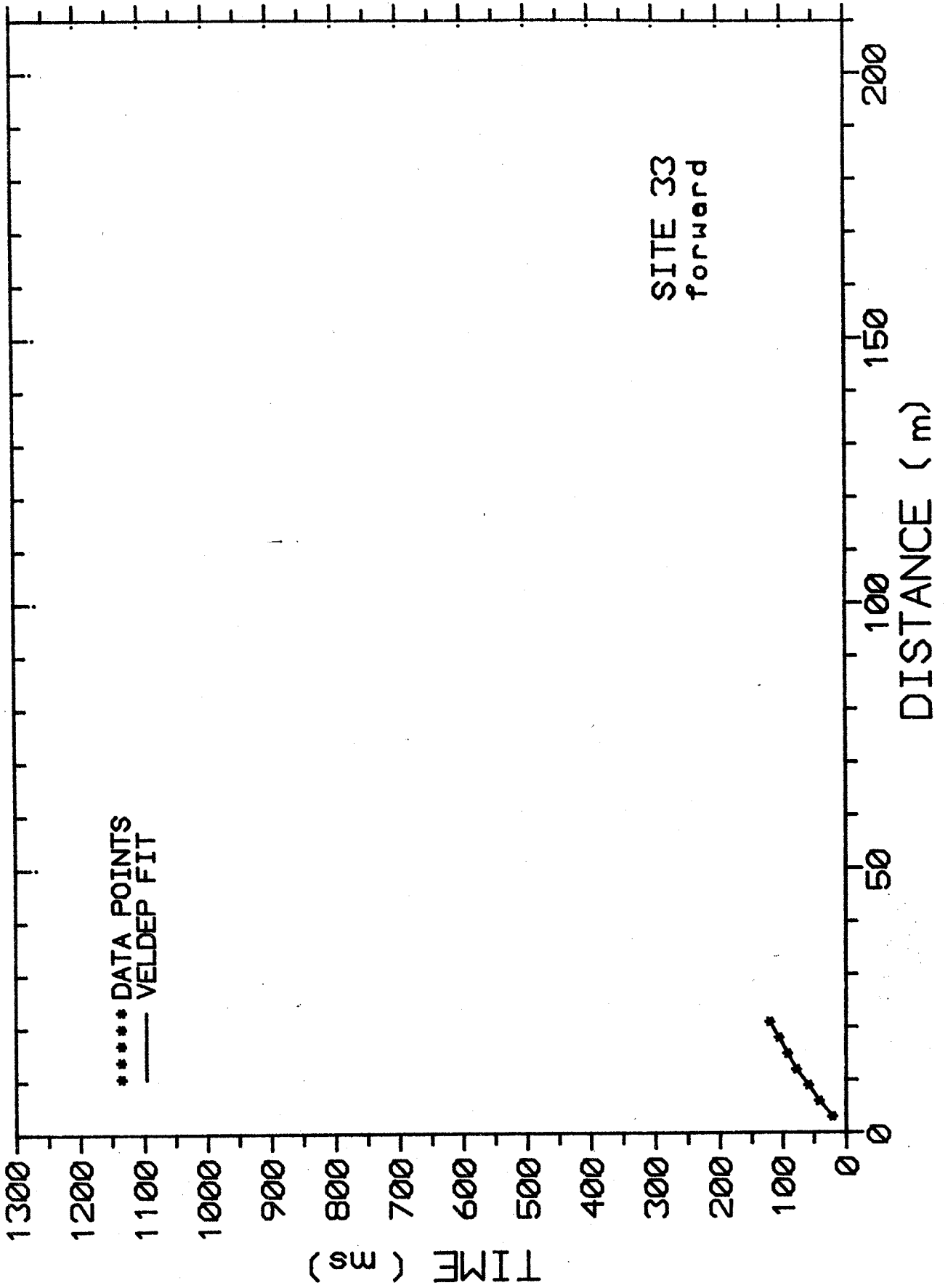


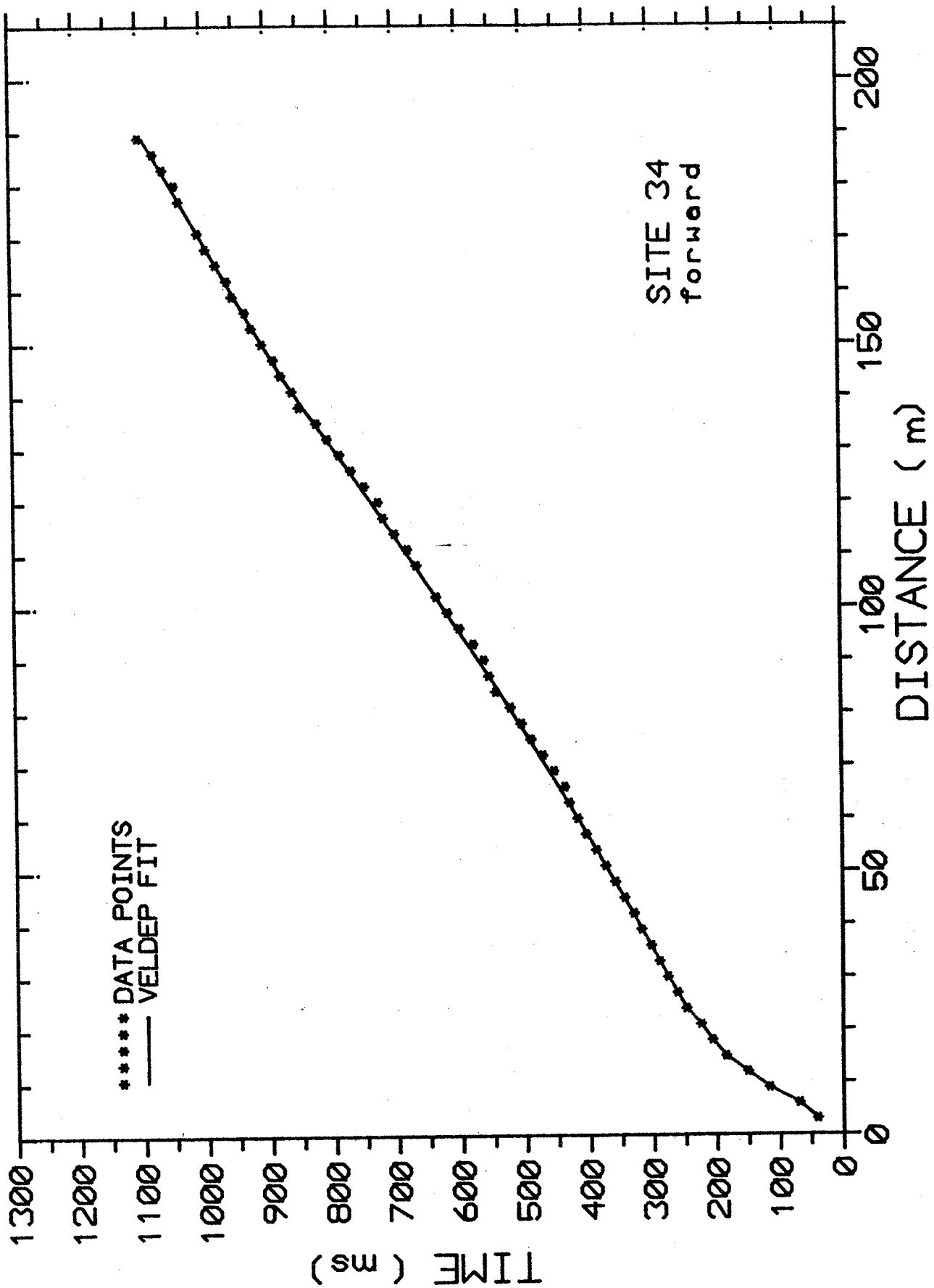


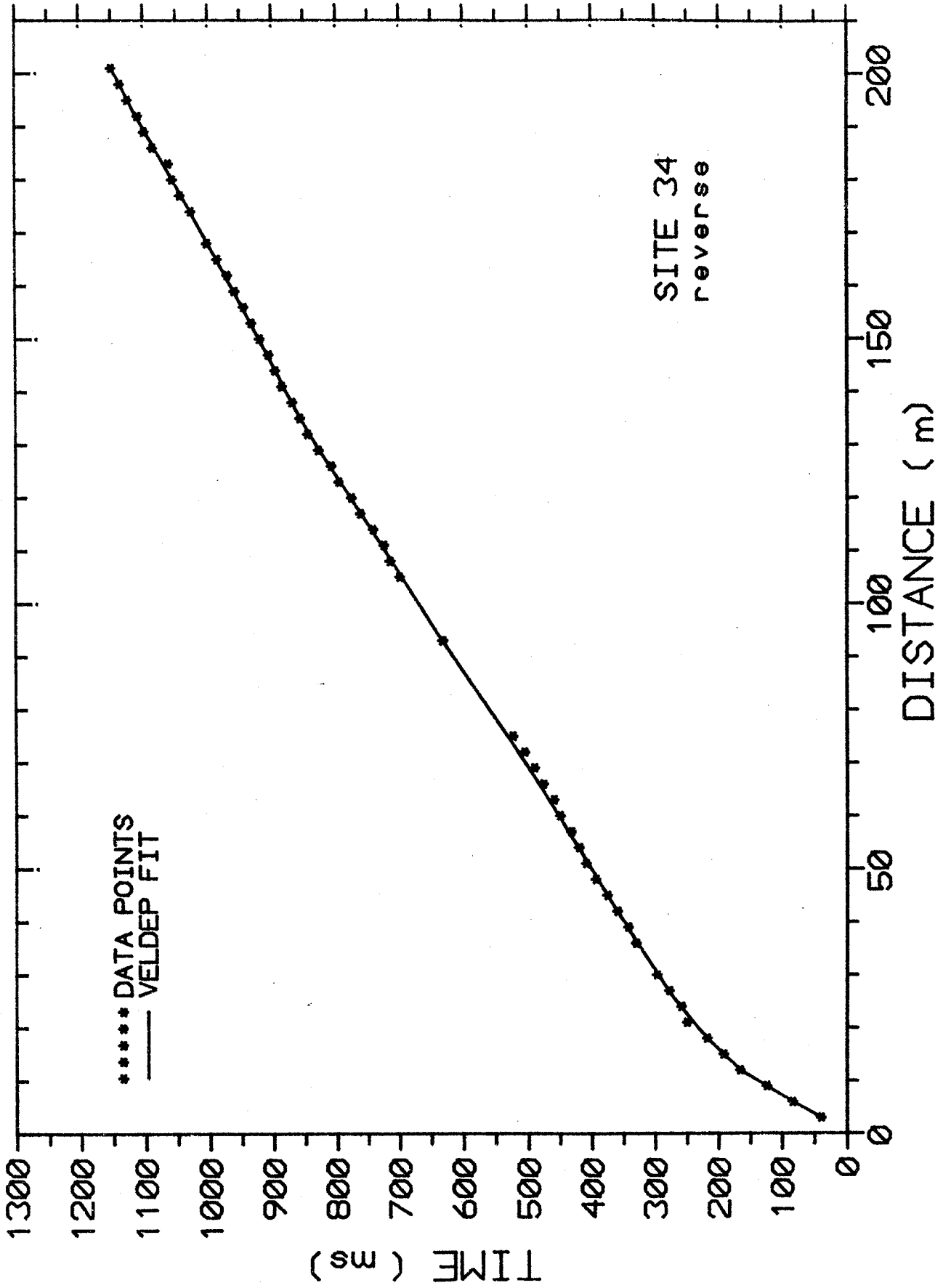






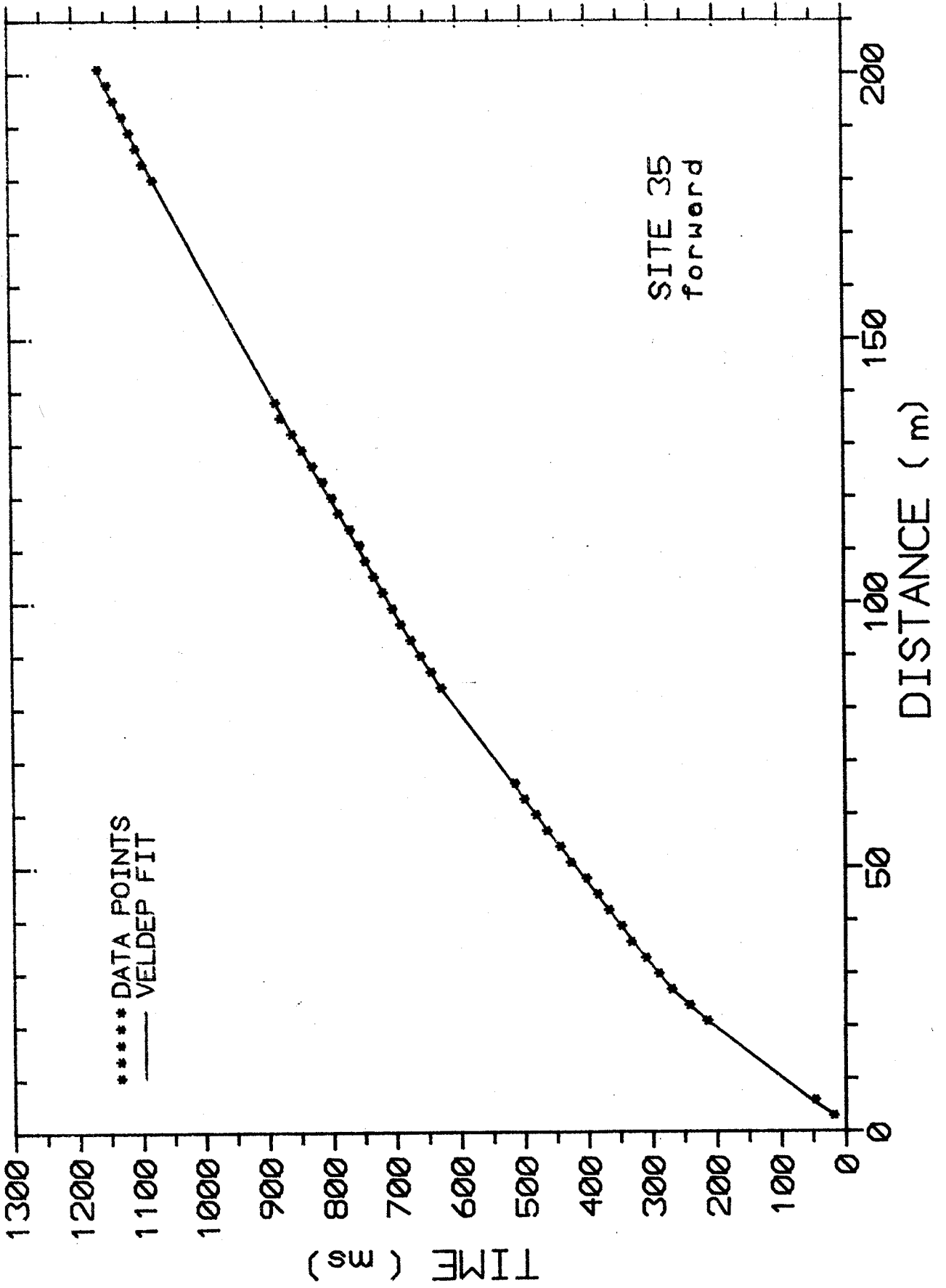


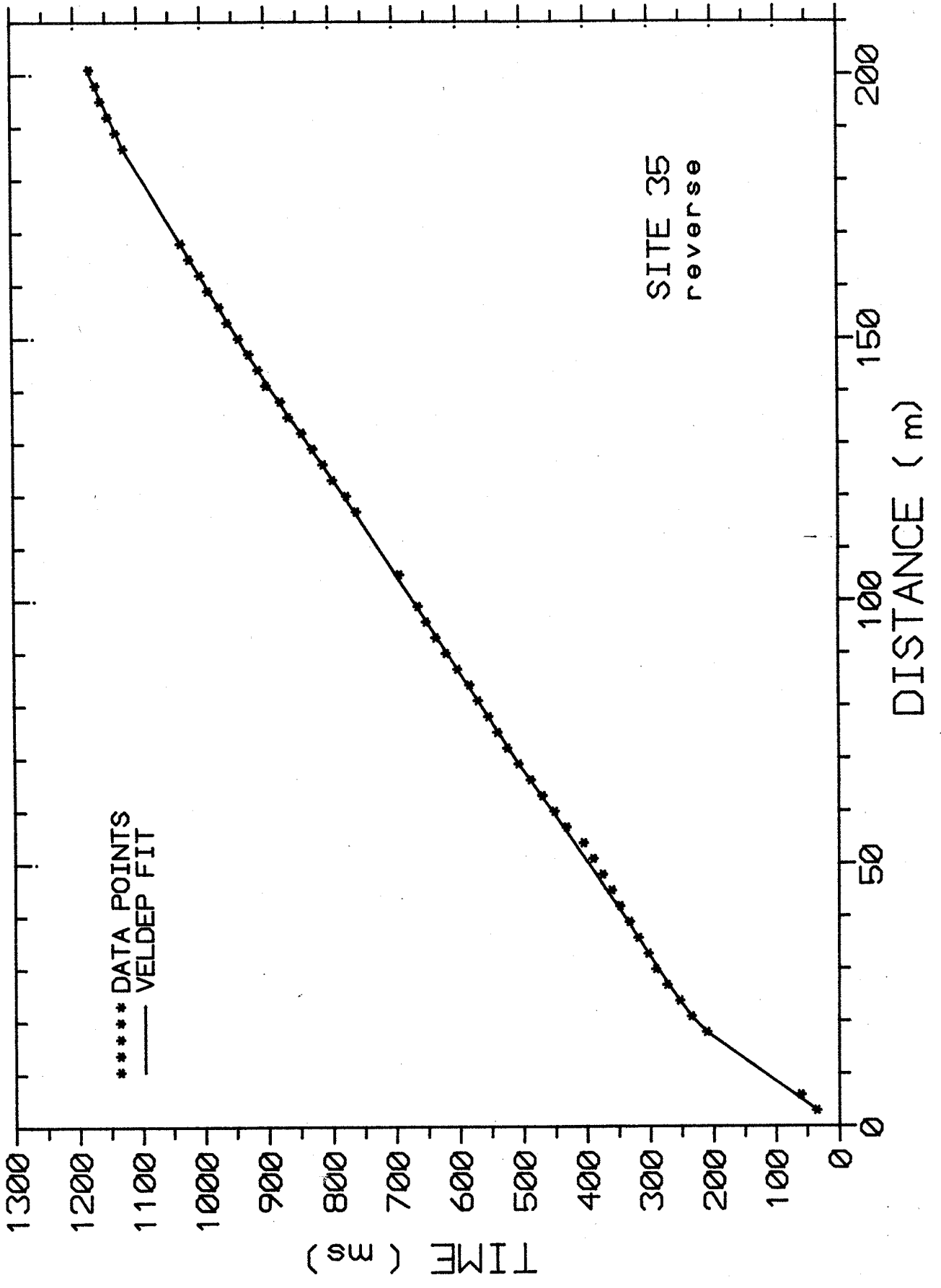




***** DATA POINTS
— VELDEP FIT

SITE 34
reverse



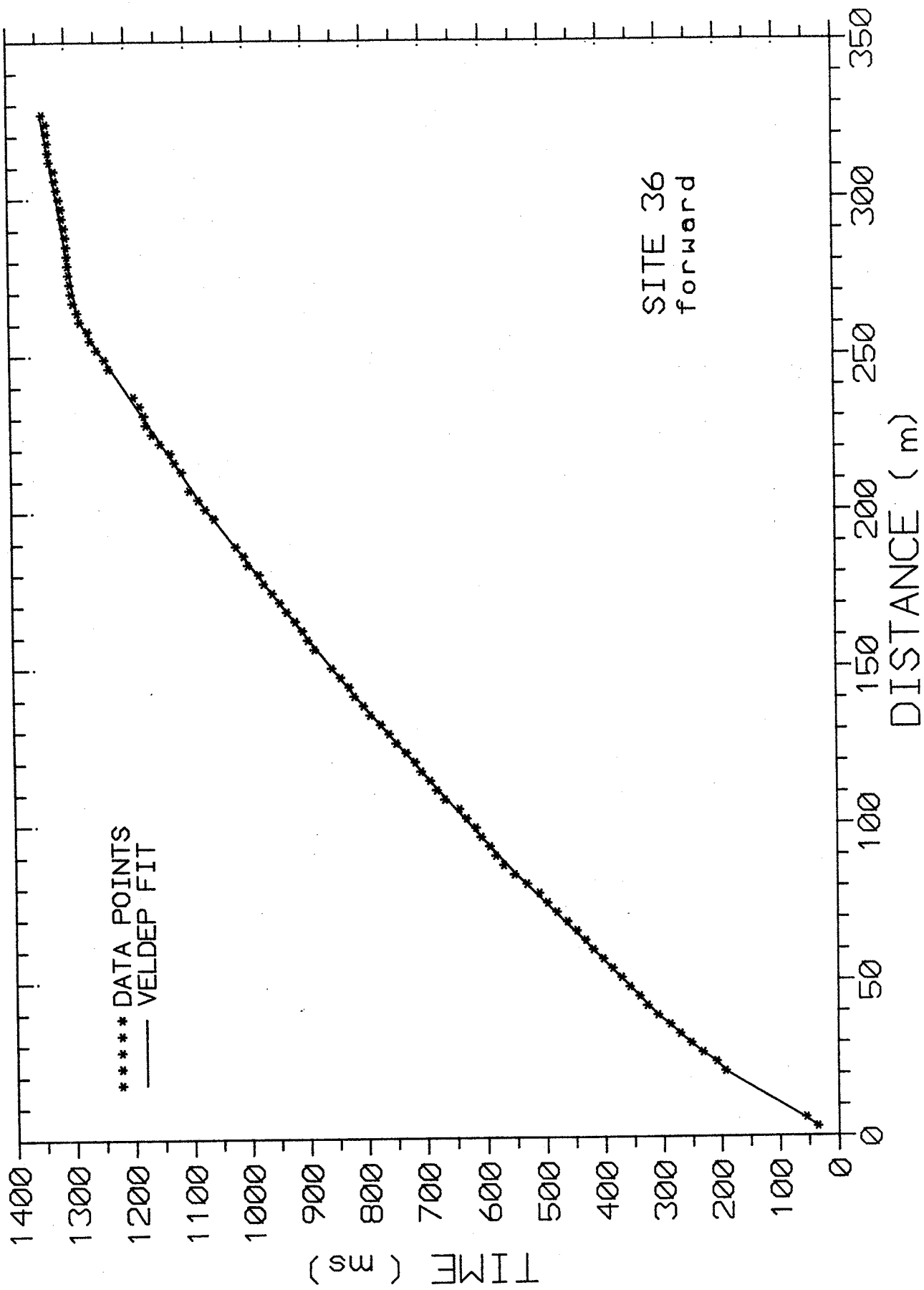


***** DATA POINTS
— VELDEP FIT

SITE 35
reverse

TIME (ms)

DISTANCE (m)

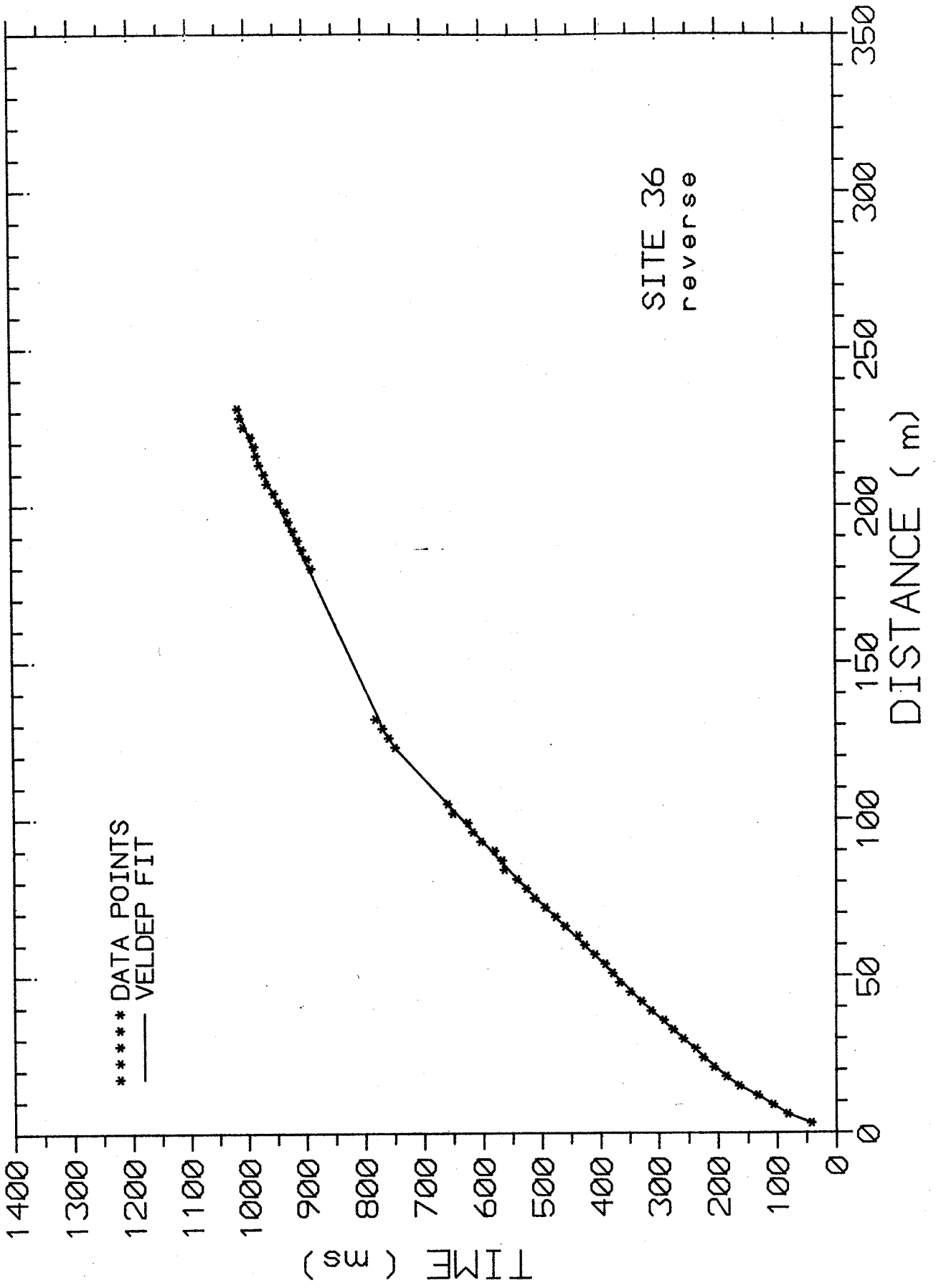


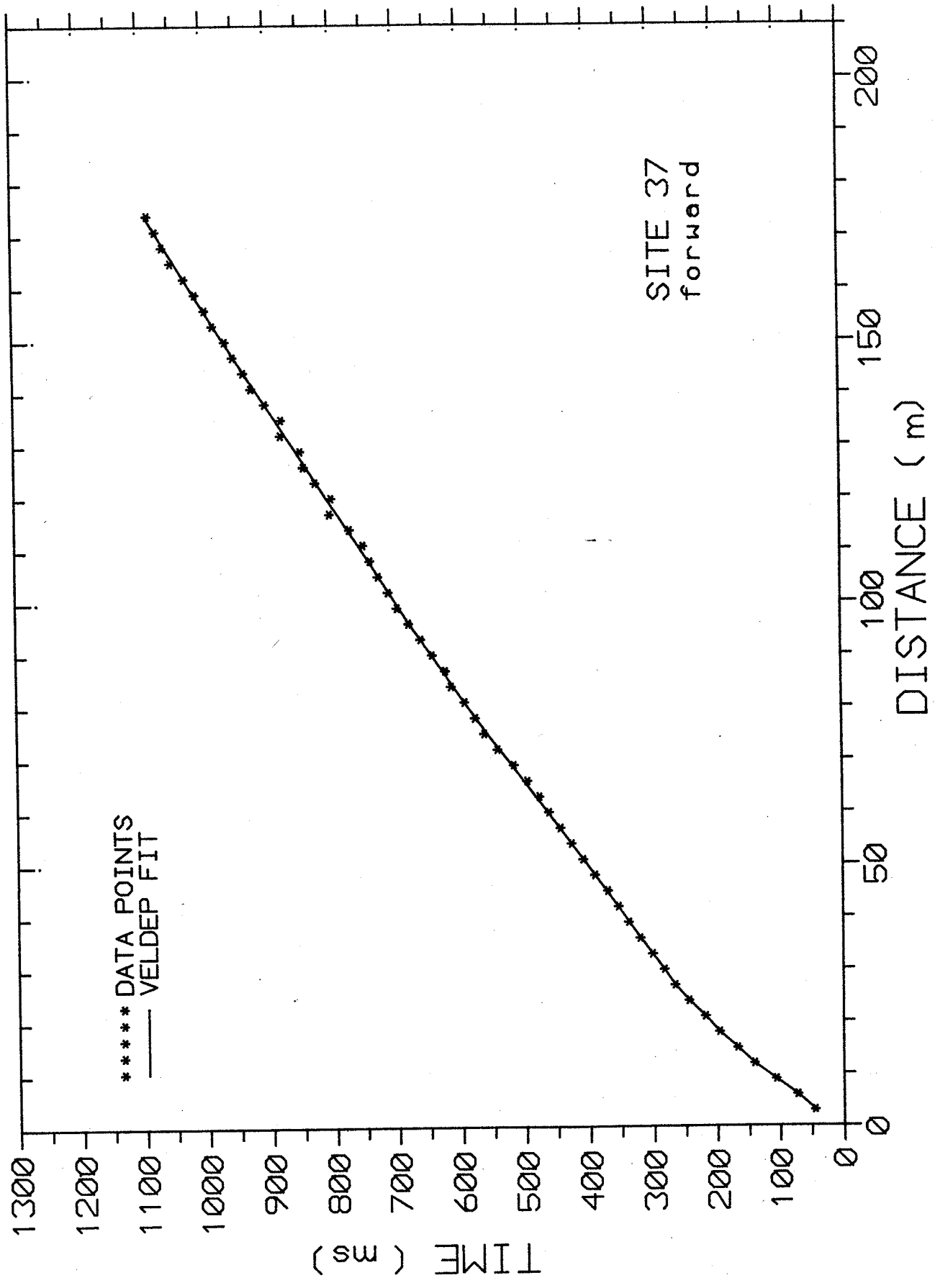
SITE 36
forward

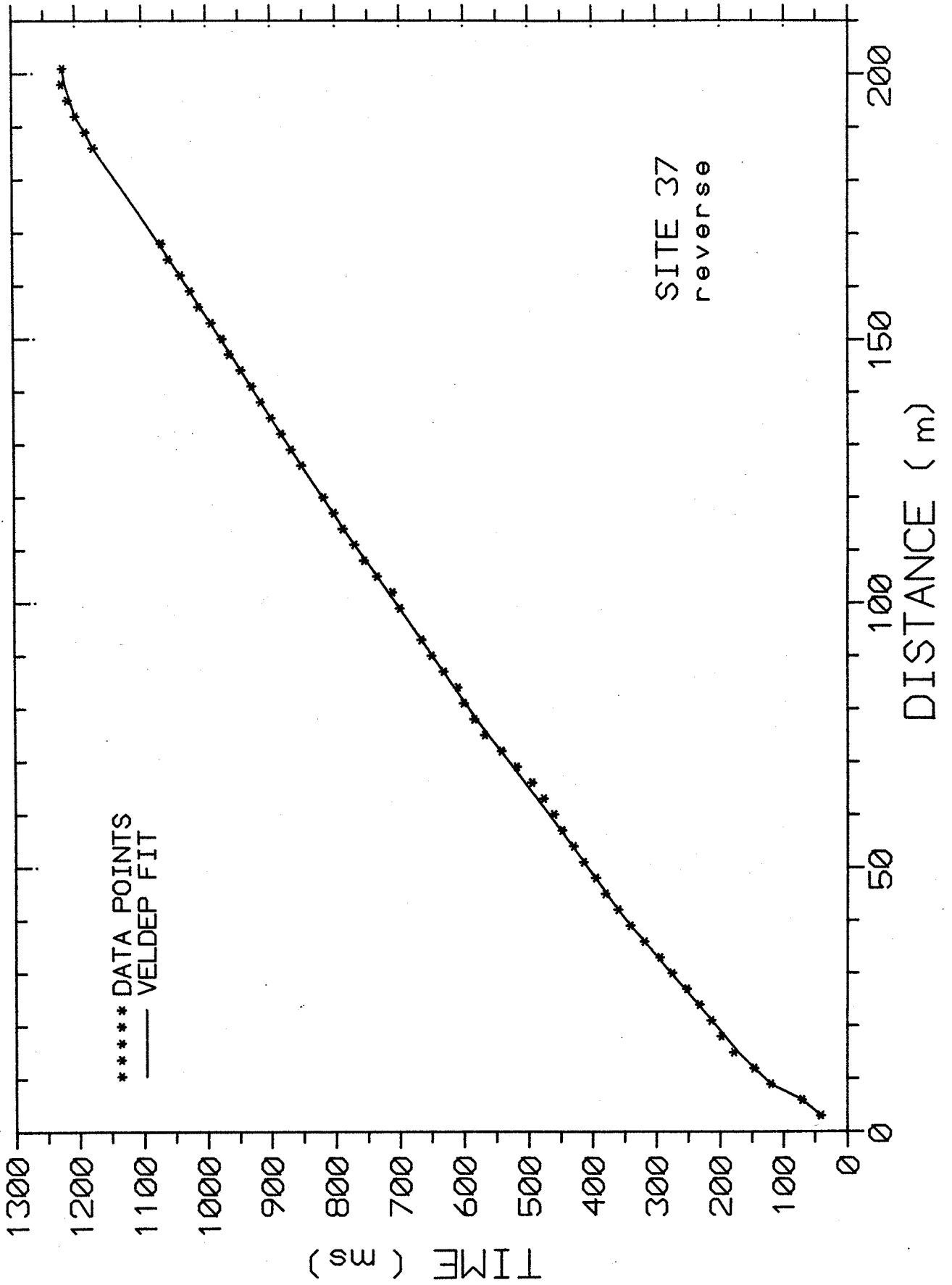
***** DATA POINTS
—— VELDEP FIT

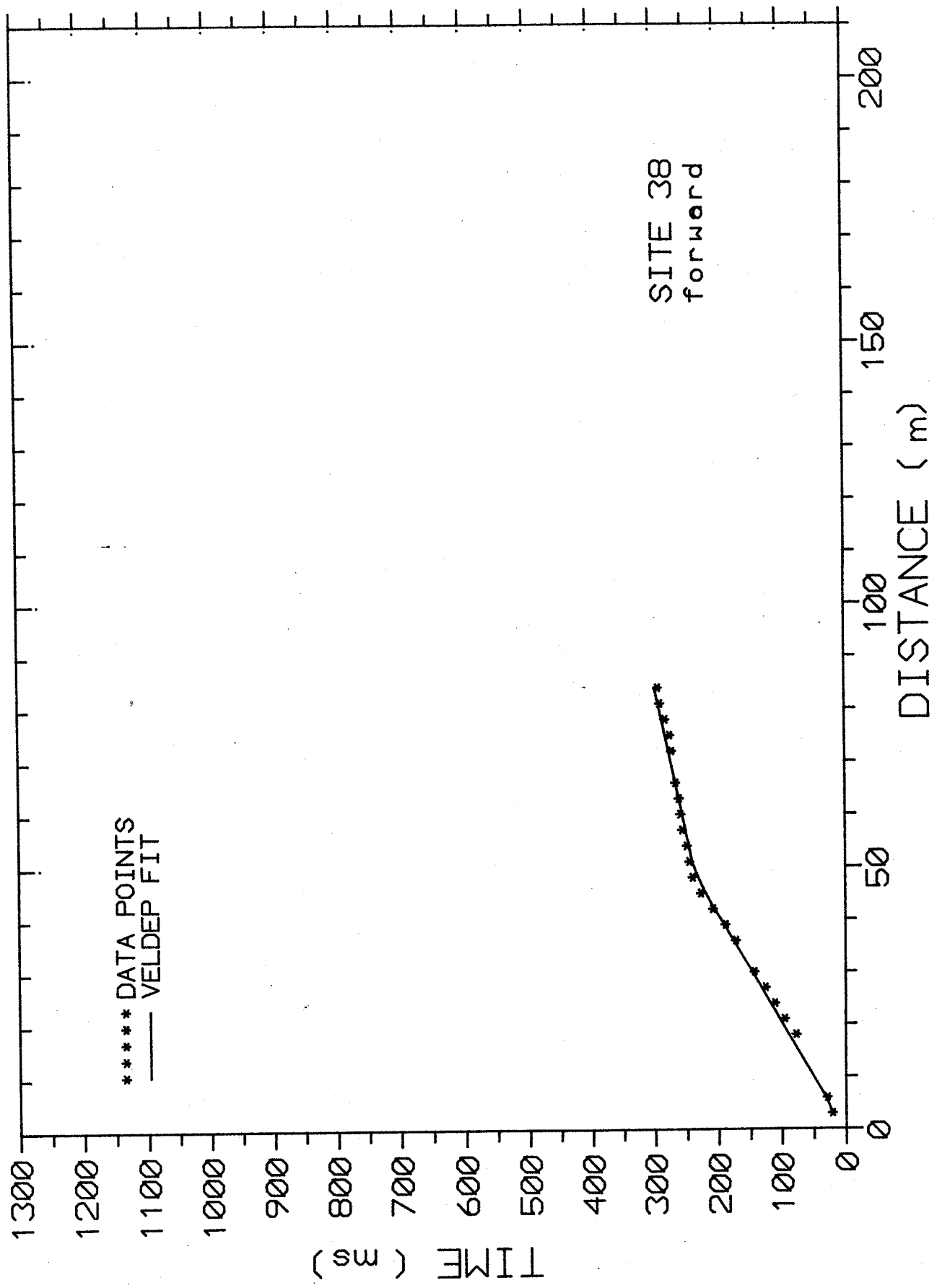
TIME (s)

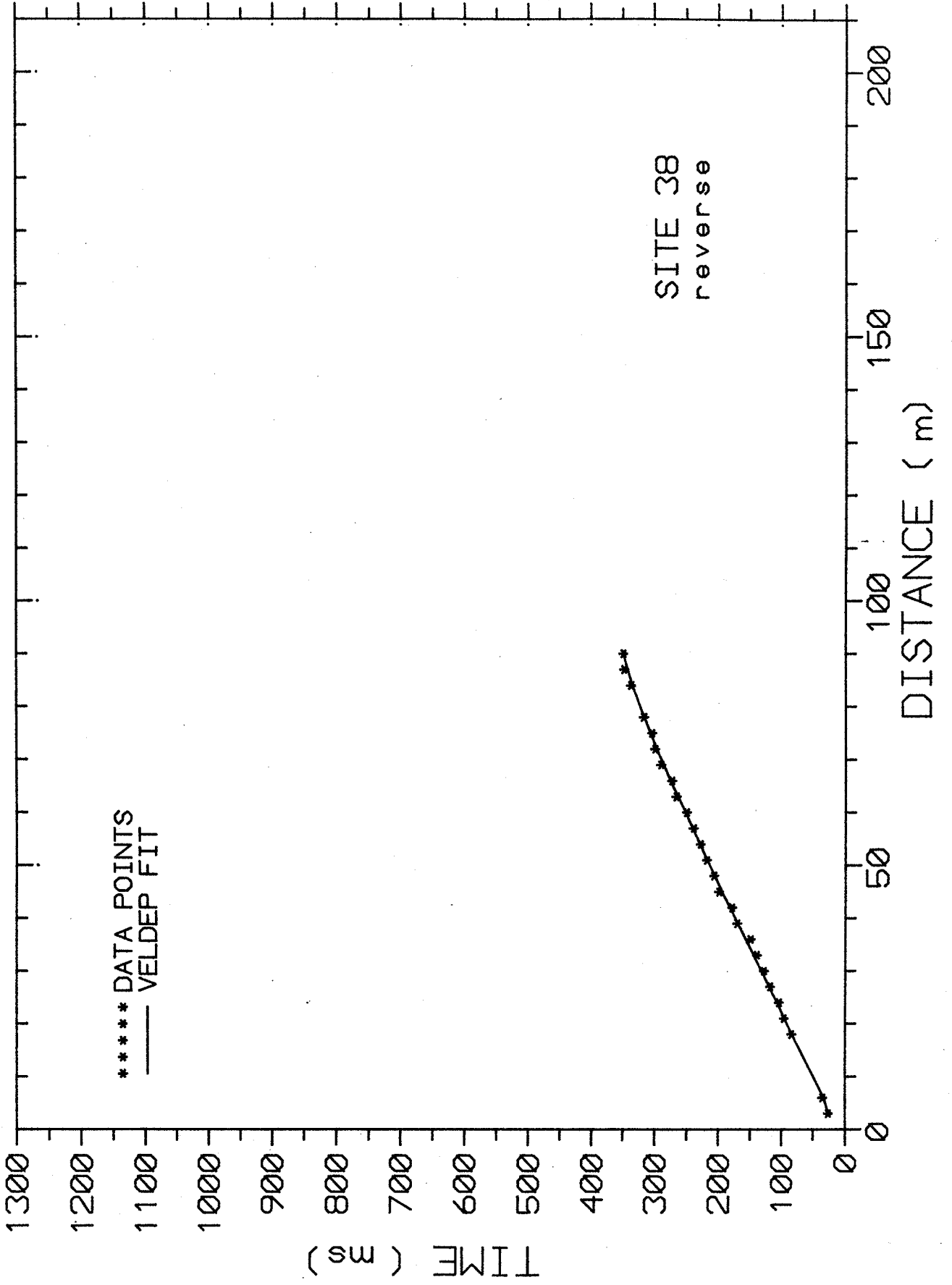
DISTANCE (m)

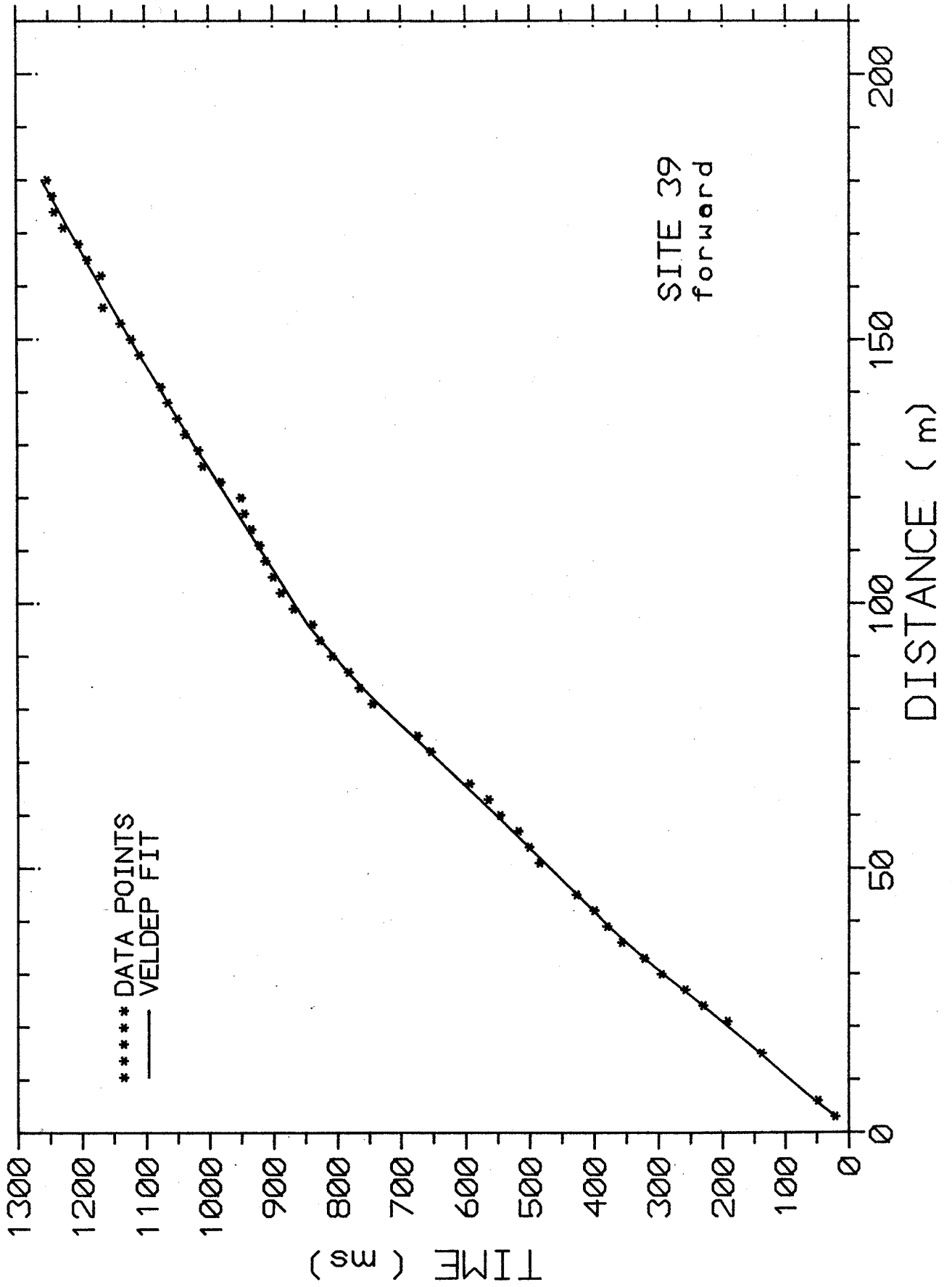


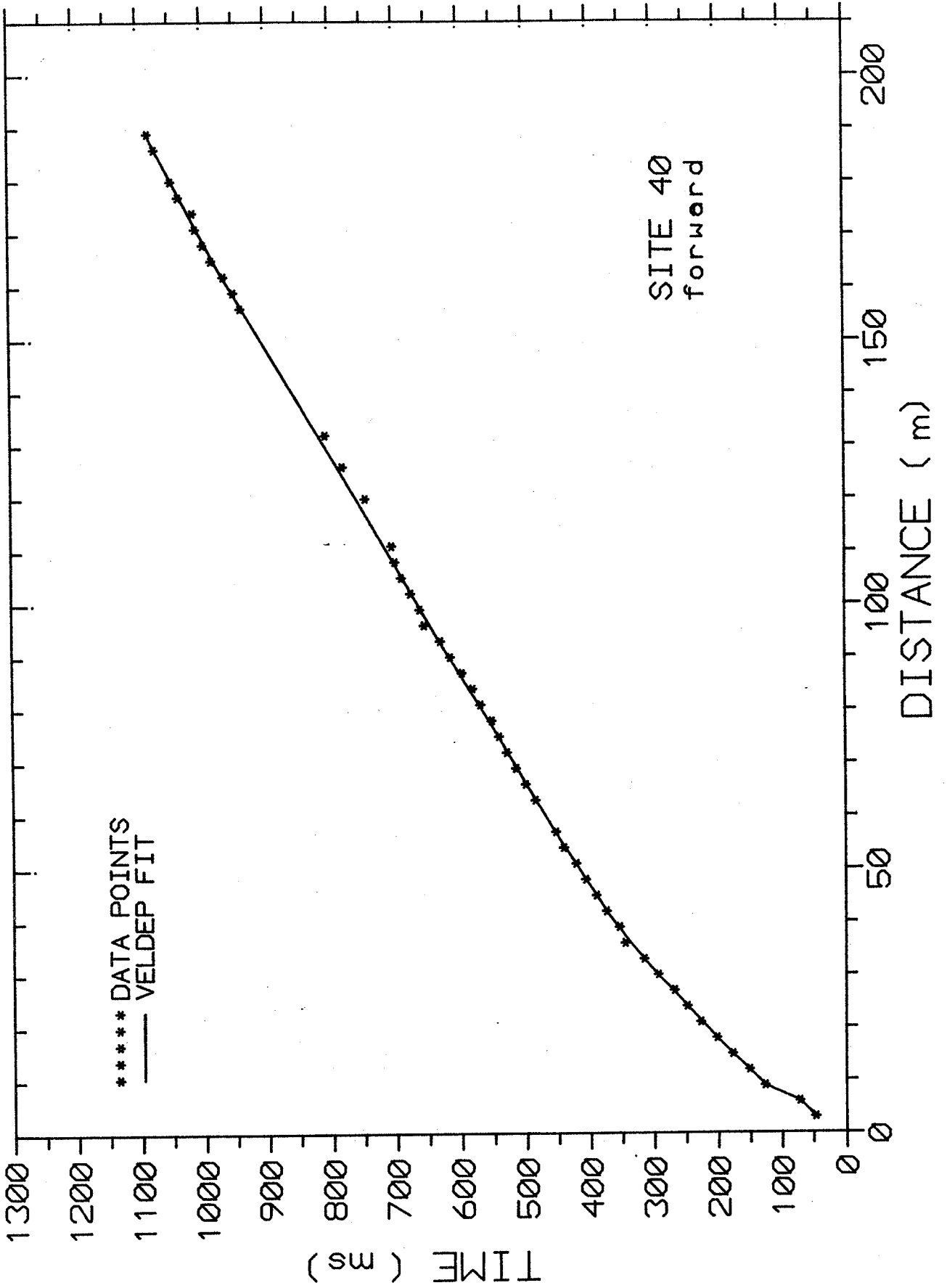


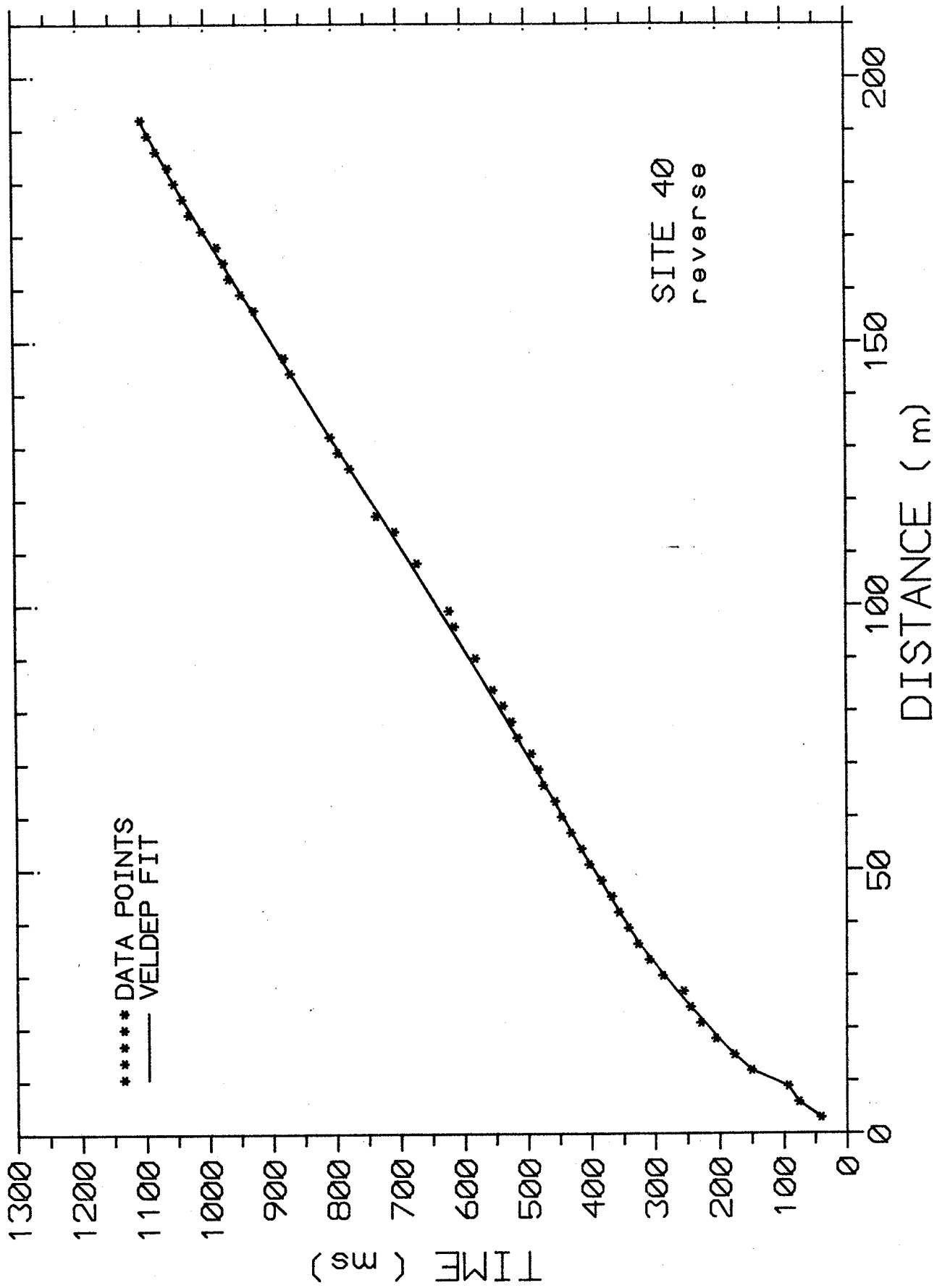


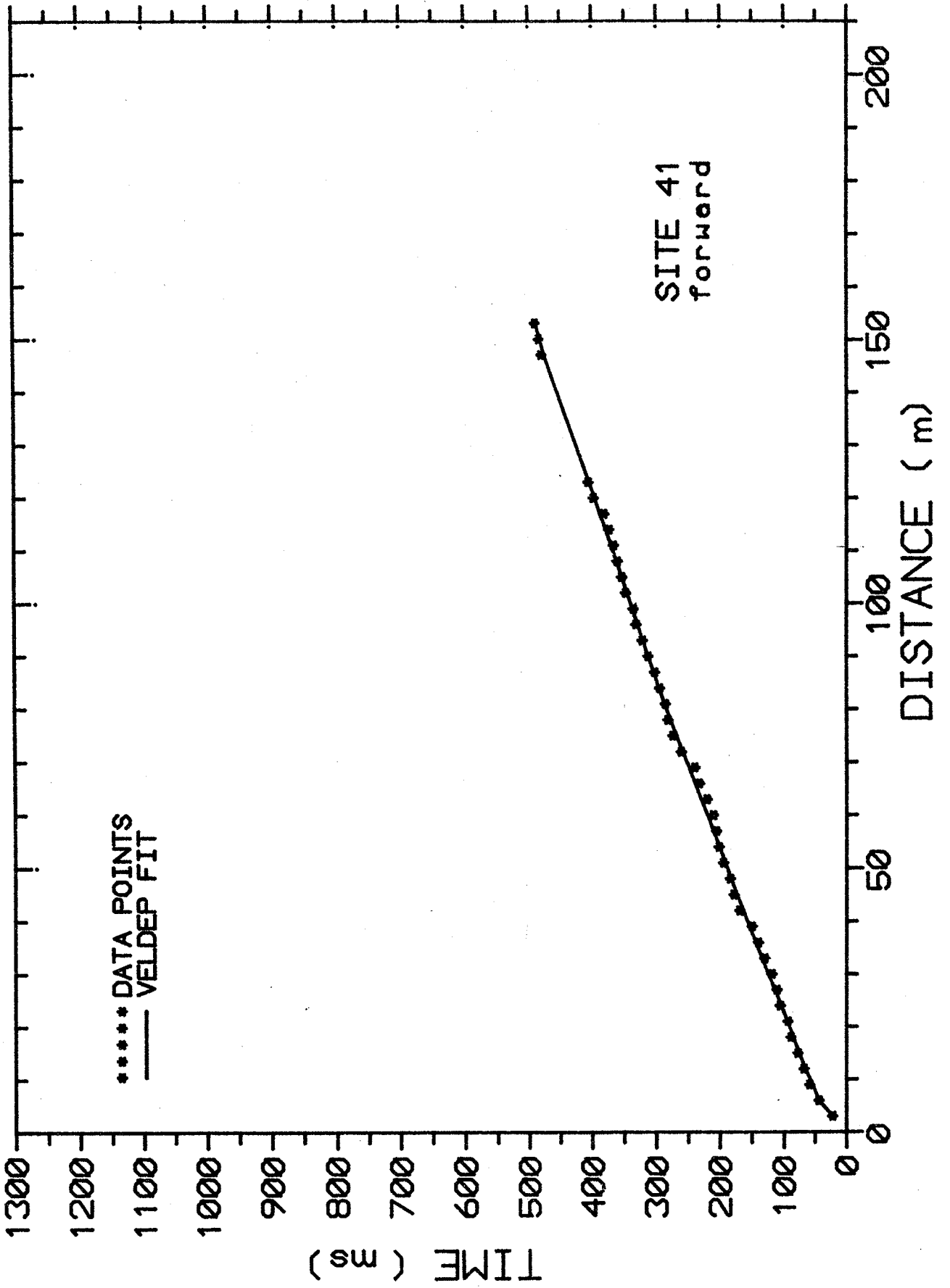


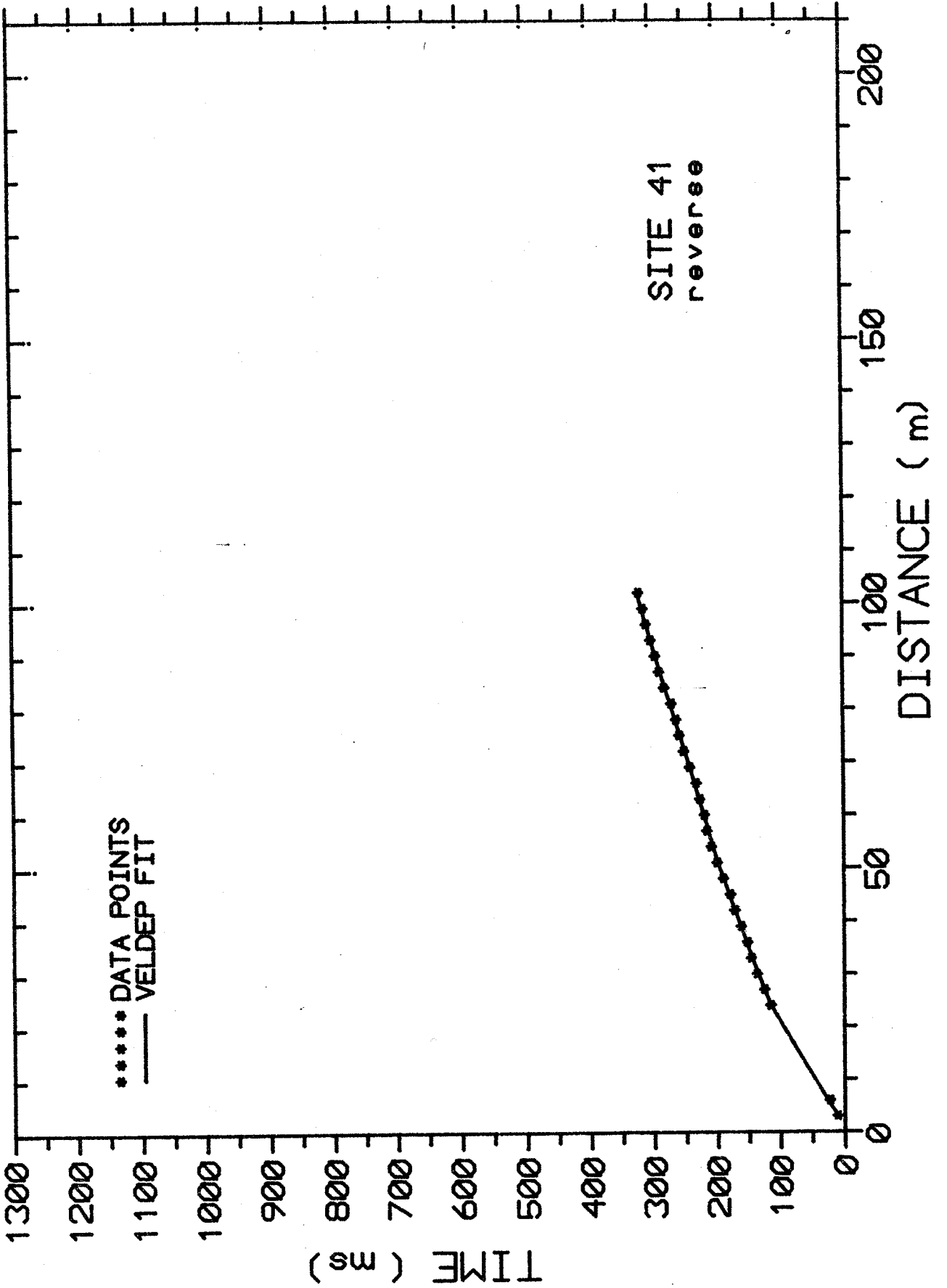


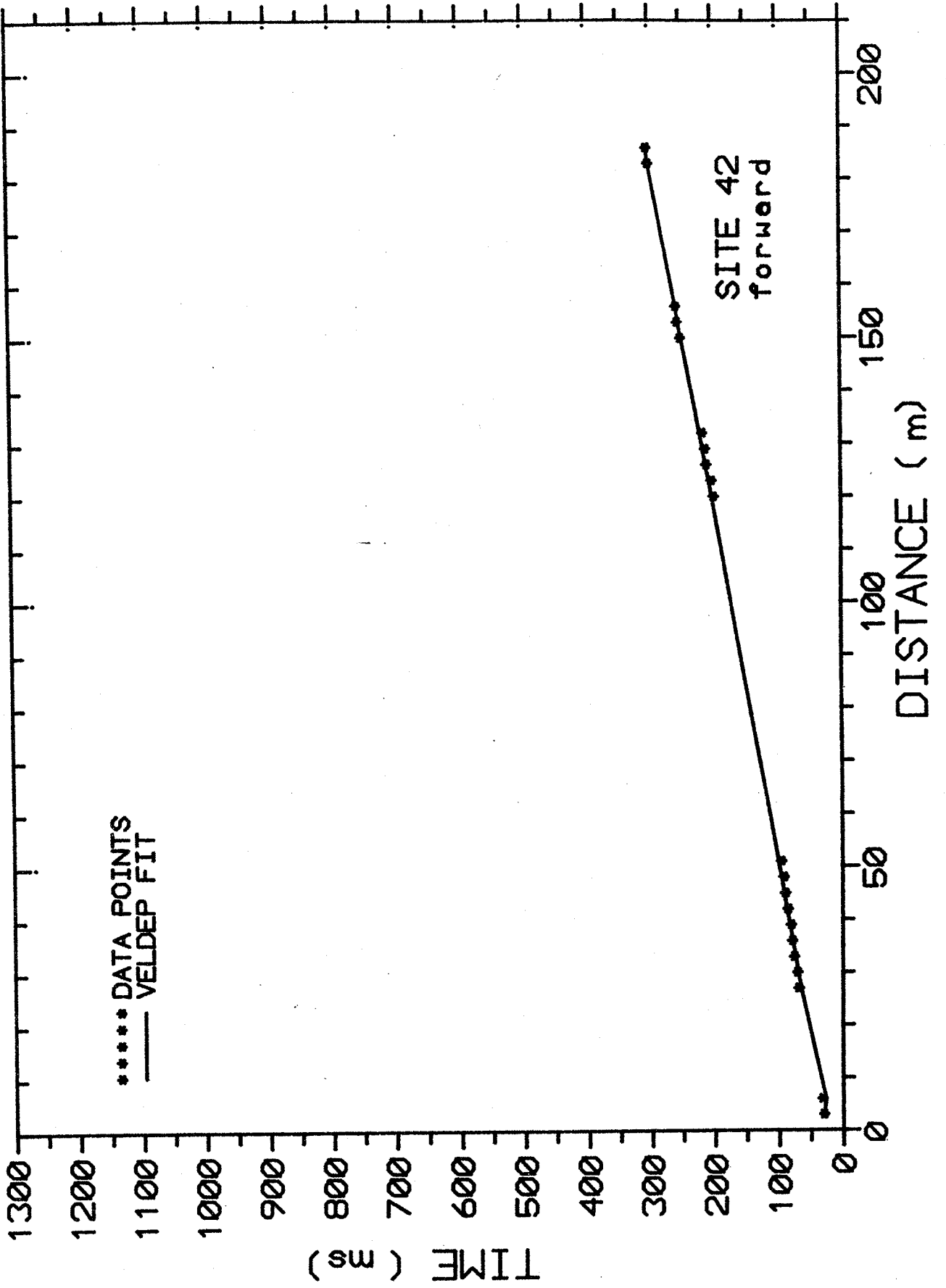


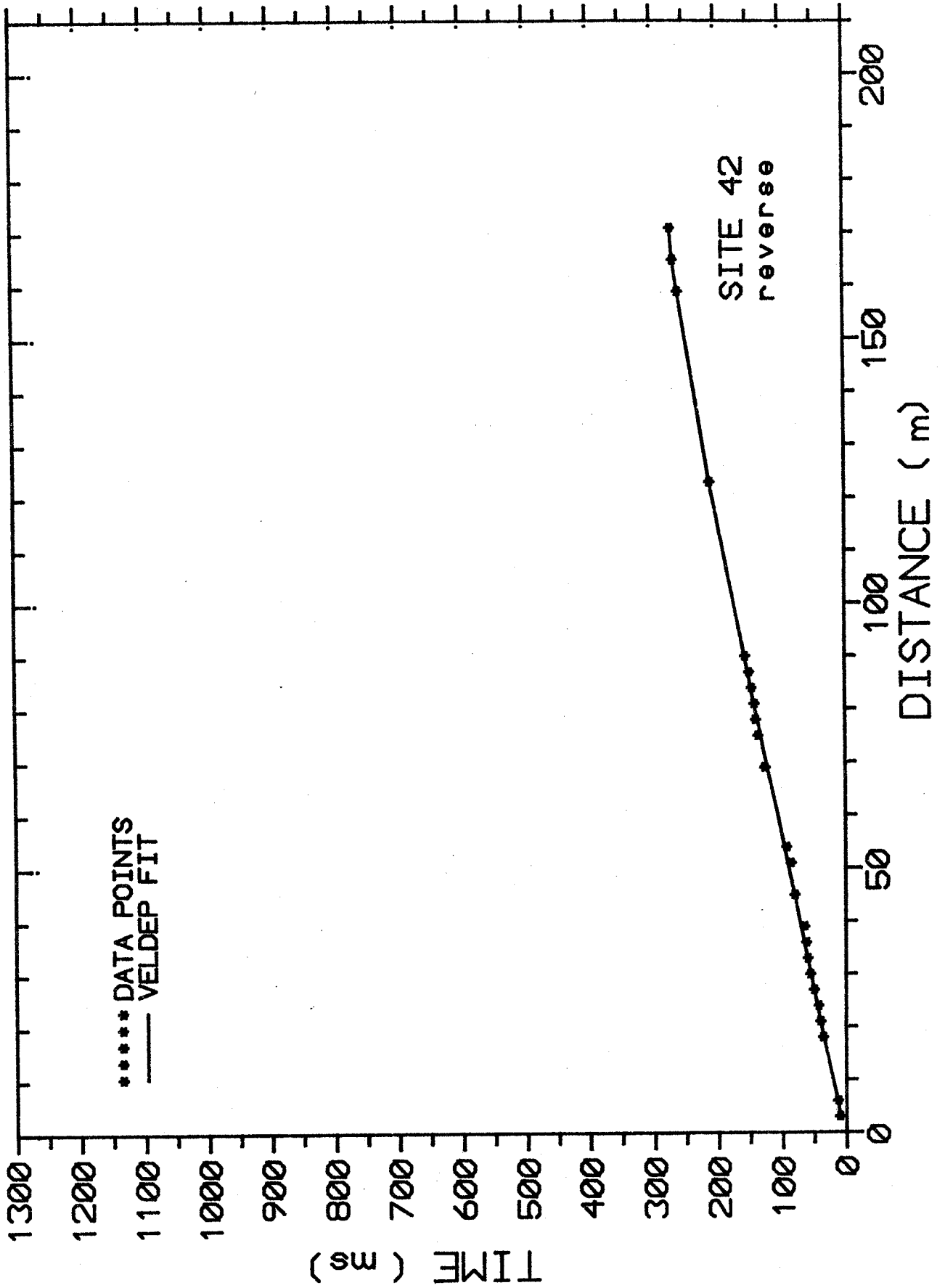


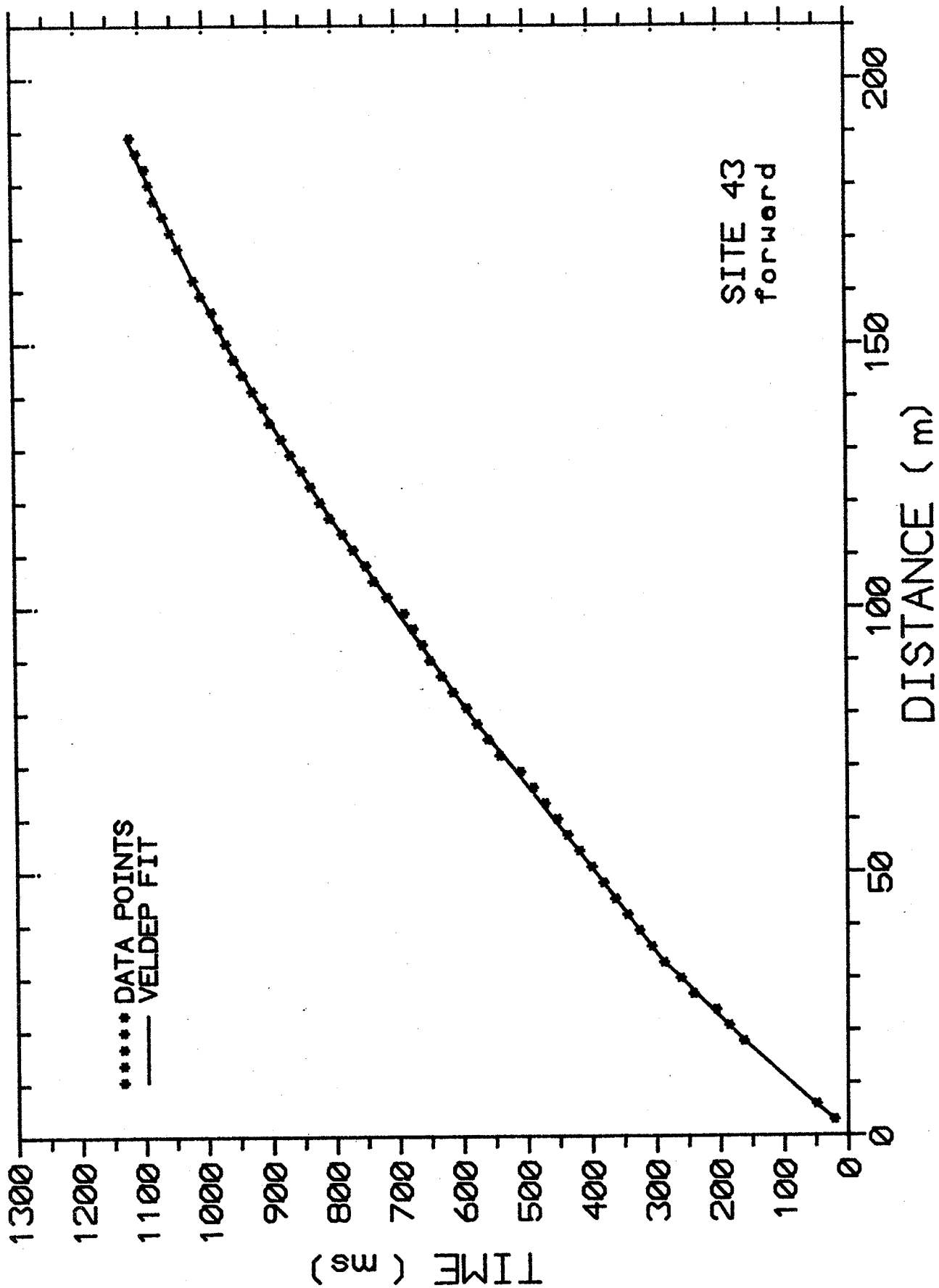


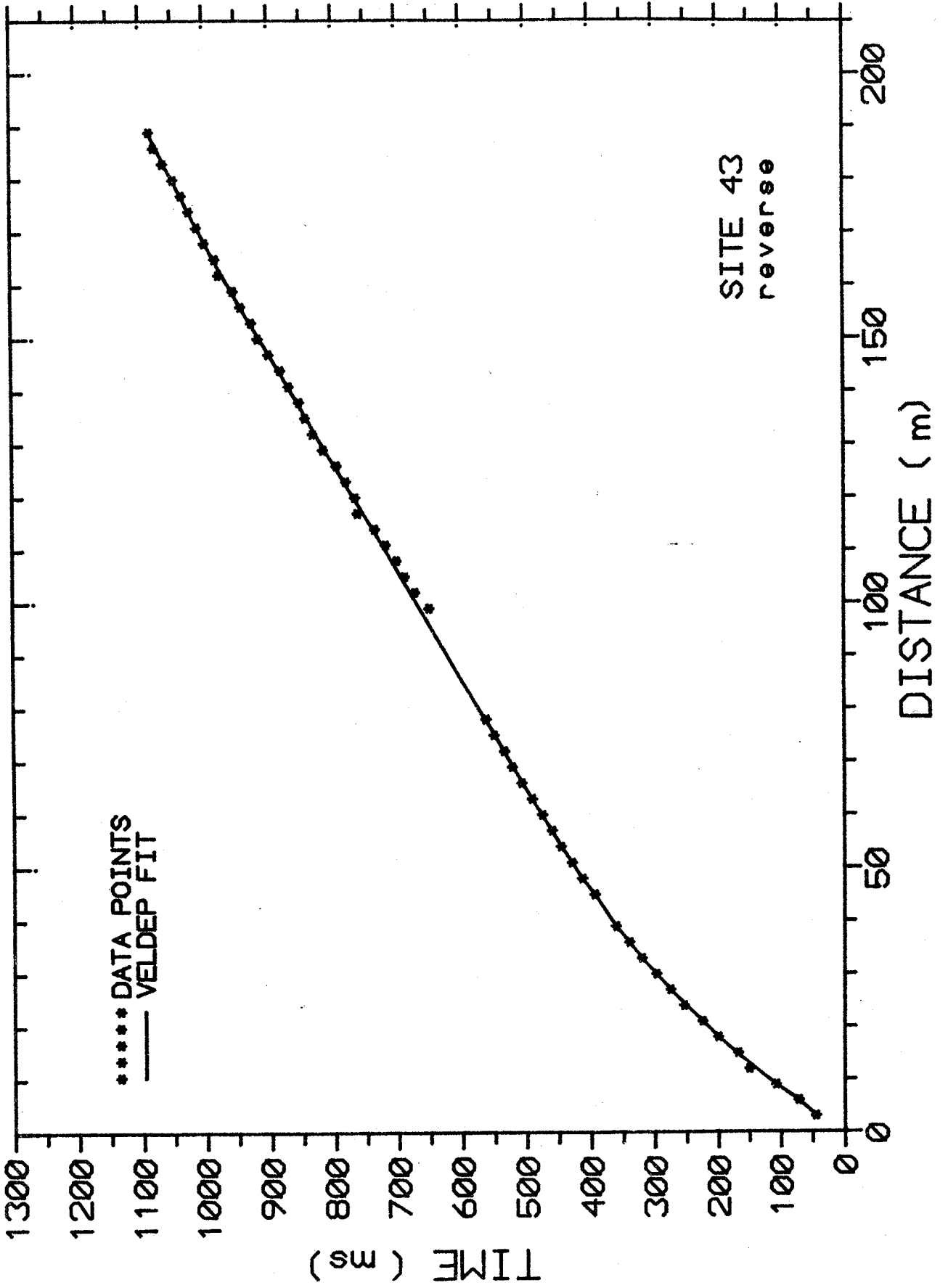






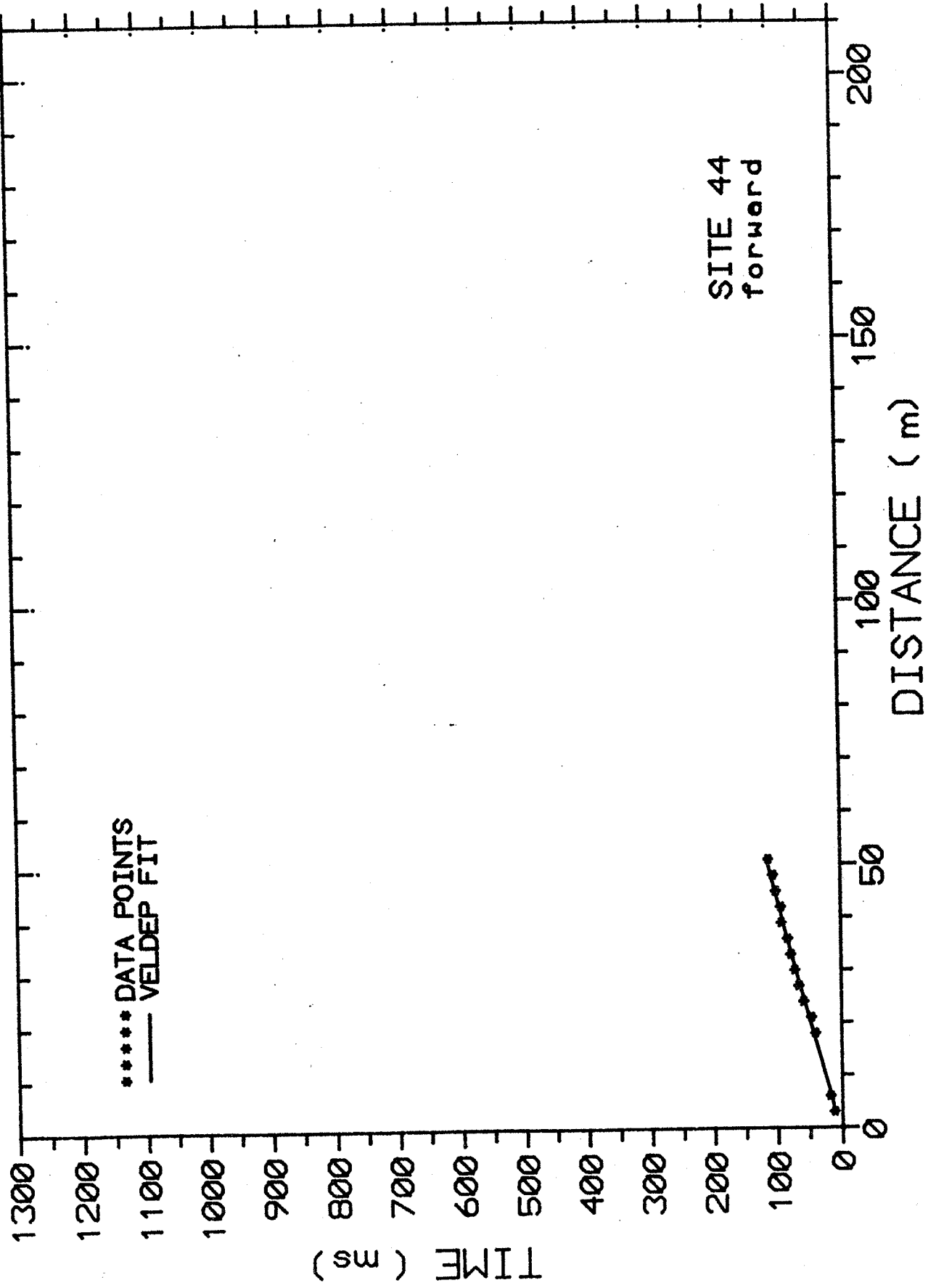


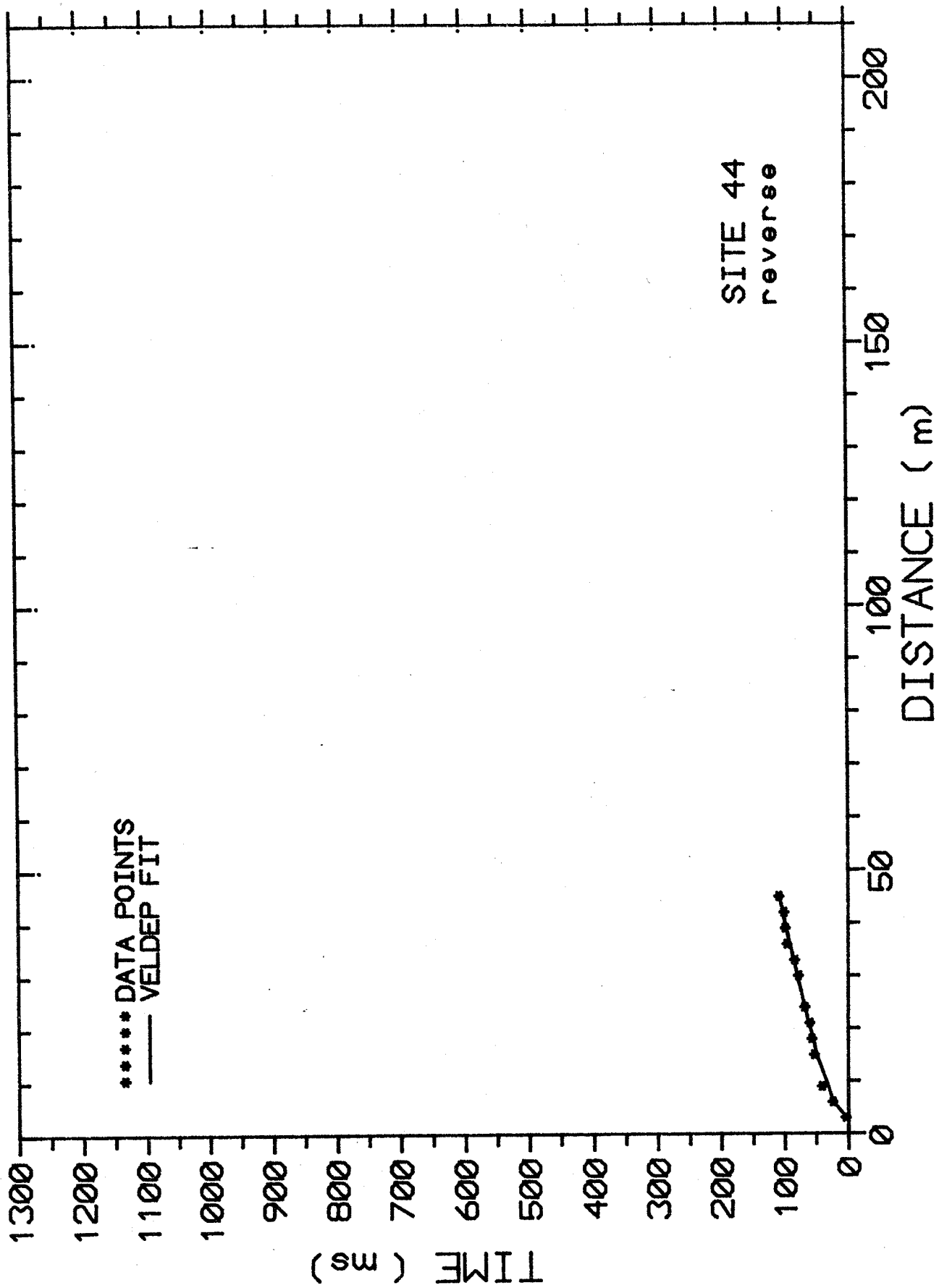


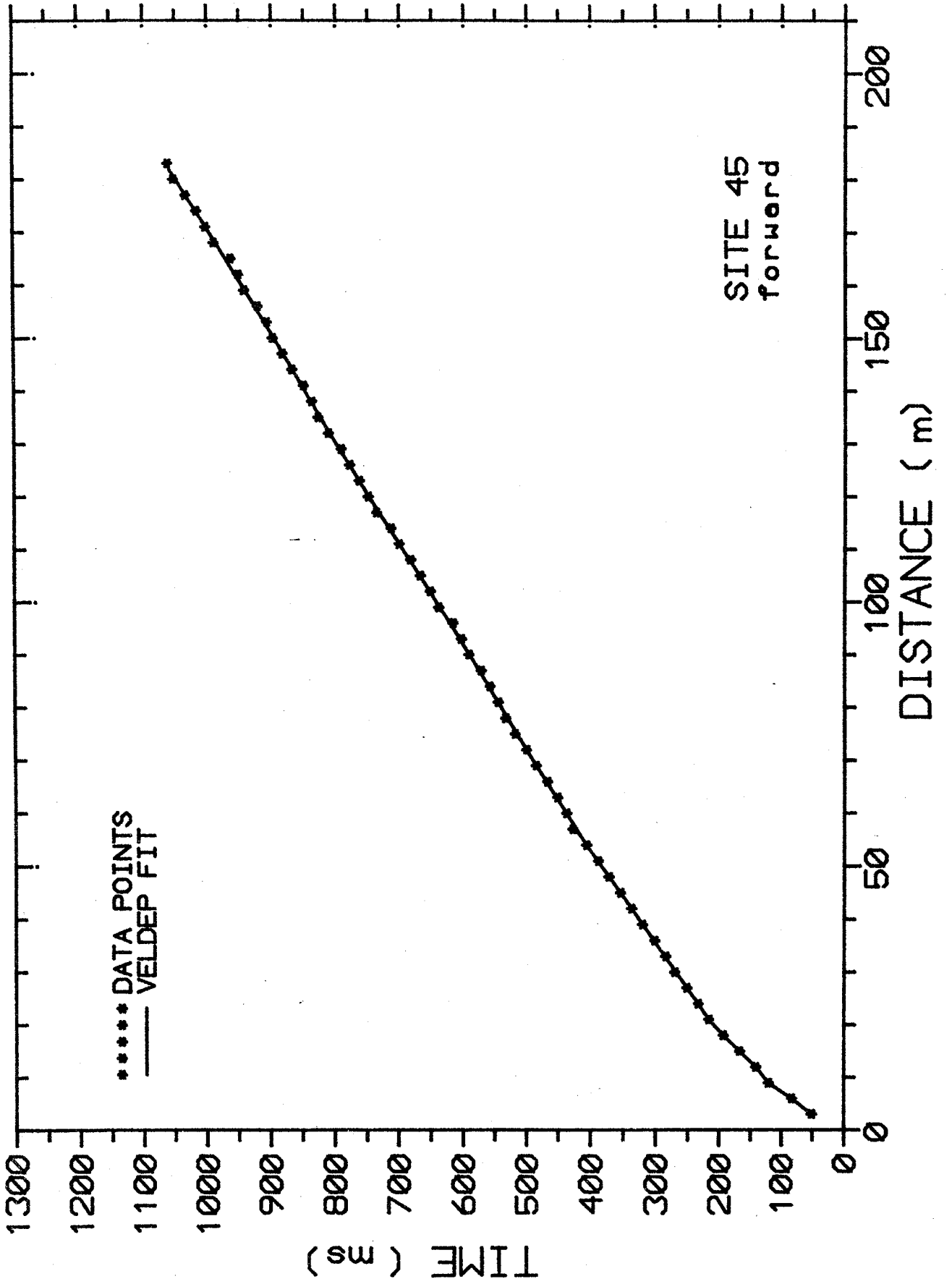


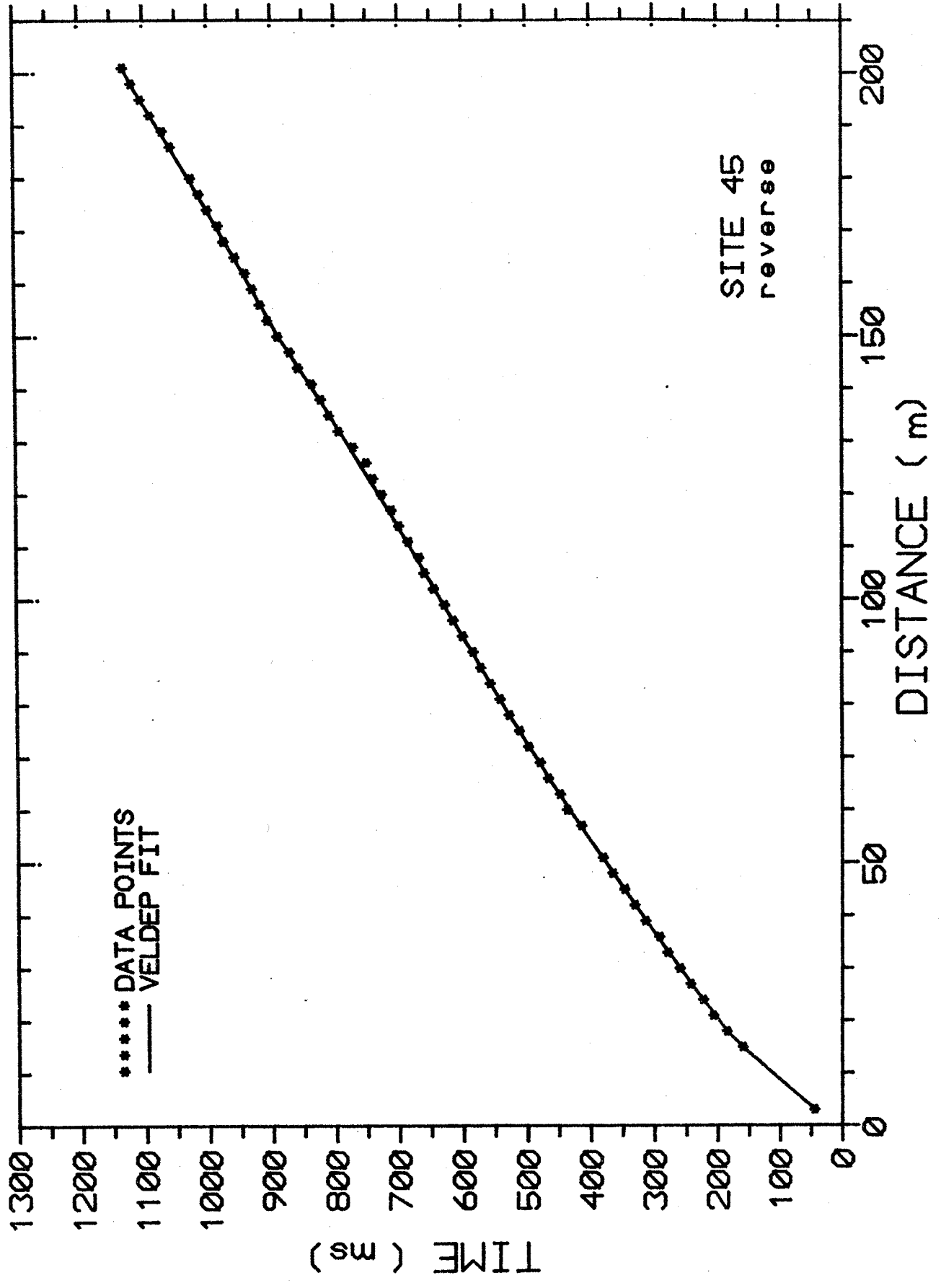
***** DATA POINTS
—— VELDEP FIT

SITE 43
reverse







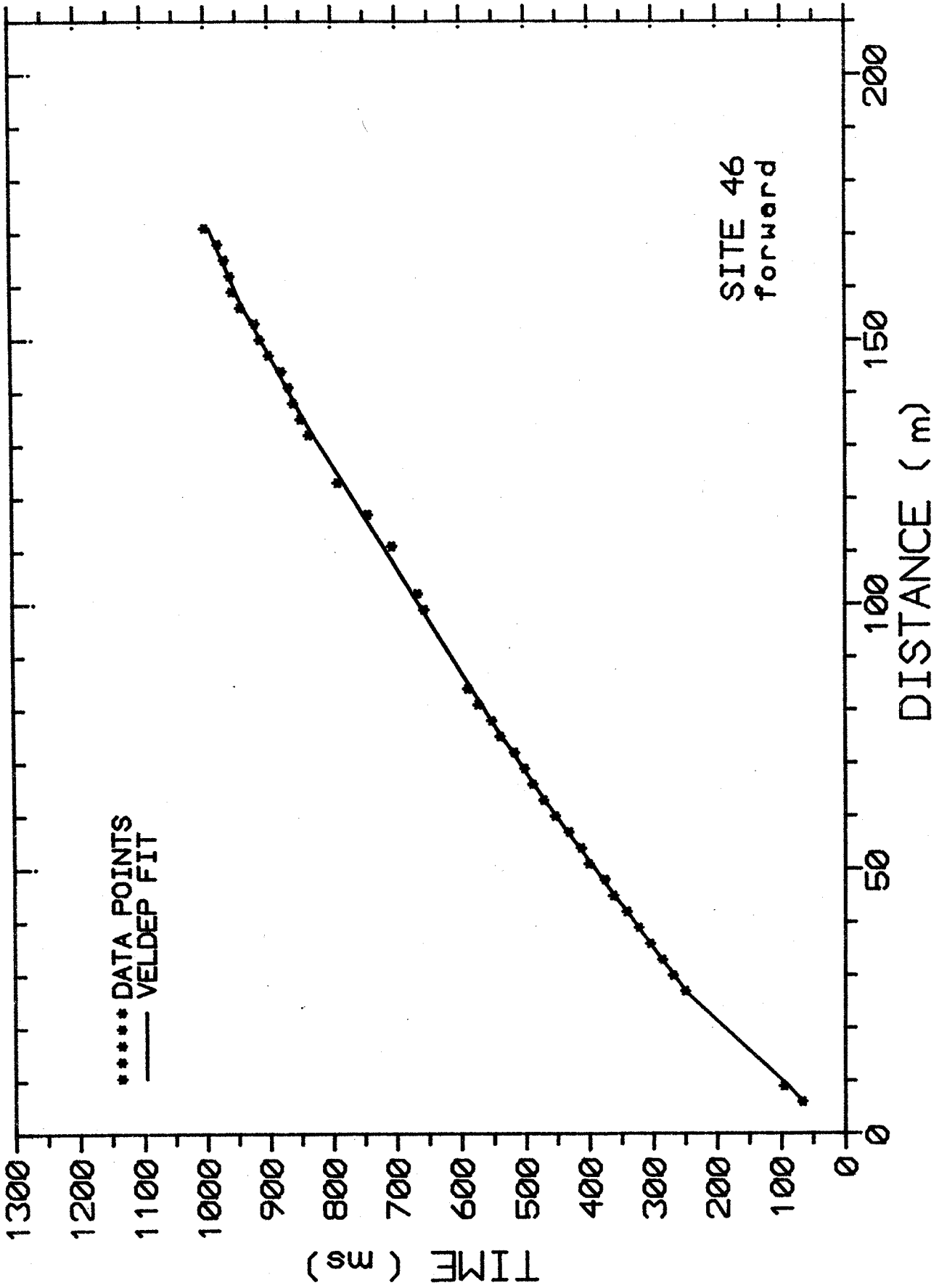


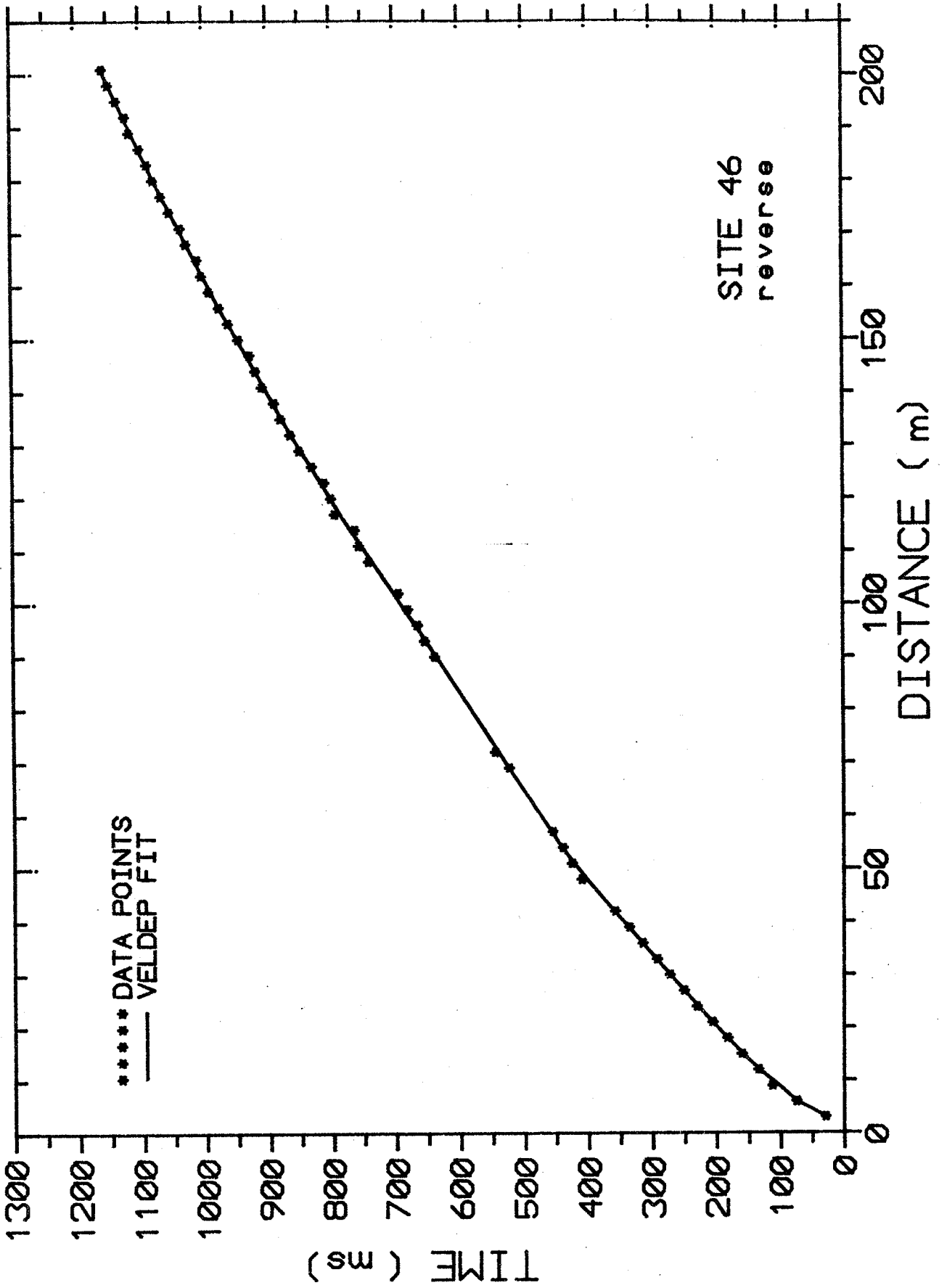
***** DATA POINTS
—— VELDEP FIT

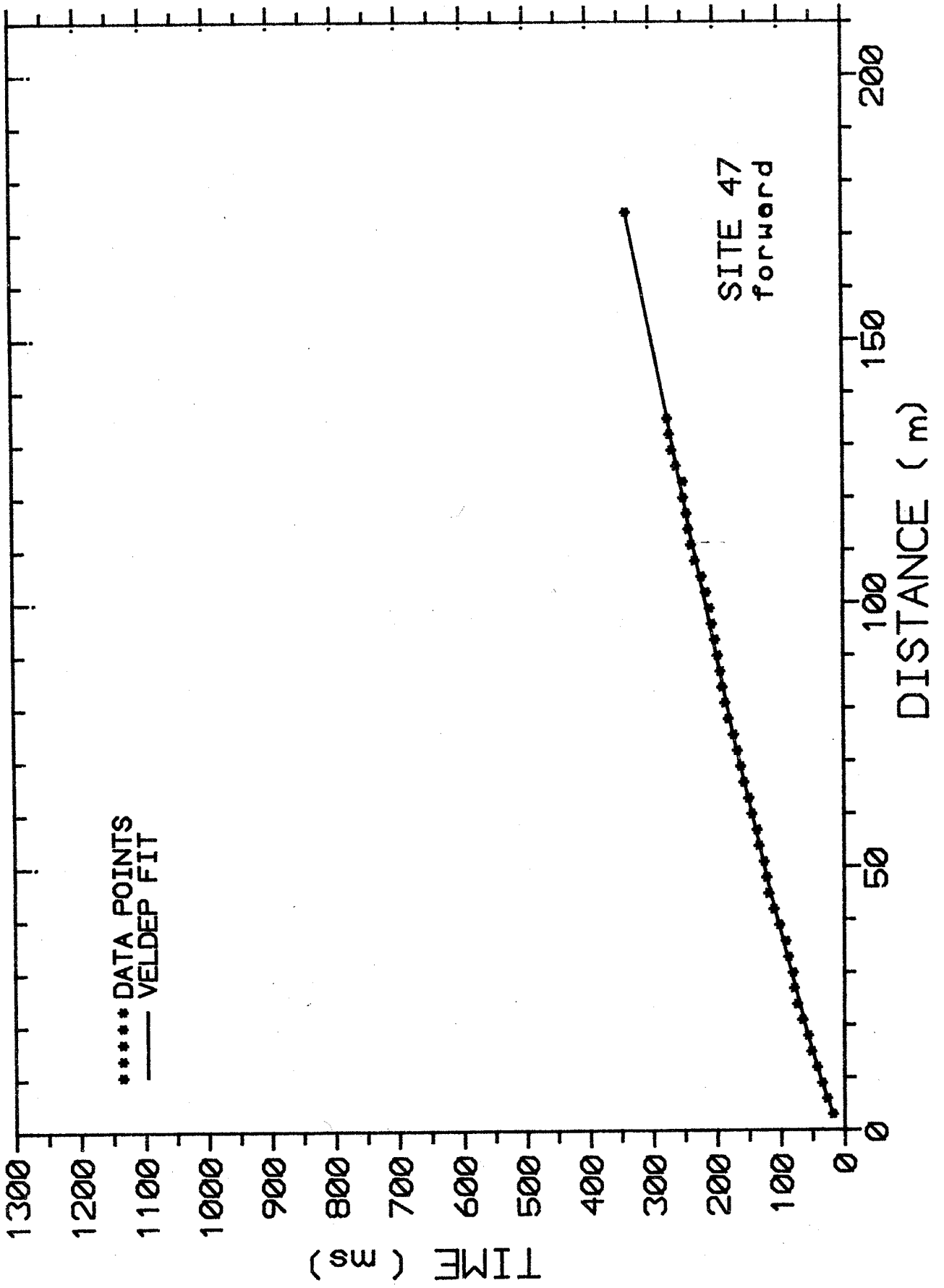
SITE 45
reverse

TIME (ms)

DISTANCE (m)

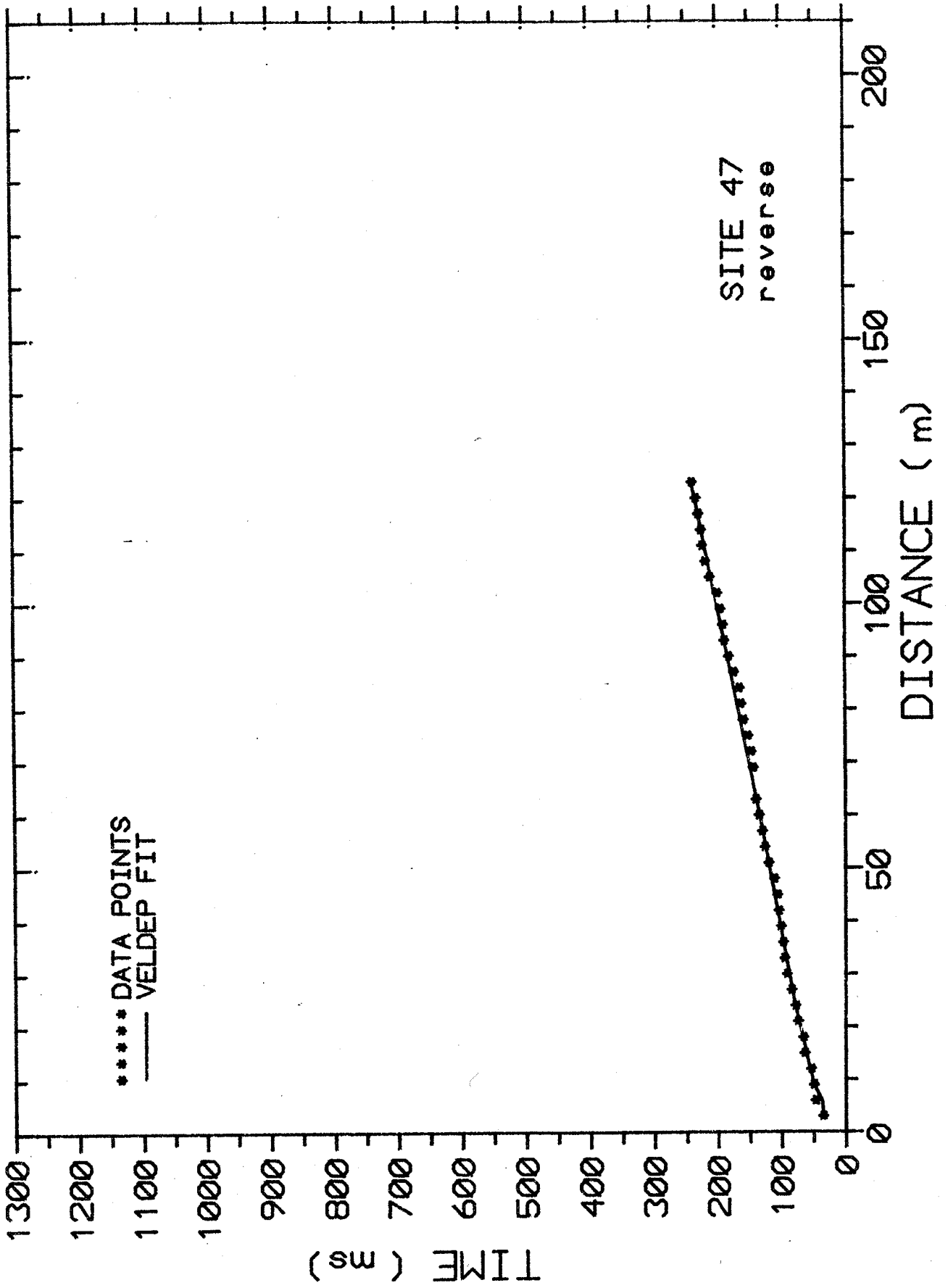


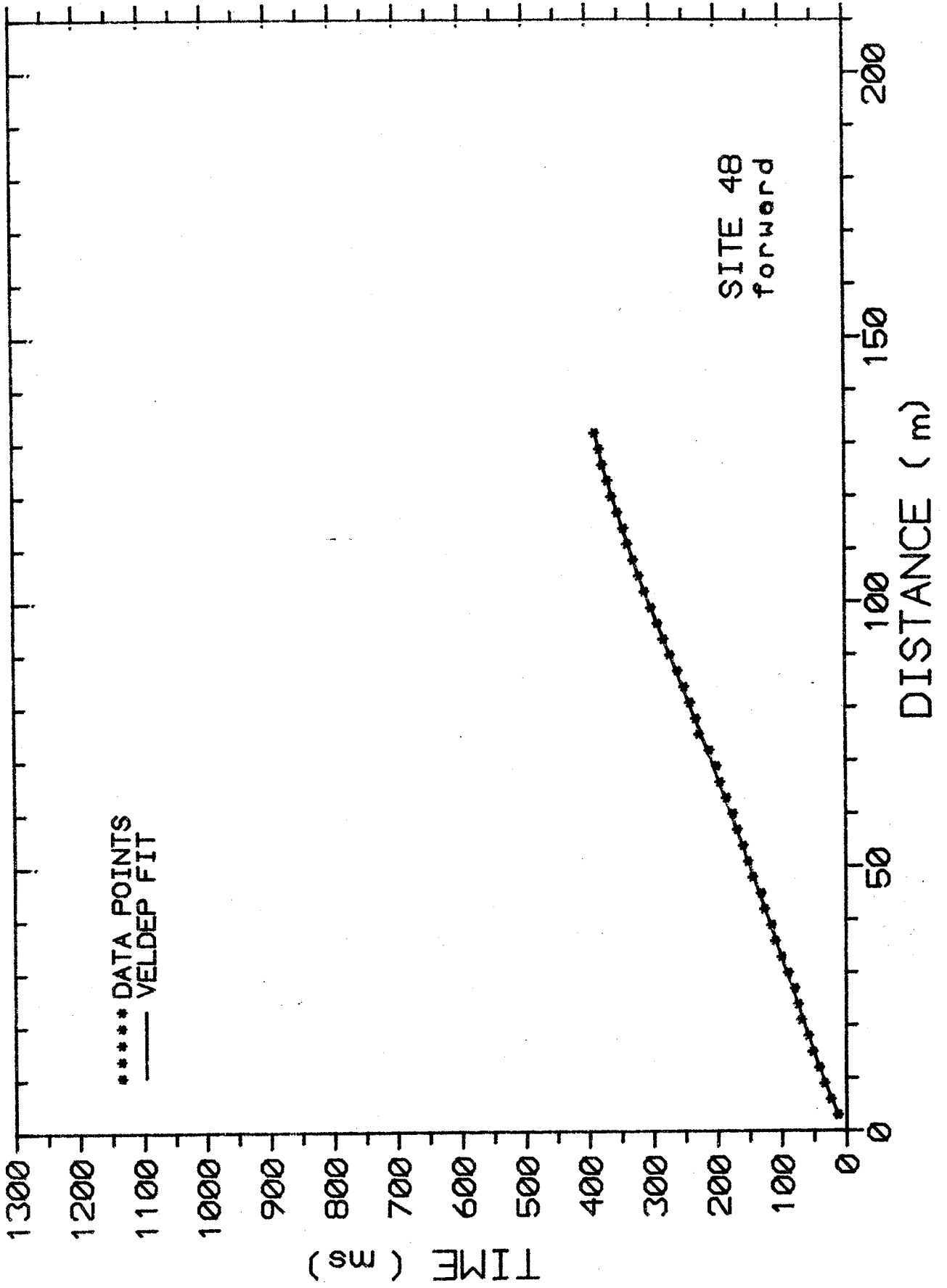


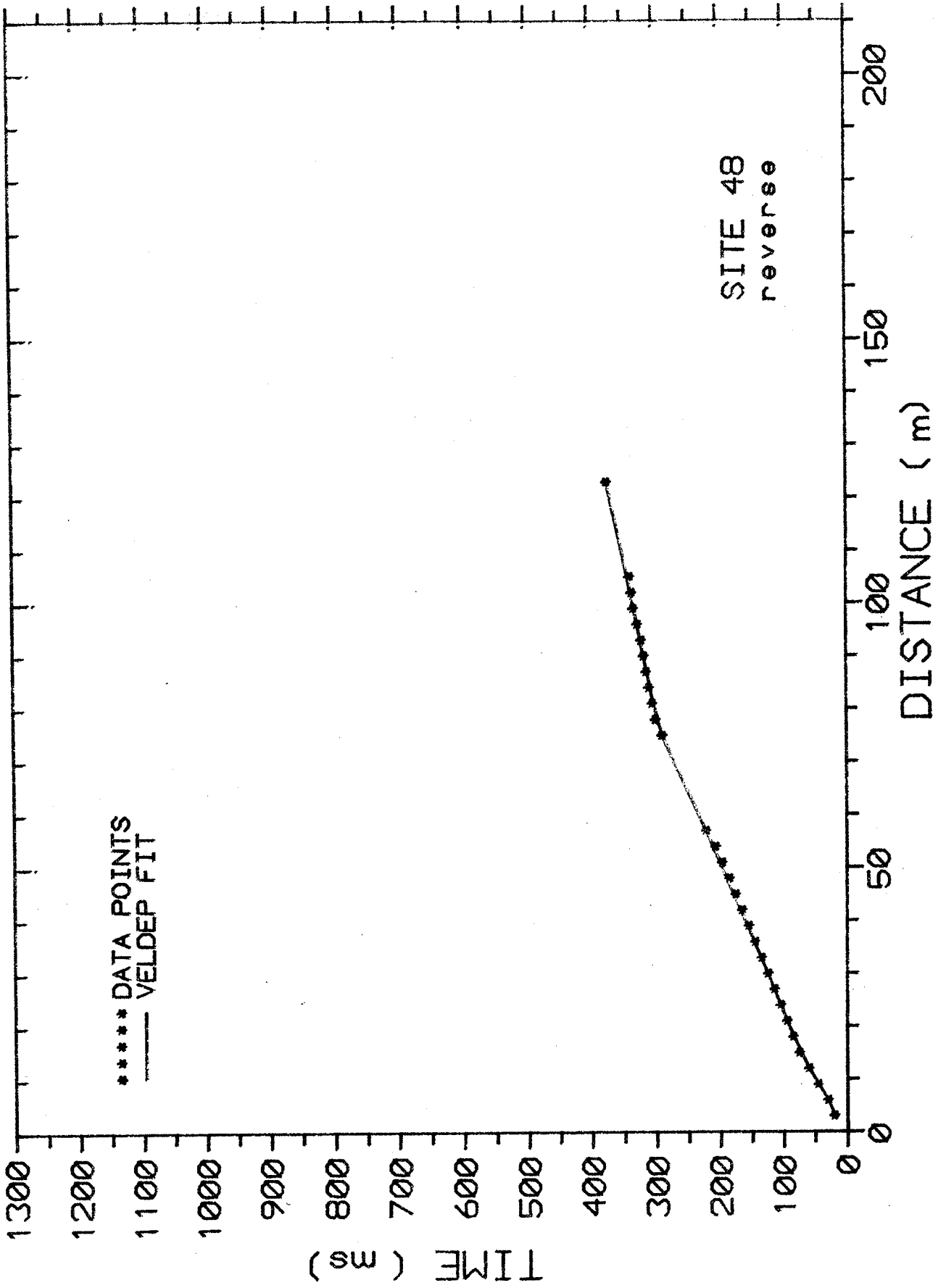


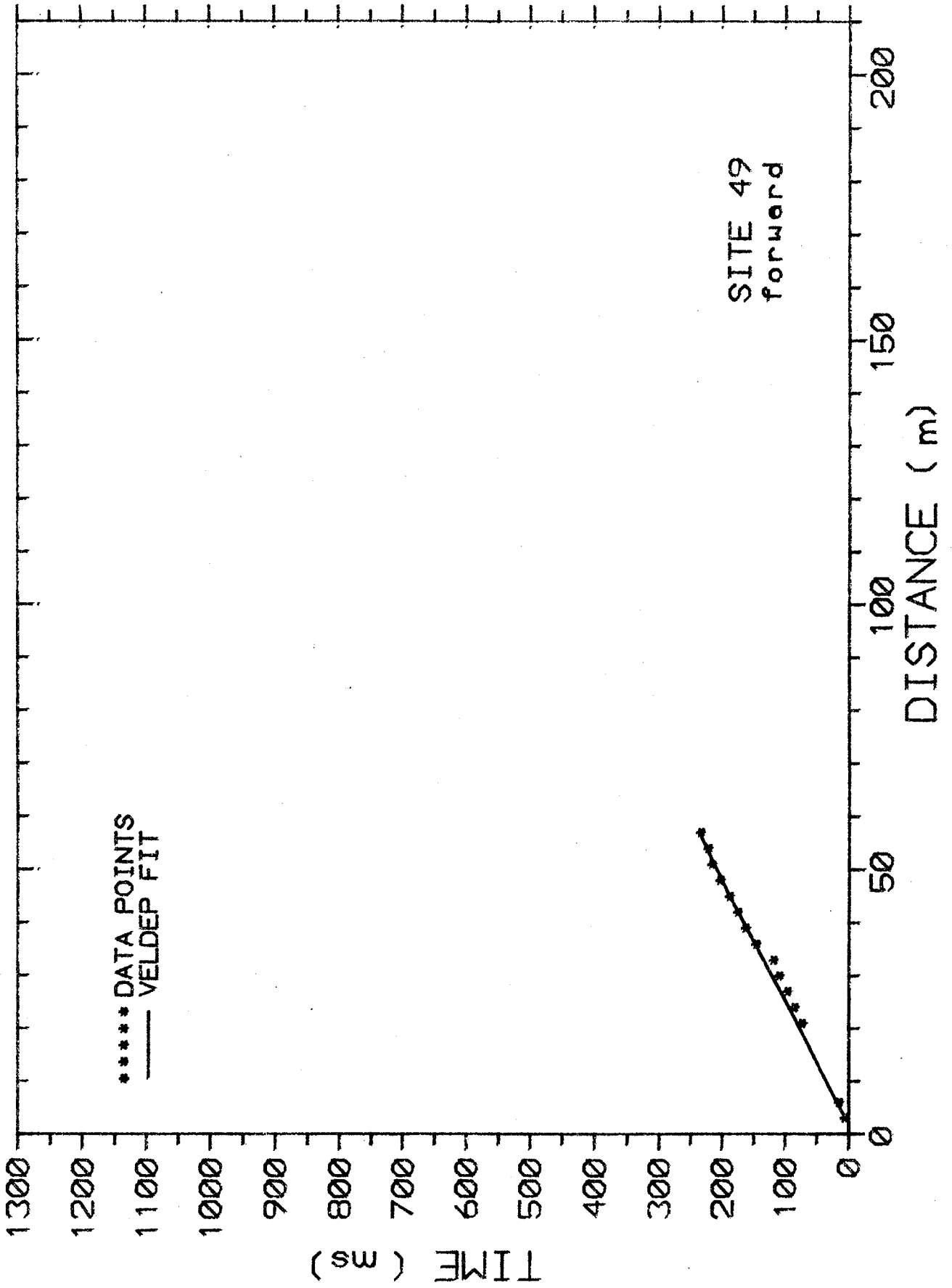
***** DATA POINTS
—— VELDEP FIT

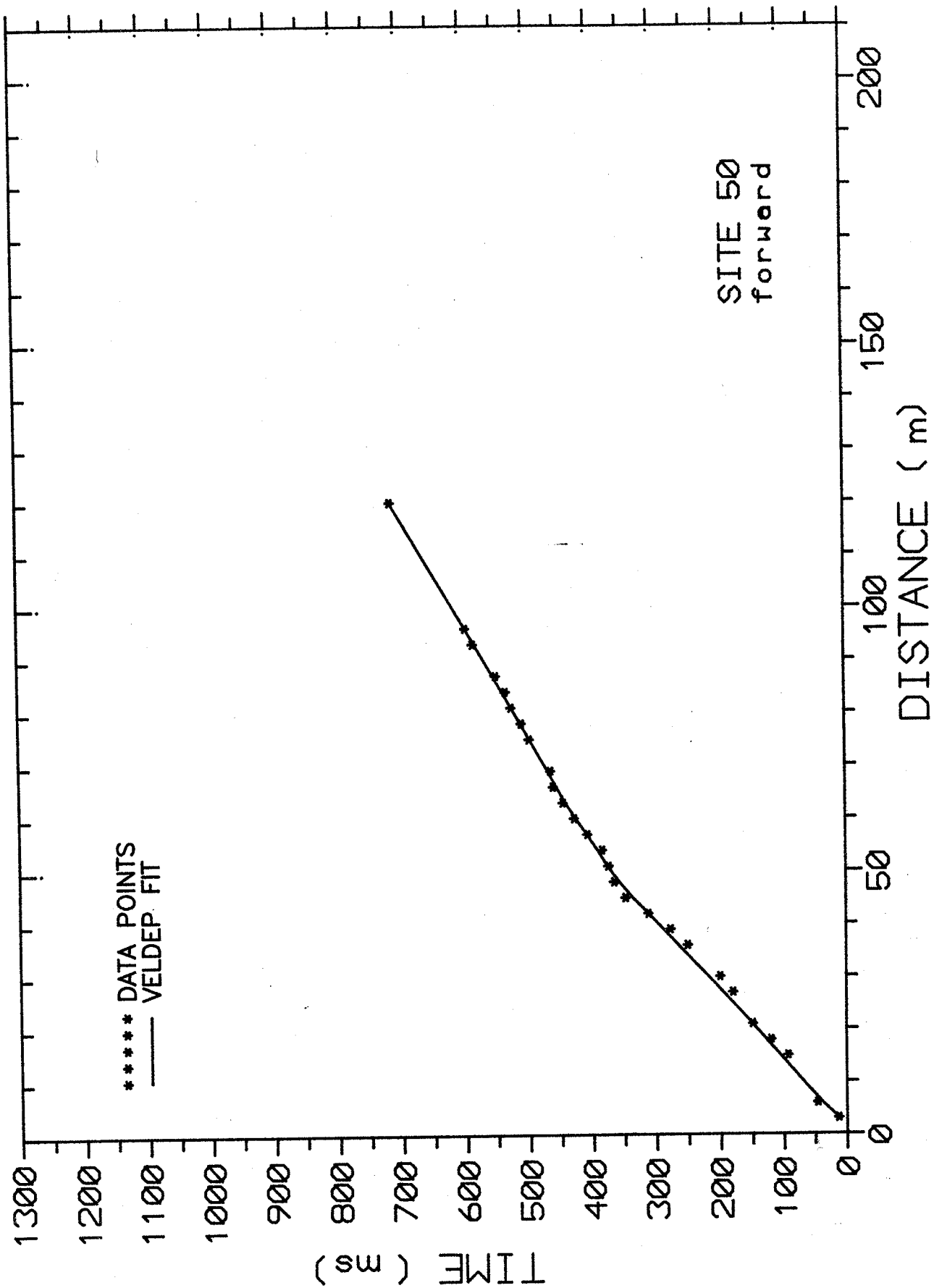
SITE 47
forward

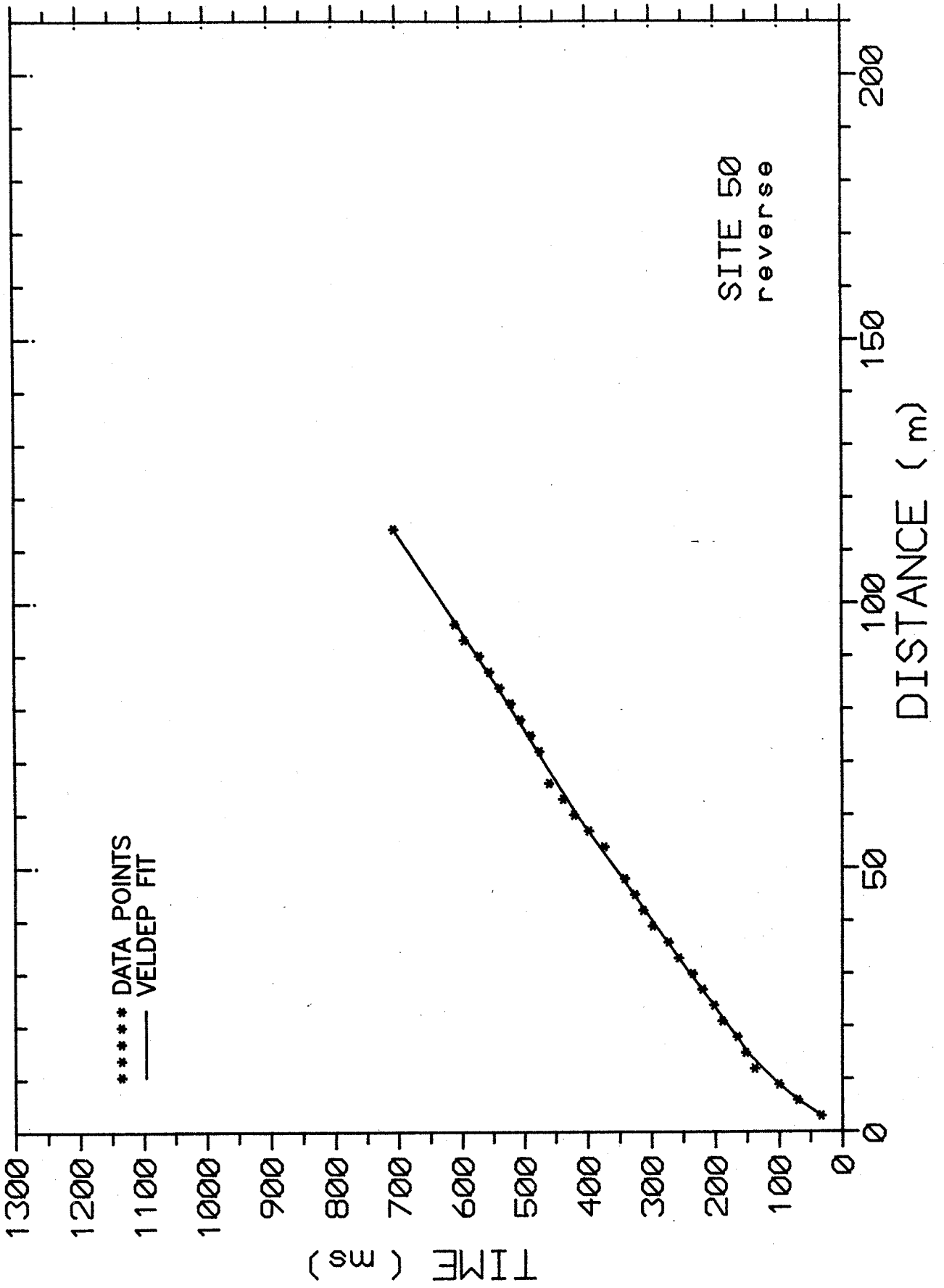


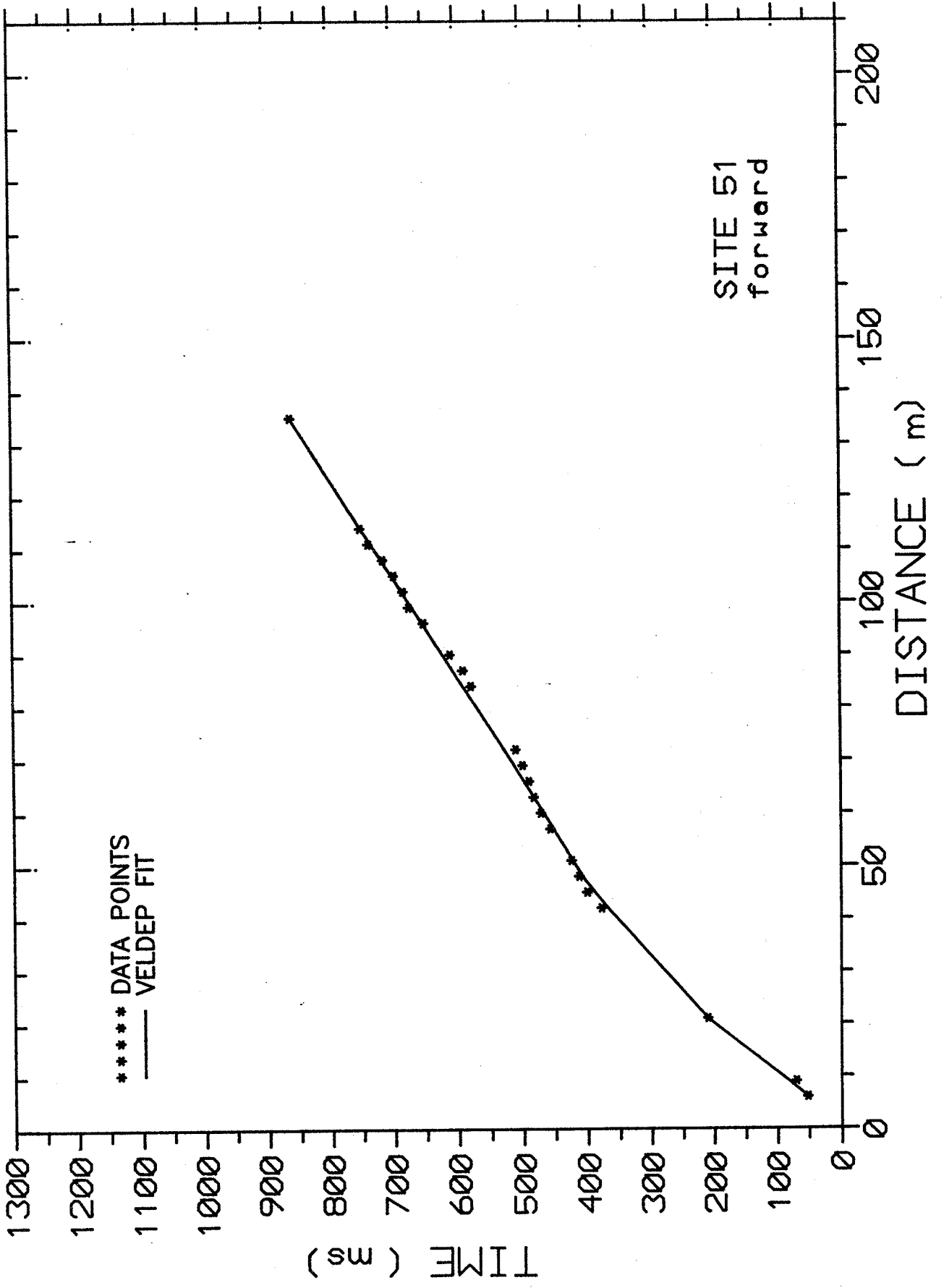


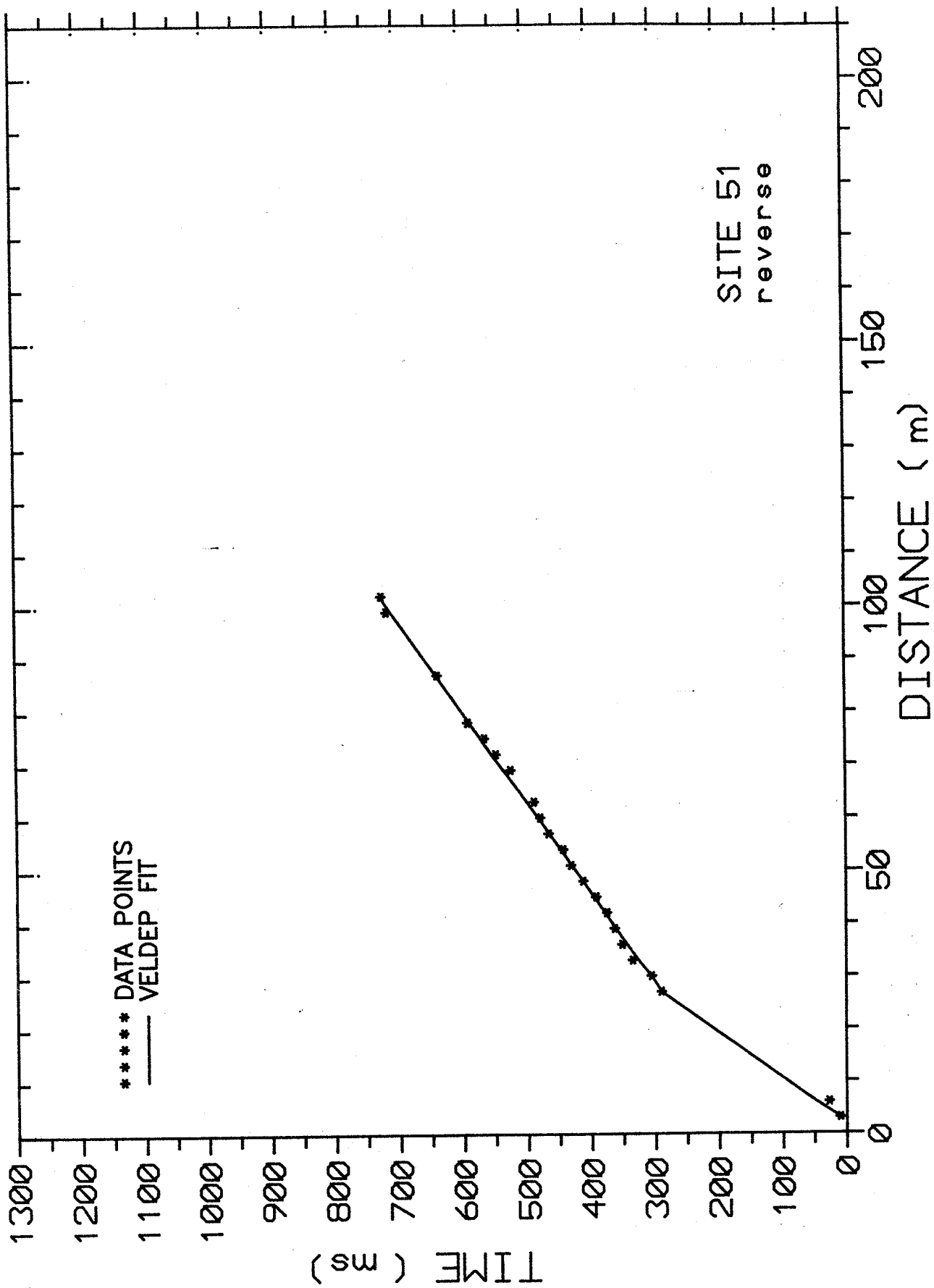


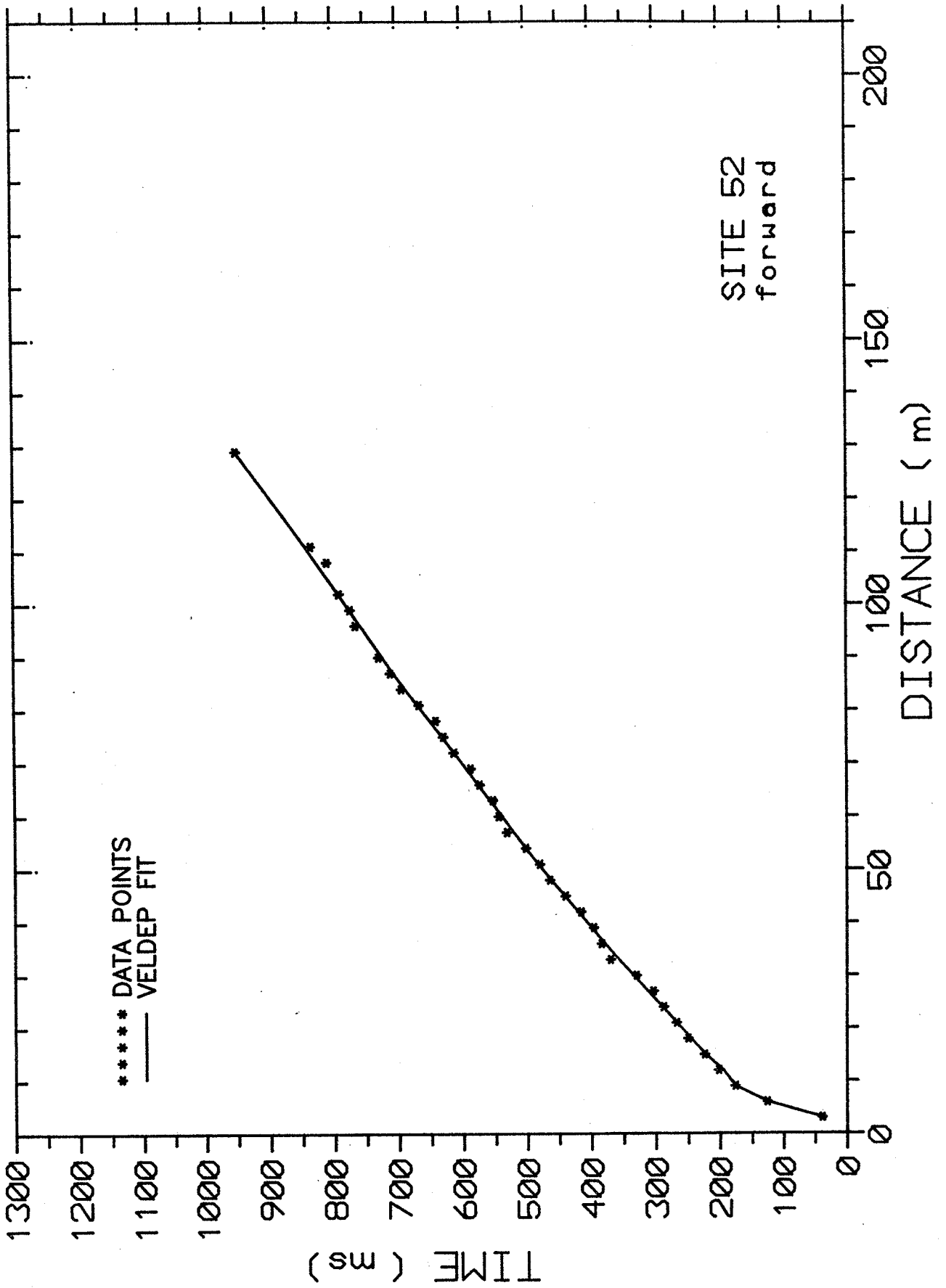


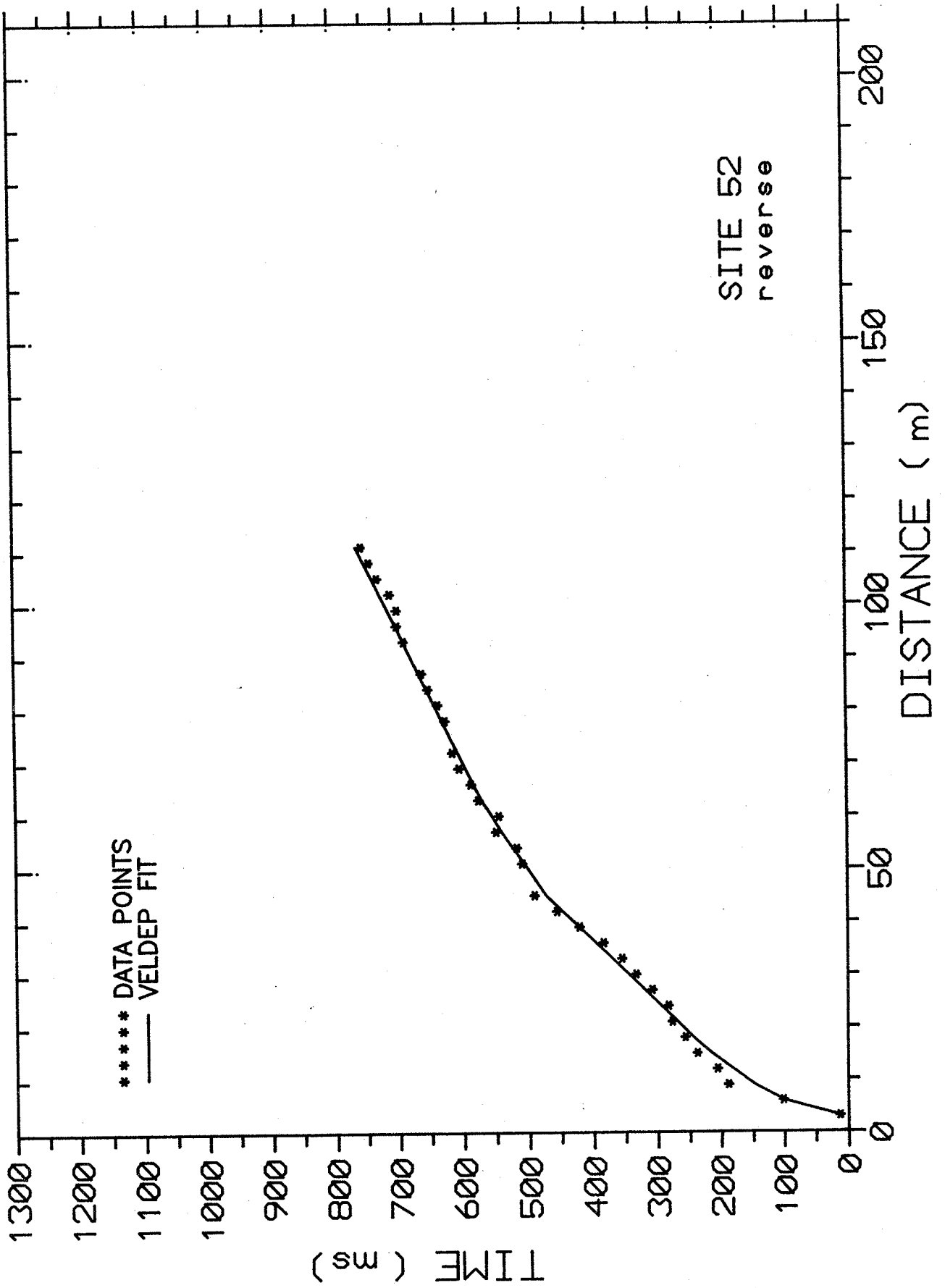


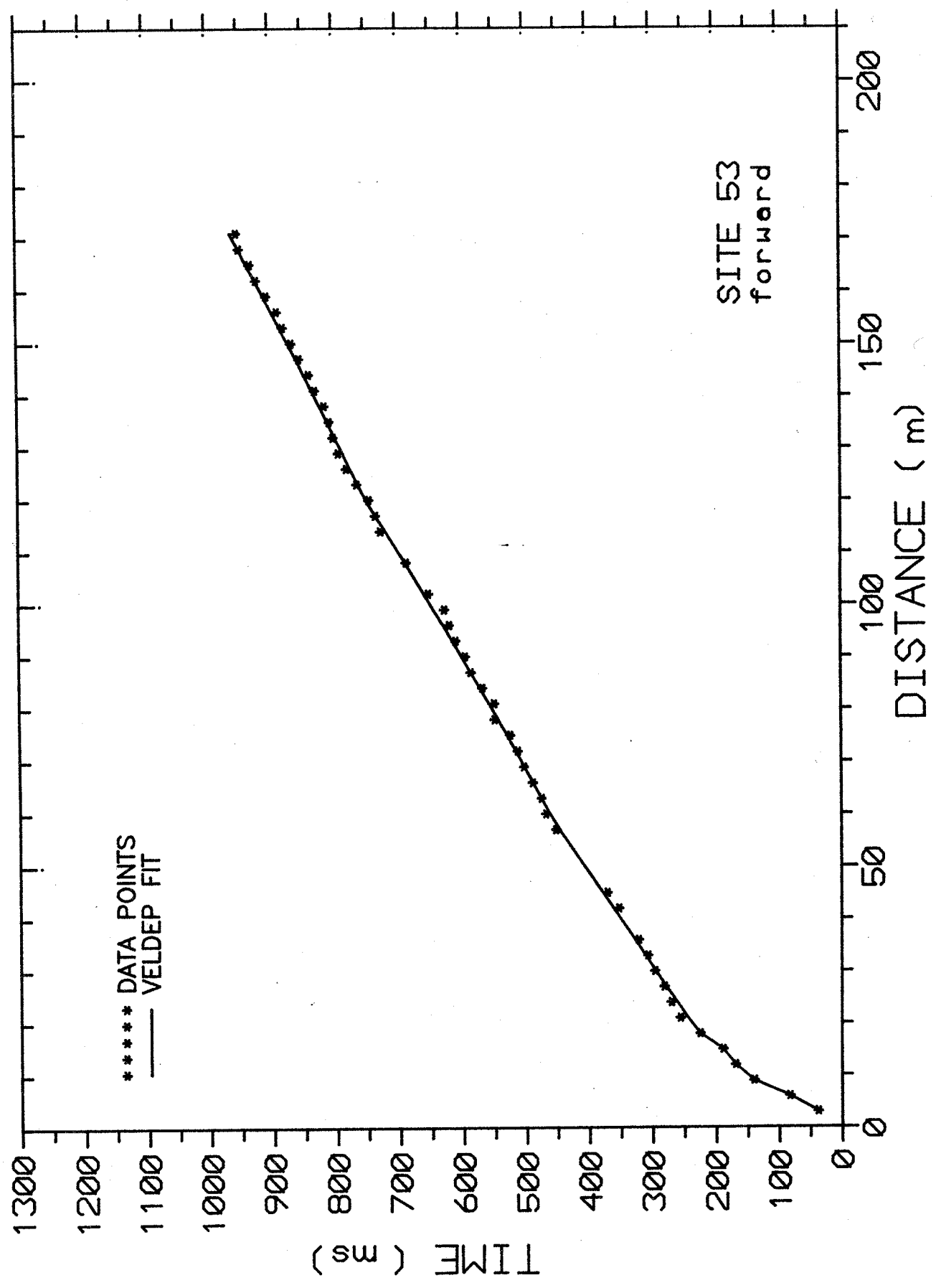










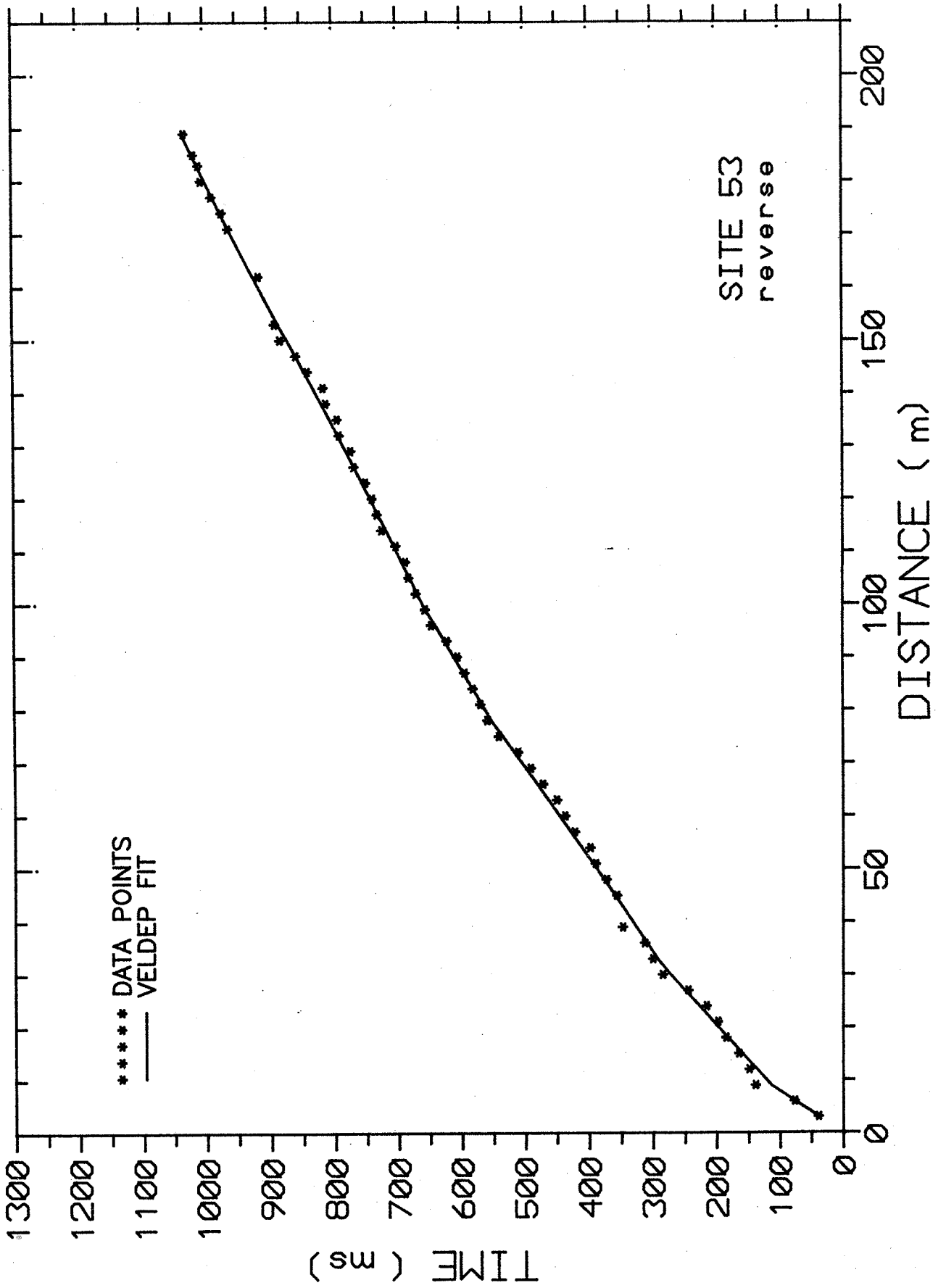


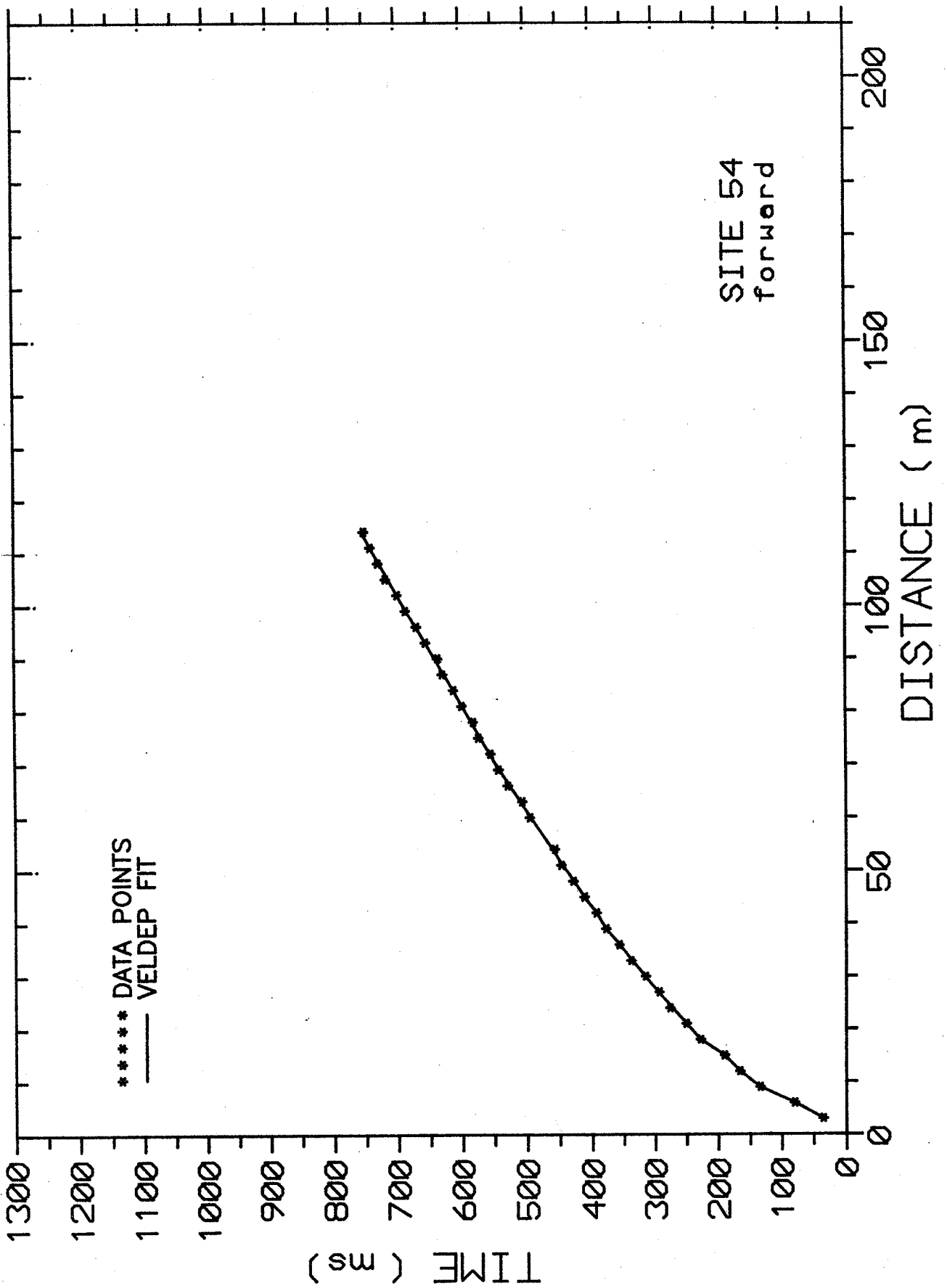
***** DATA POINTS
— VELDEP FIT

SITE 53
forward

TIME (ms)

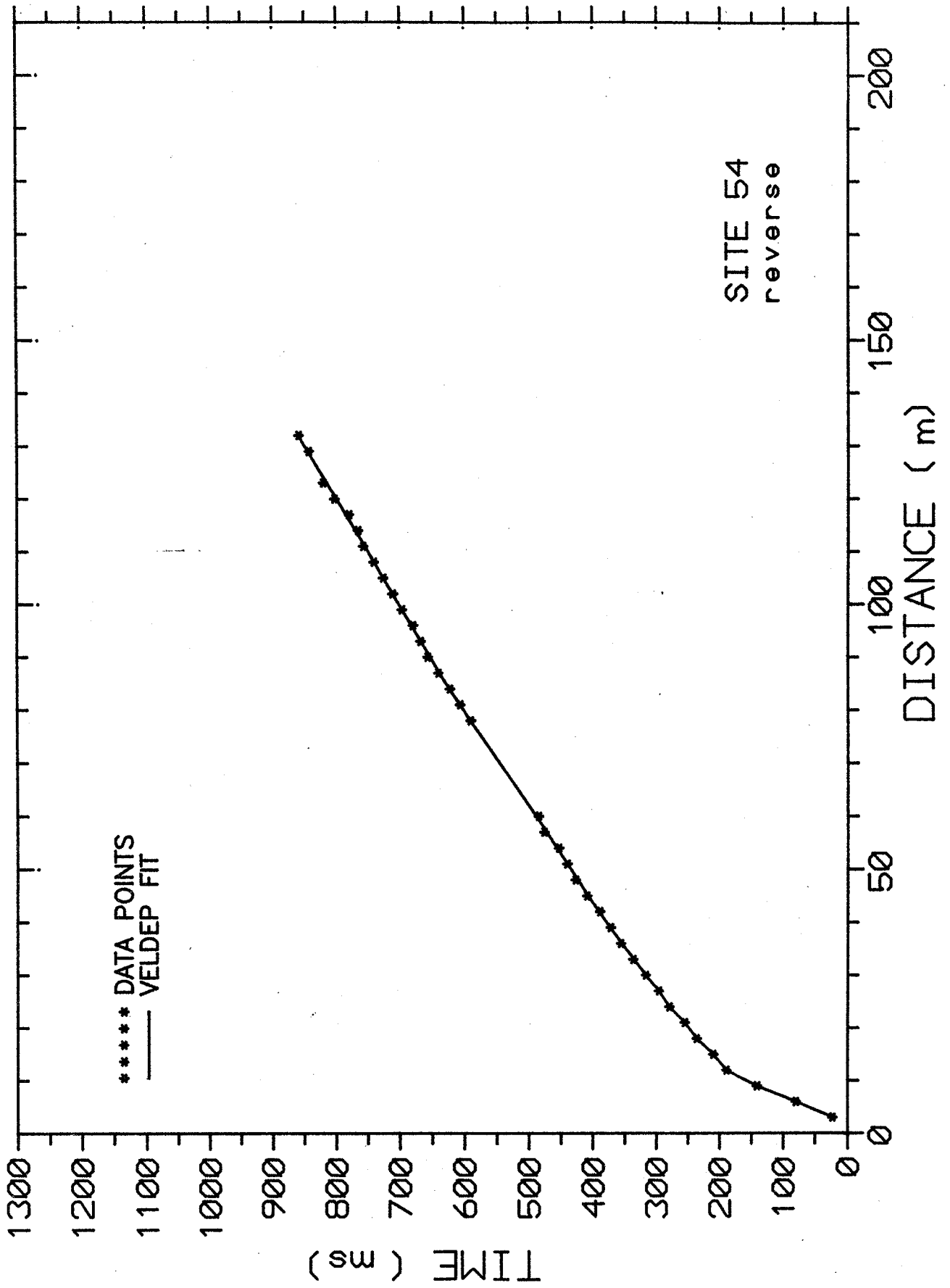
DISTANCE (m)





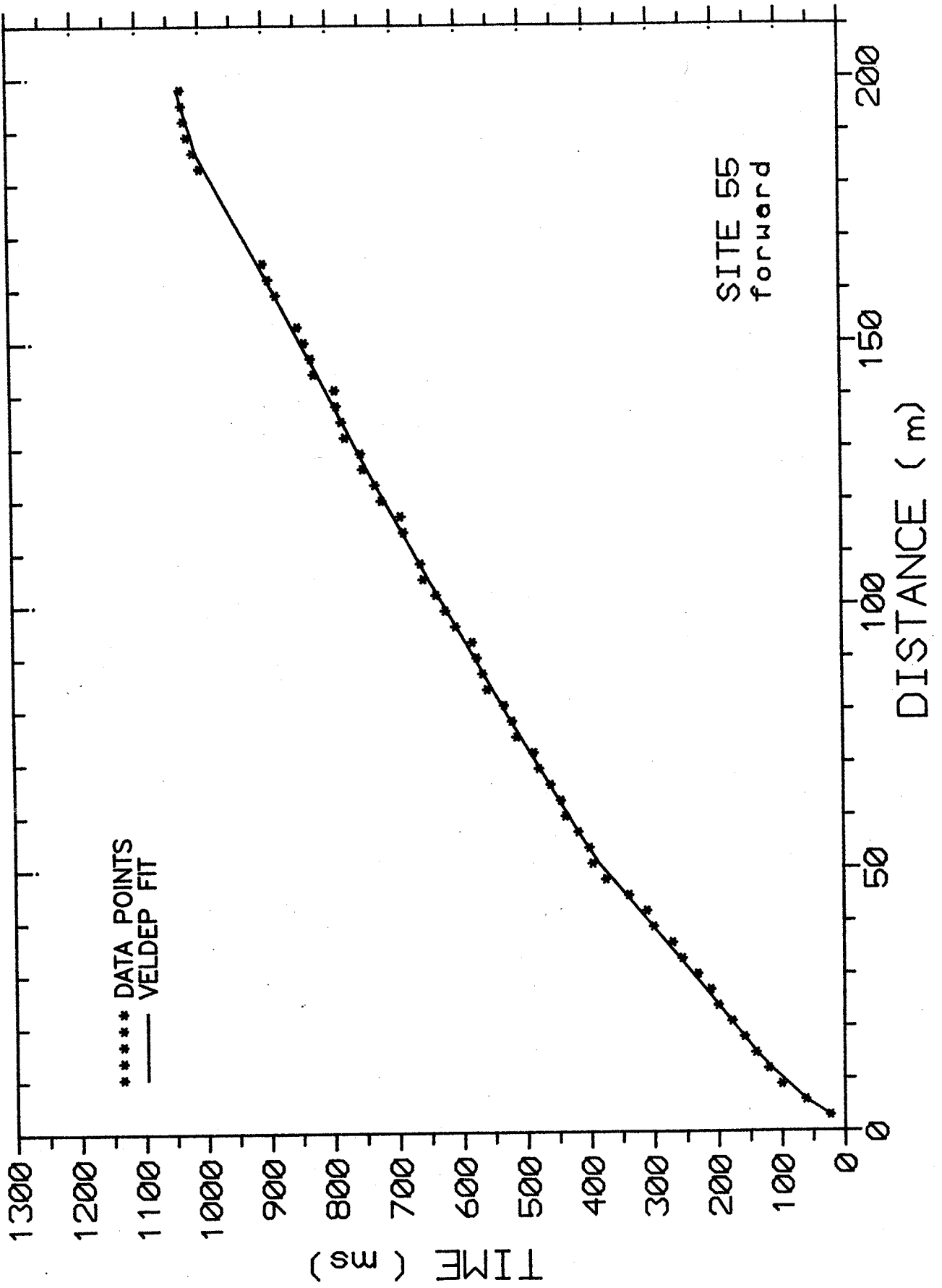
SITE 54
forward

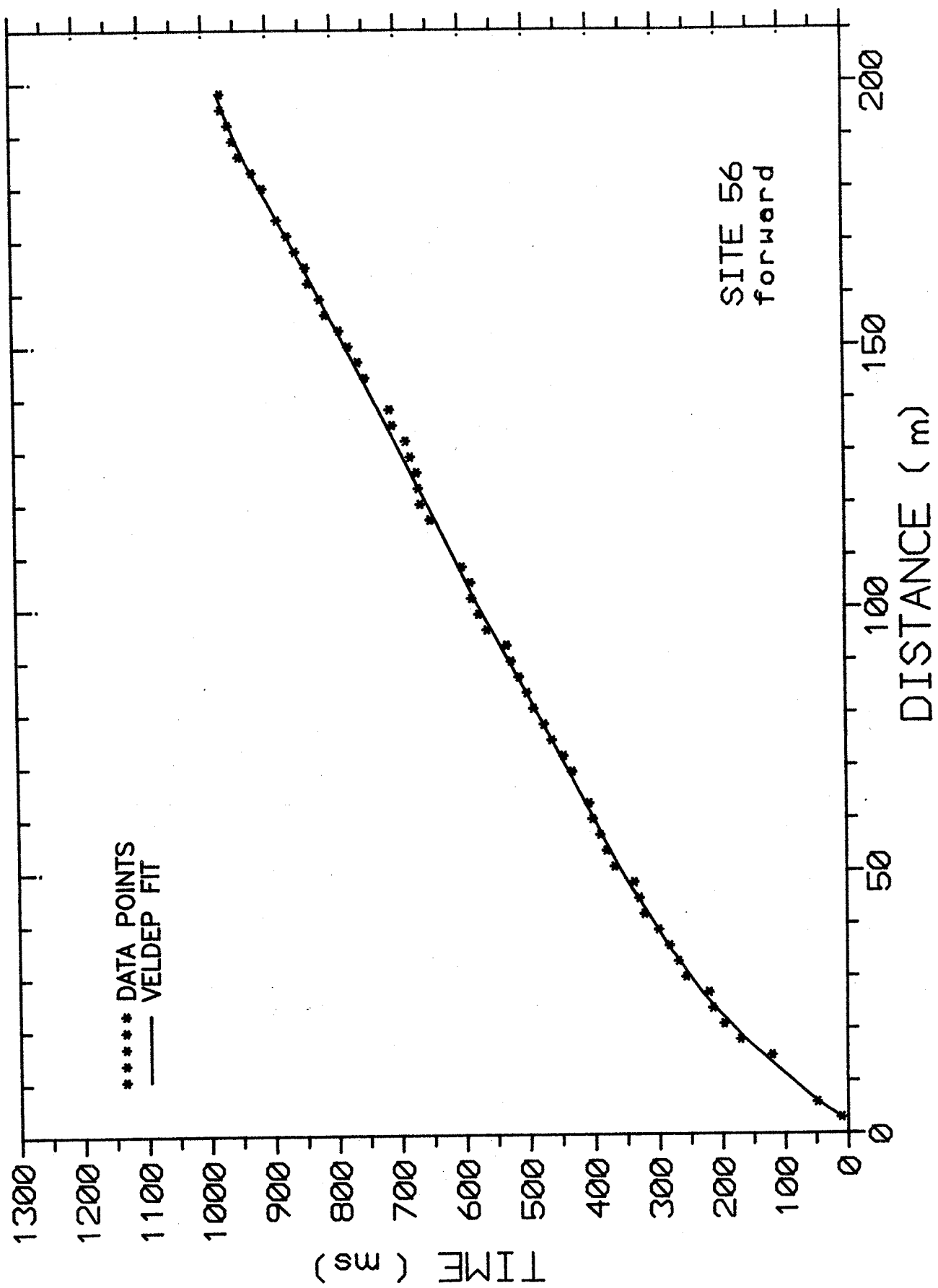
***** DATA POINTS
—— VELDEP FIT



***** DATA POINTS
— VELDEP FIT

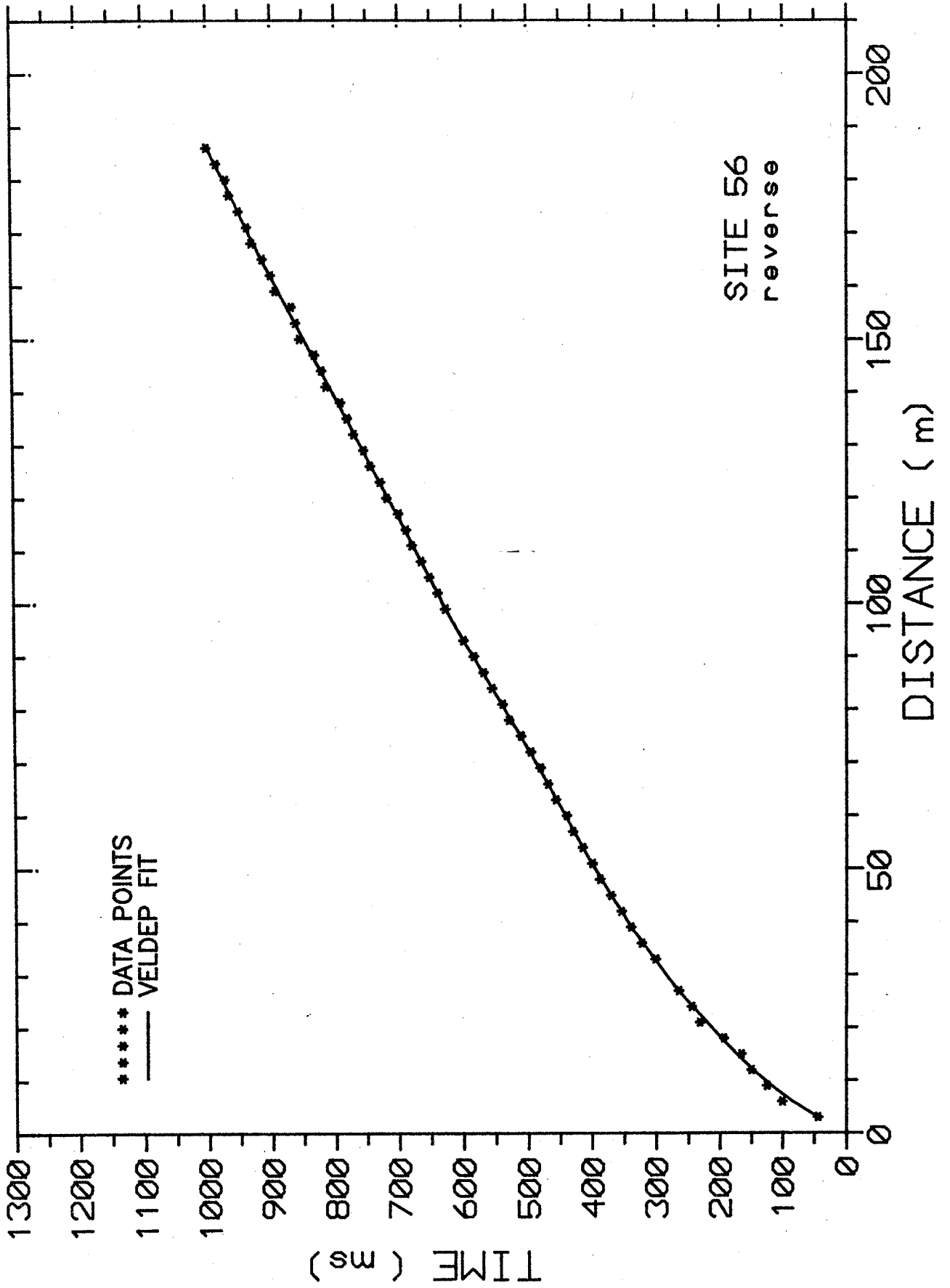
SITE 54
reverse

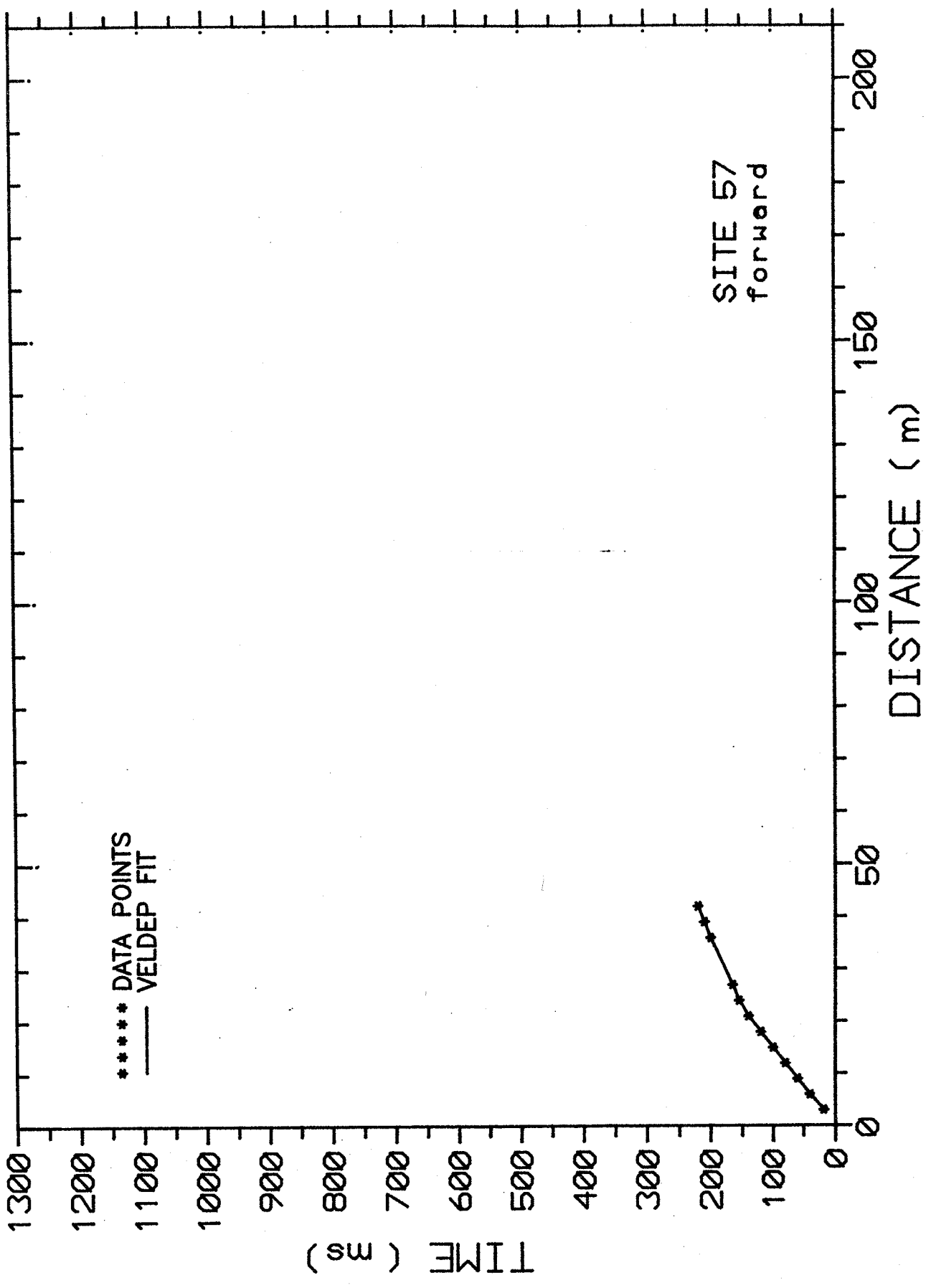


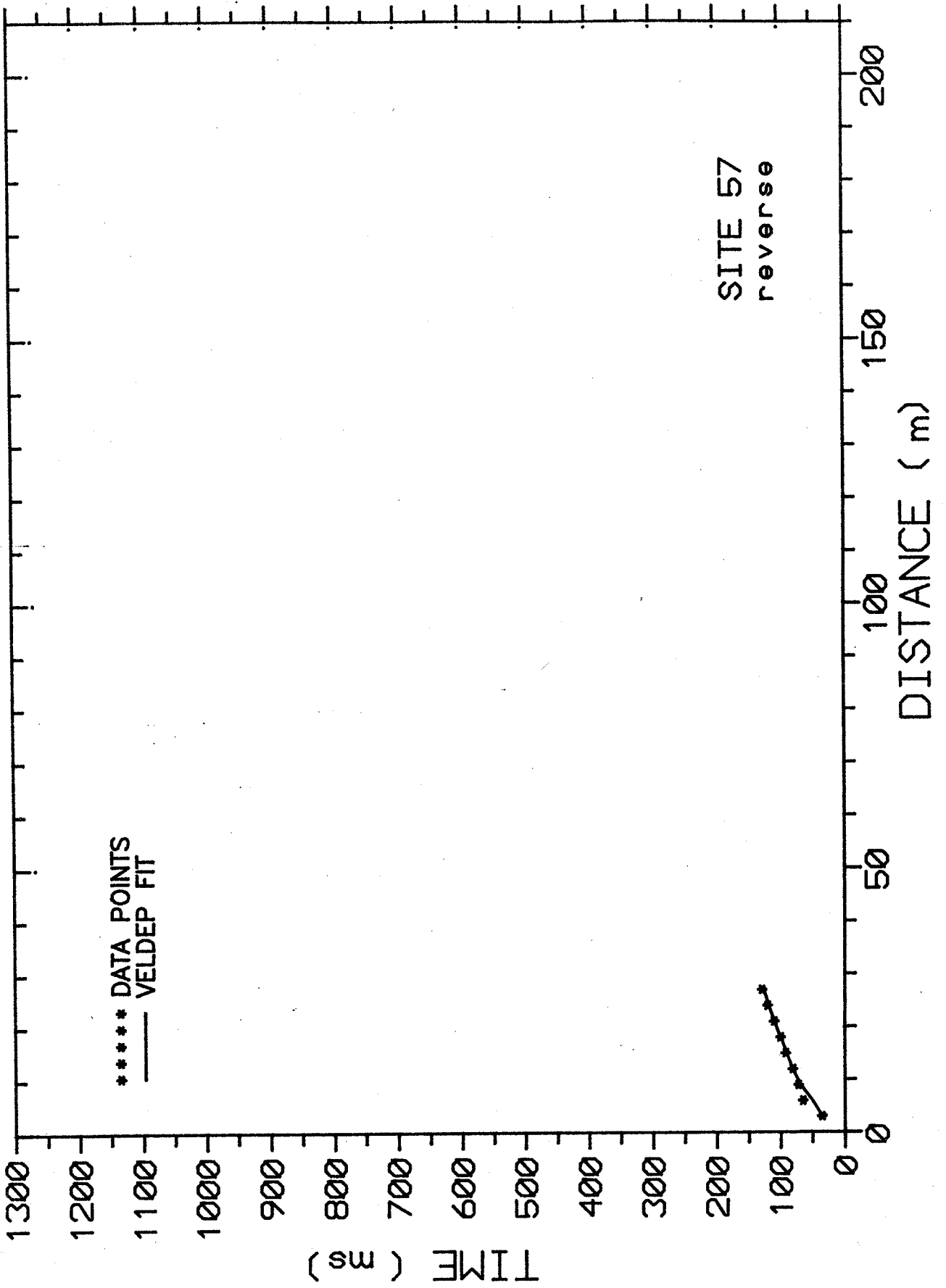


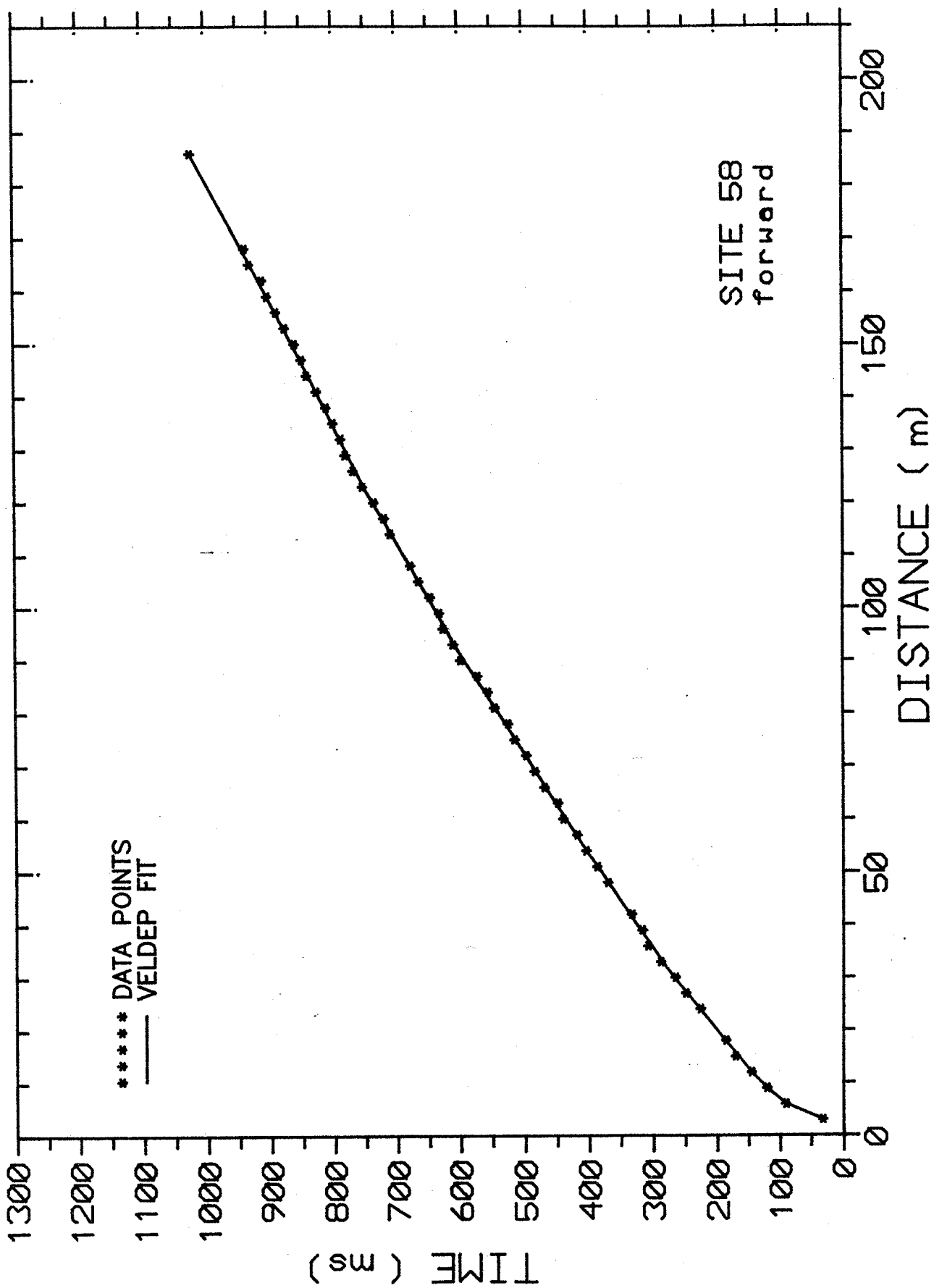
SITE 56
forward

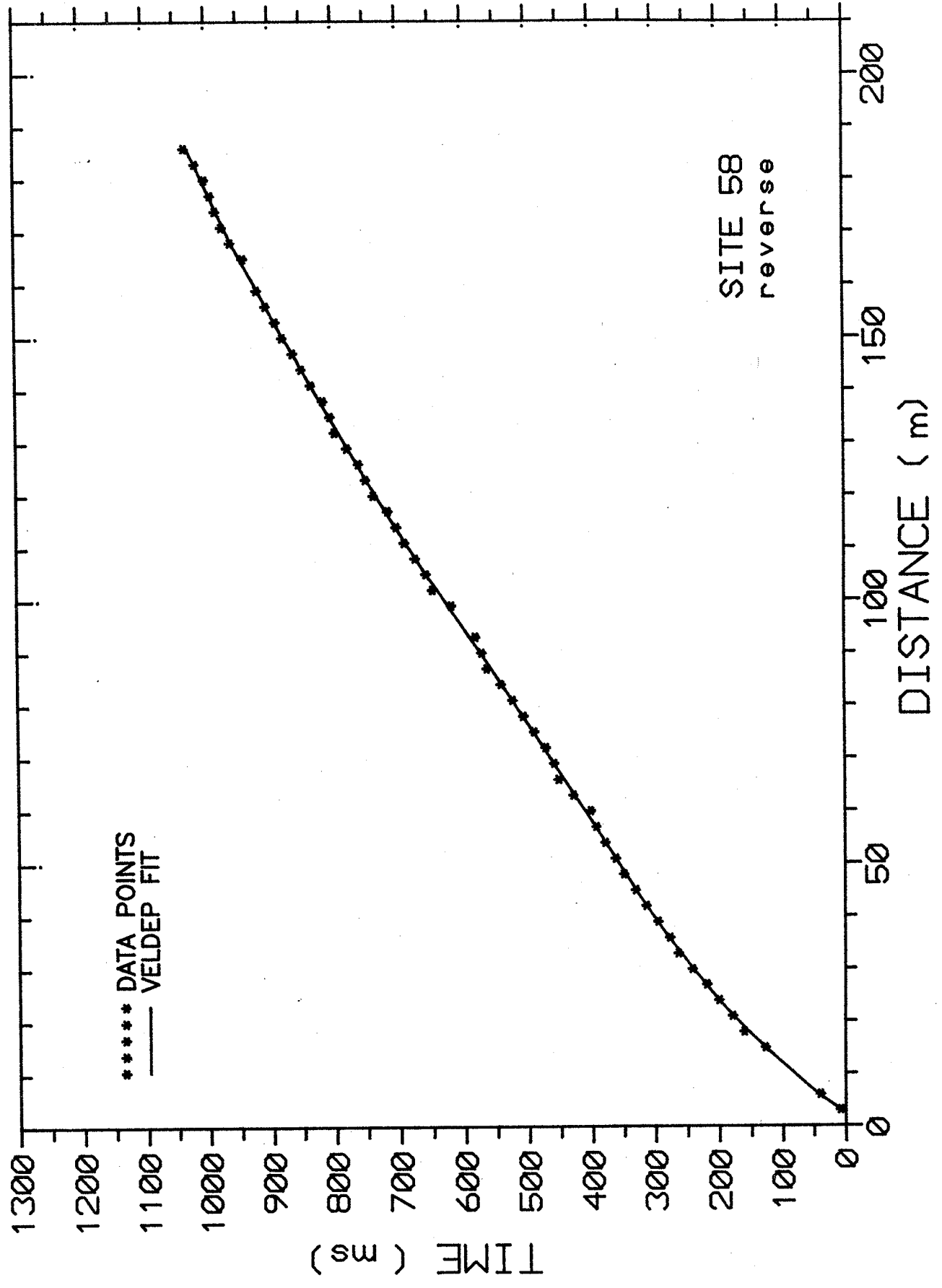
***** DATA POINTS
— VELDEP FIT









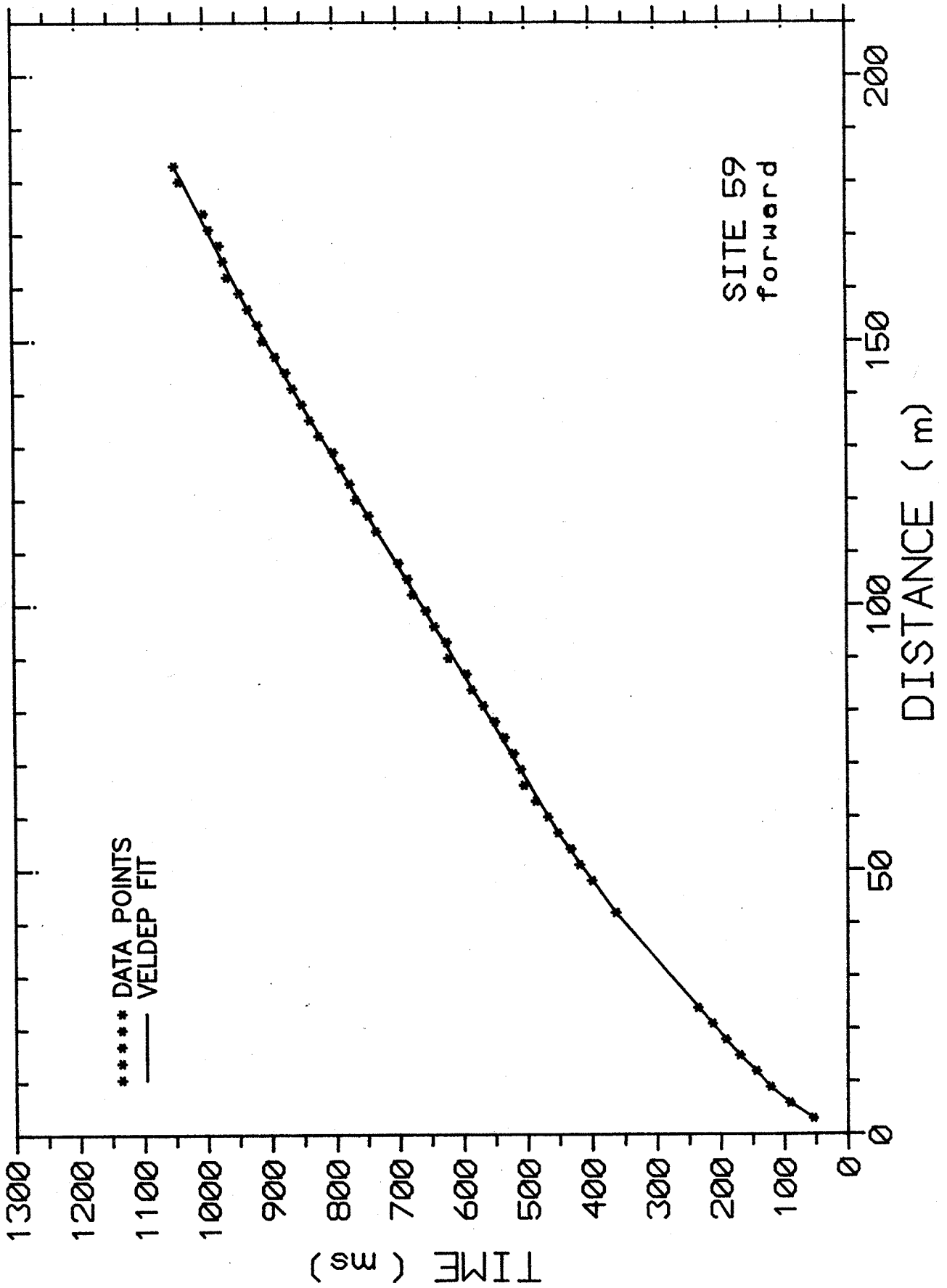


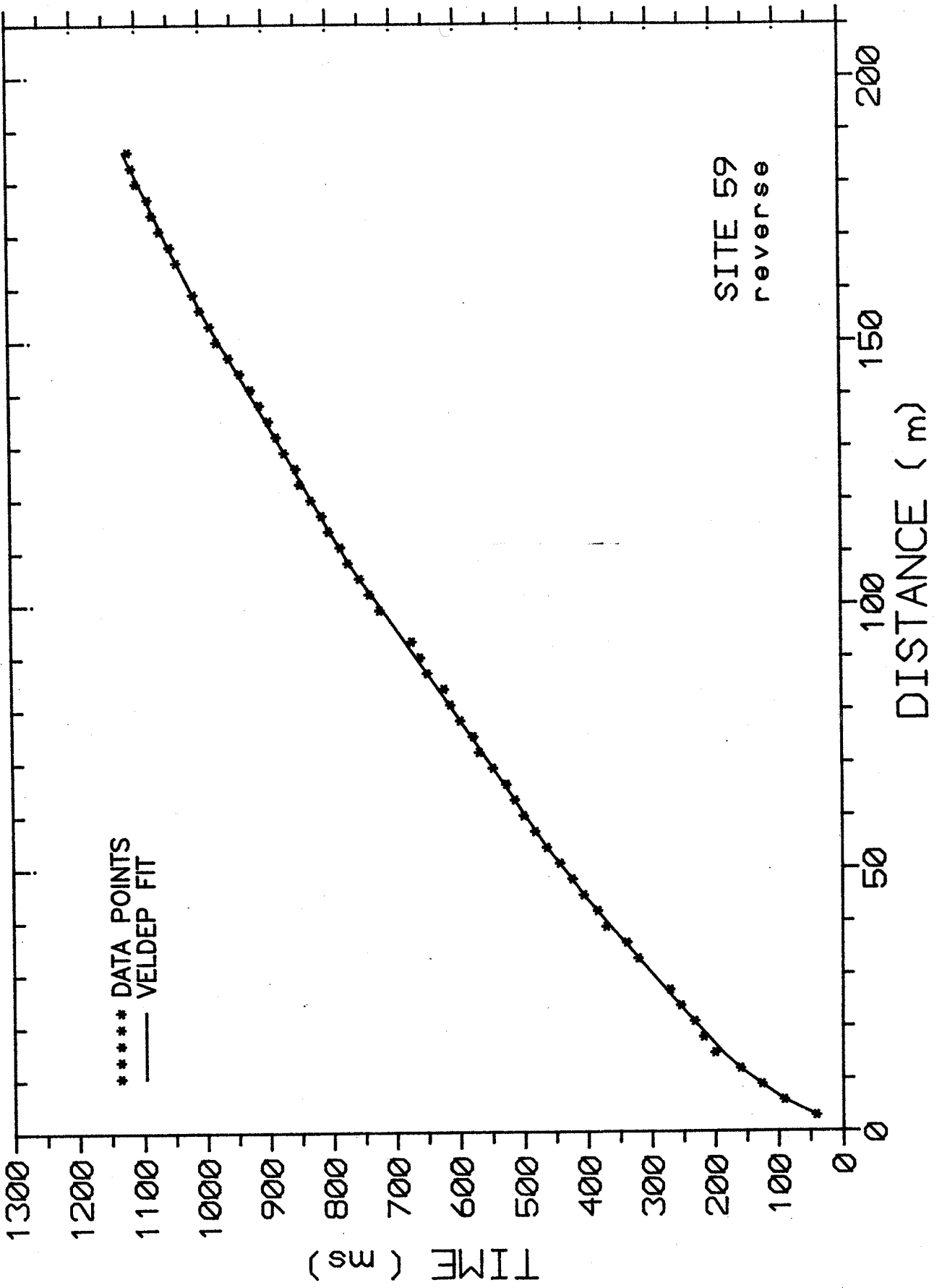
***** DATA POINTS
——— VELDEP FIT

SITE 58
reverse

TIME (ms)

DISTANCE (m)



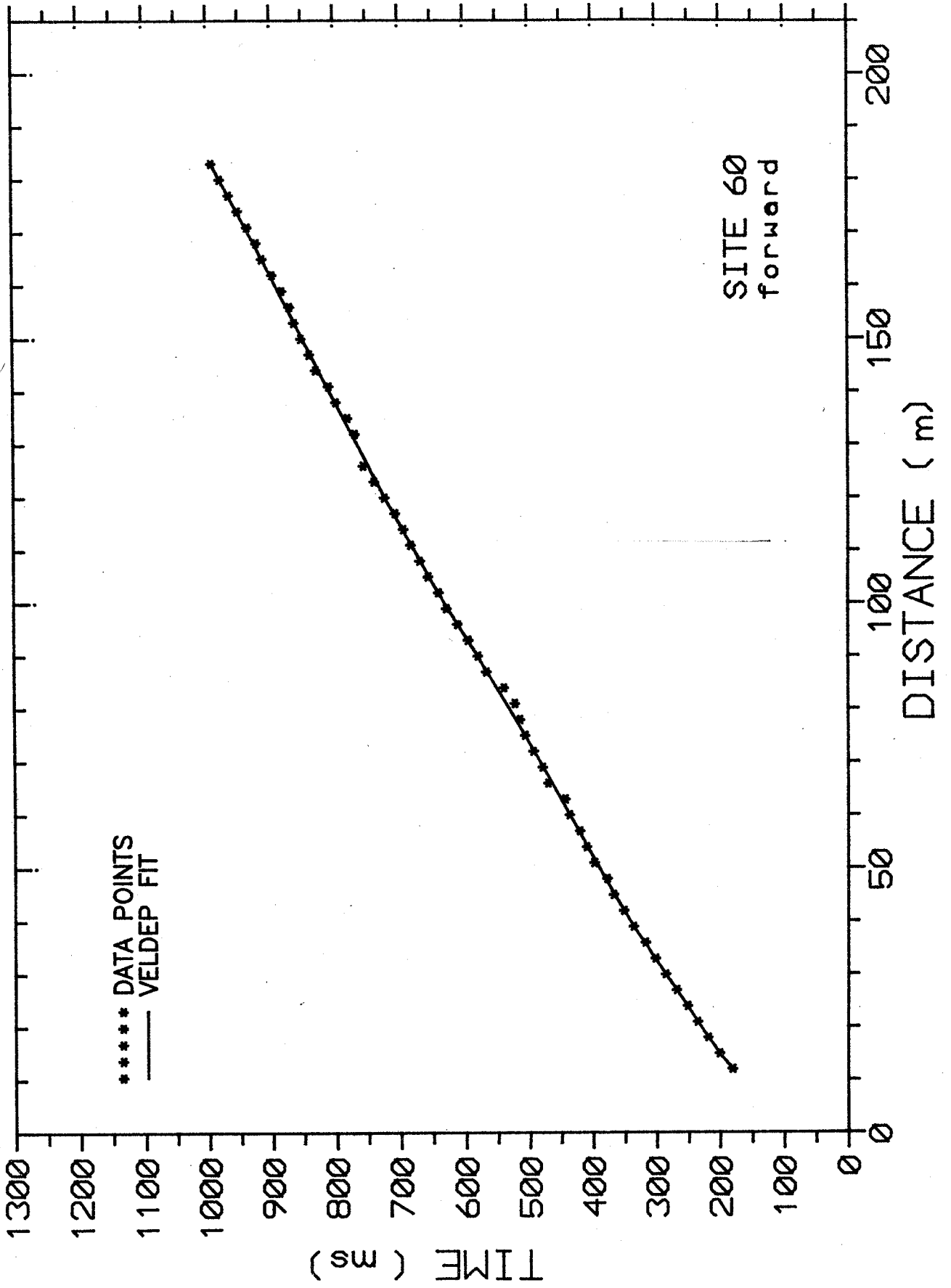


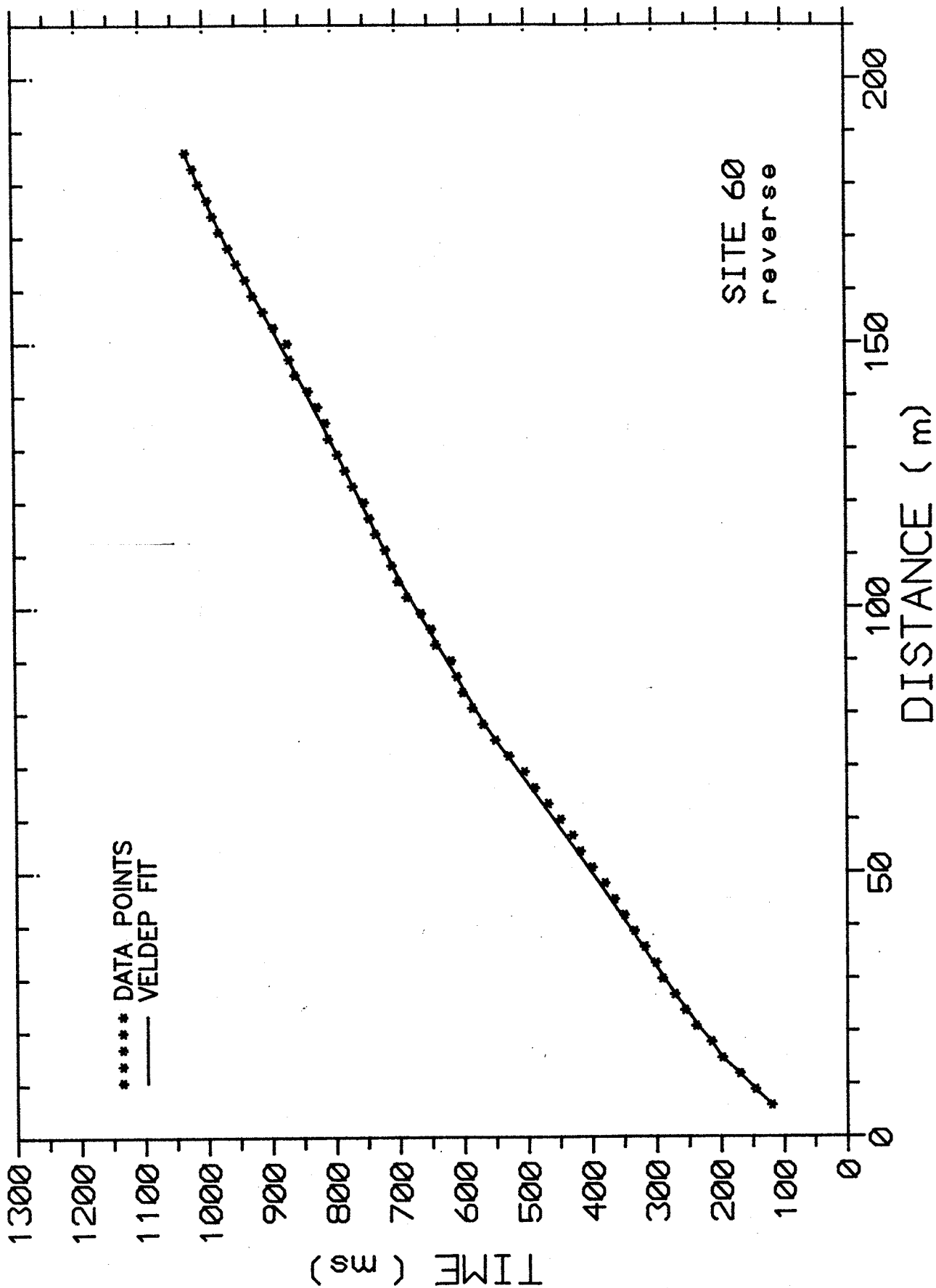
SITE 59
reverse

***** DATA POINTS
— VELDEP FIT

TIME (ms)

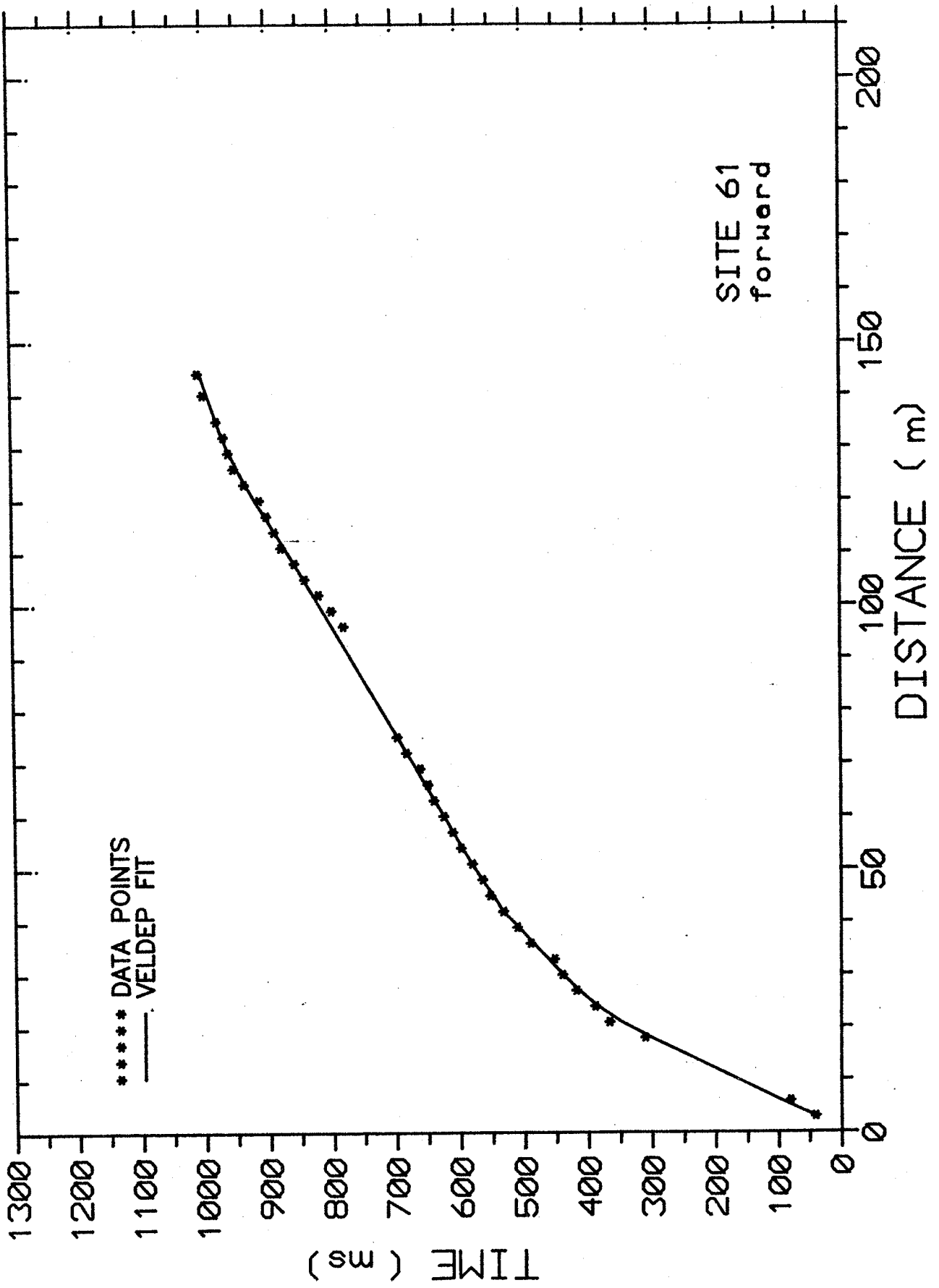
DISTANCE (m)

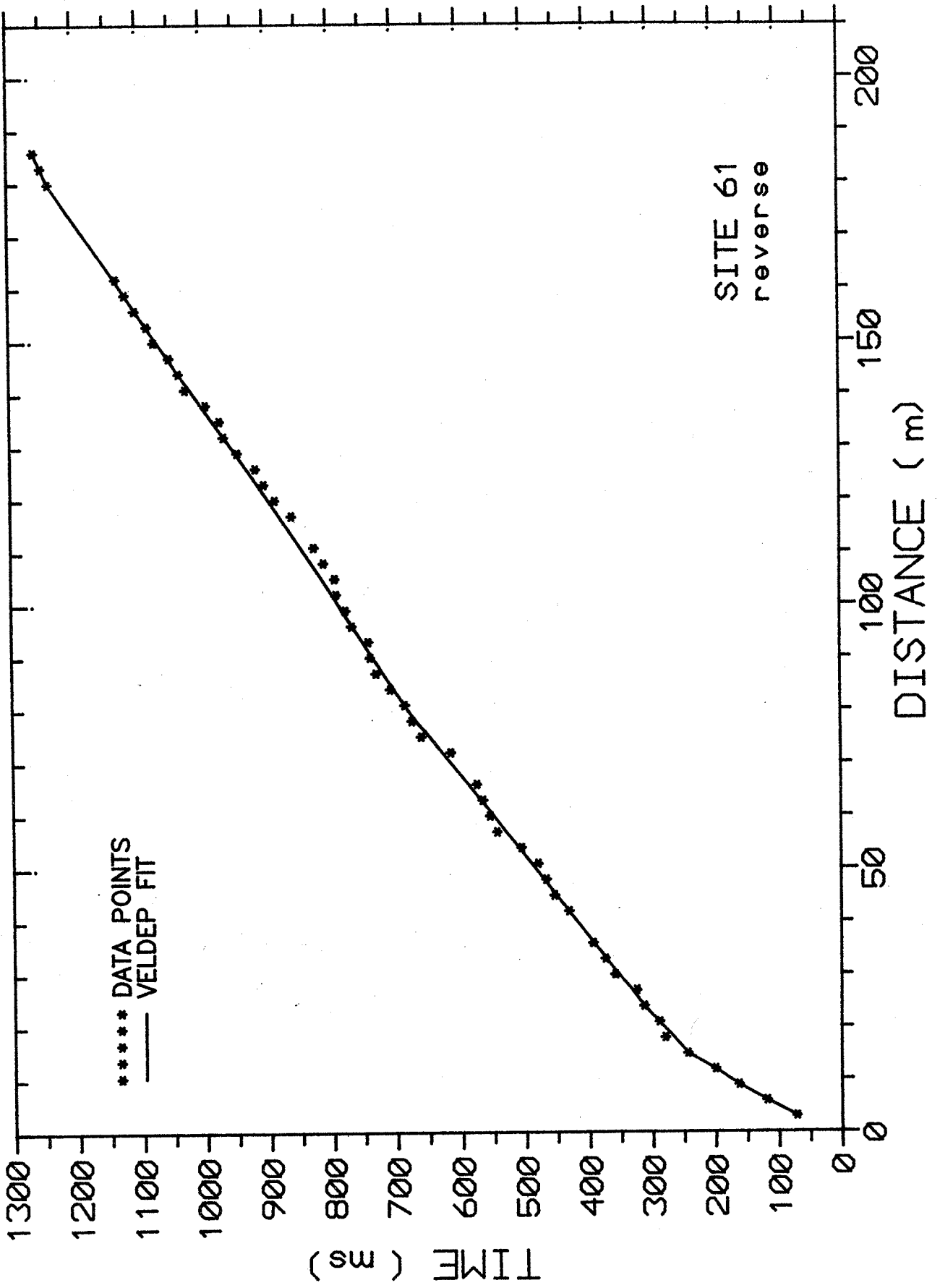


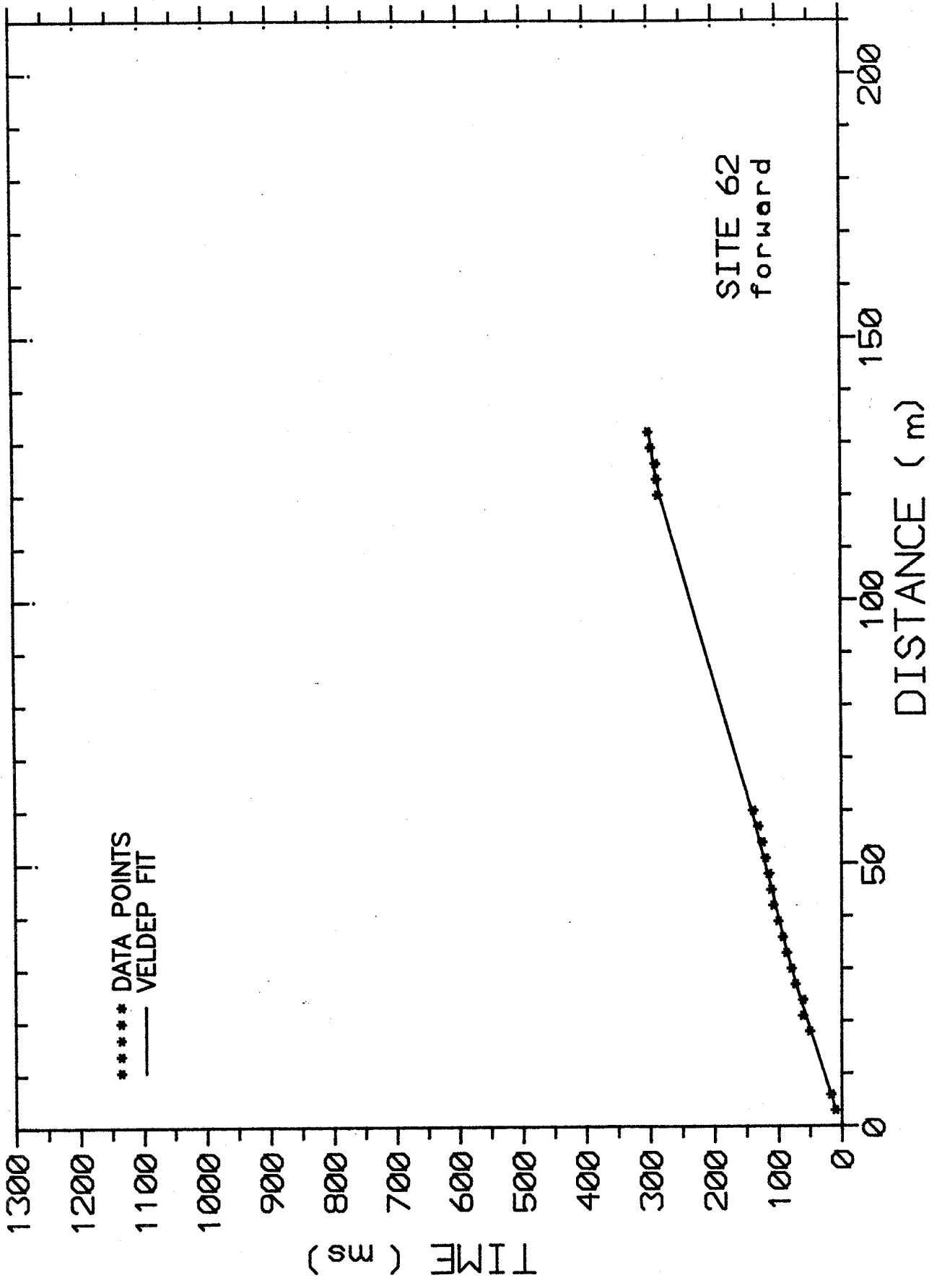


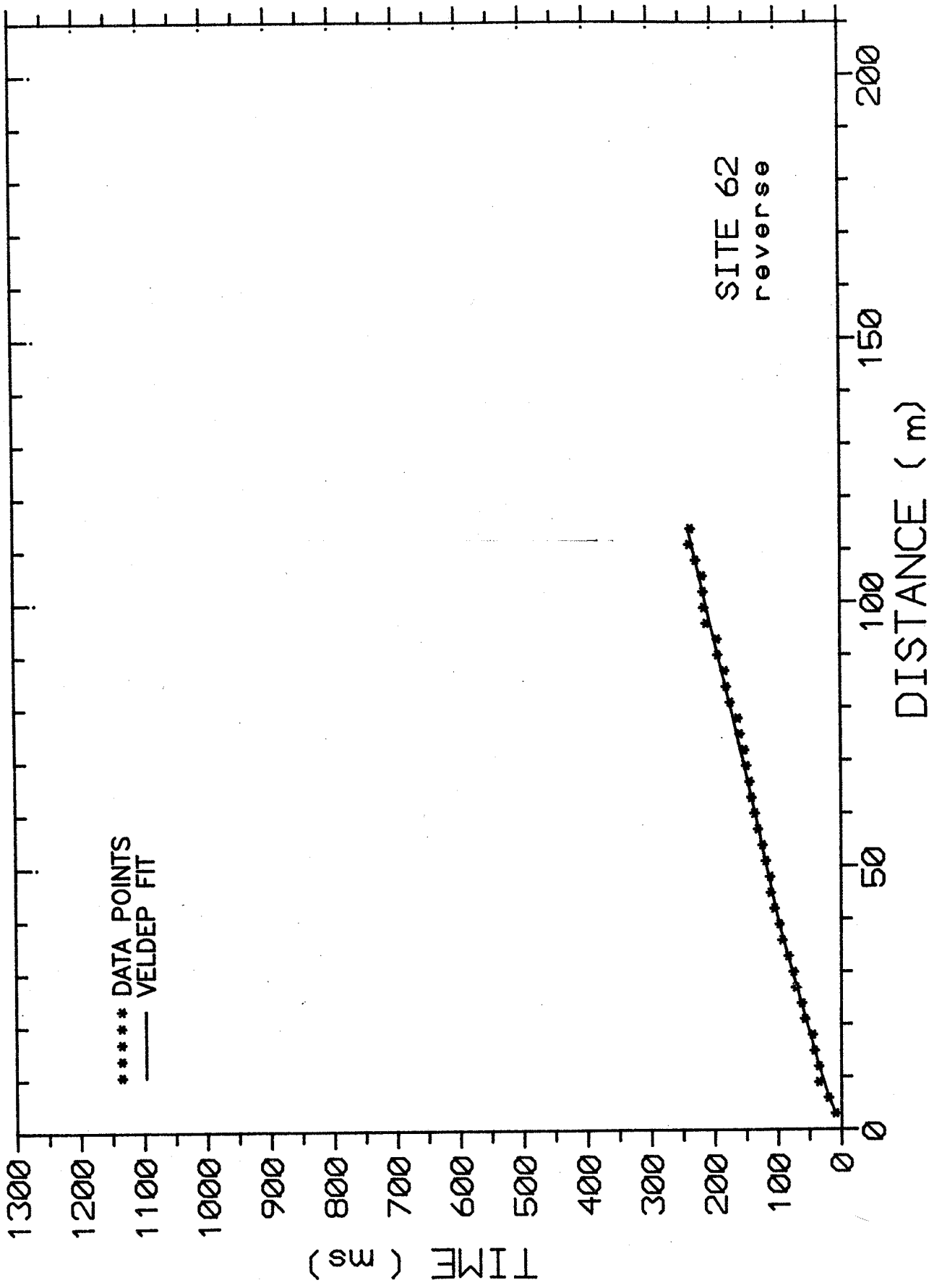
***** DATA POINTS
—— VELDEP FIT

SITE 60
reverse



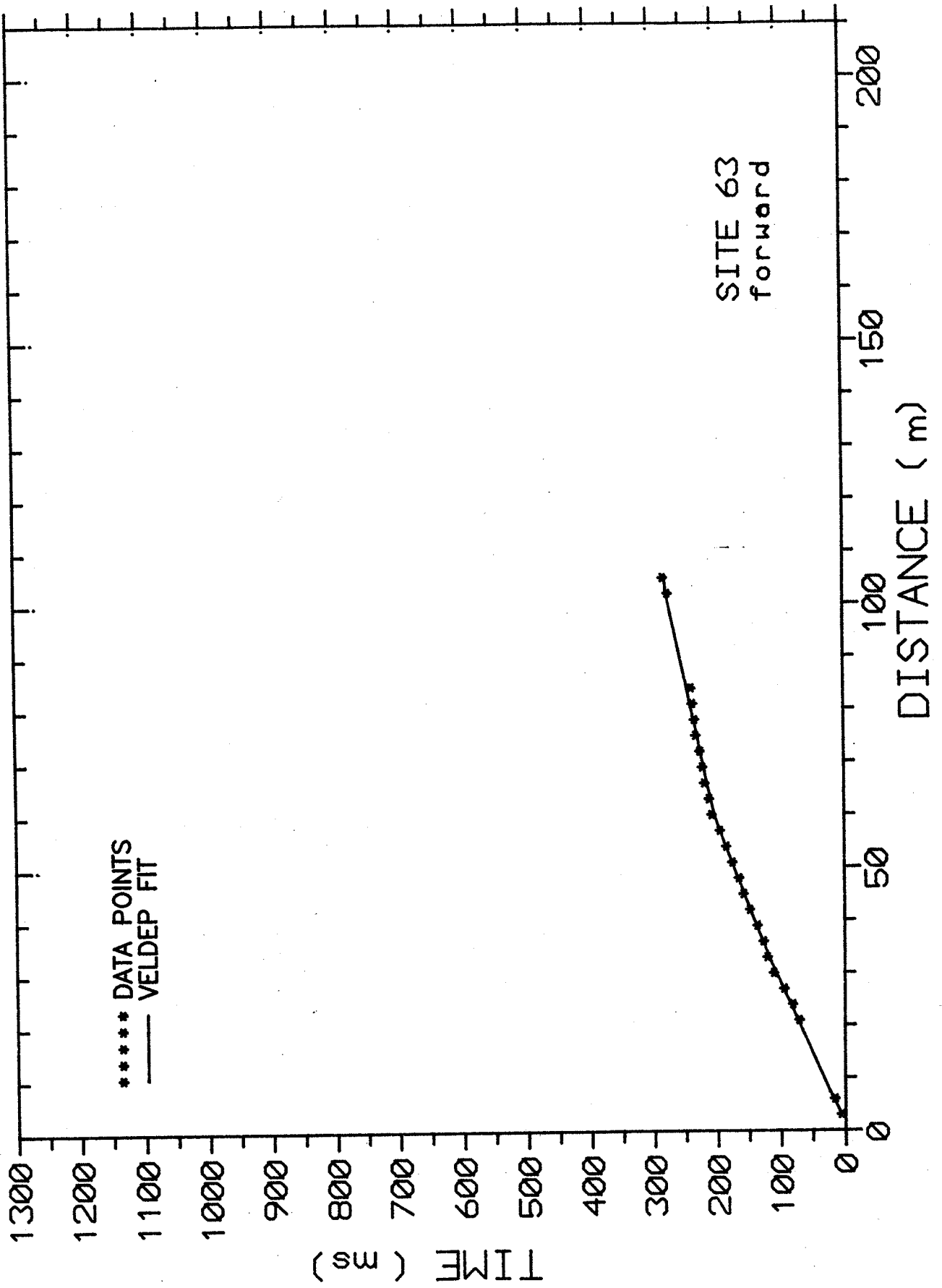


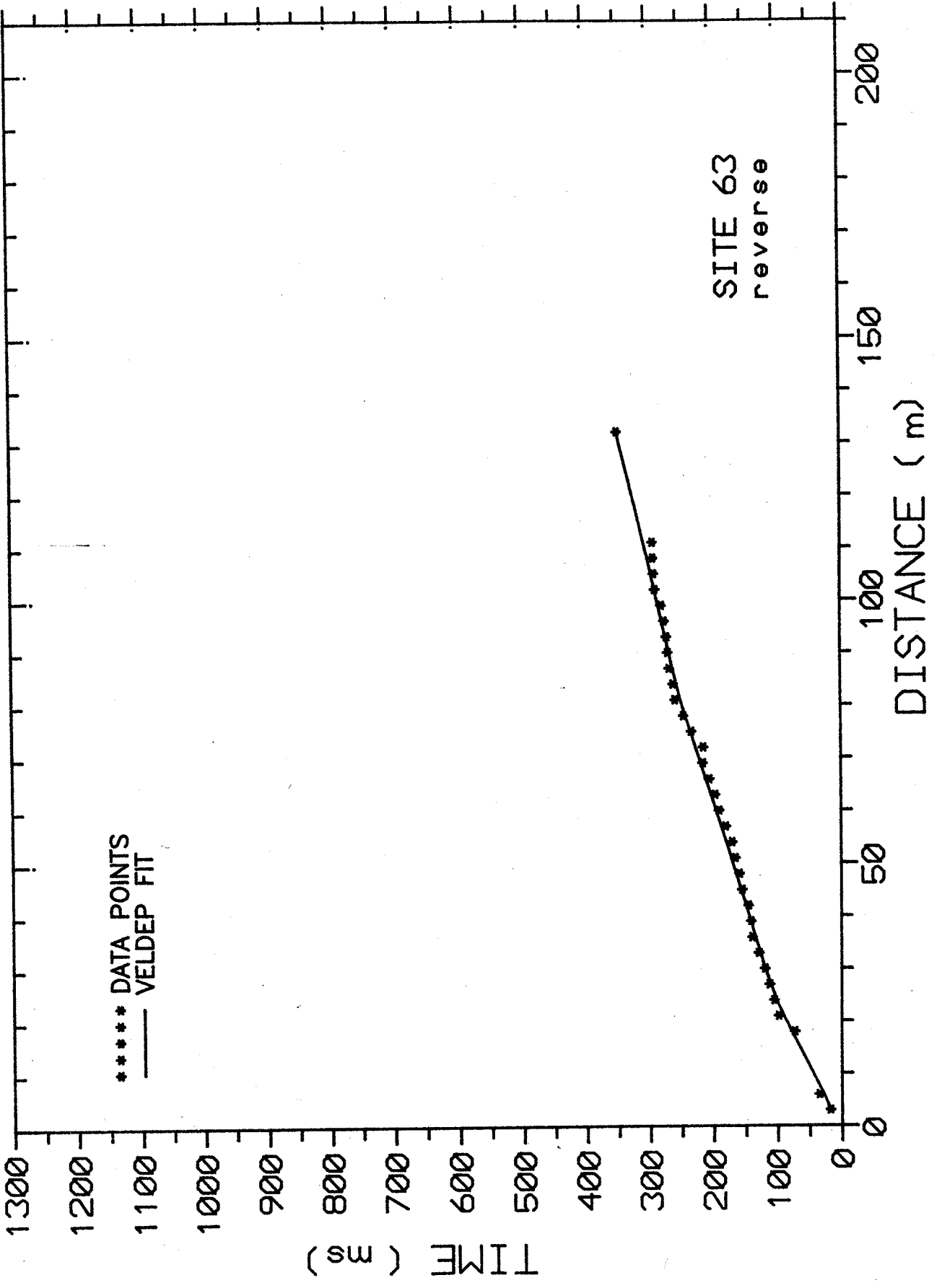




***** DATA POINTS
— VELDEP FIT

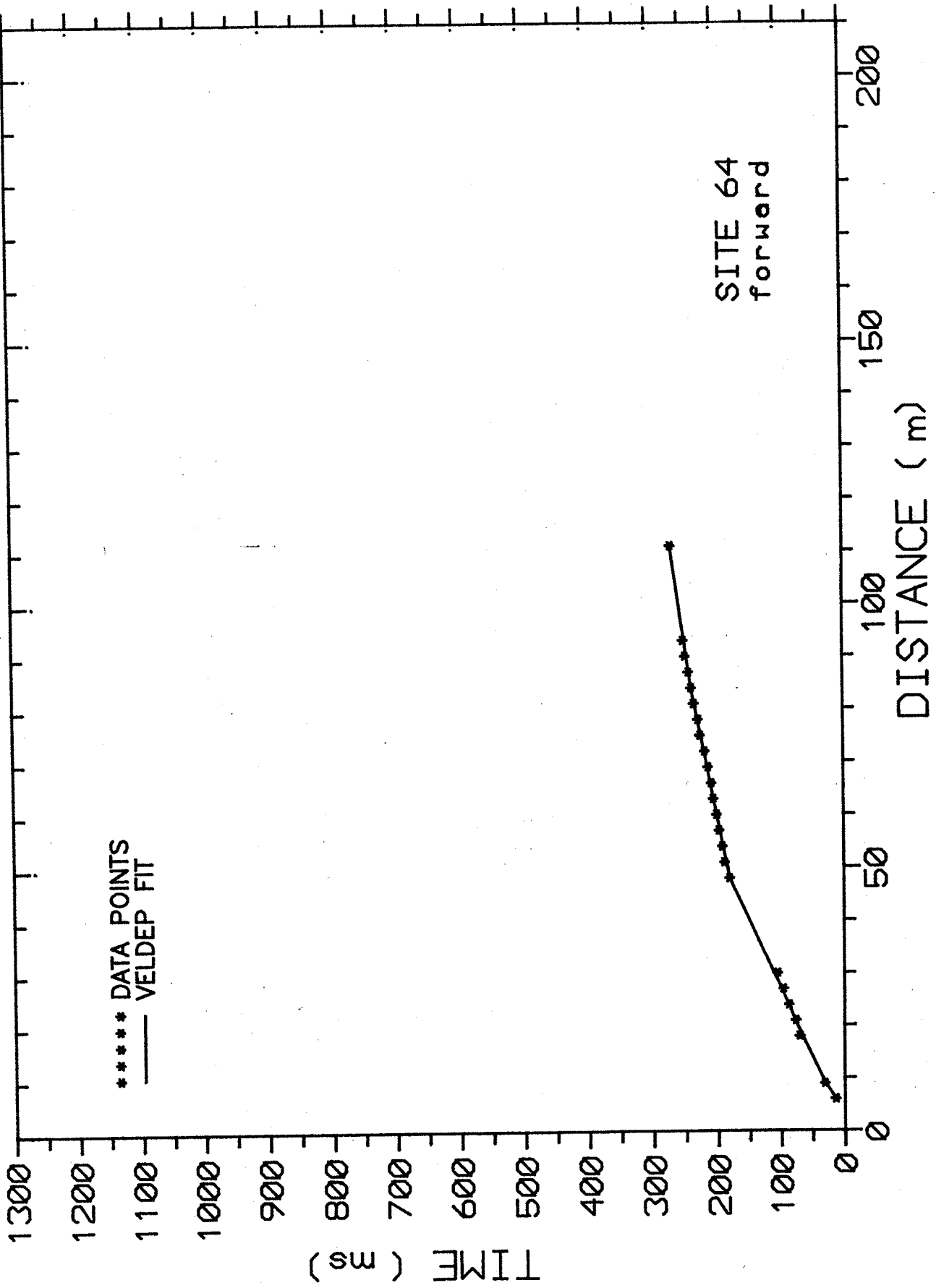
SITE 62
reverse

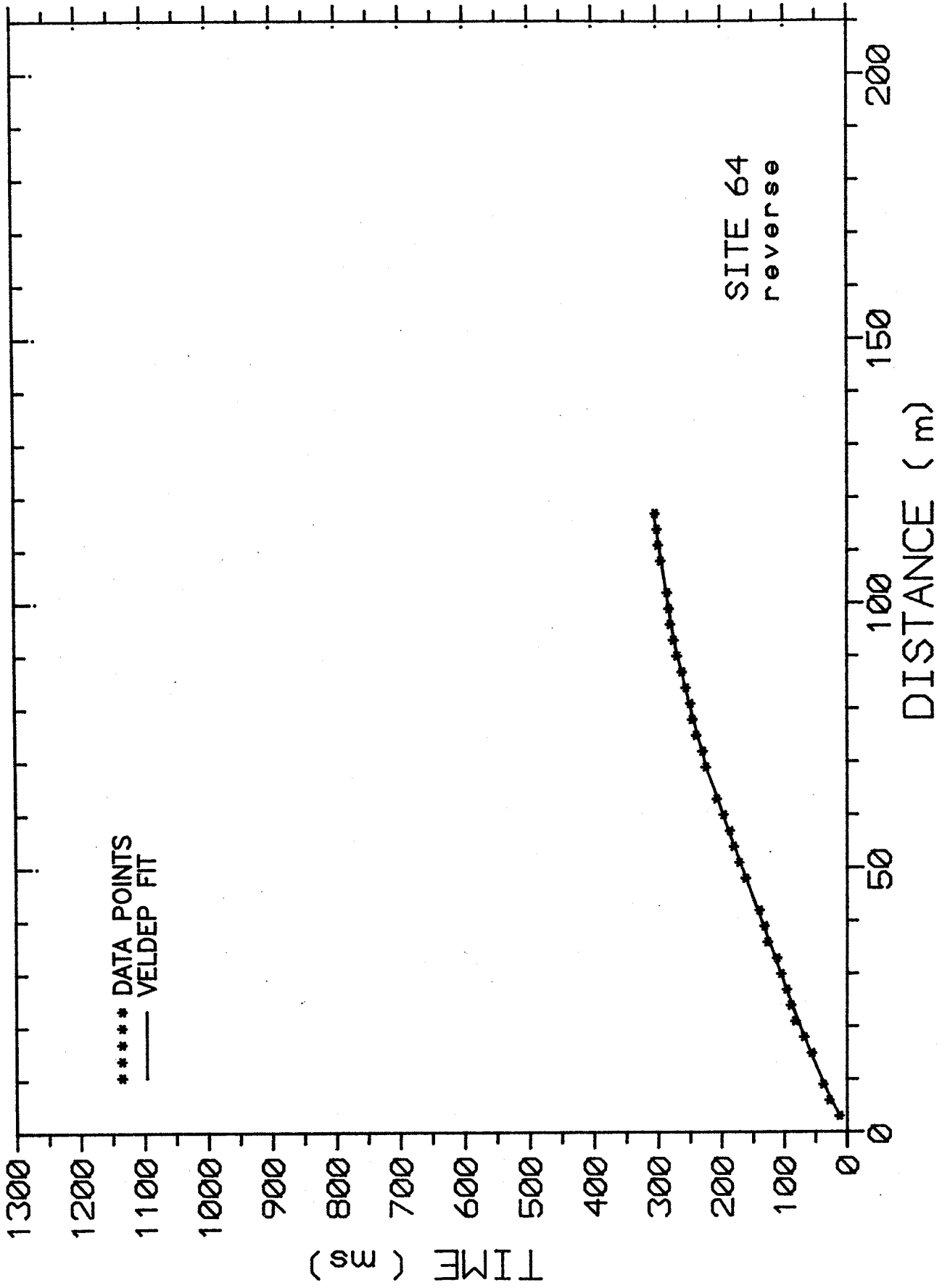


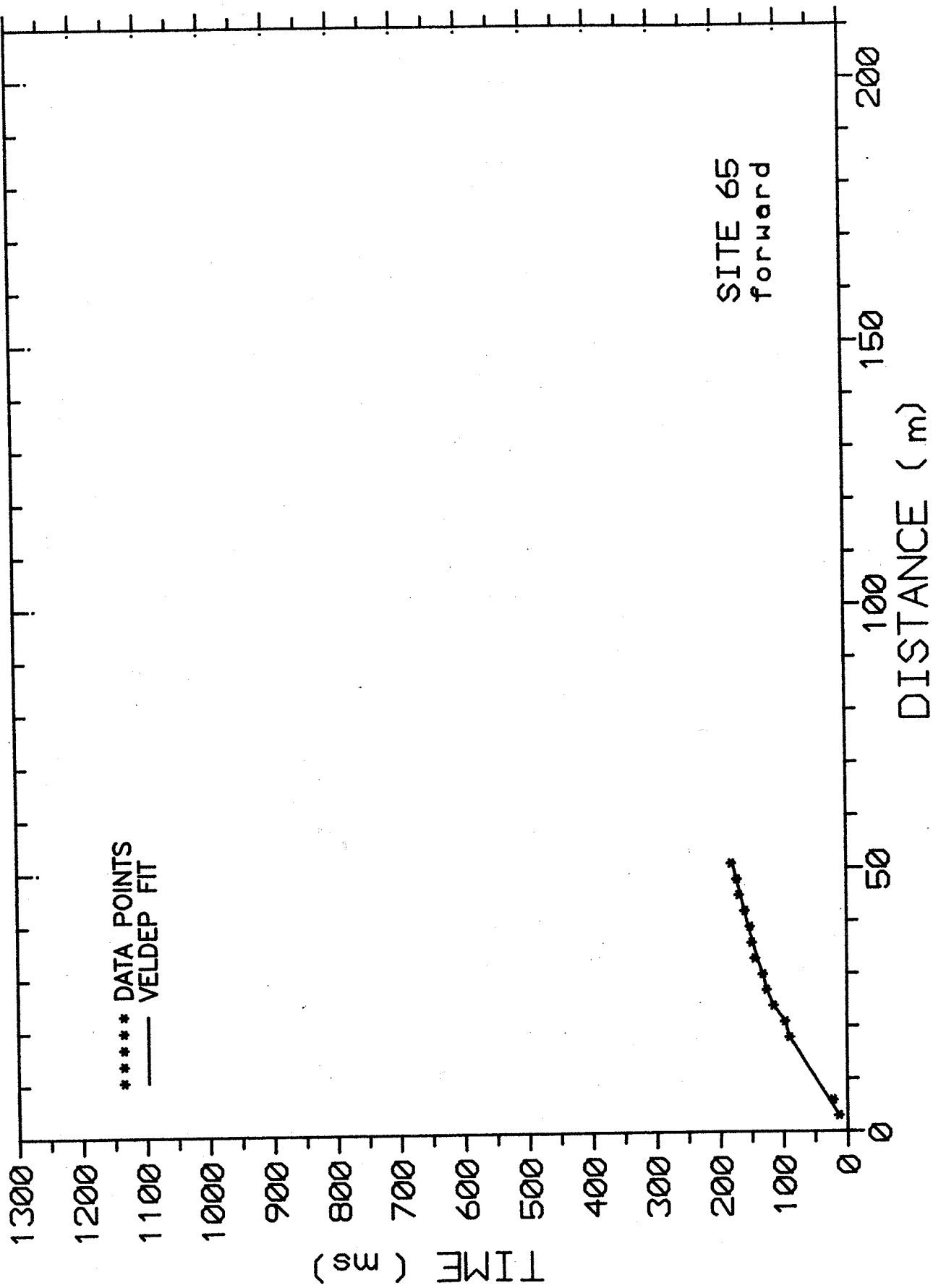


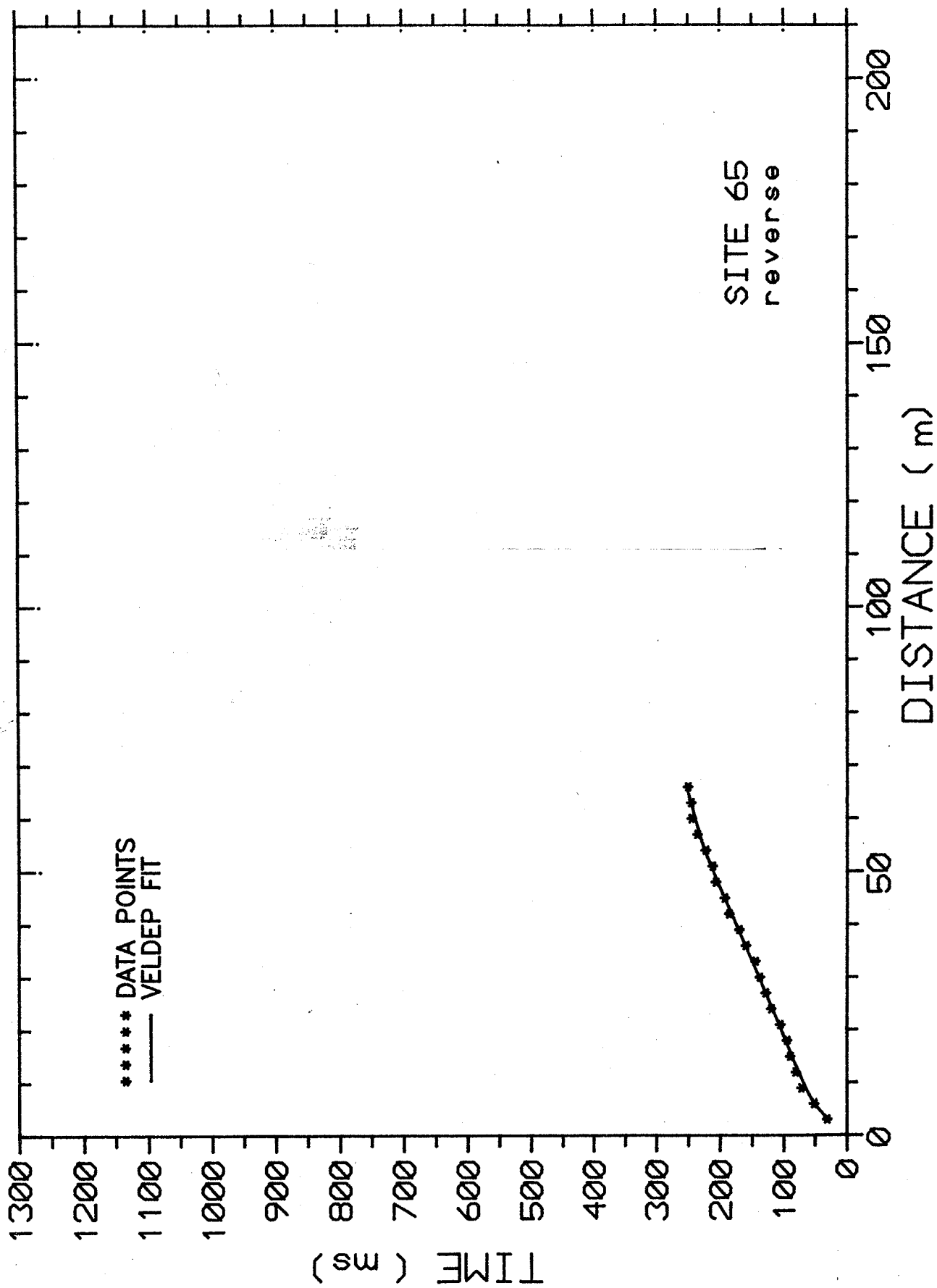
***** DATA POINTS
— VELDEP FIT

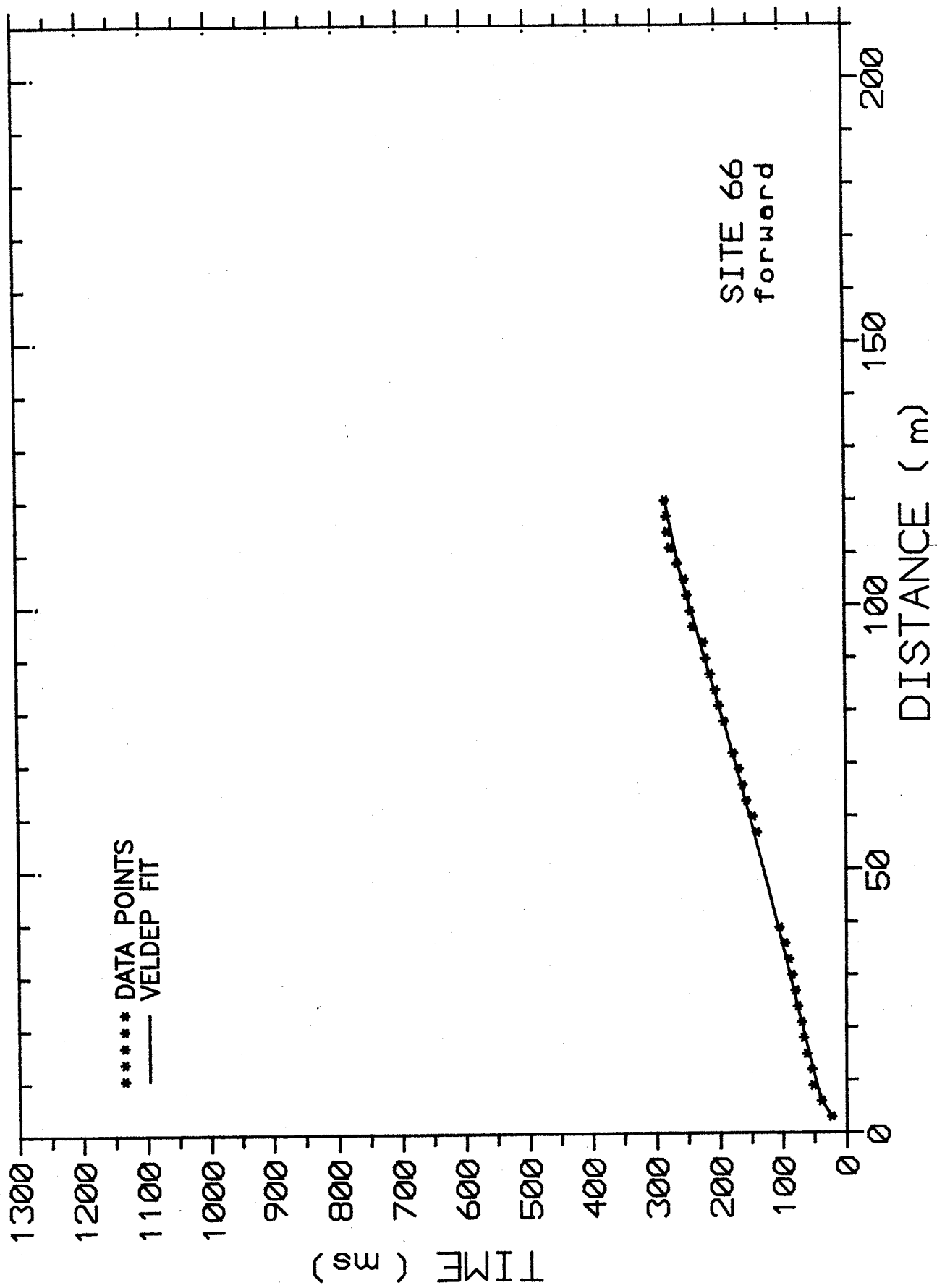
SITE 63
reverse

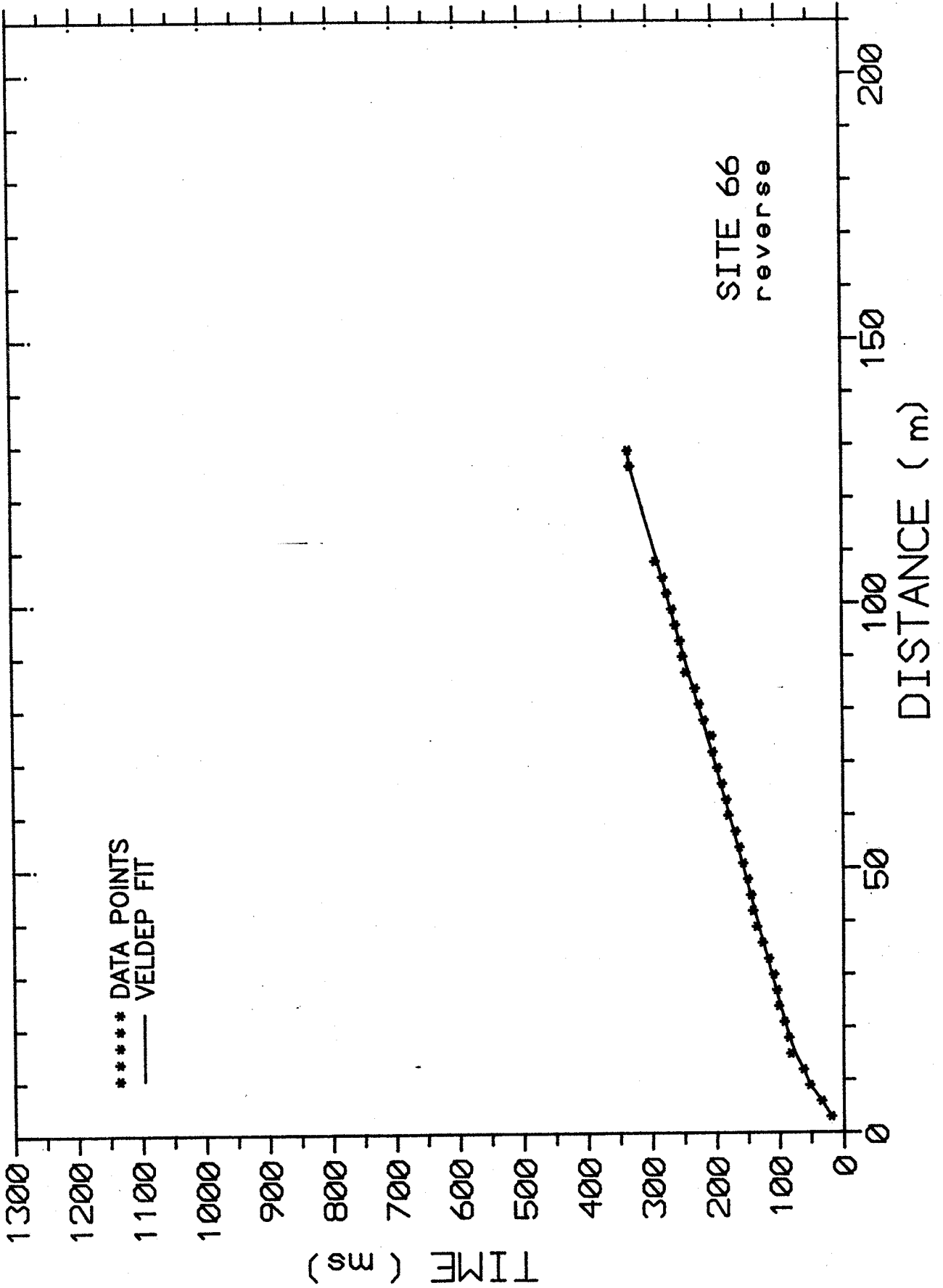


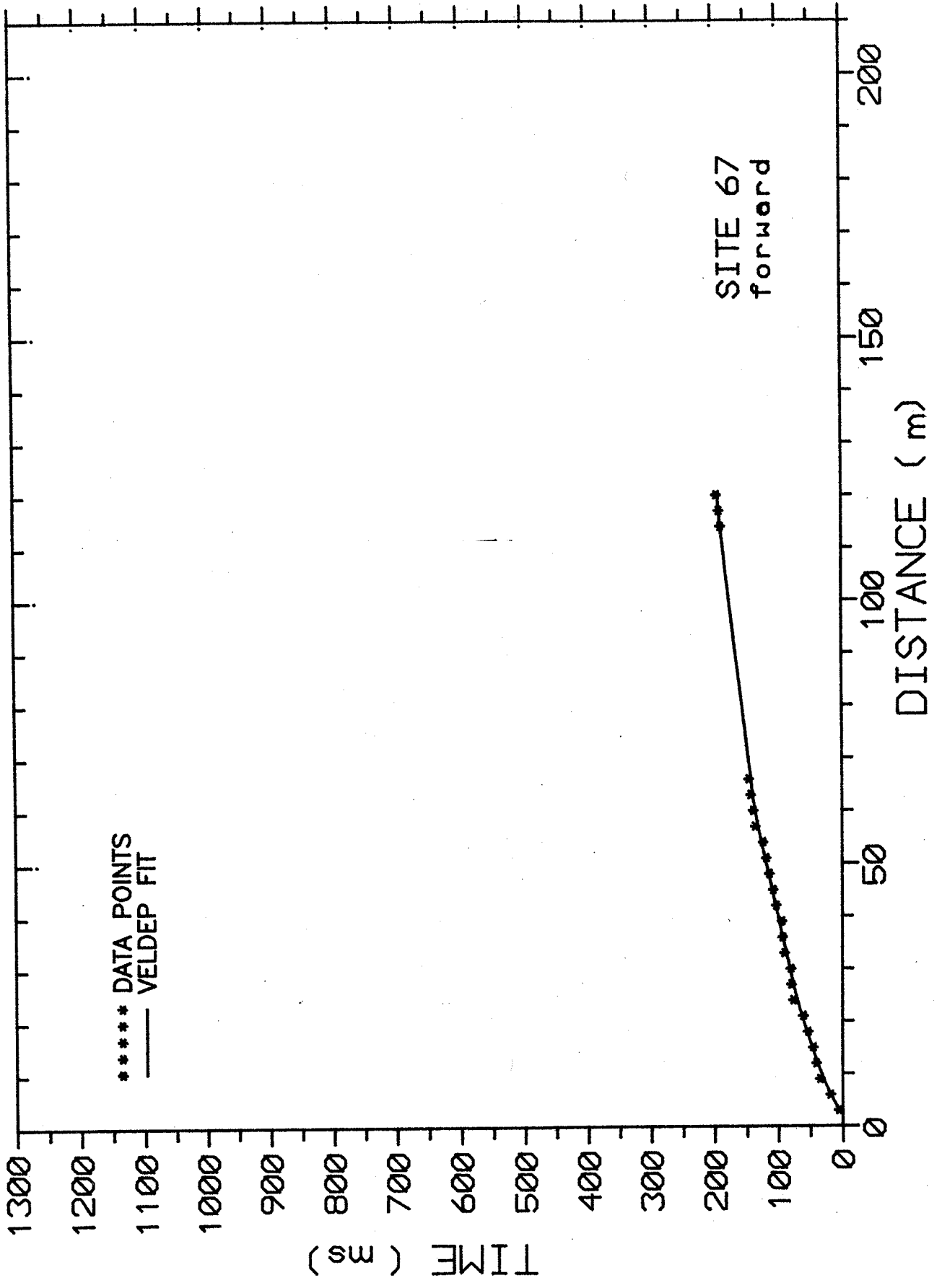












***** DATA POINTS
—— VELDEP FIT

SITE 67
forward

1300

1200

1100

1000

900

800

700

600

500

400

300

200

100

0

TIME (ms)

200

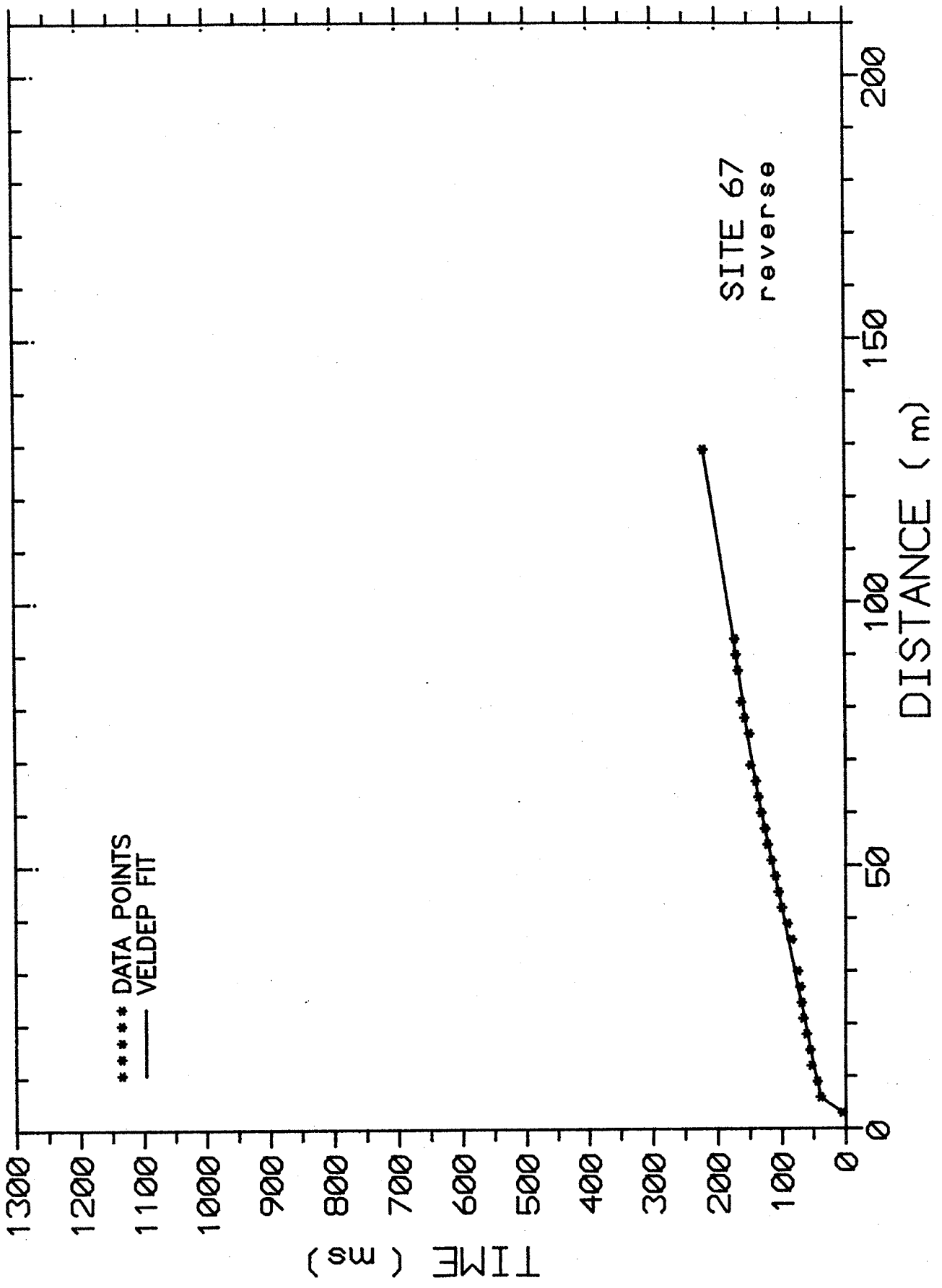
150

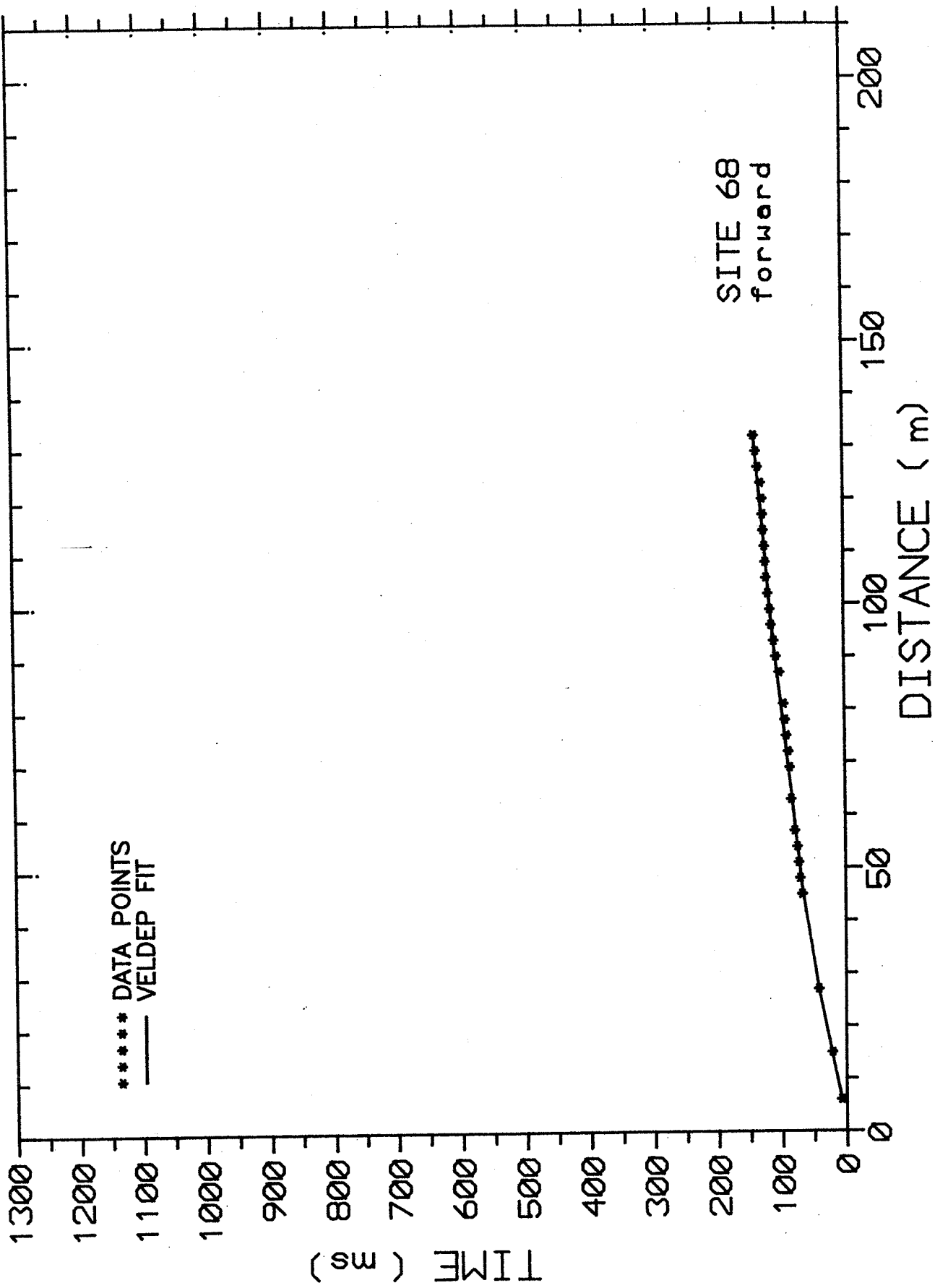
100

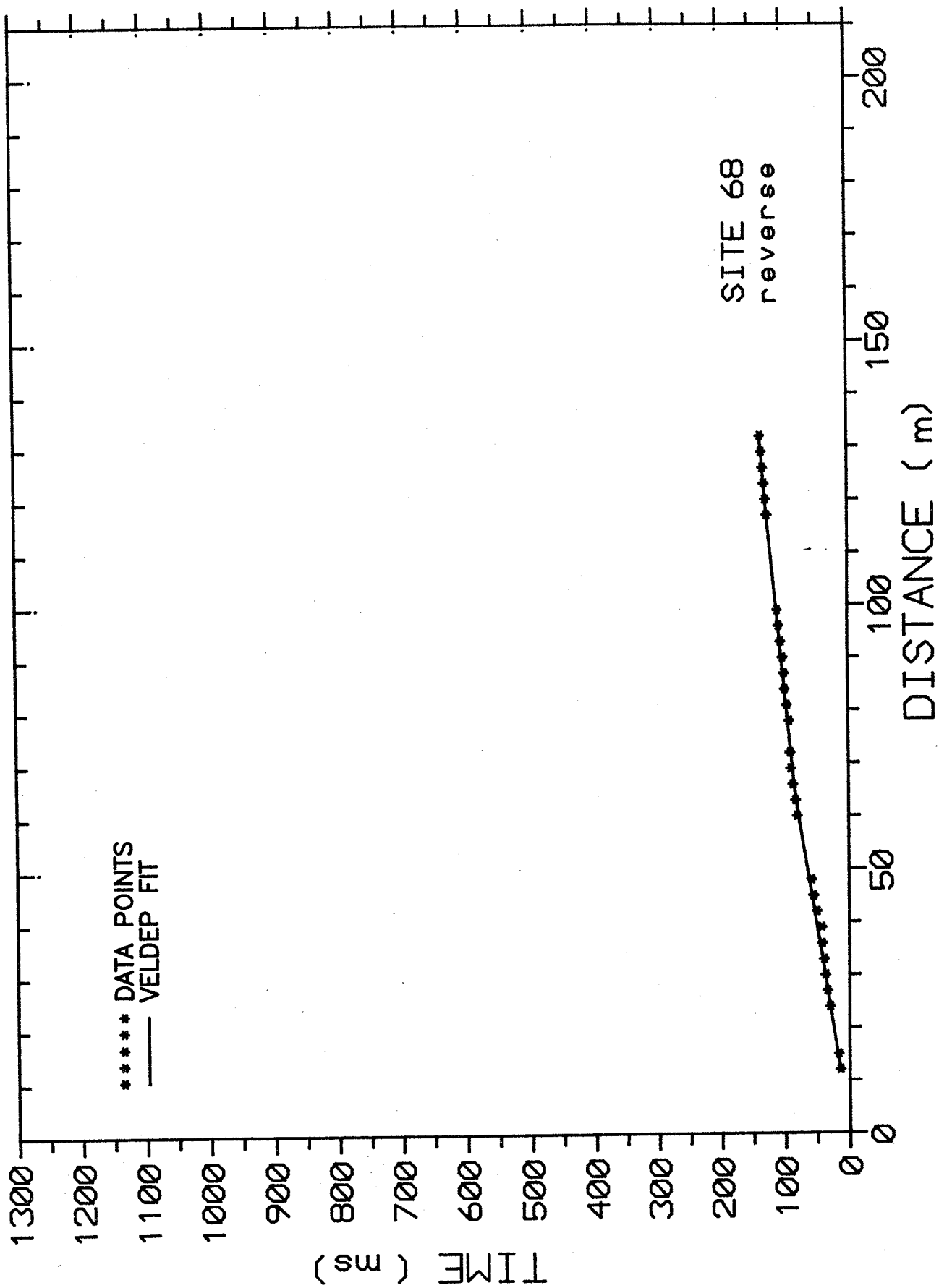
50

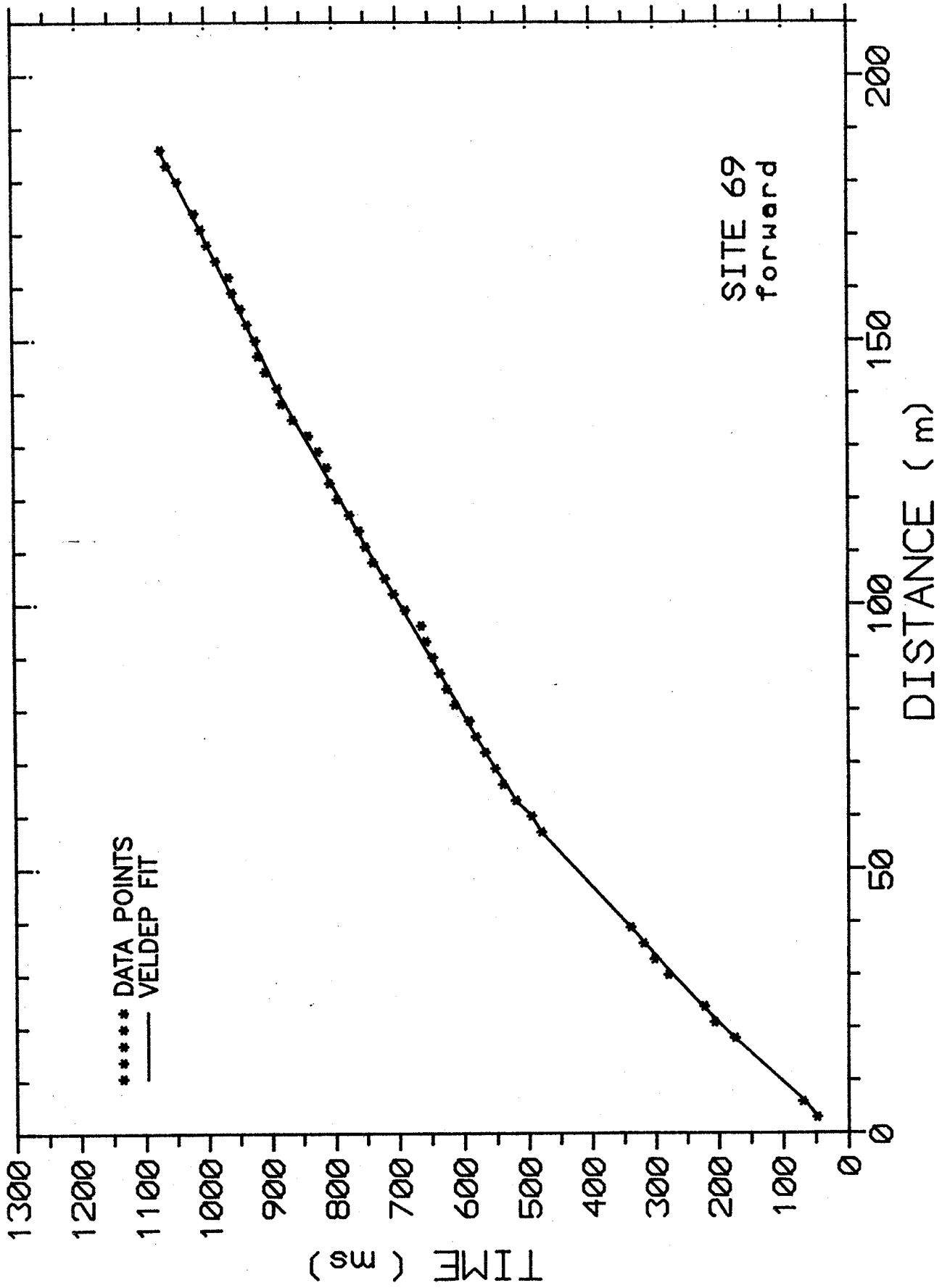
0

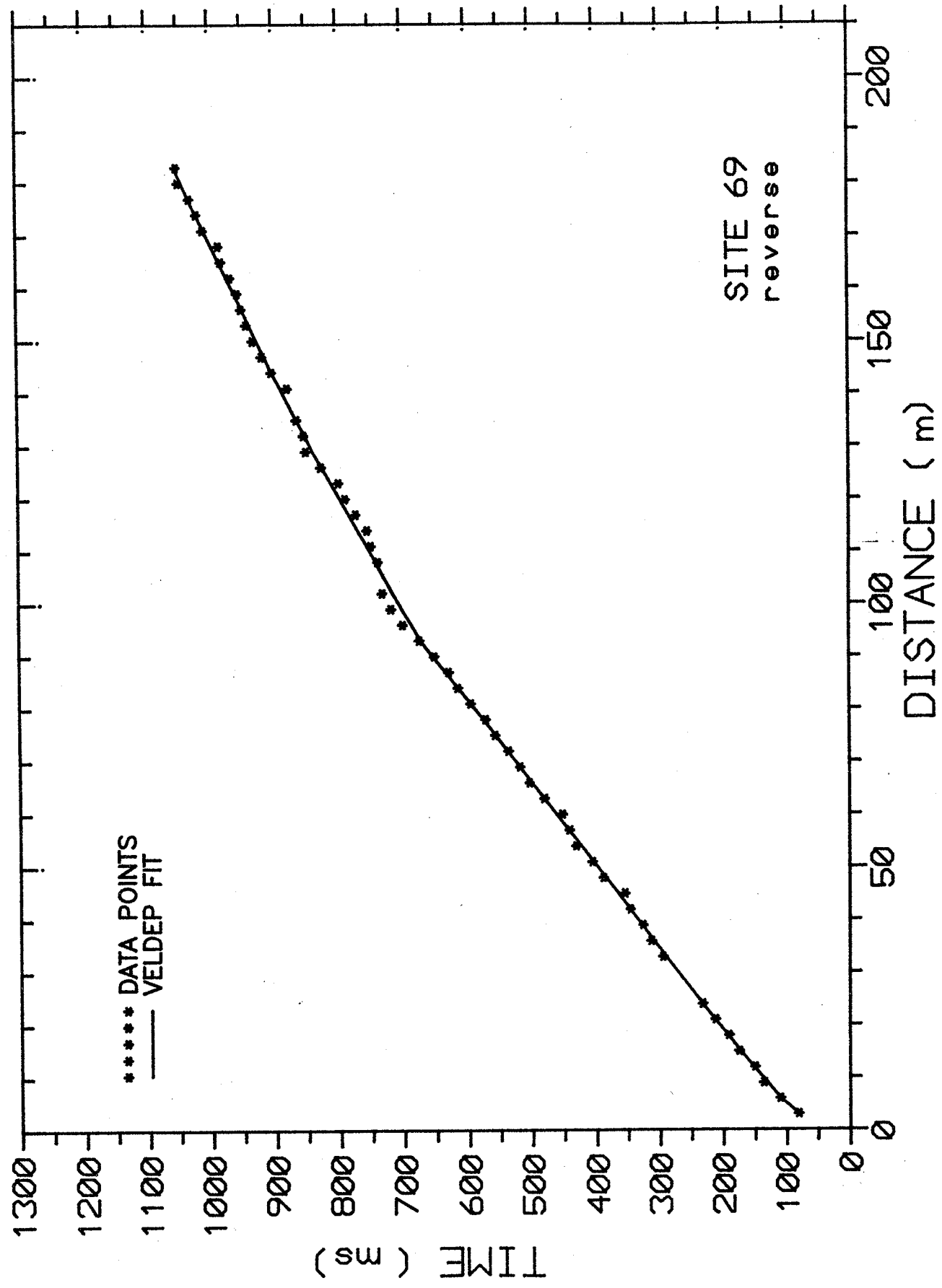
DISTANCE (m)









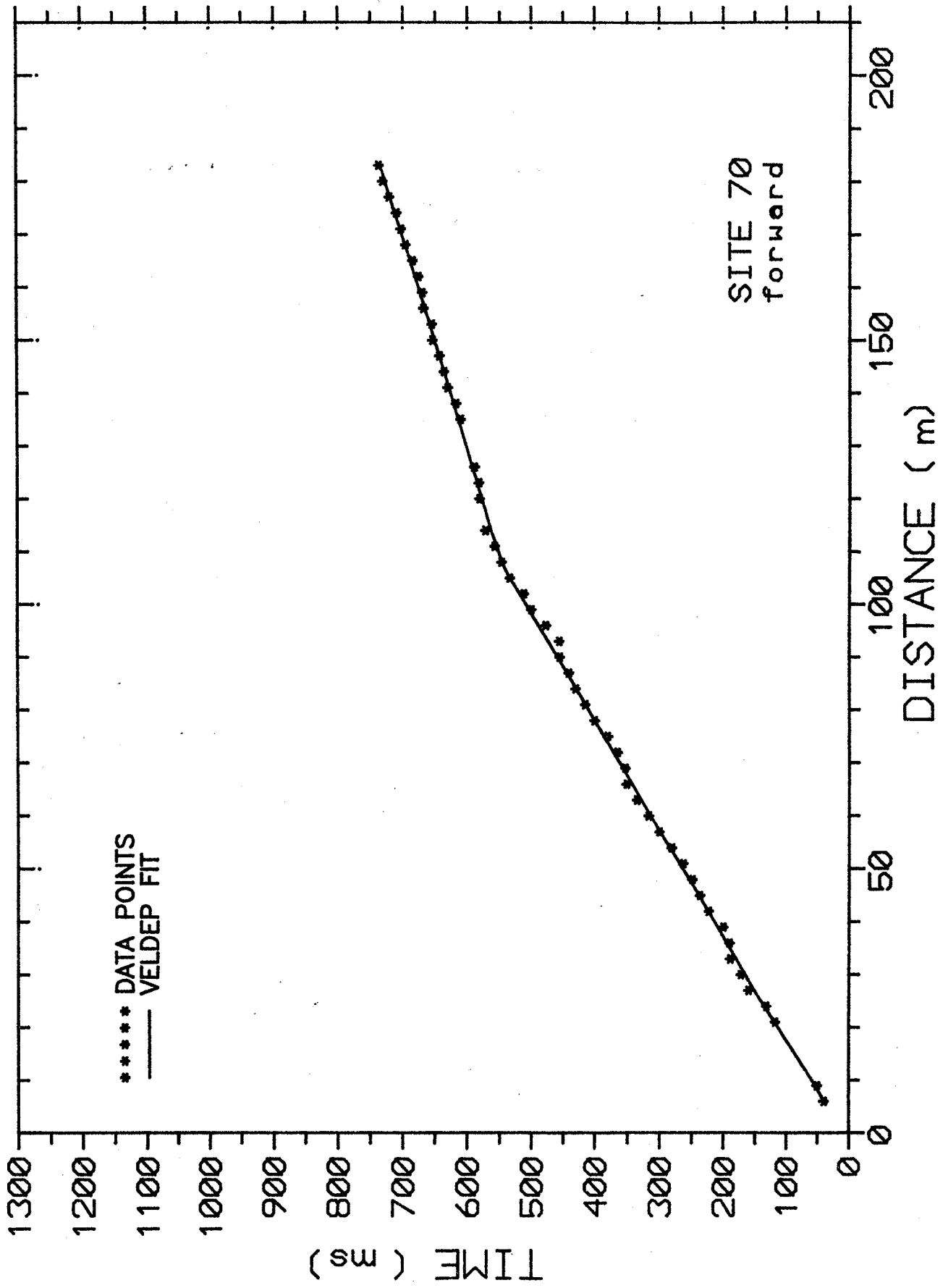


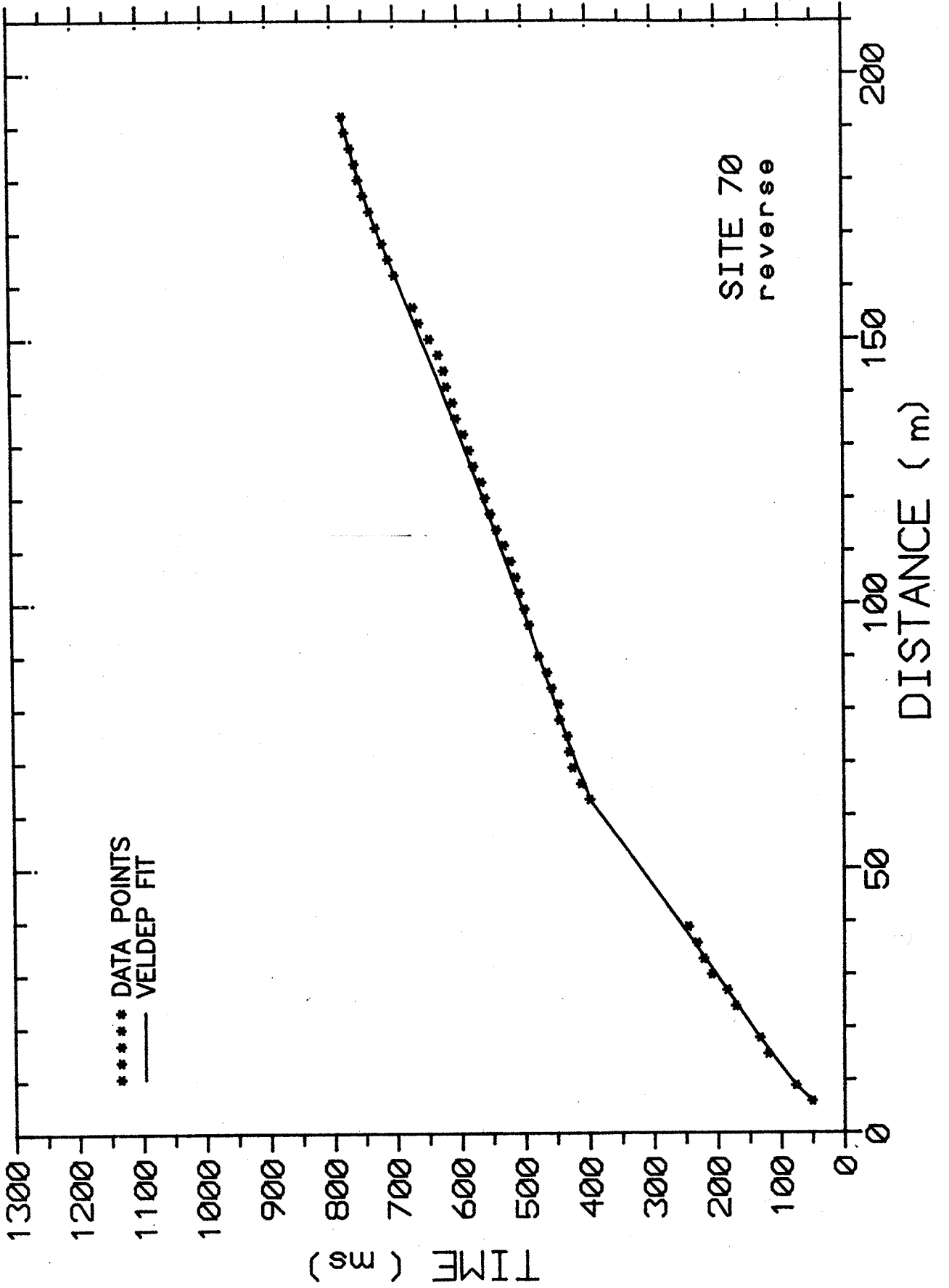
***** DATA POINTS
— VELDEP FIT

SITE 69
reverse

TIME (ms)

DISTANCE (m)





***** DATA POINTS
— VELDEP FIT

SITE 70
reverse

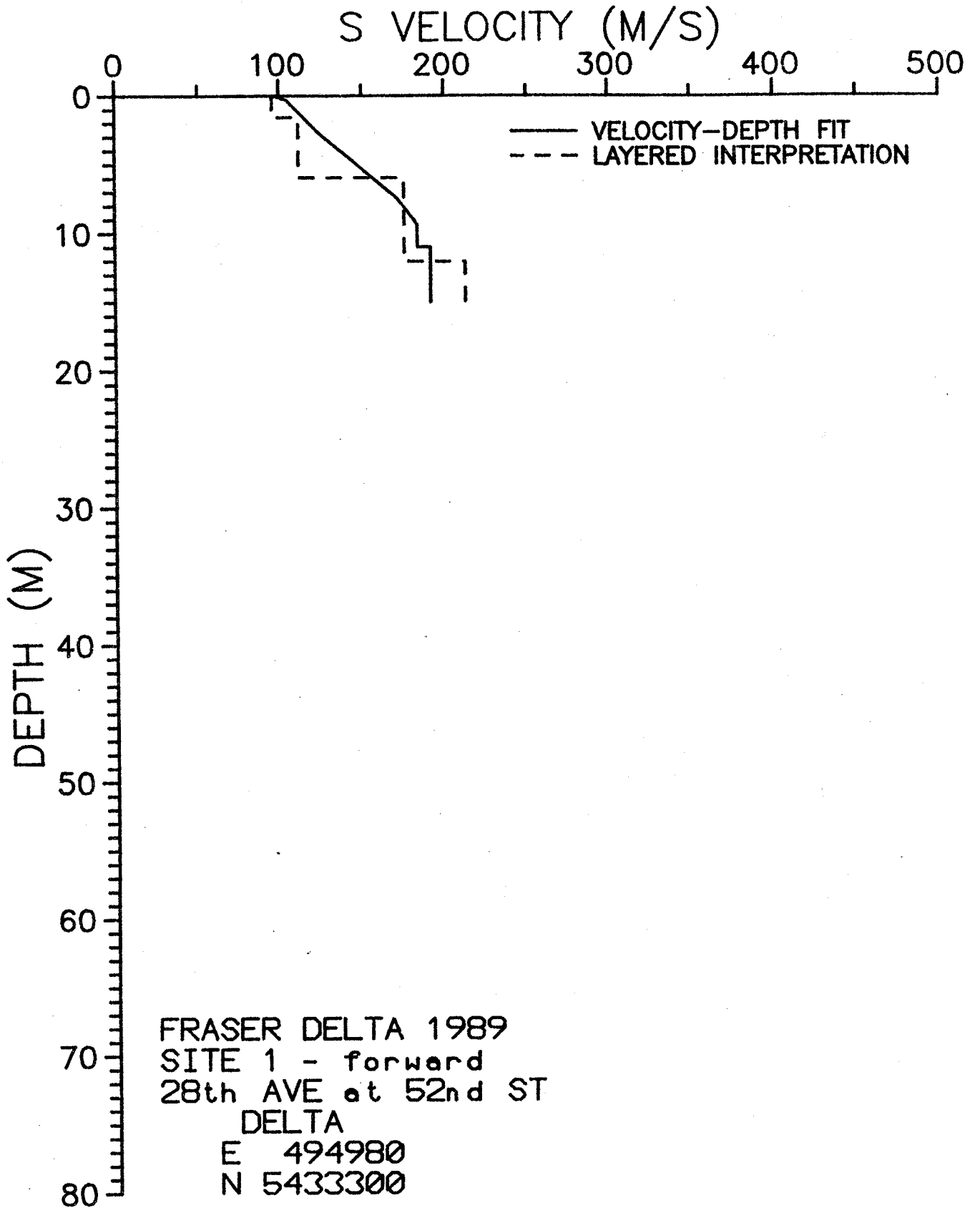
TIME (ms)

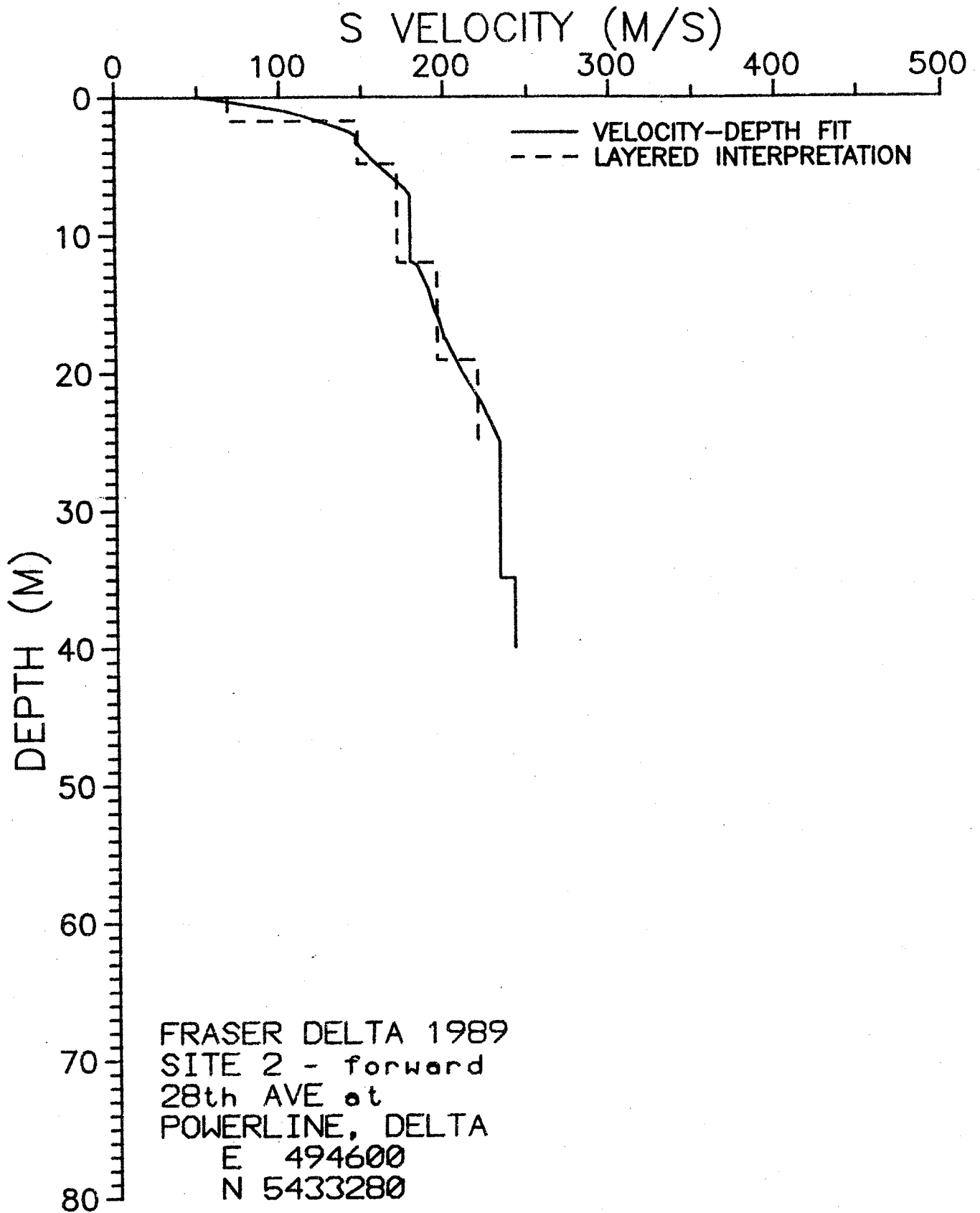
DISTANCE (m)

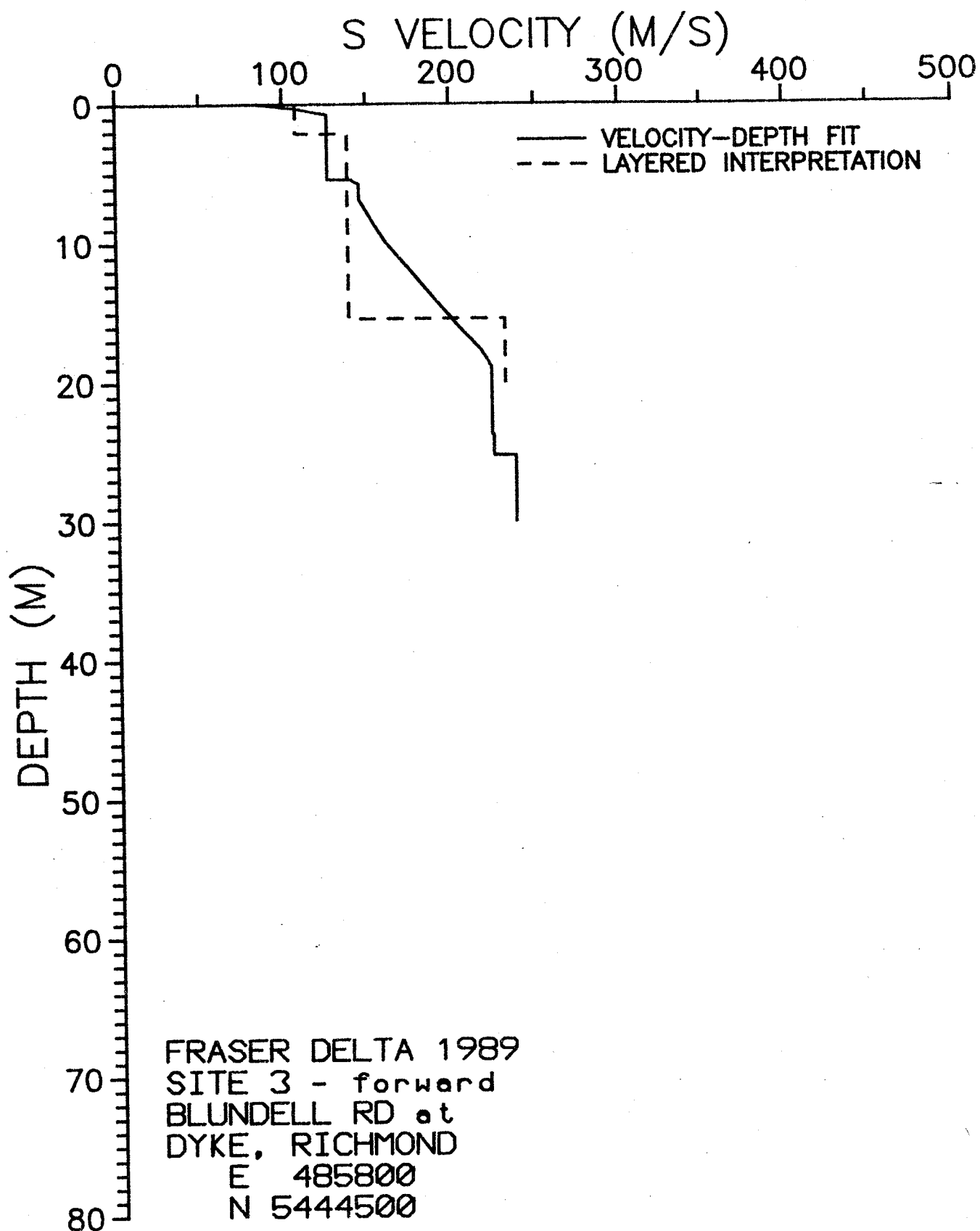
SECTION II

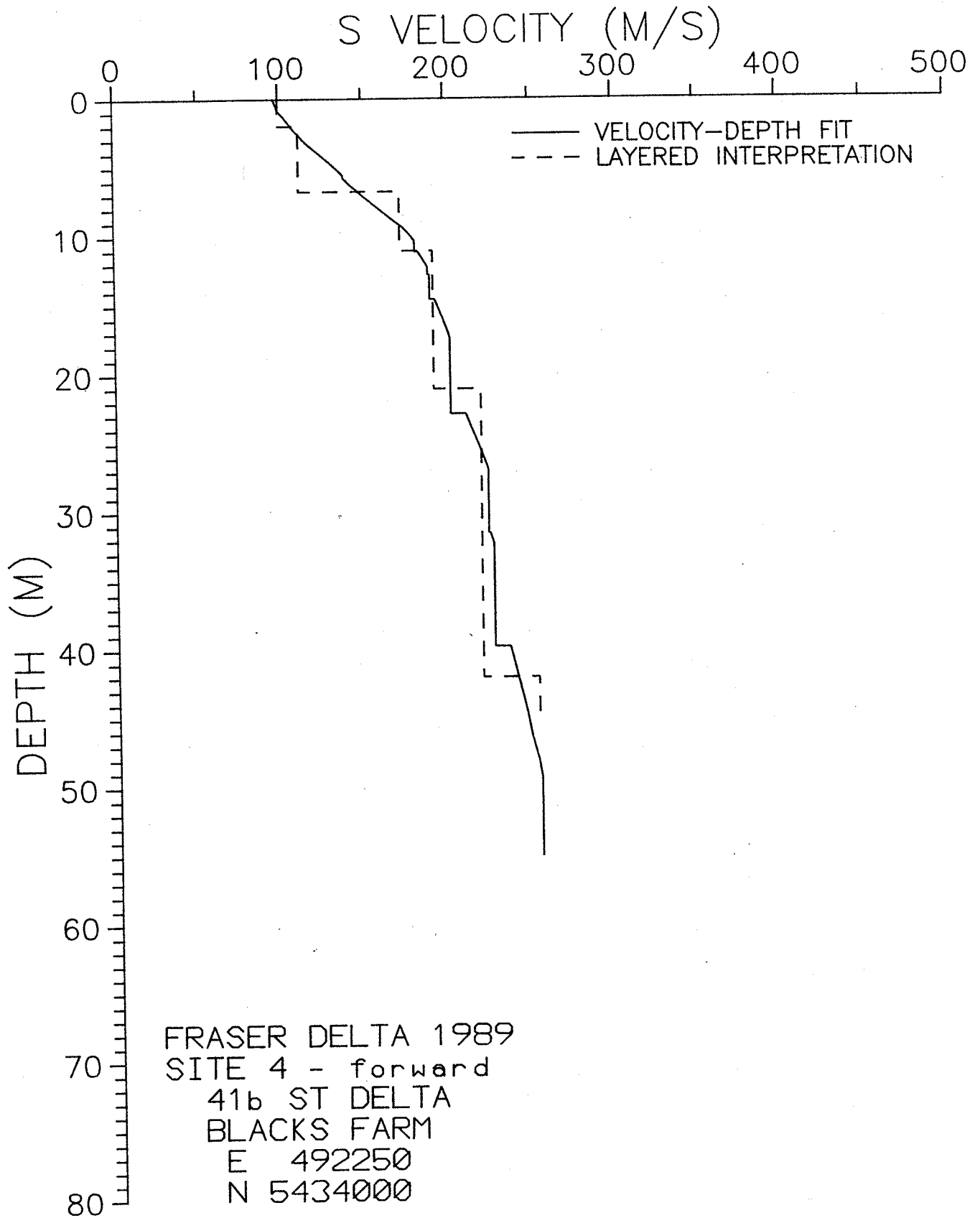
VELOCITY - DEPTH INTERPRETATIONS

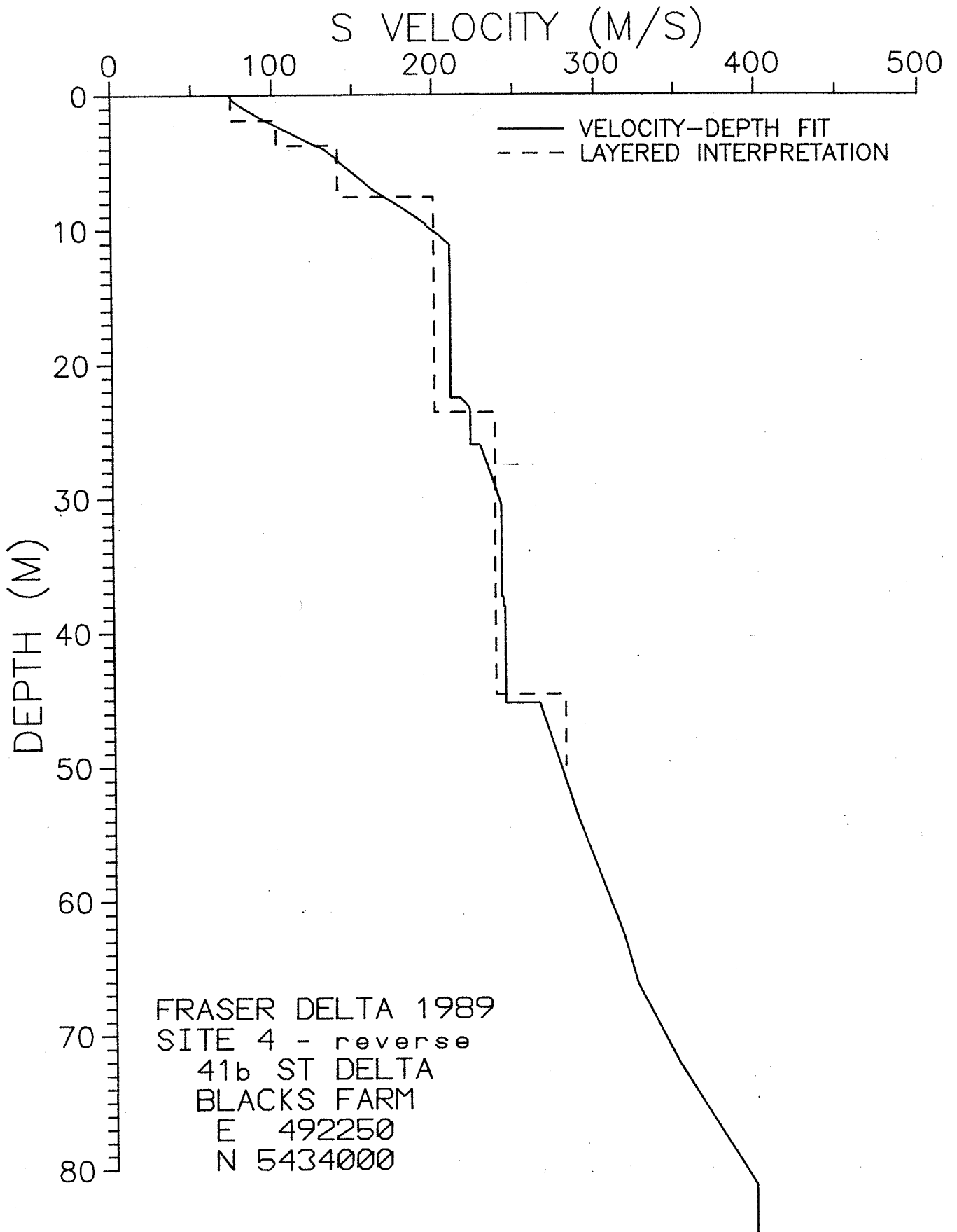
SITES 1 TO 70

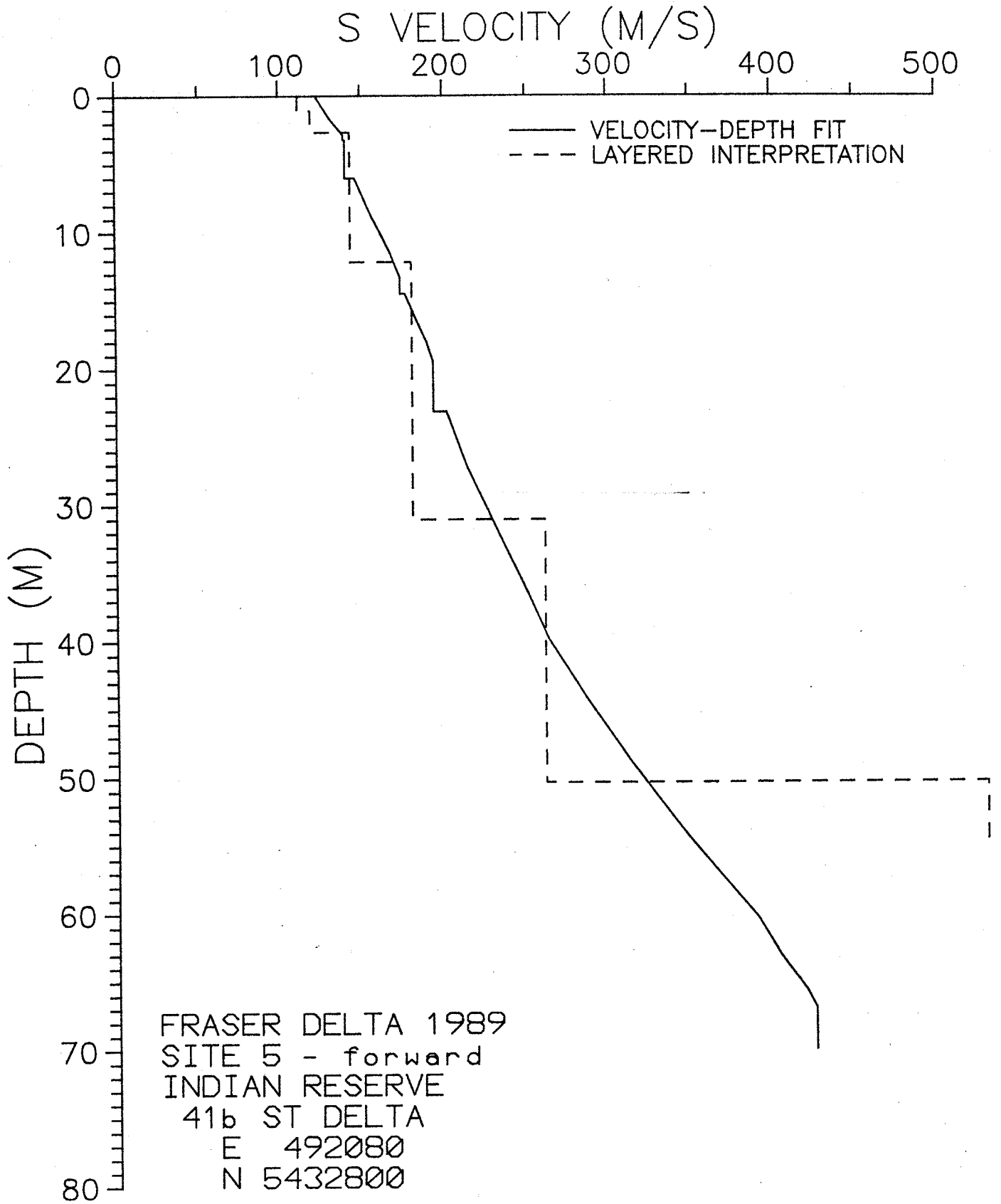


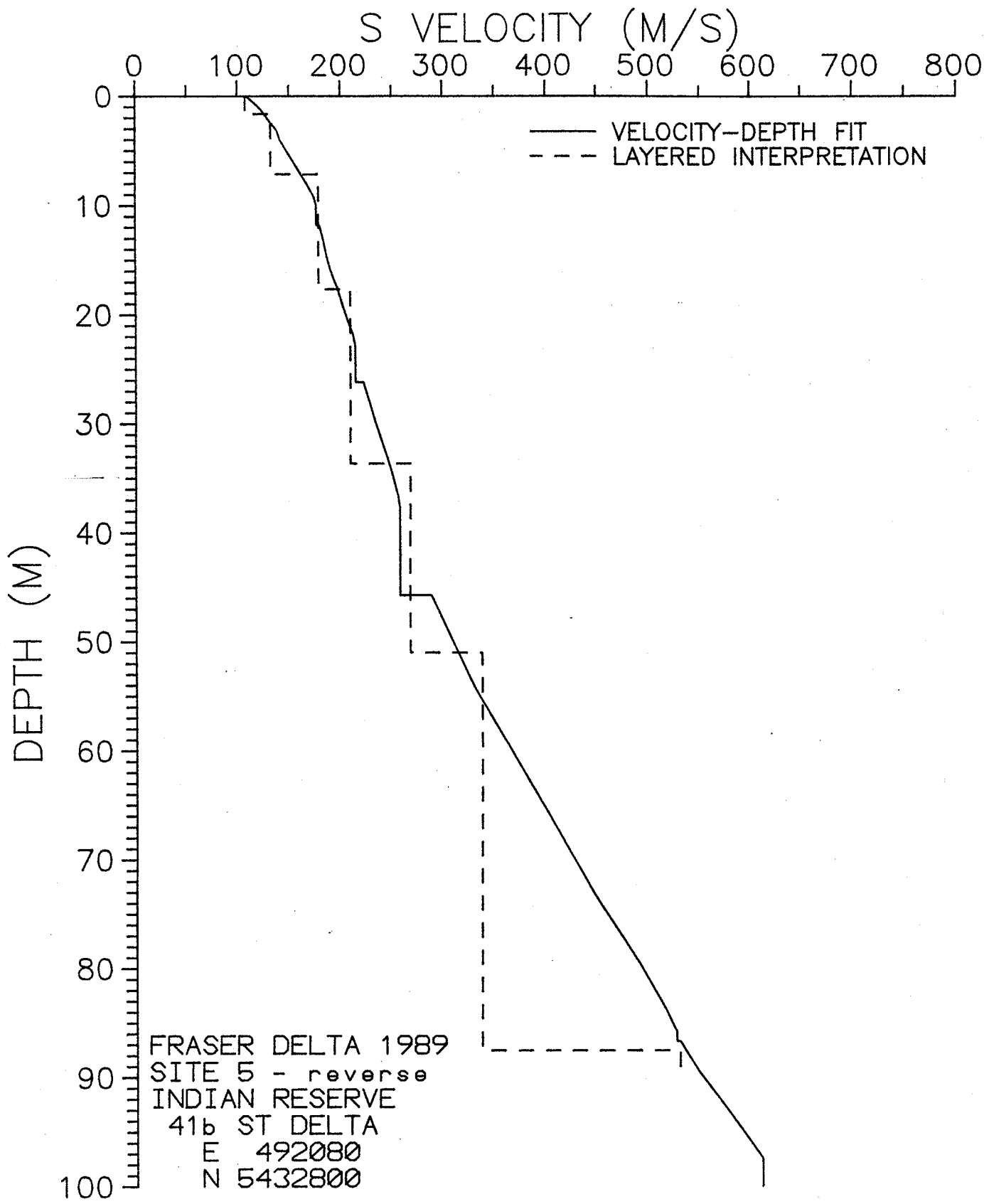


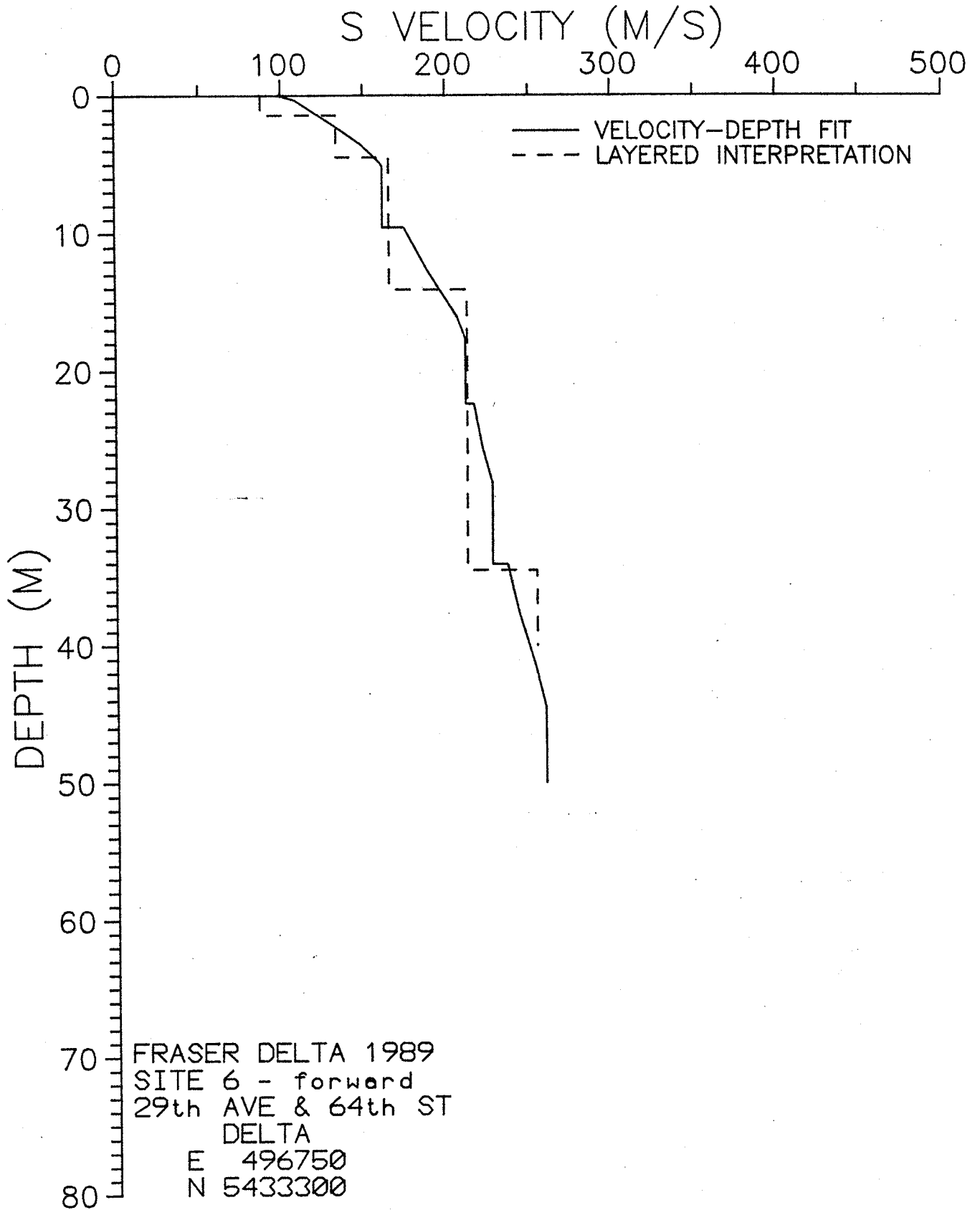


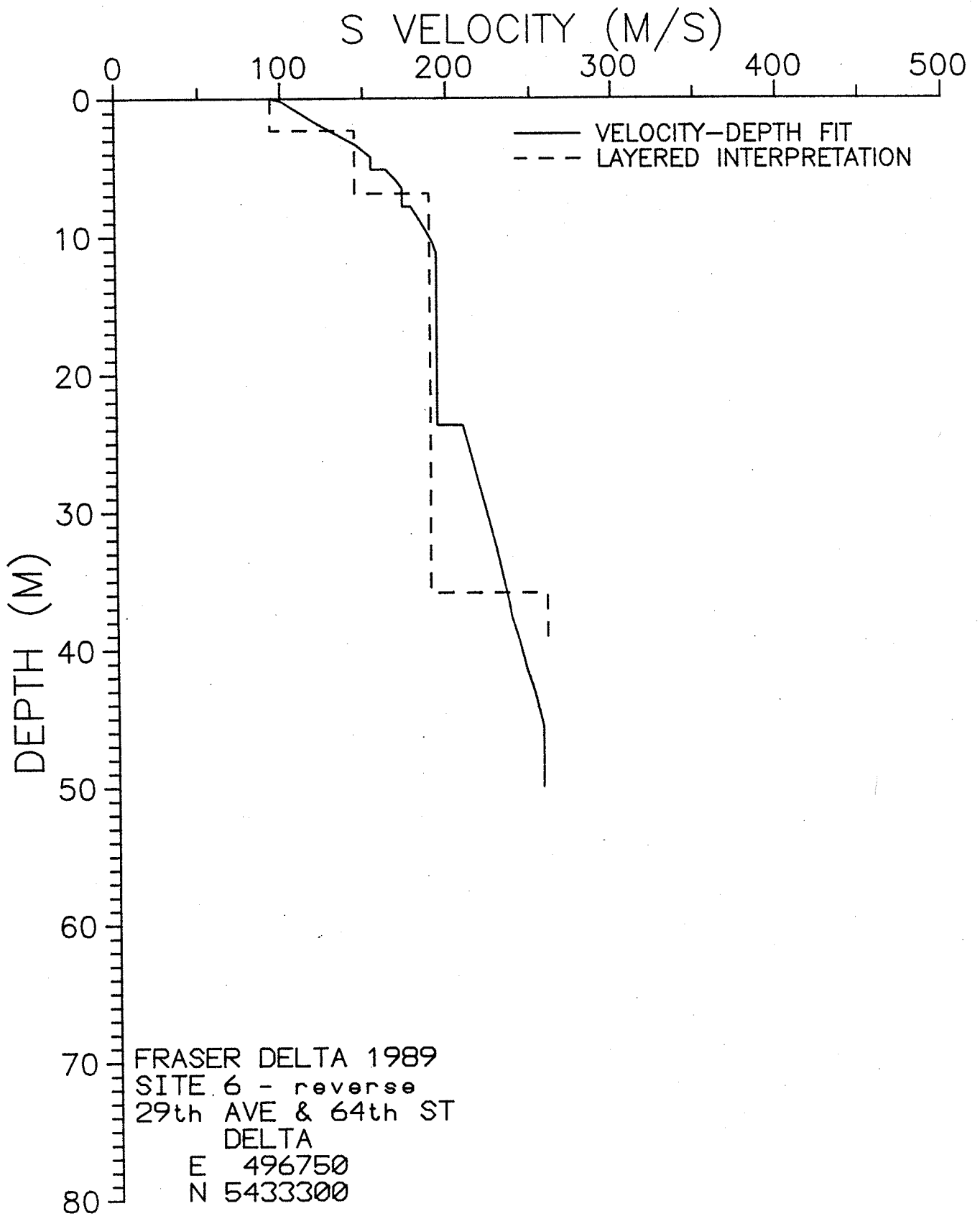


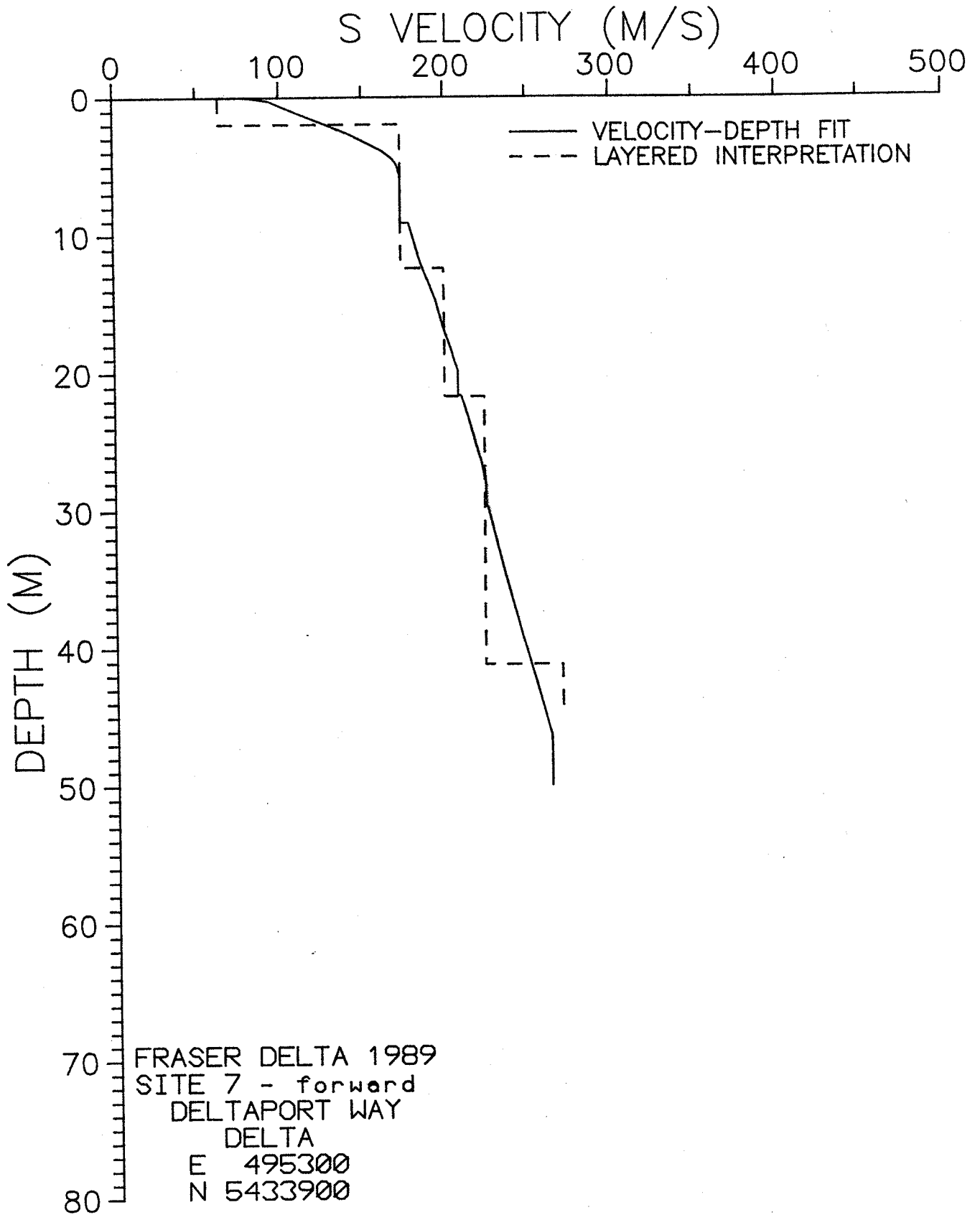


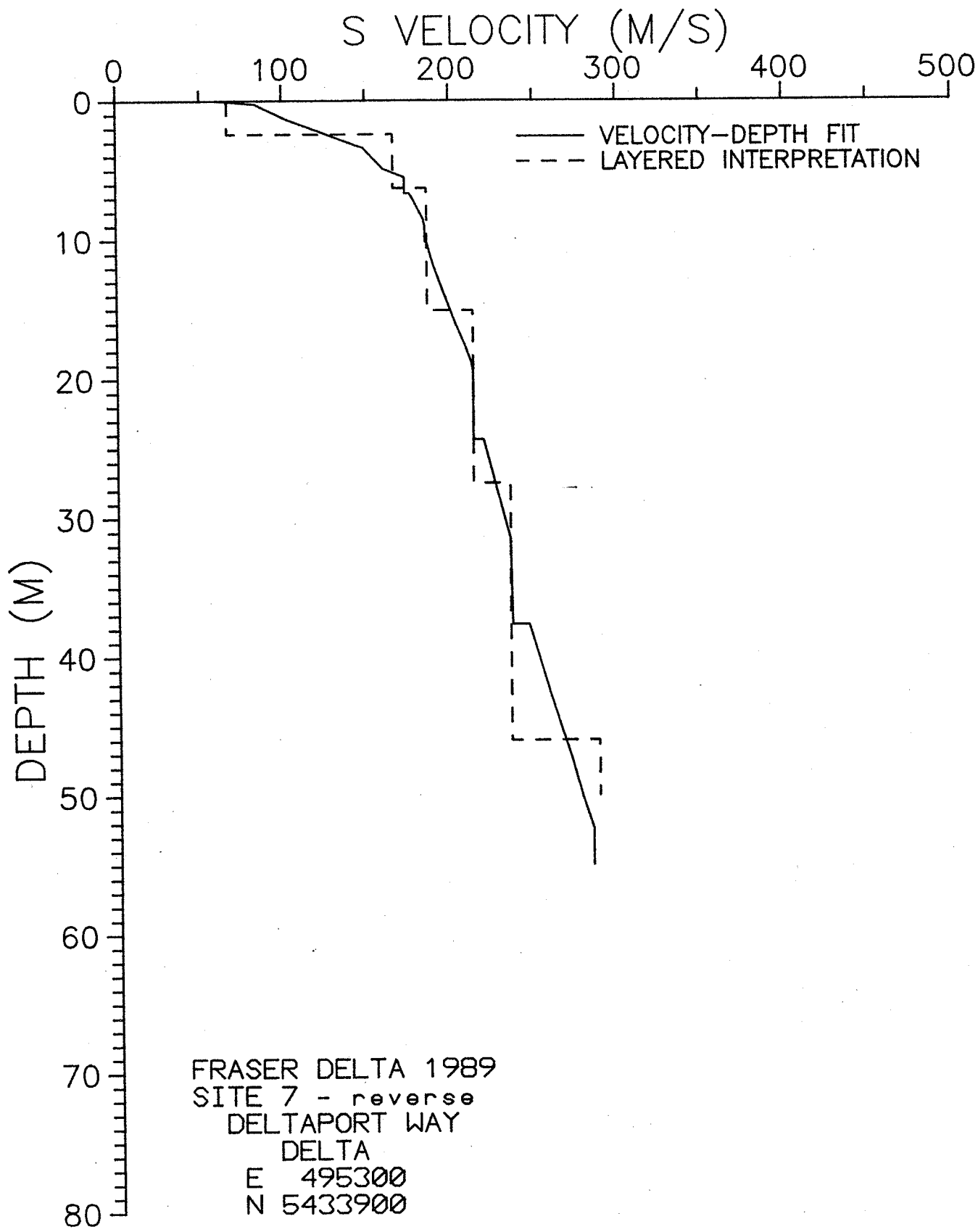


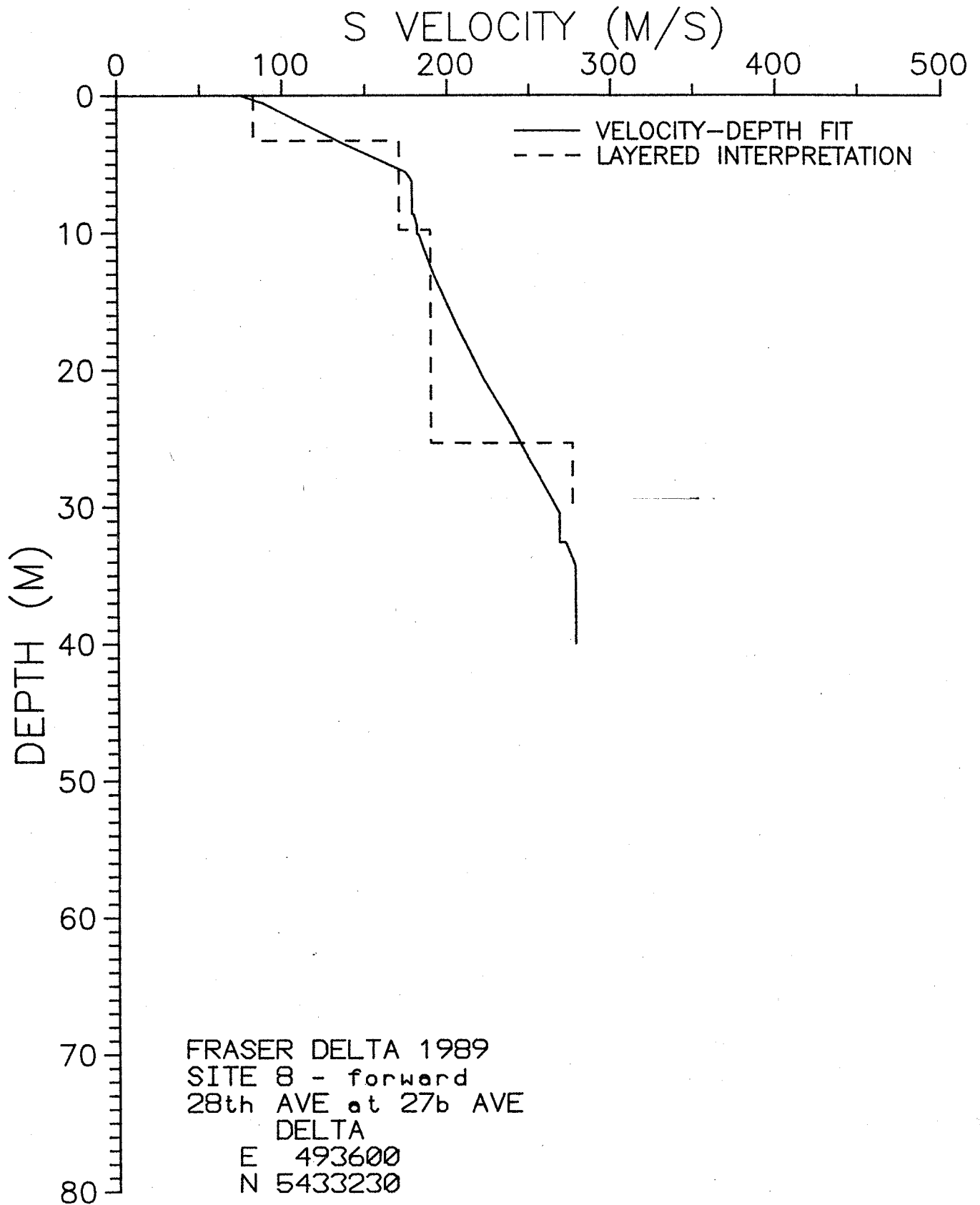


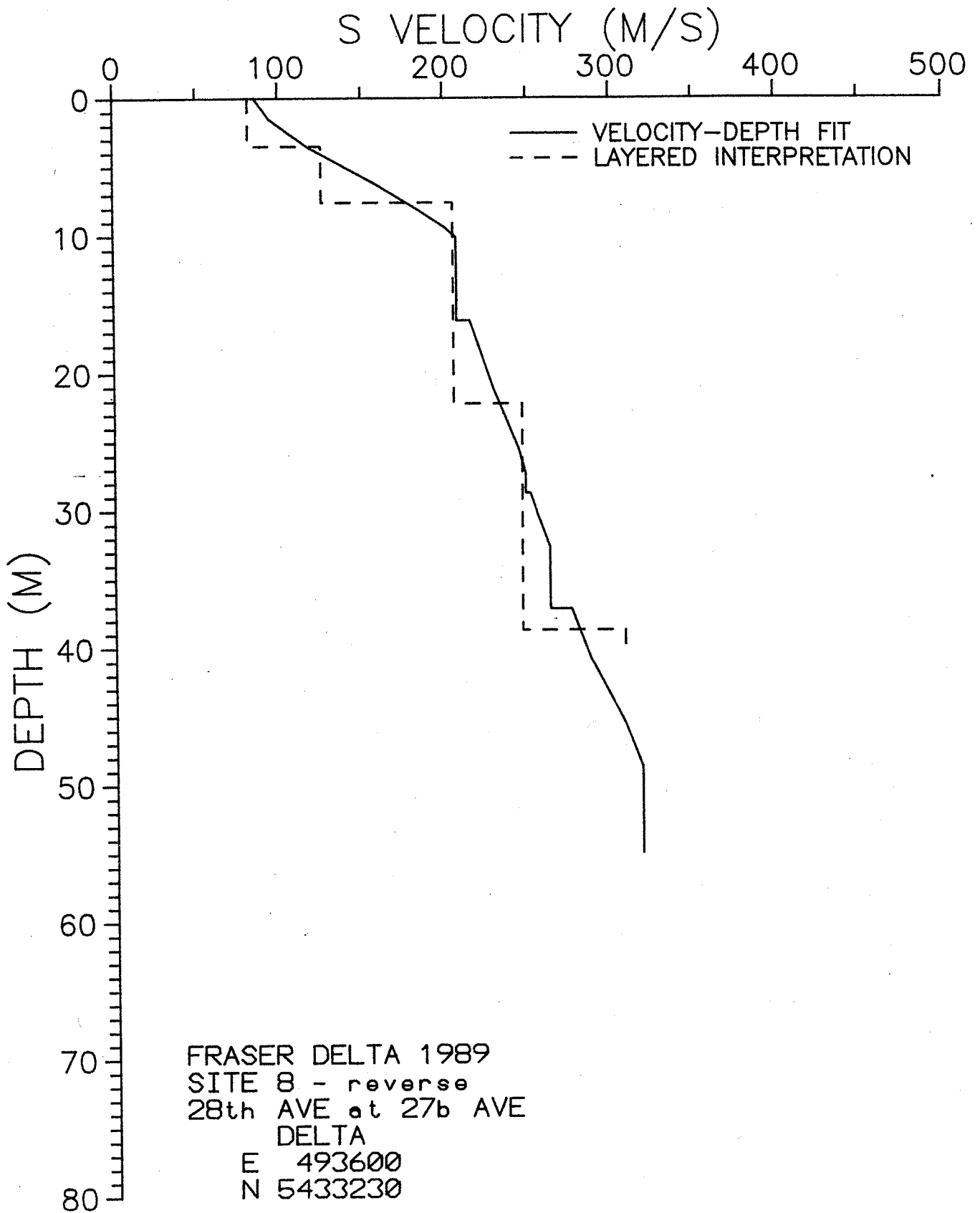


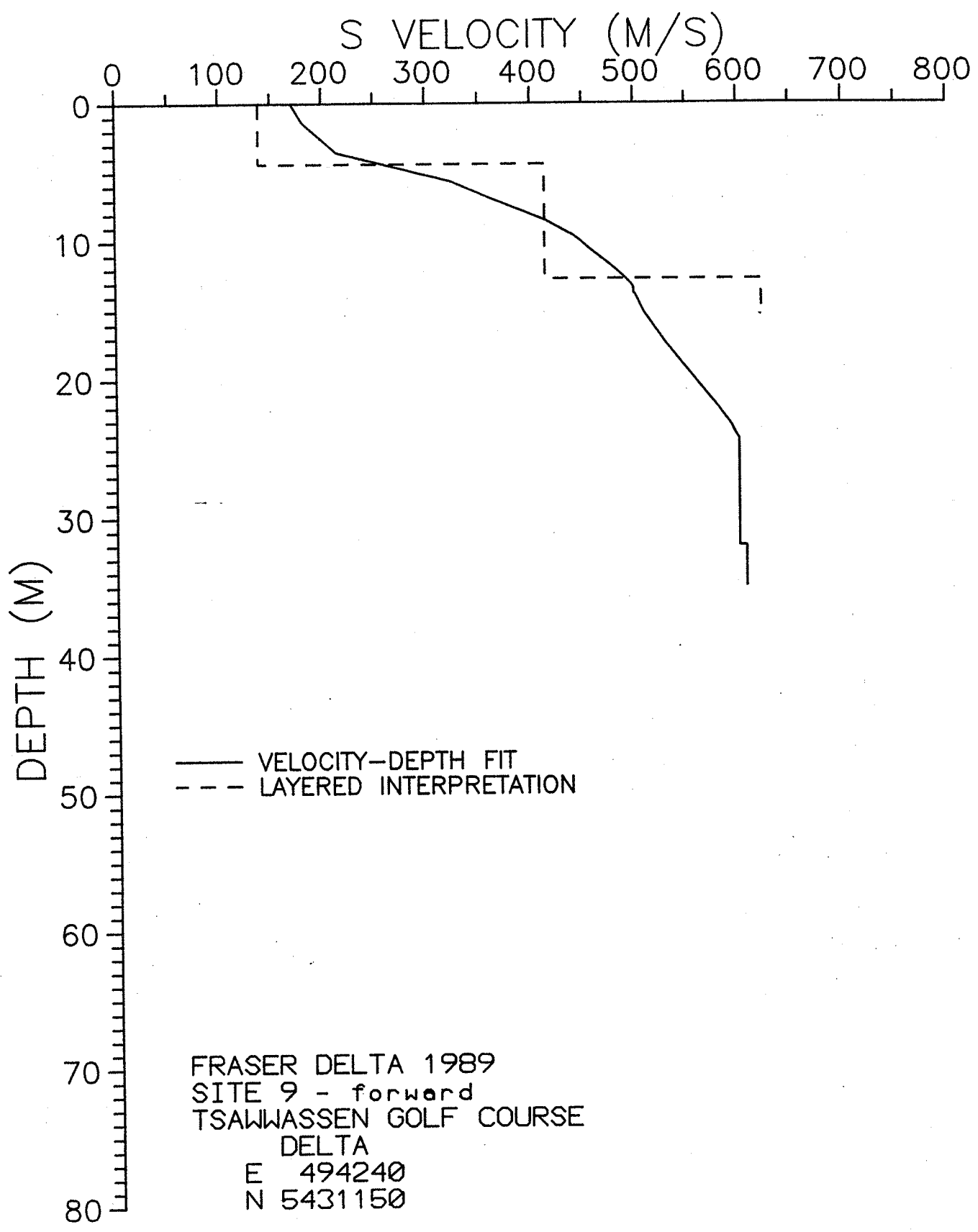


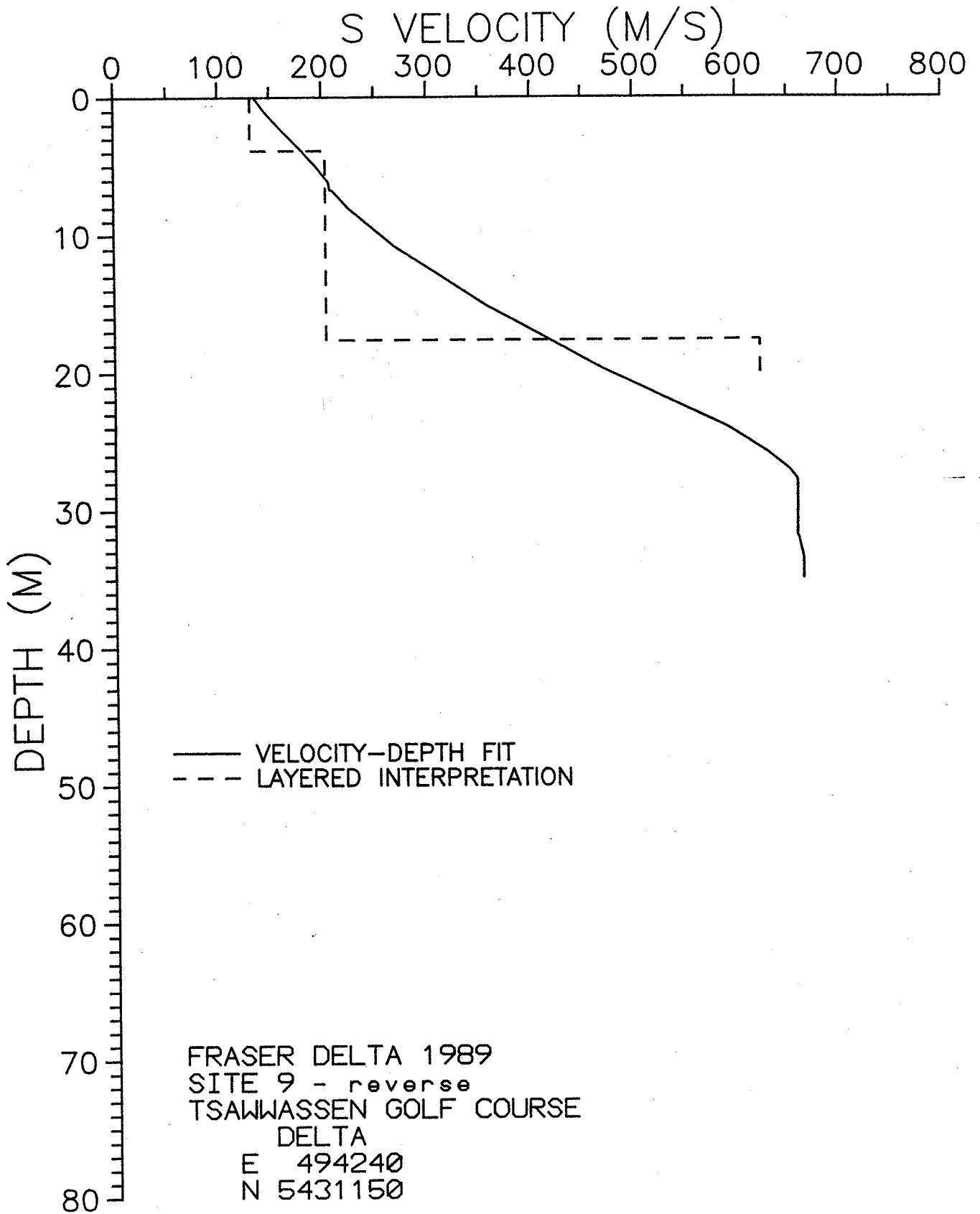


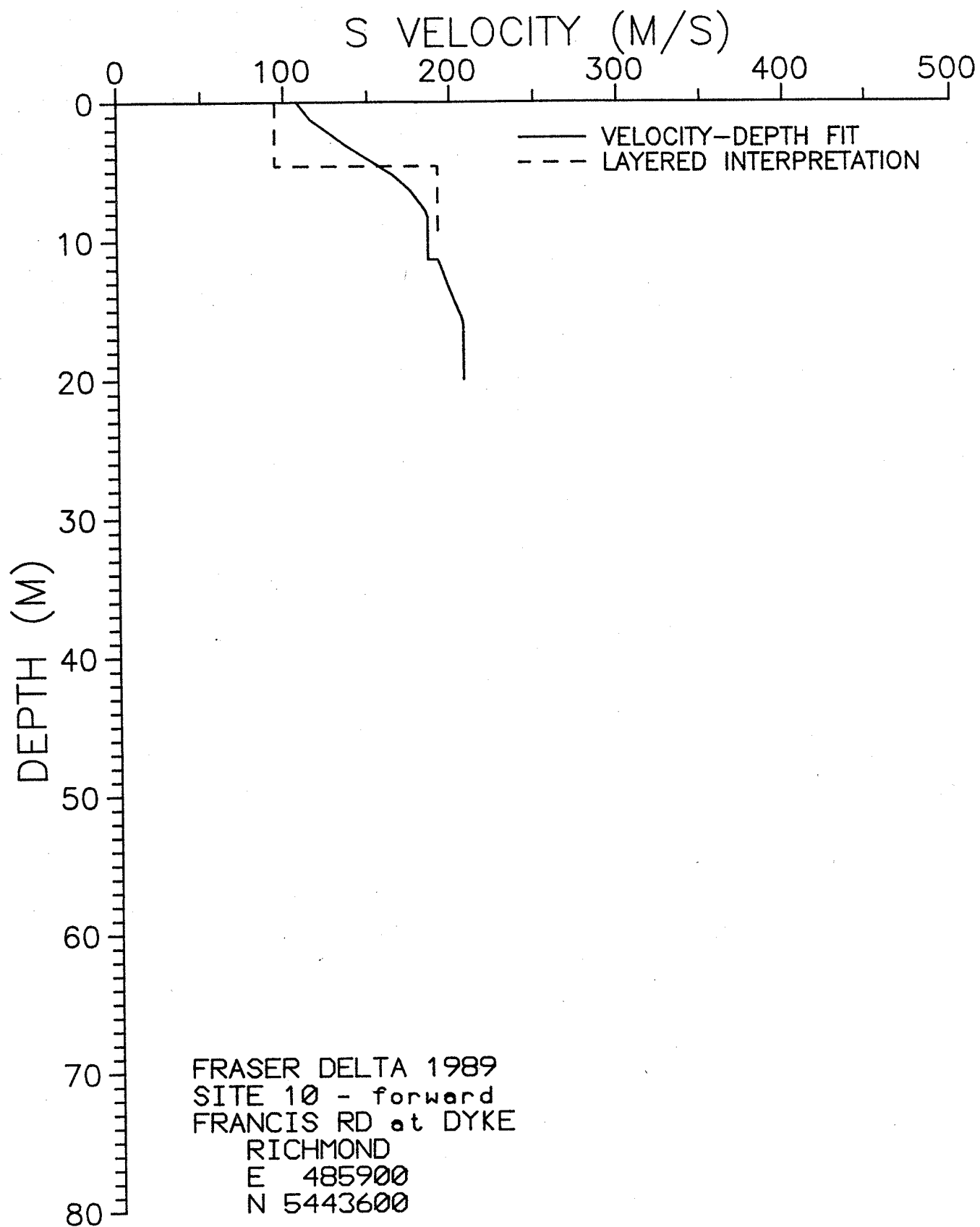


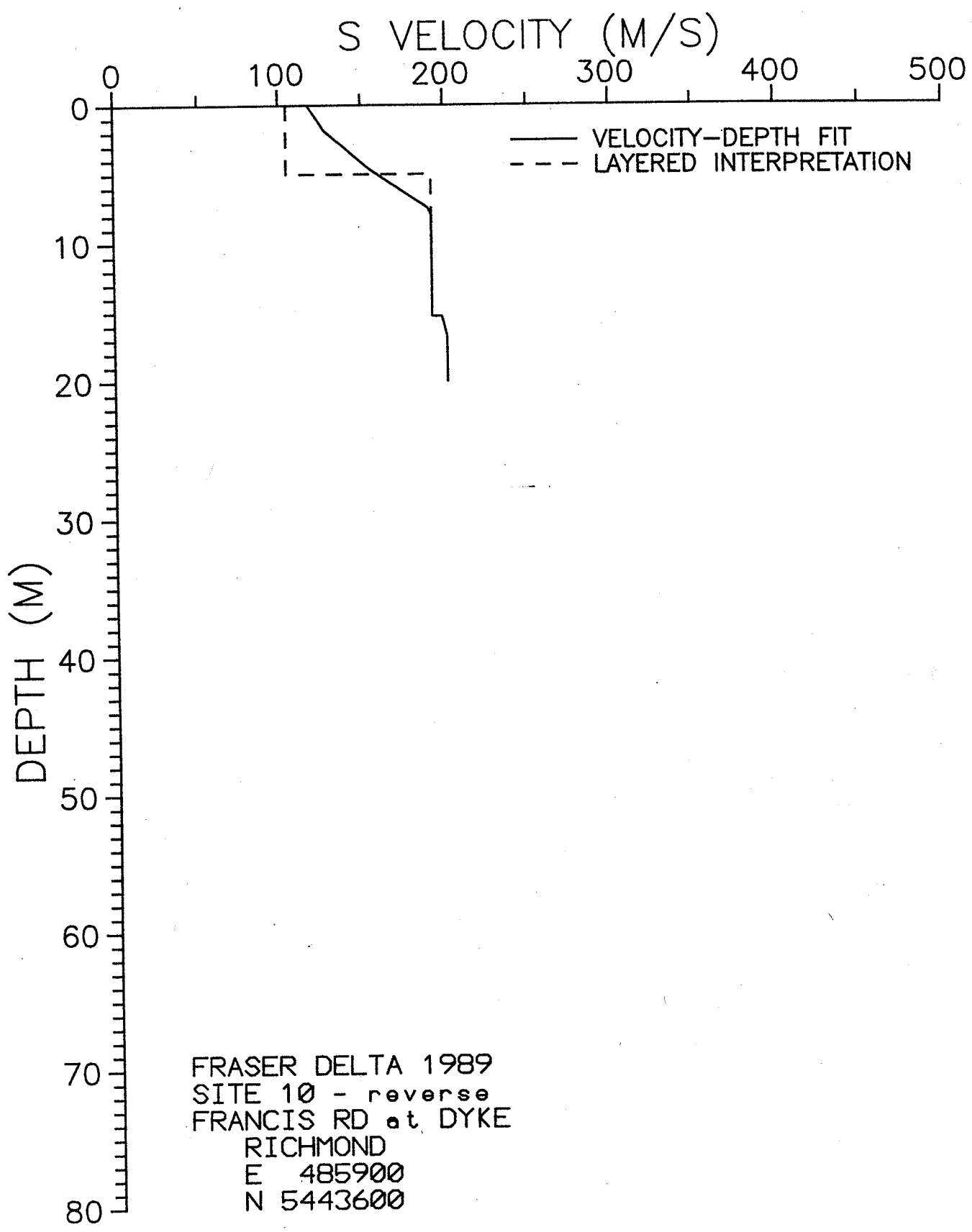


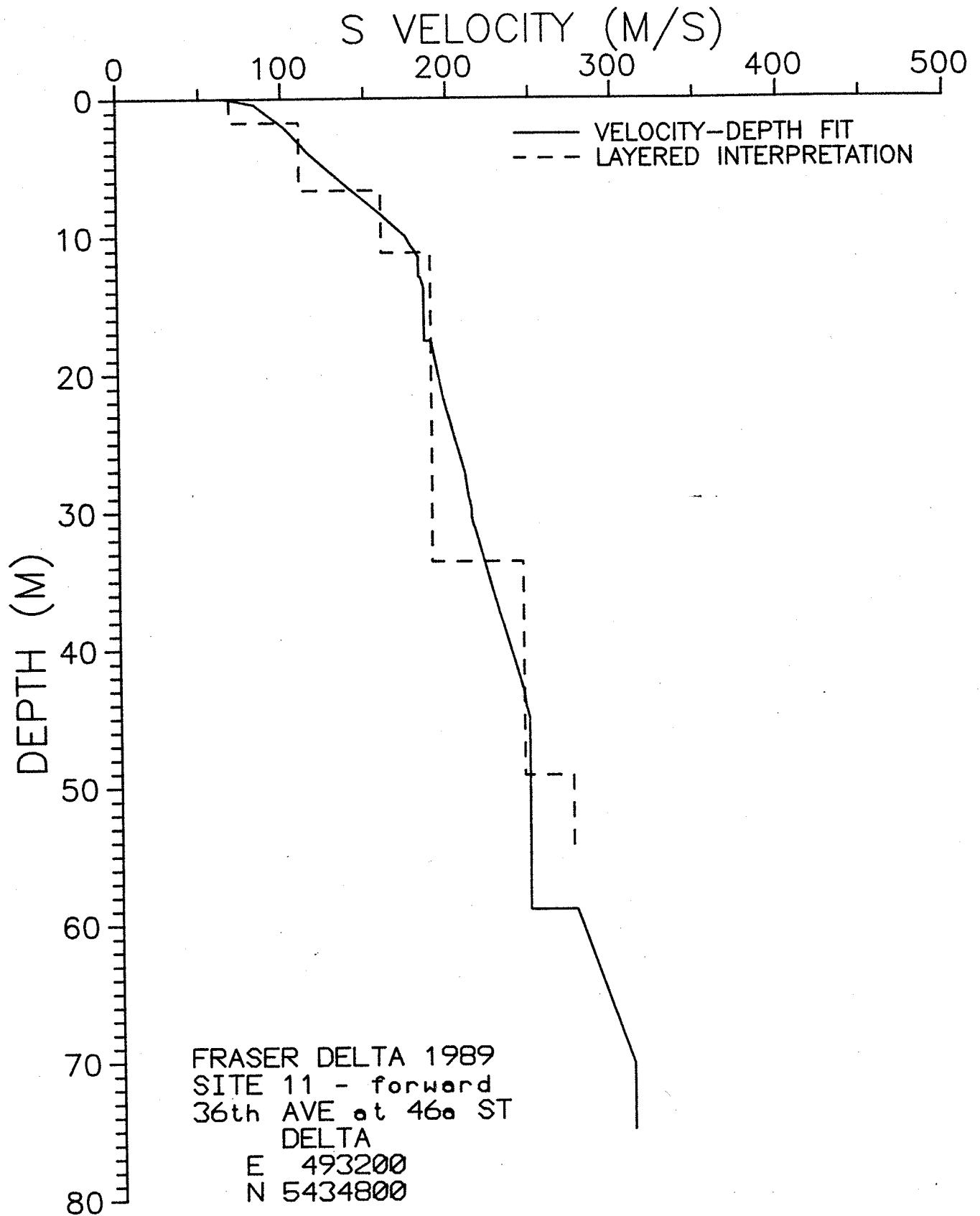


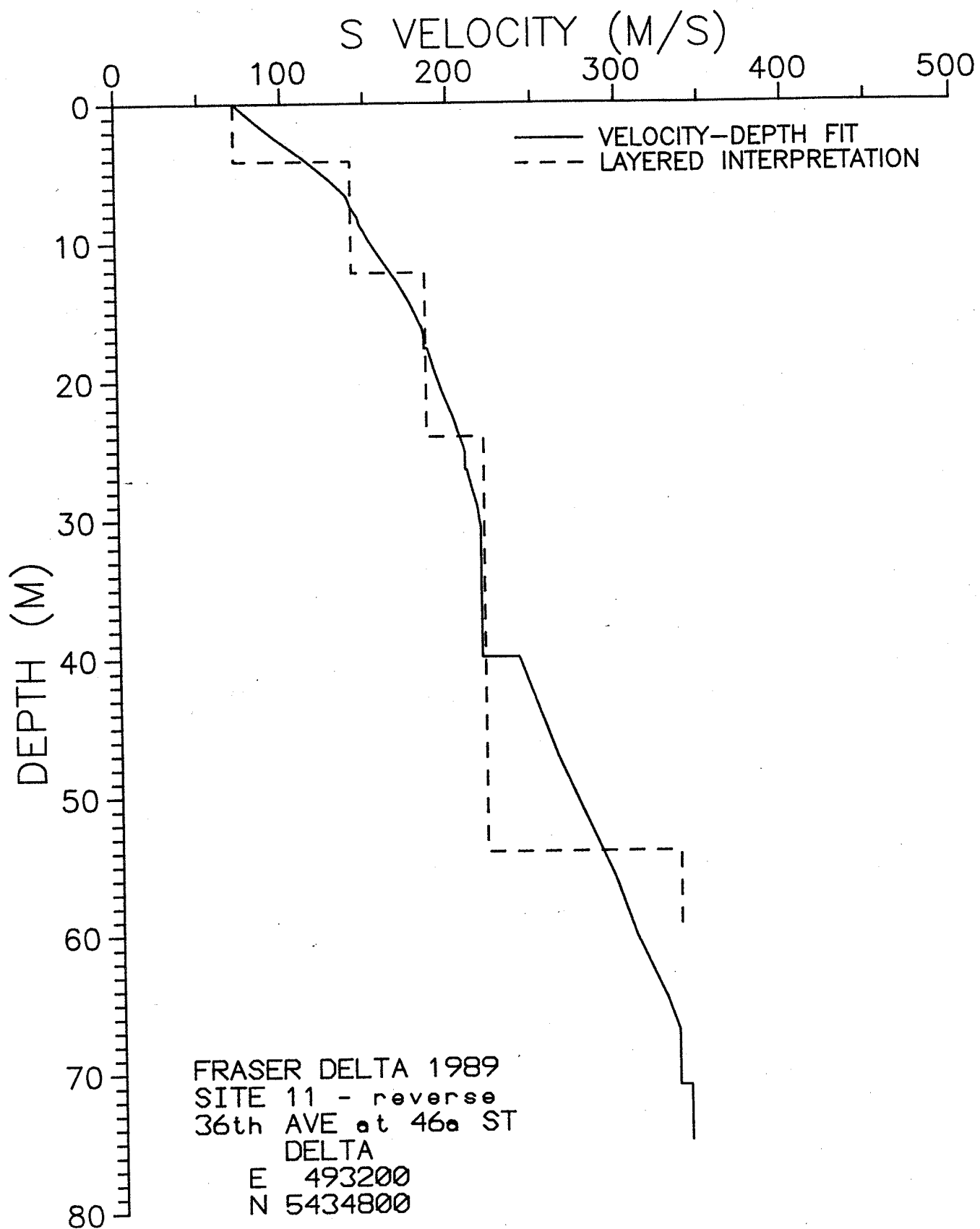


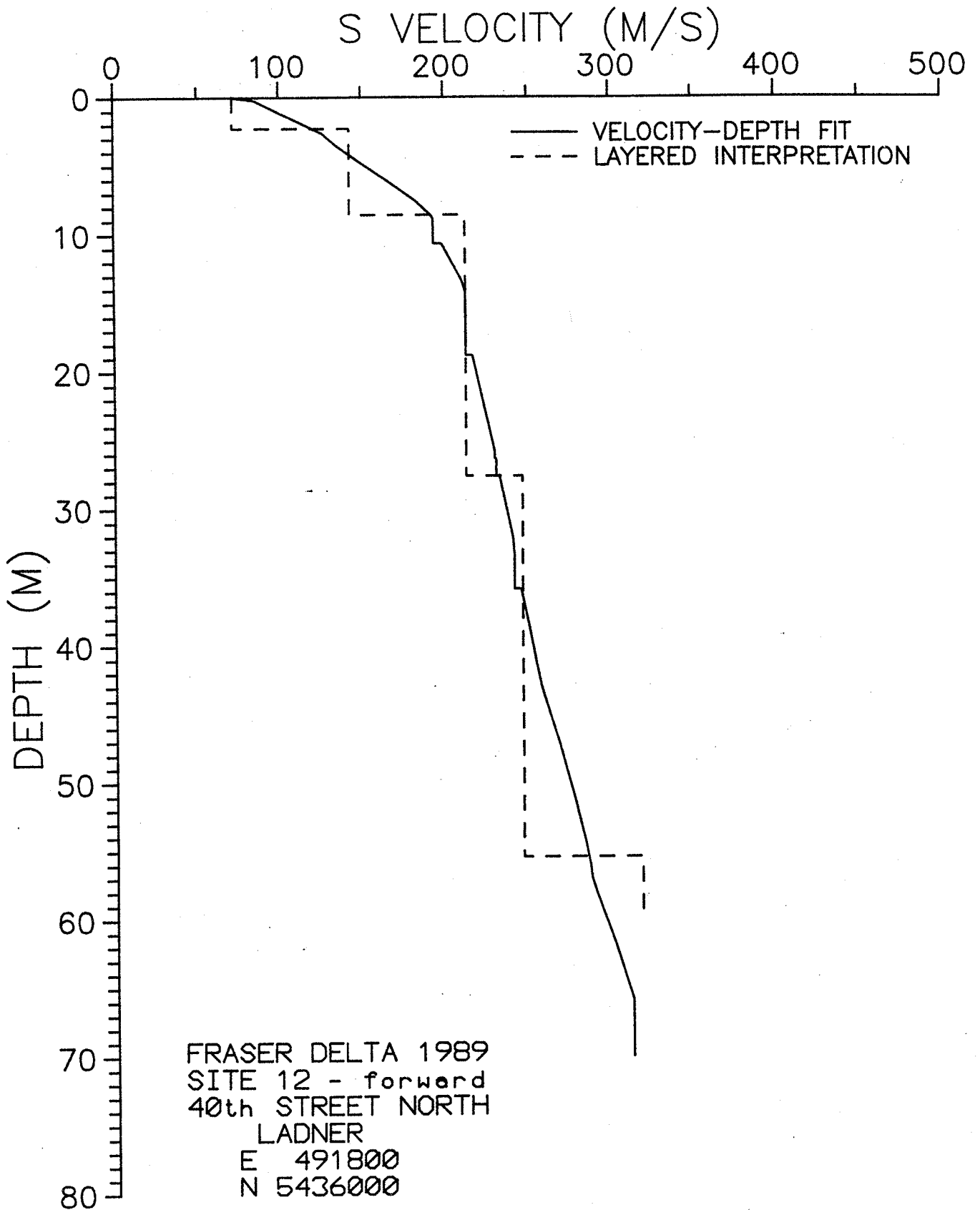


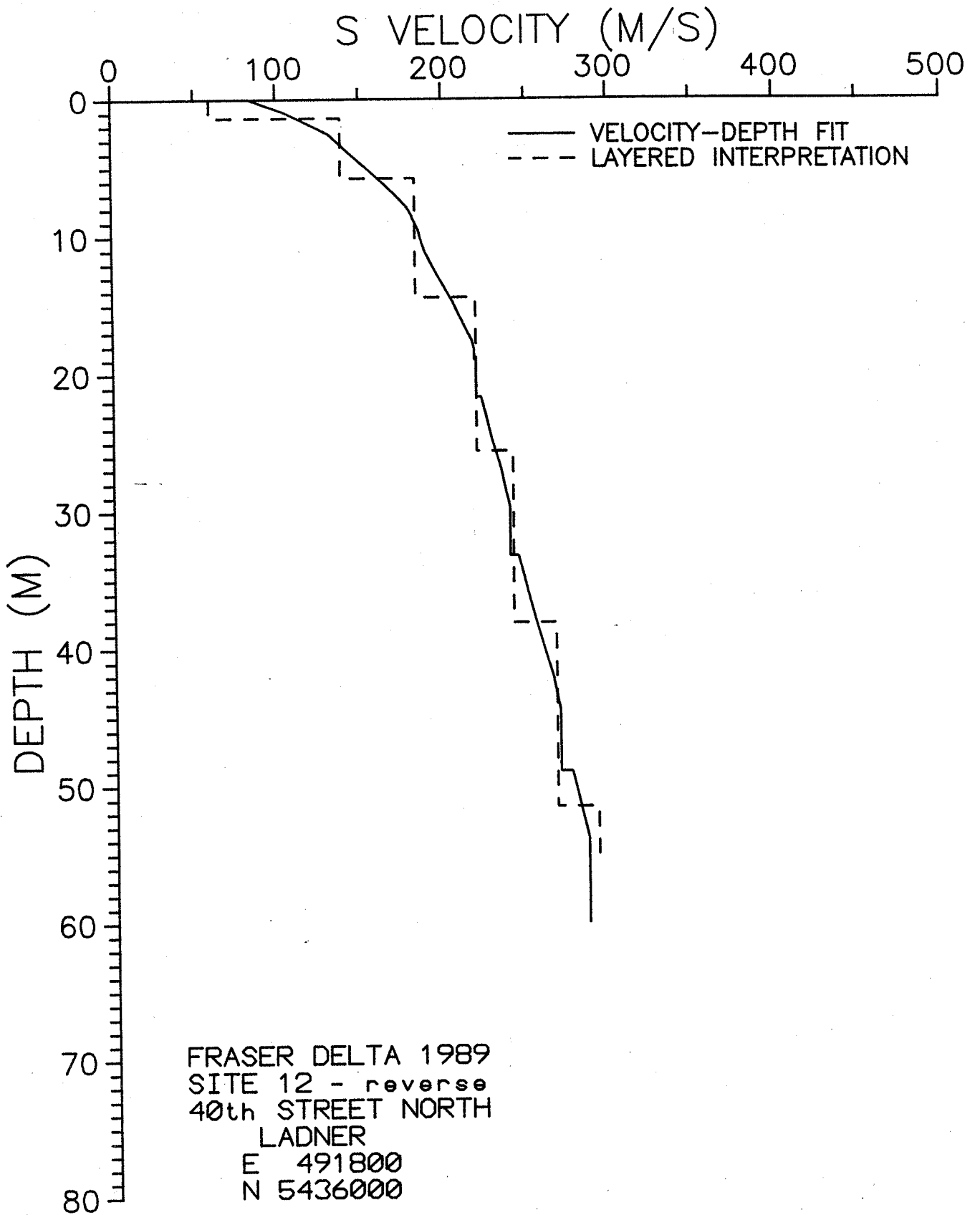


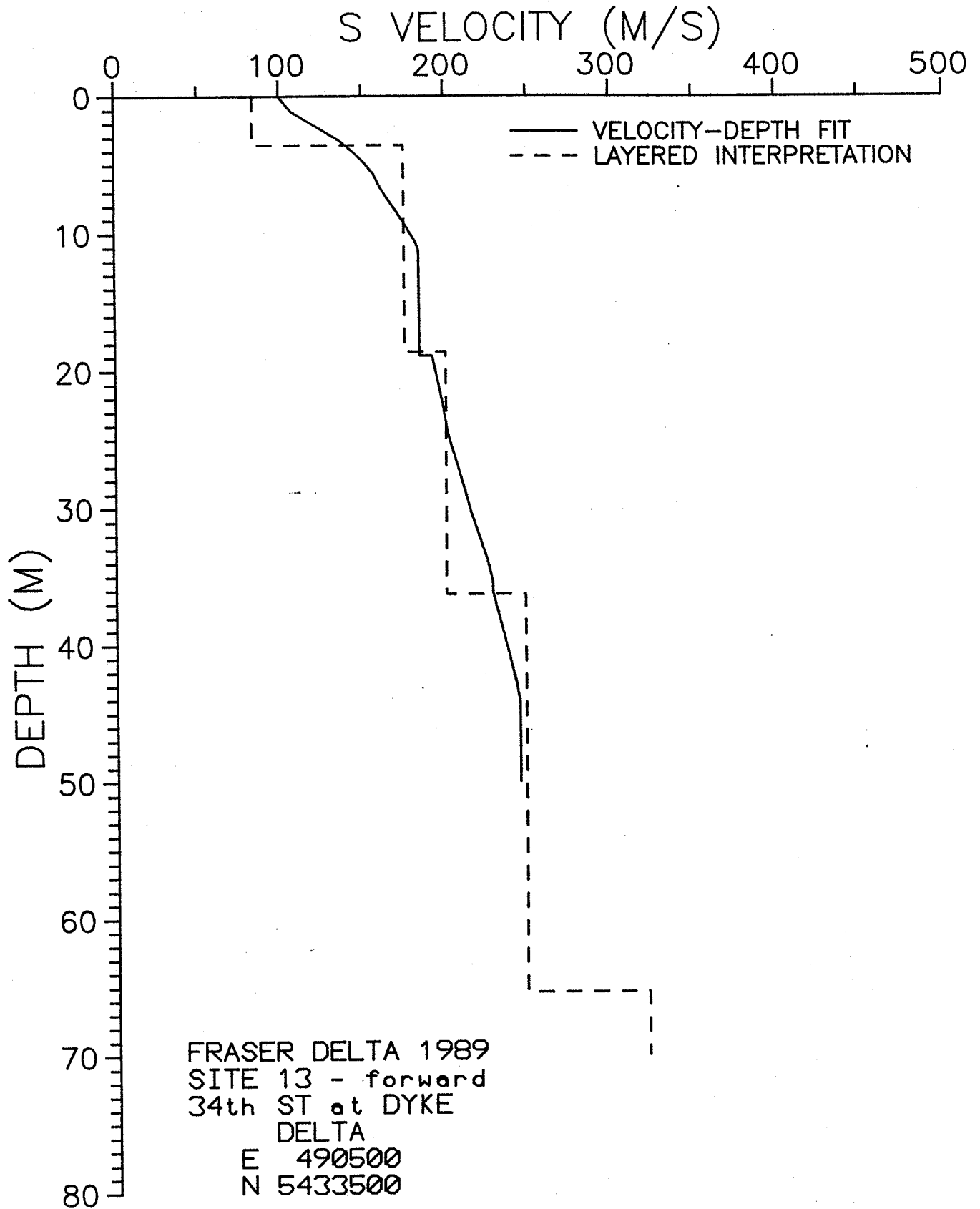


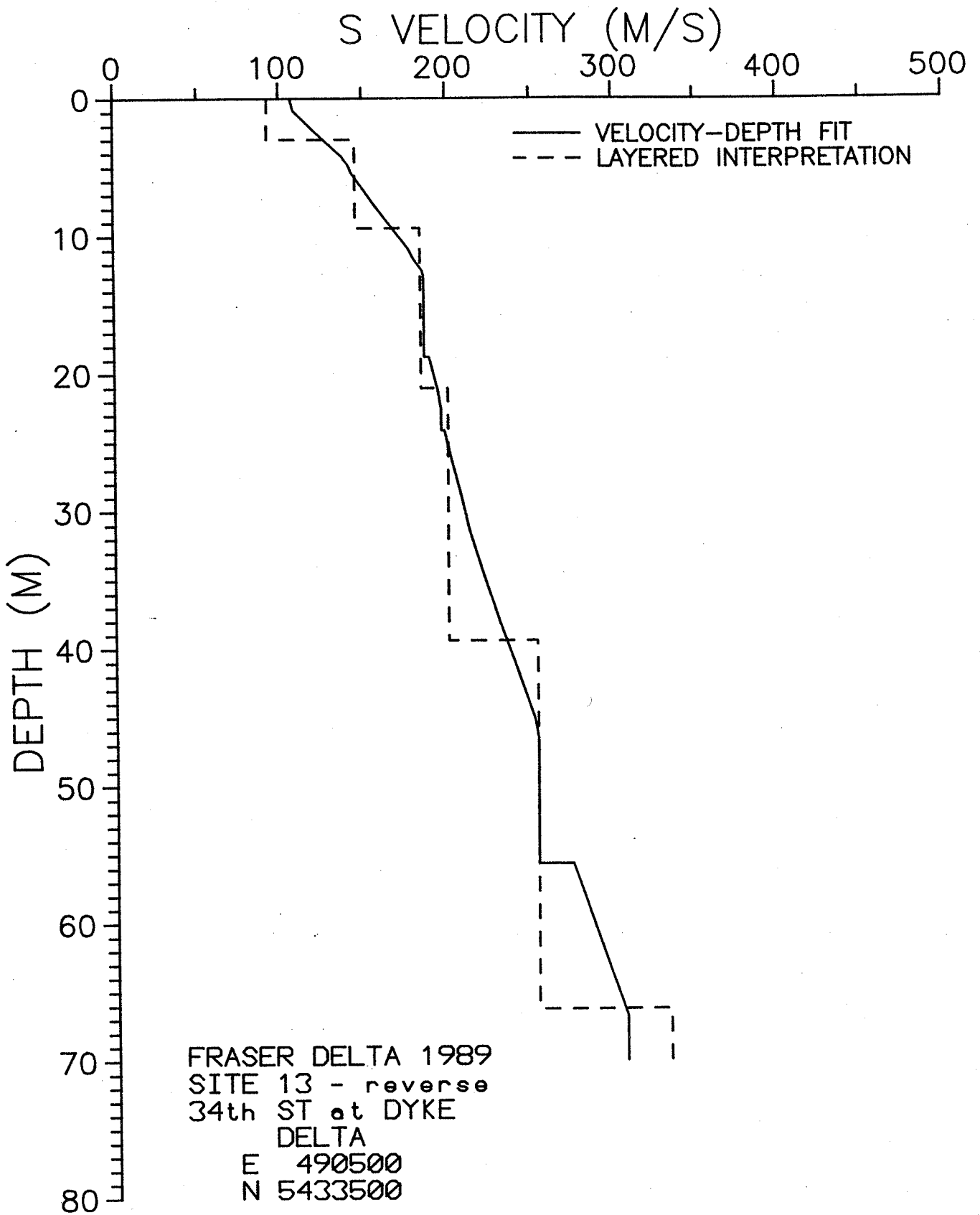


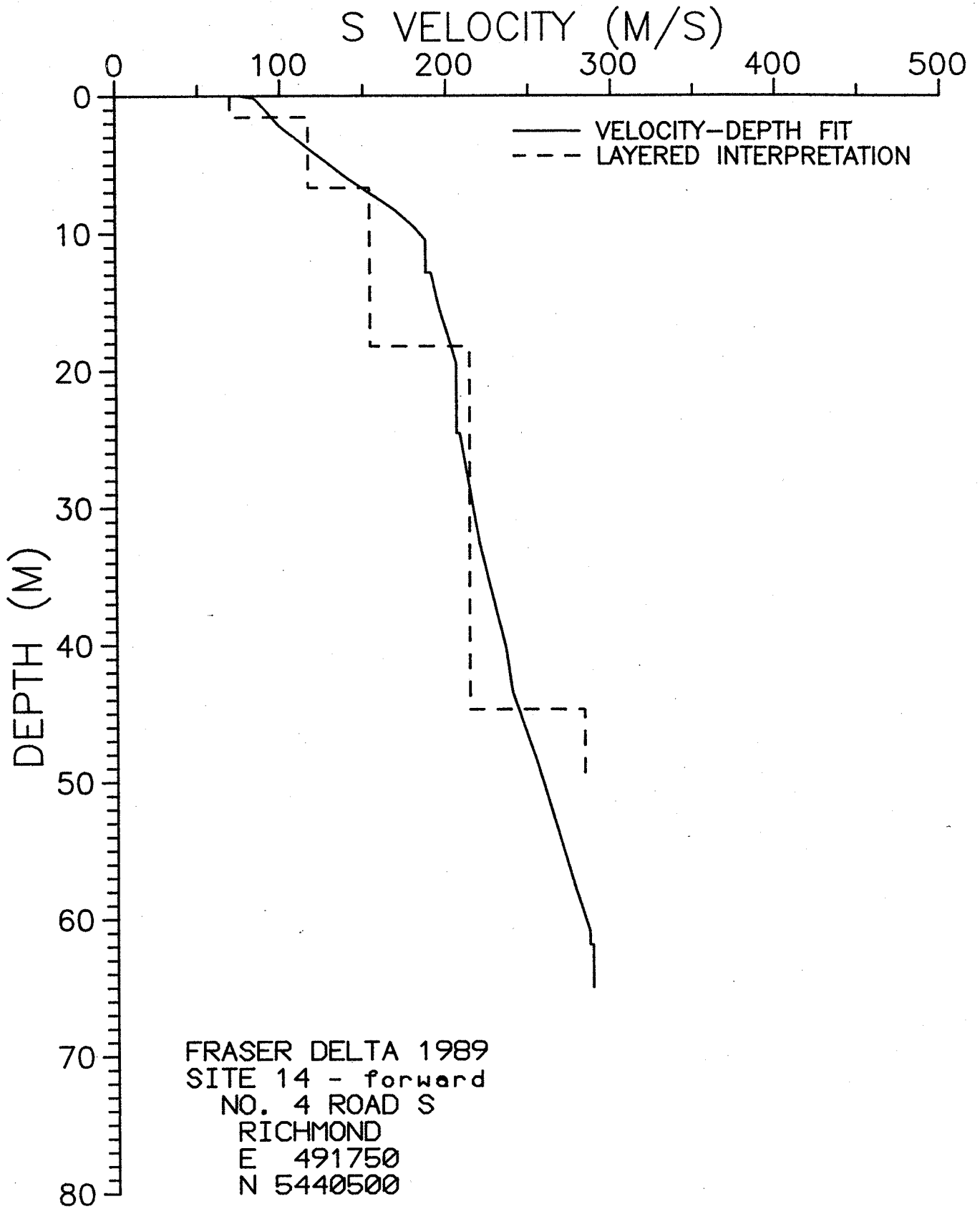


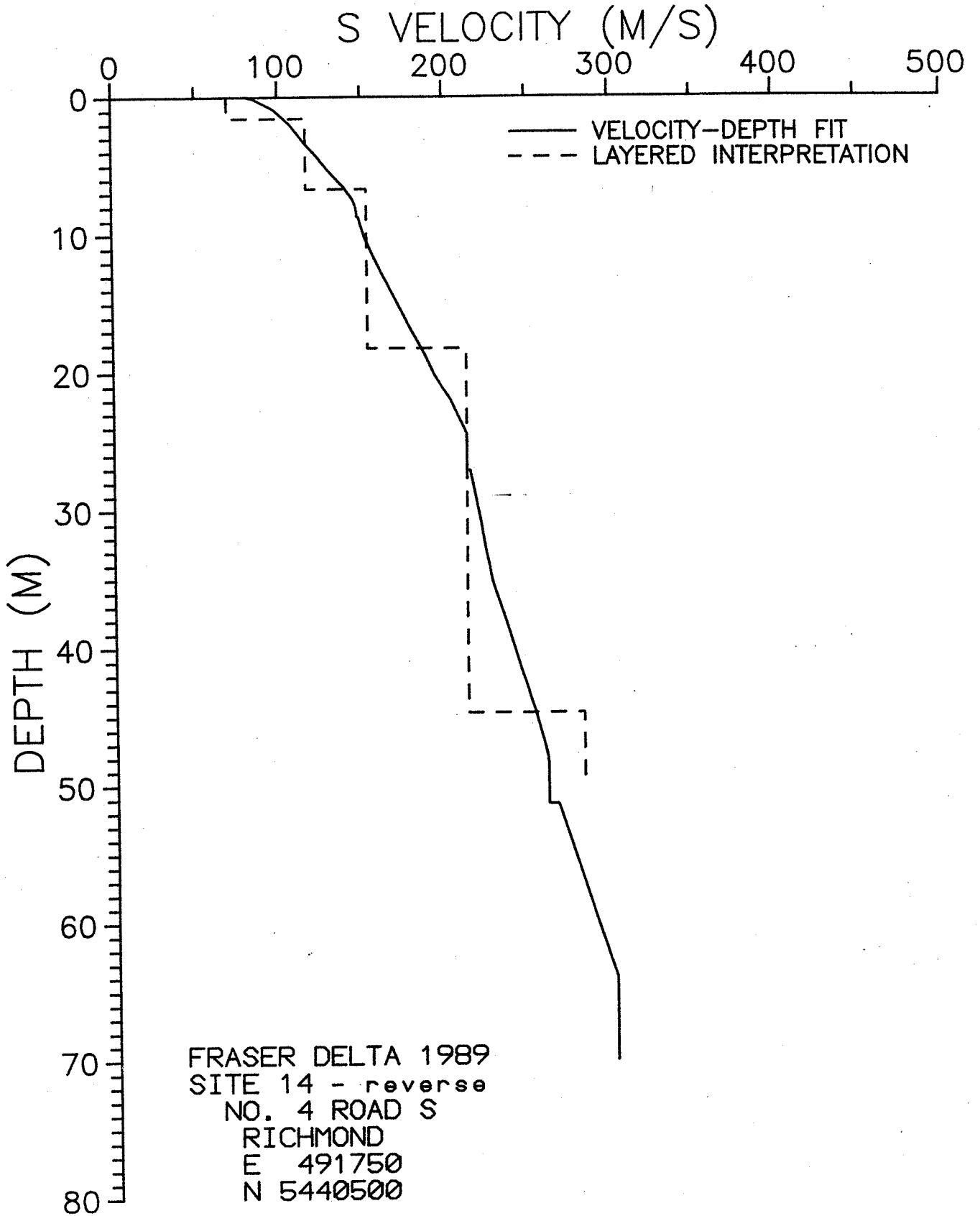


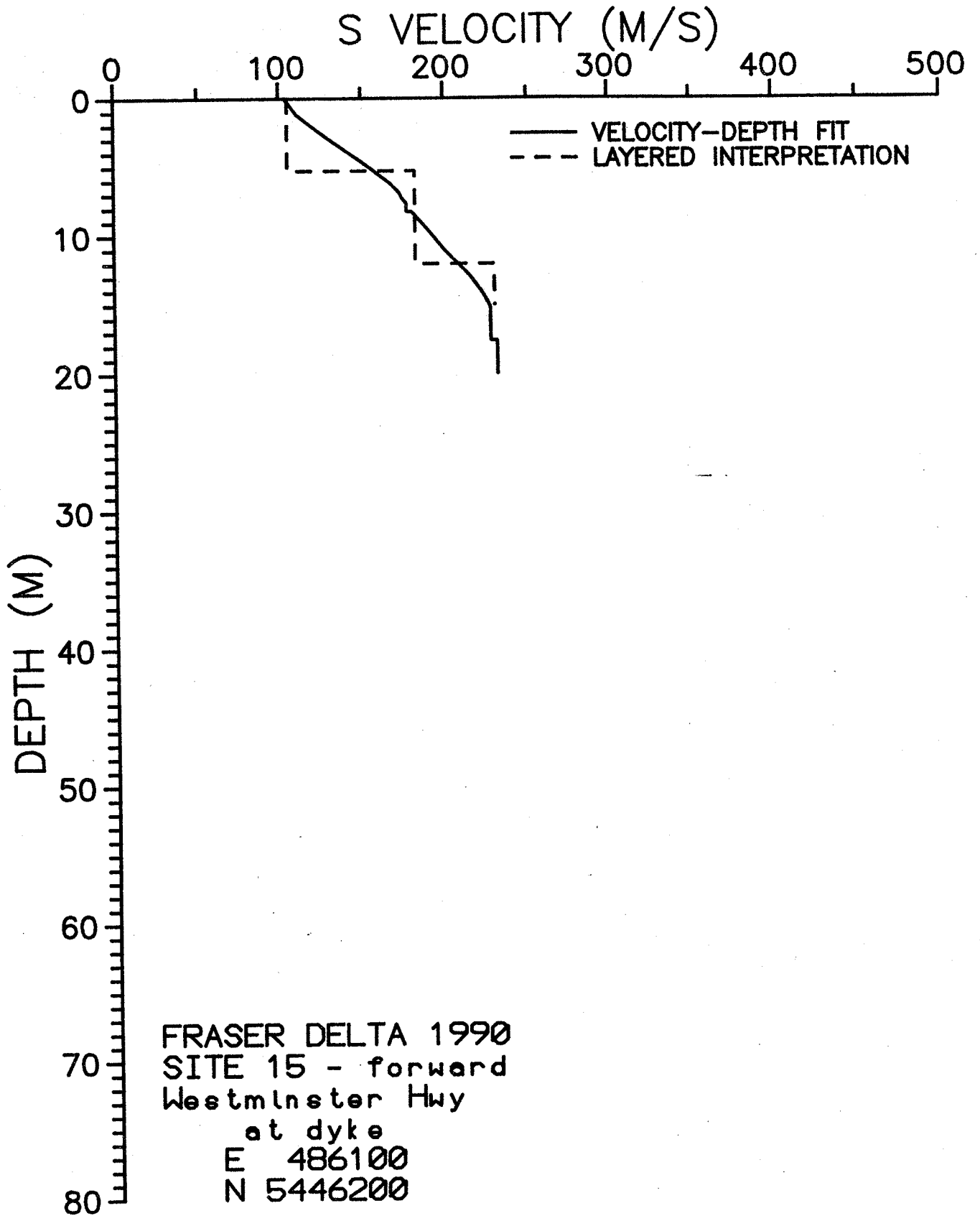


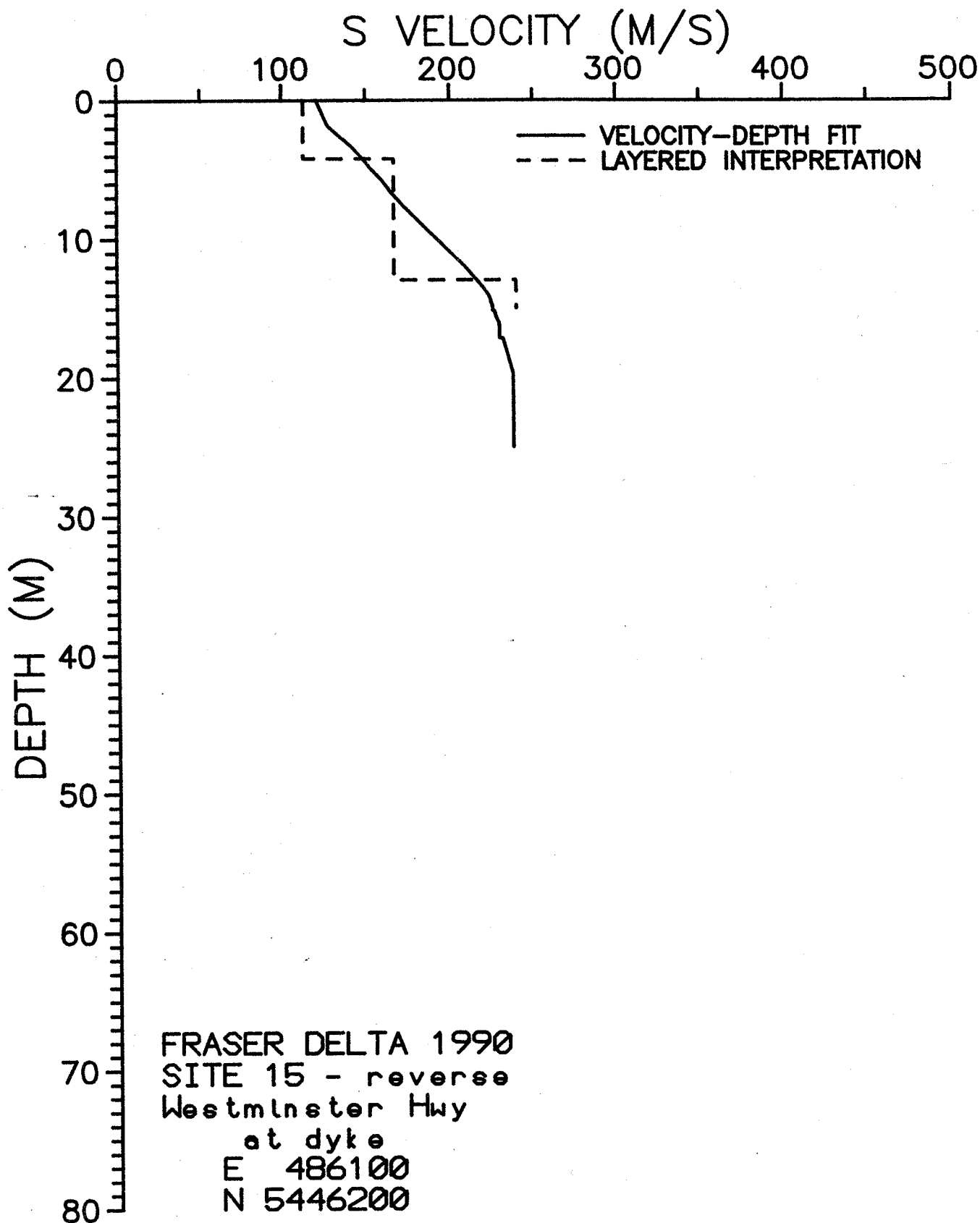


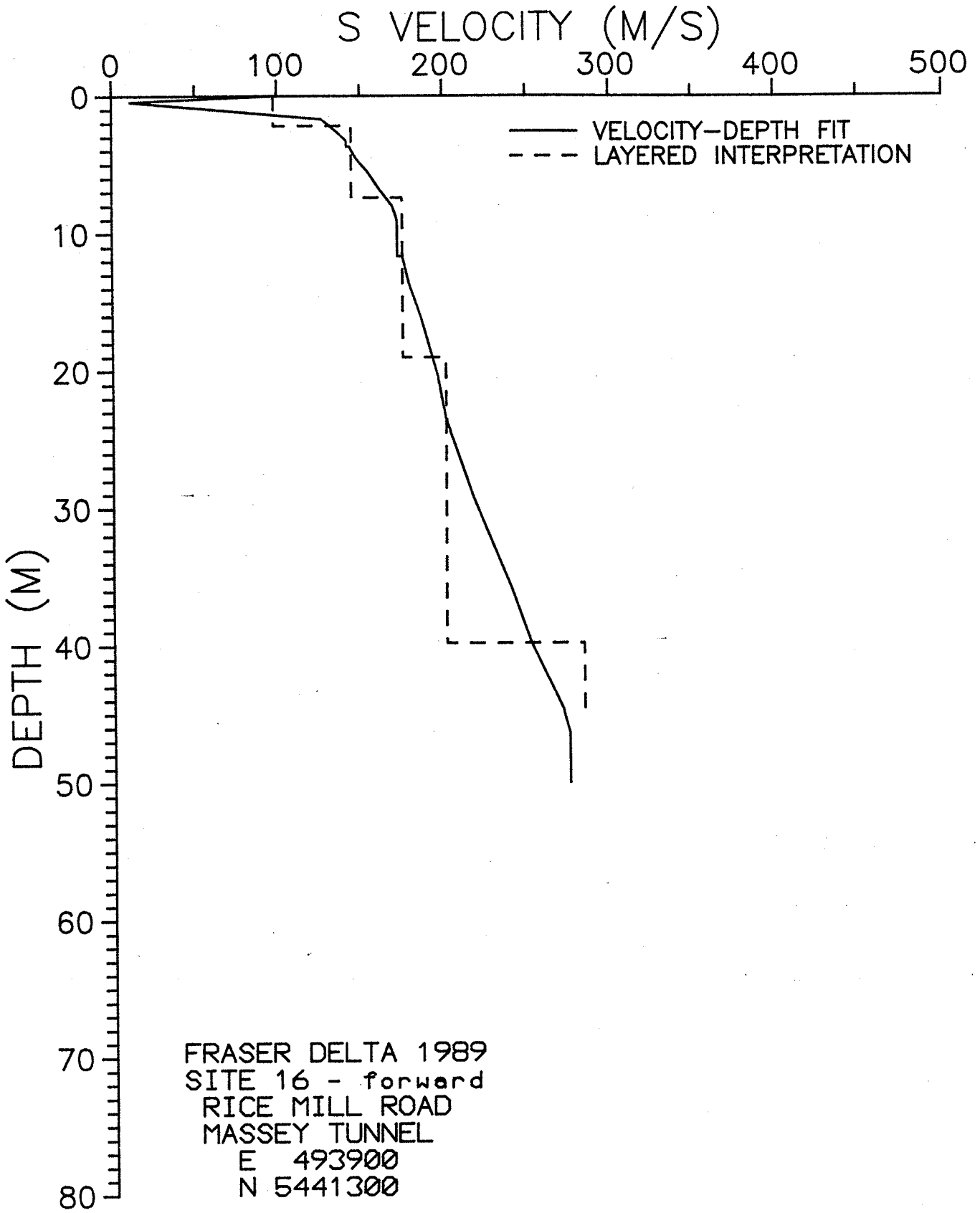


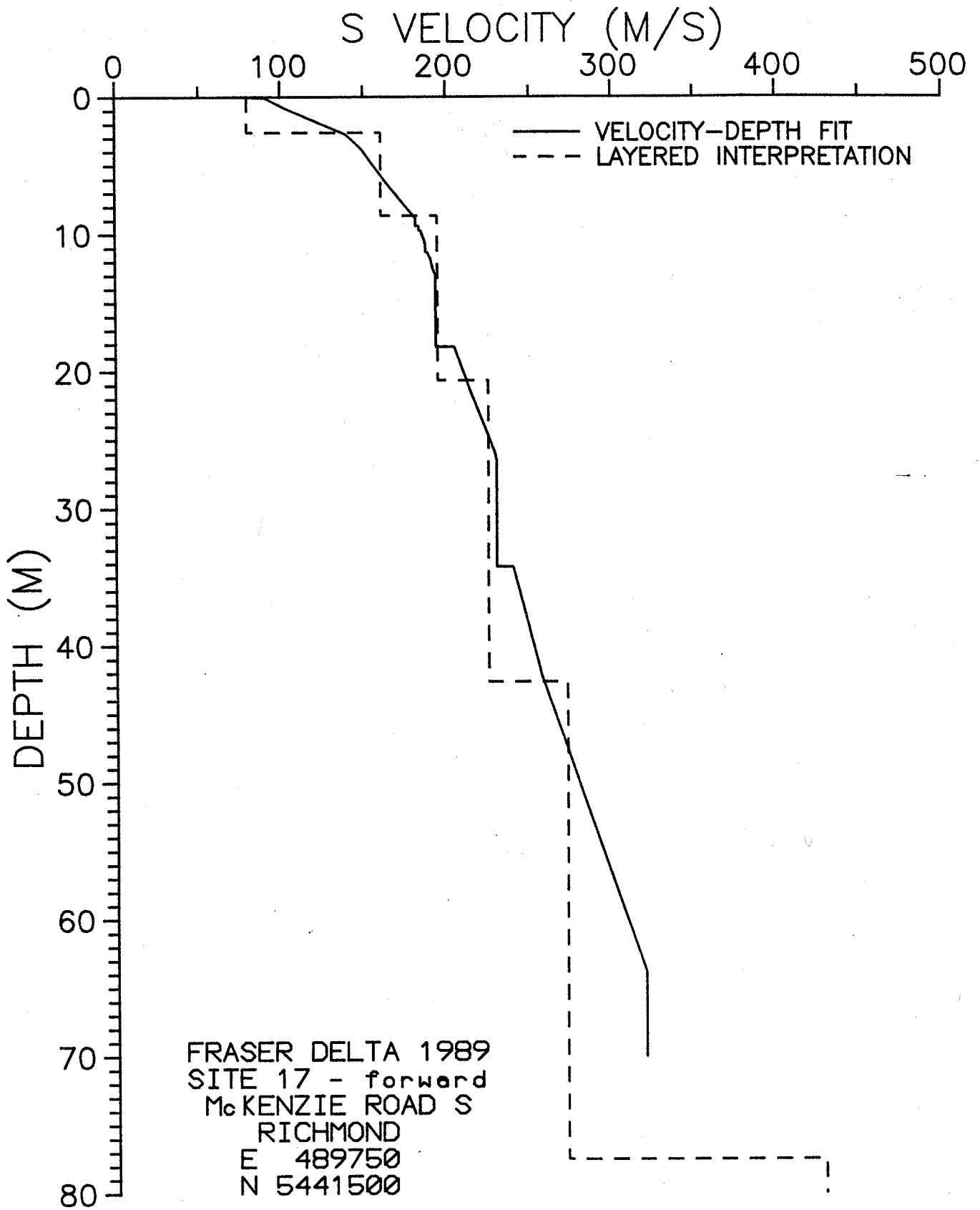


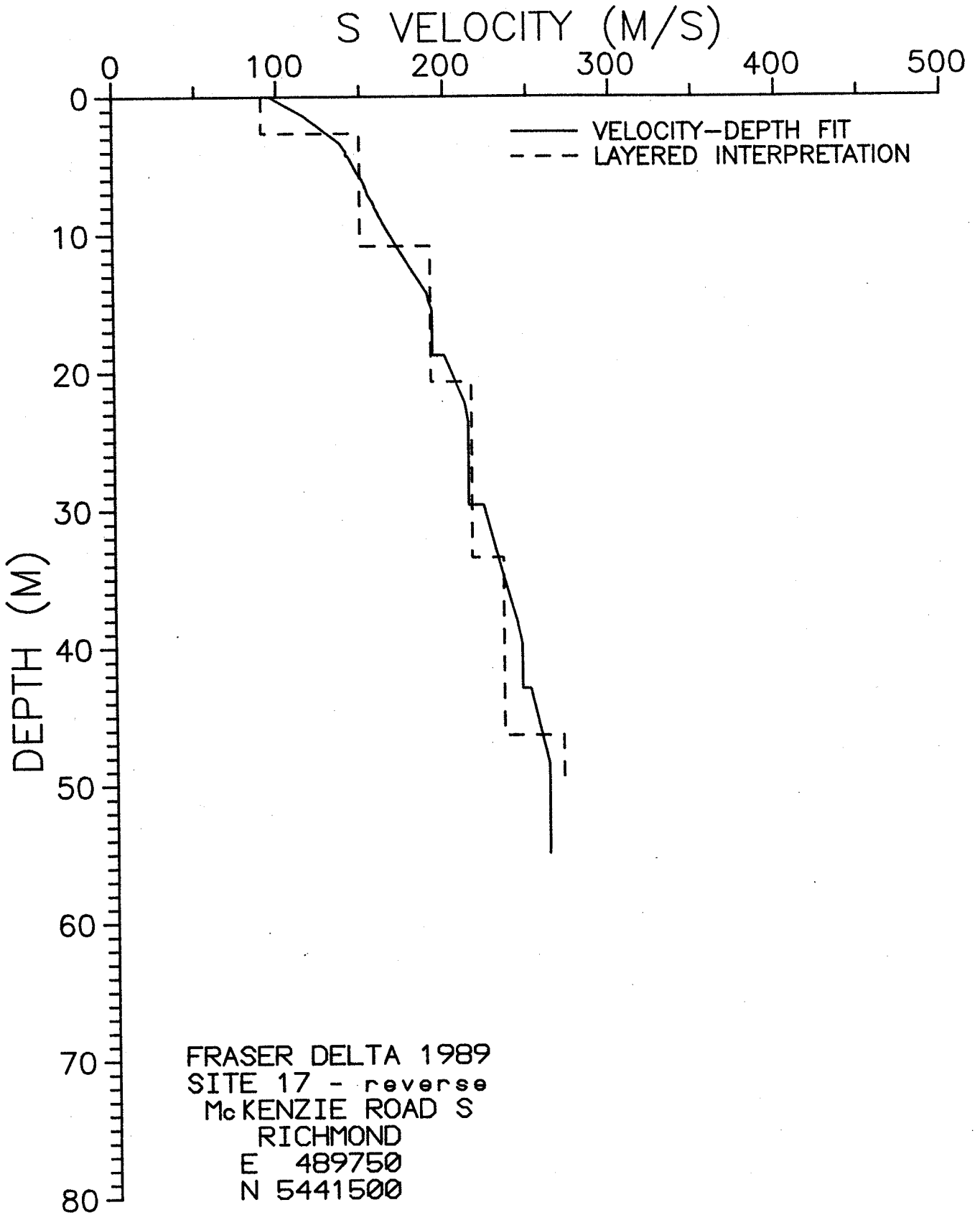


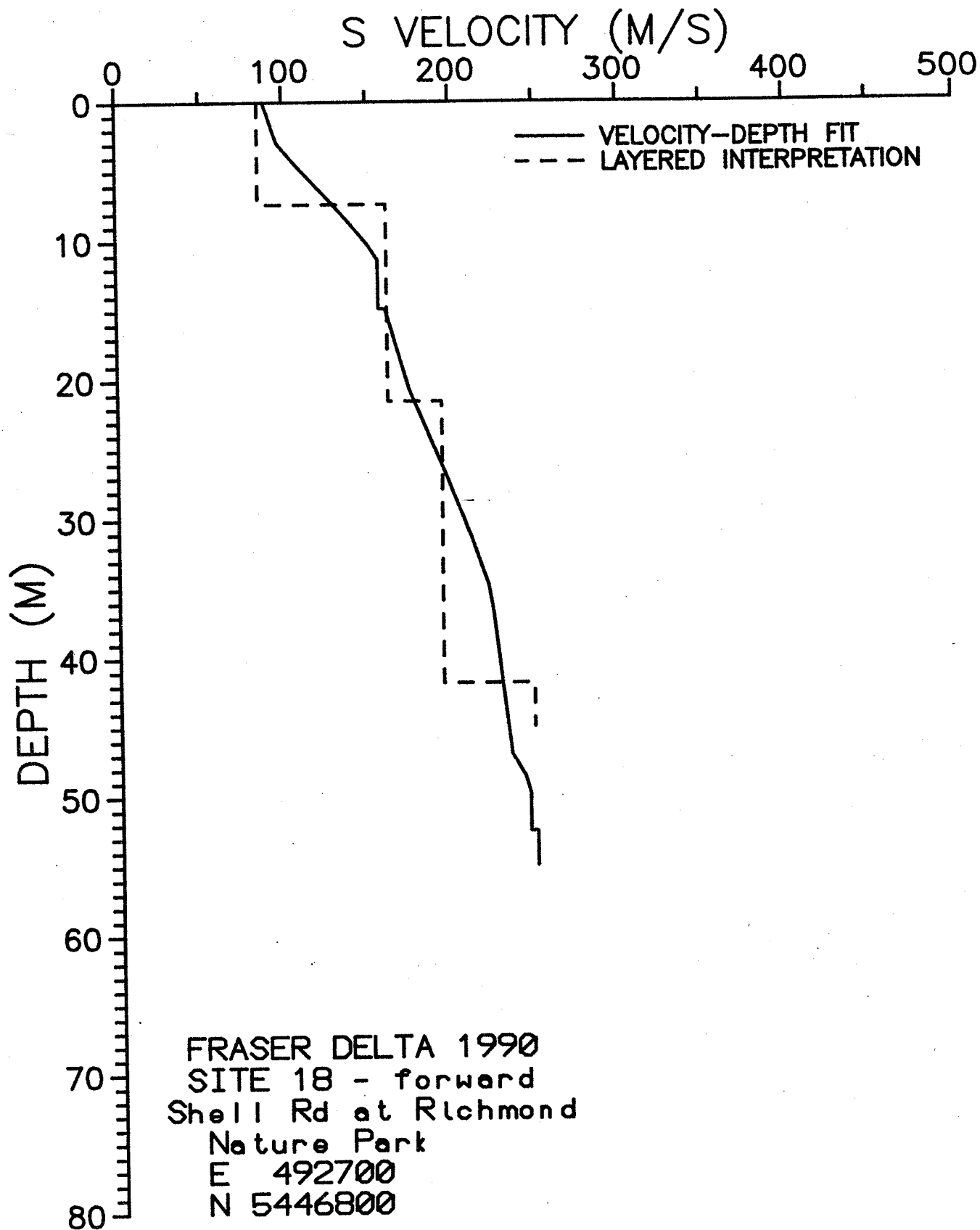


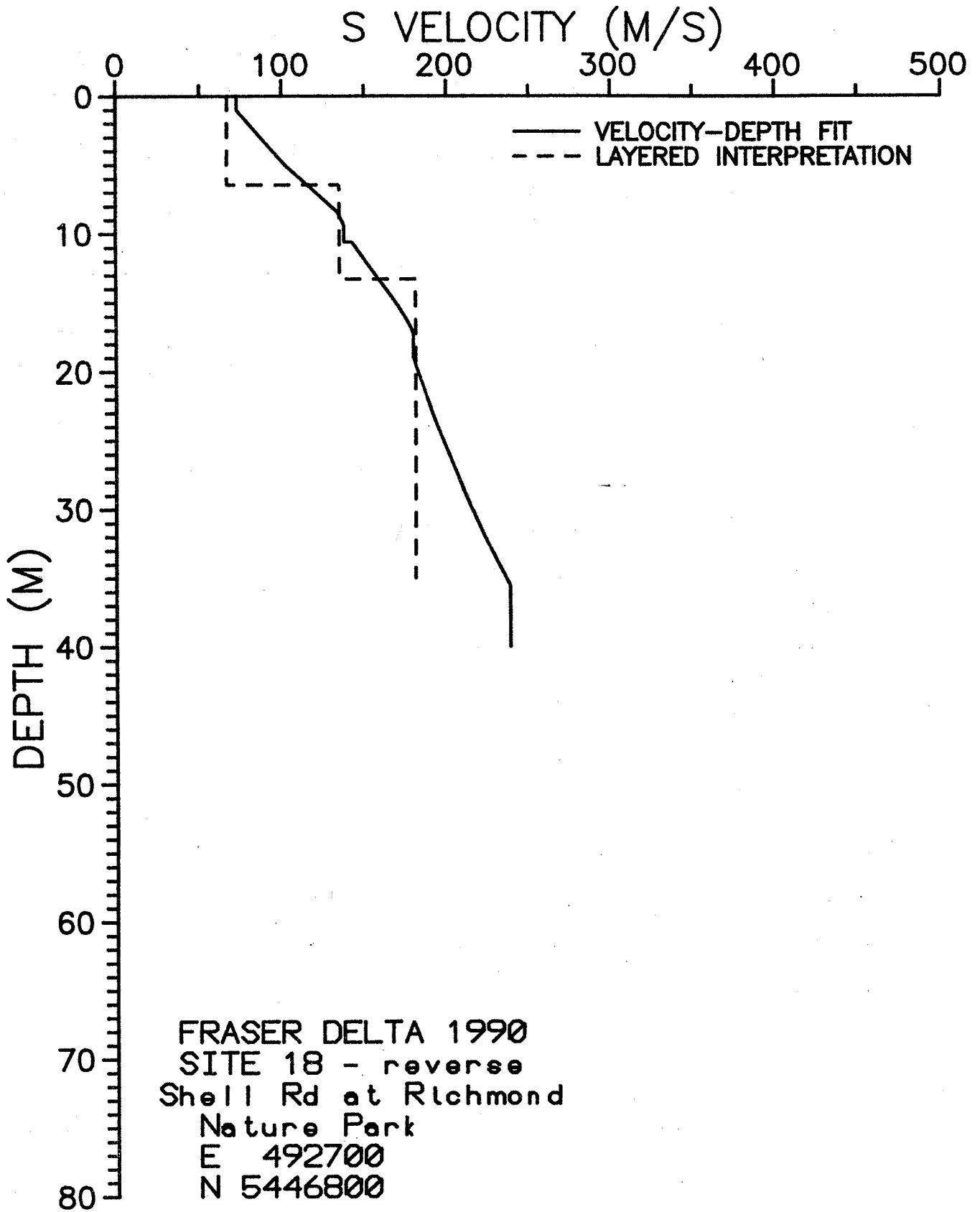


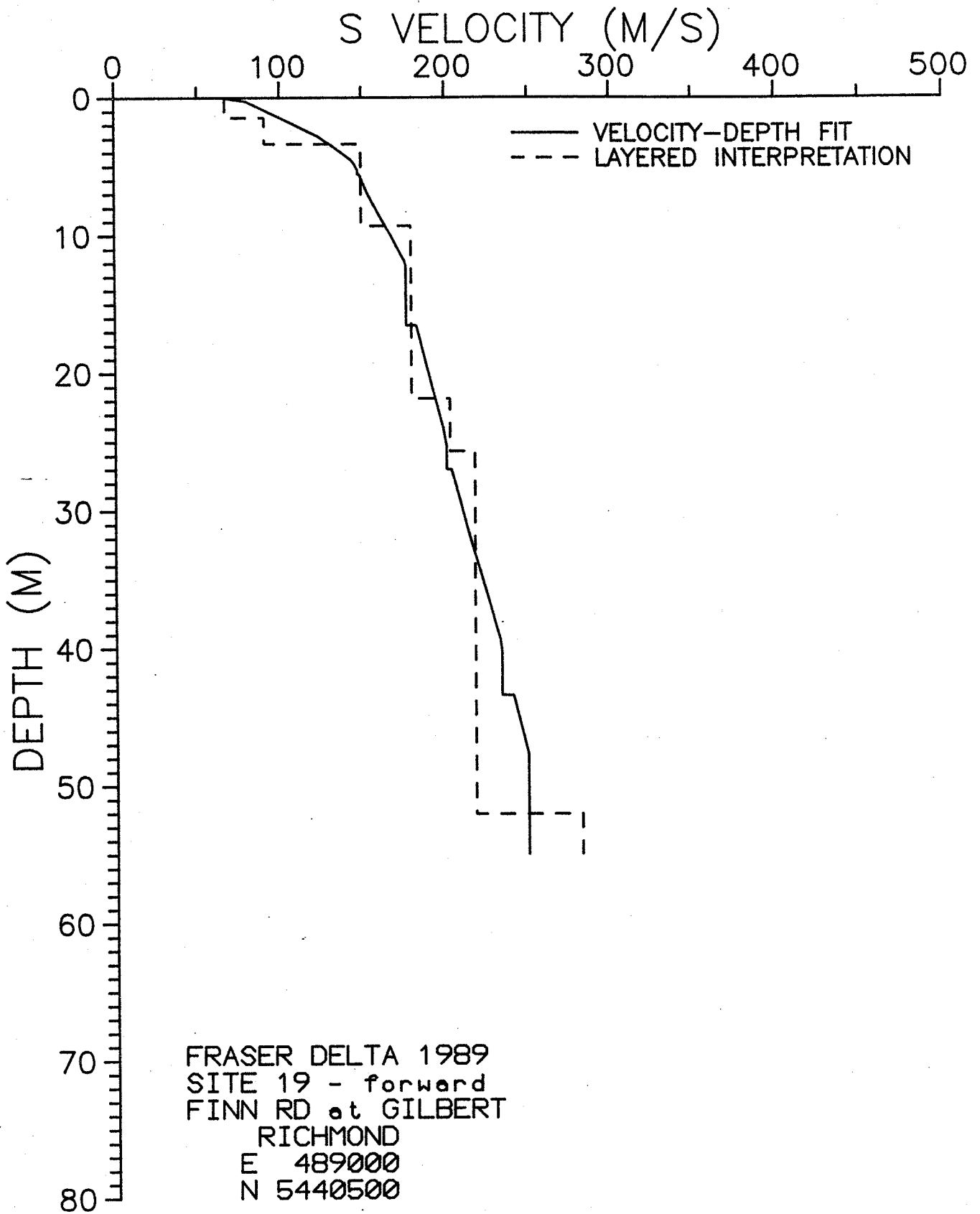


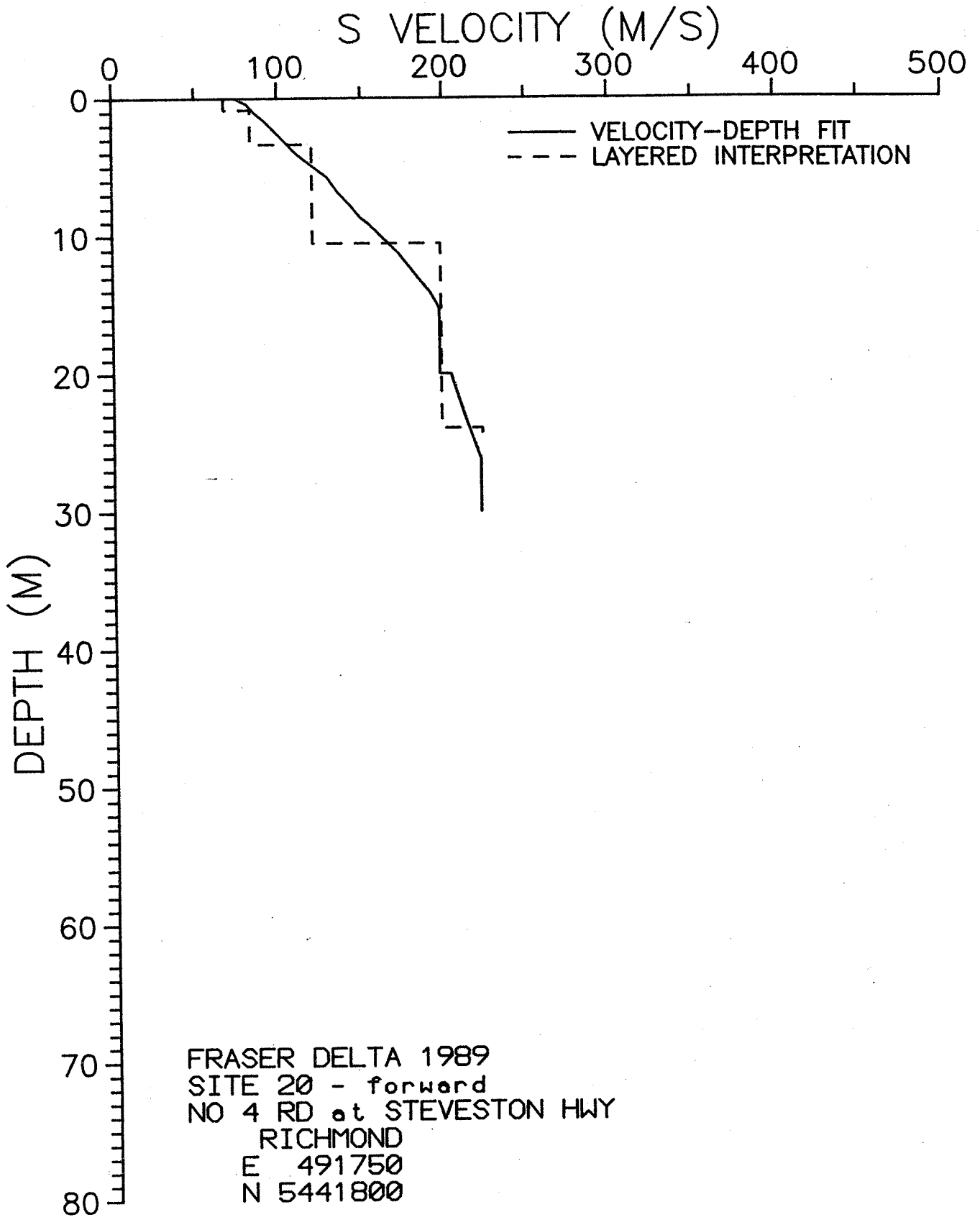


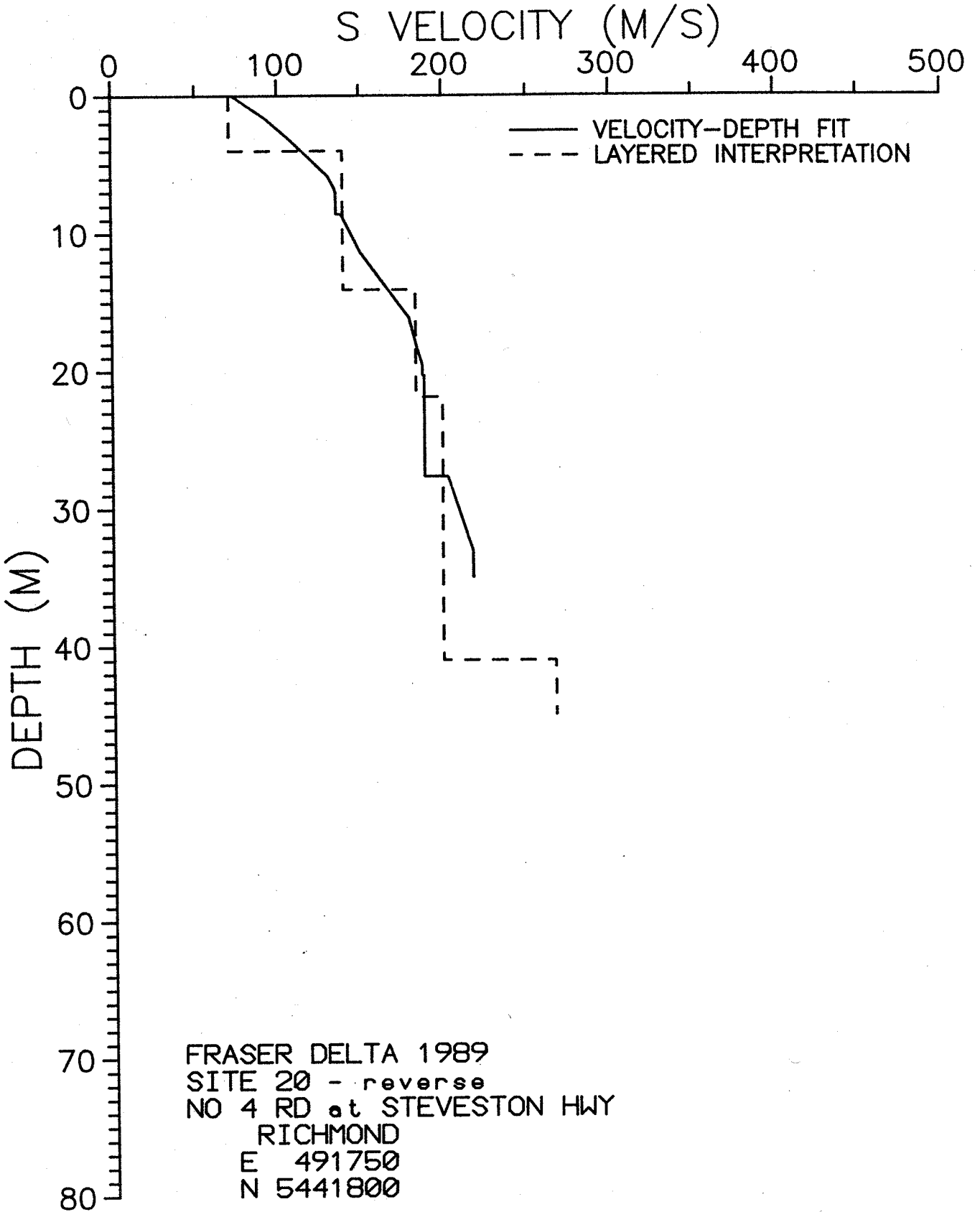


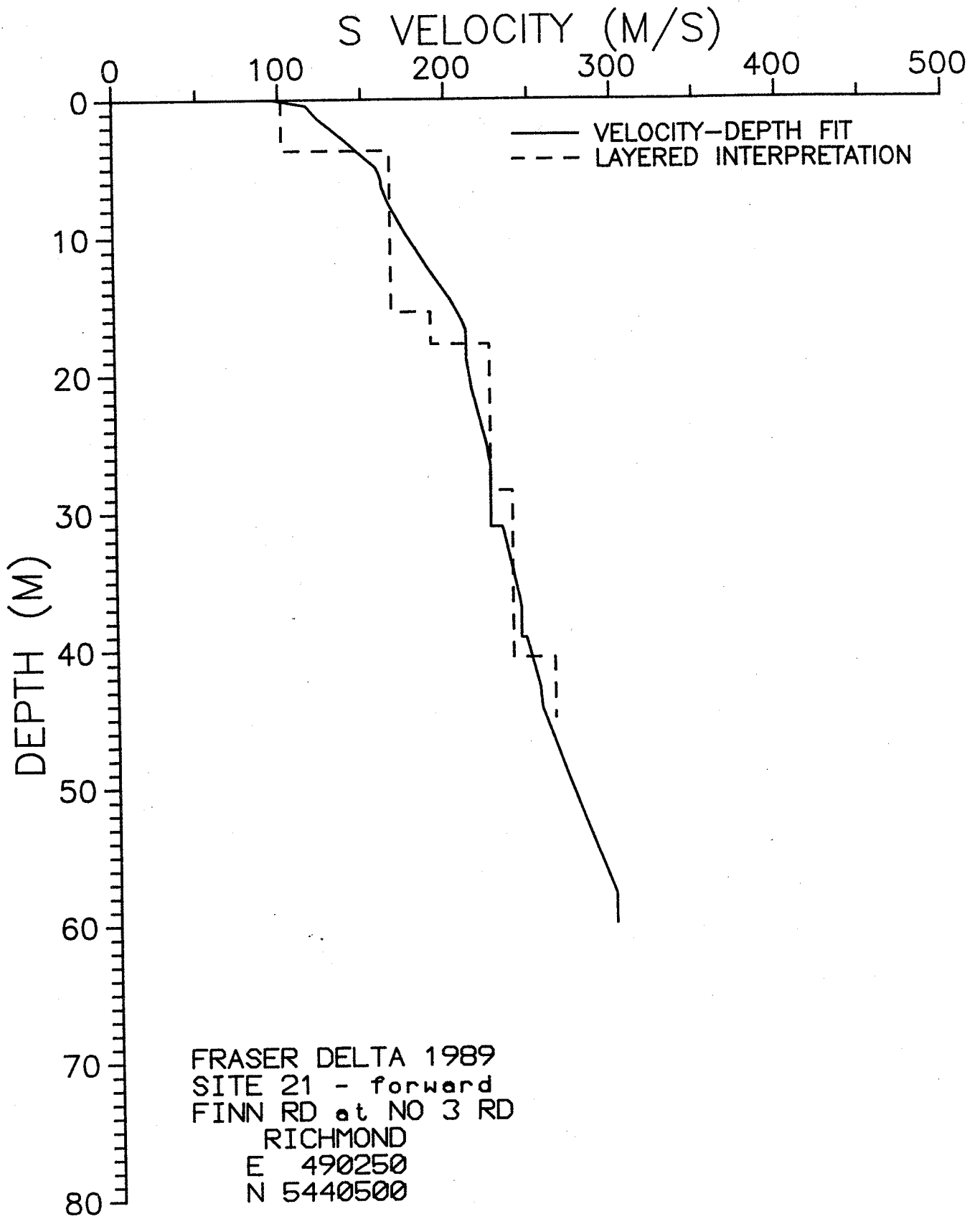


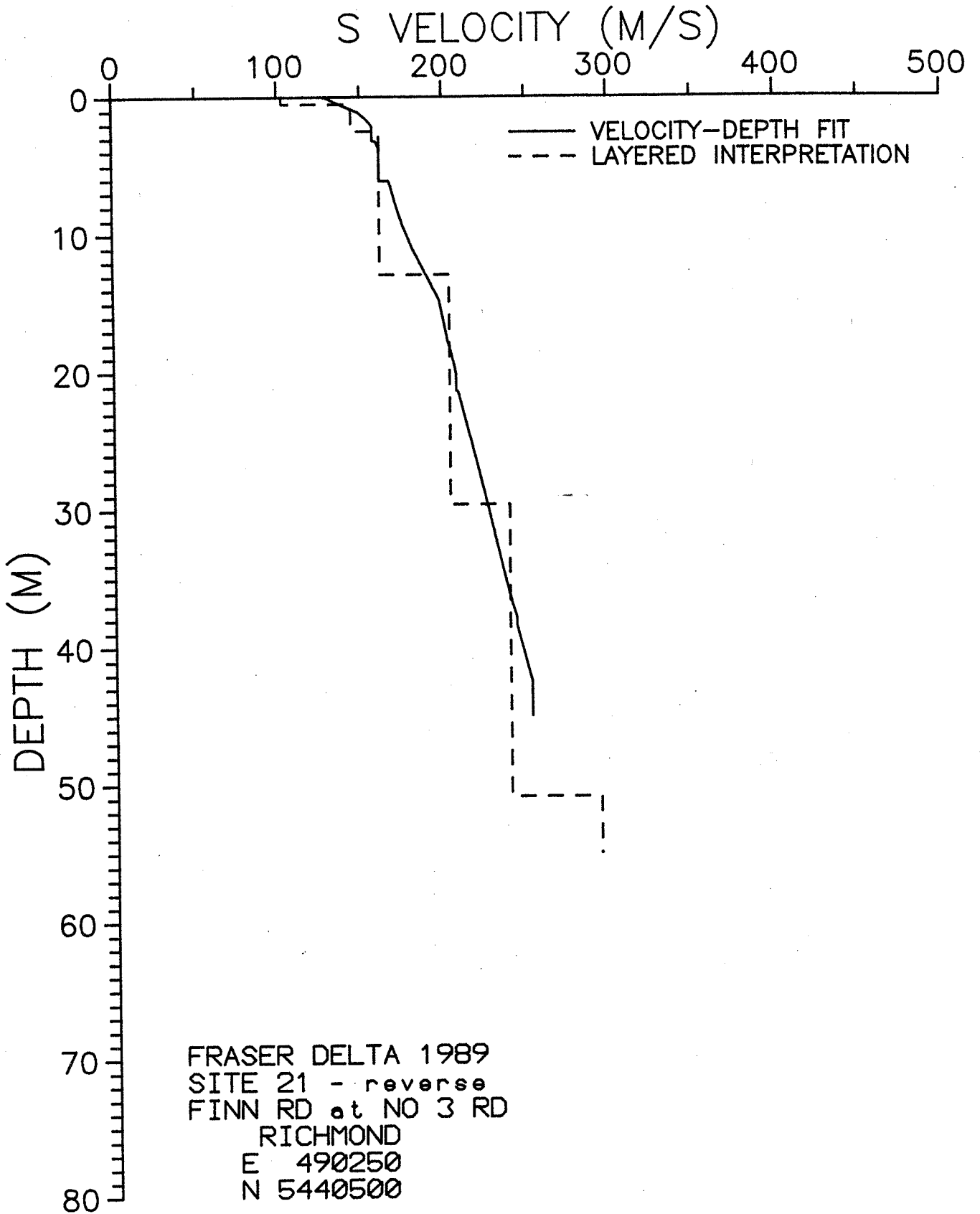


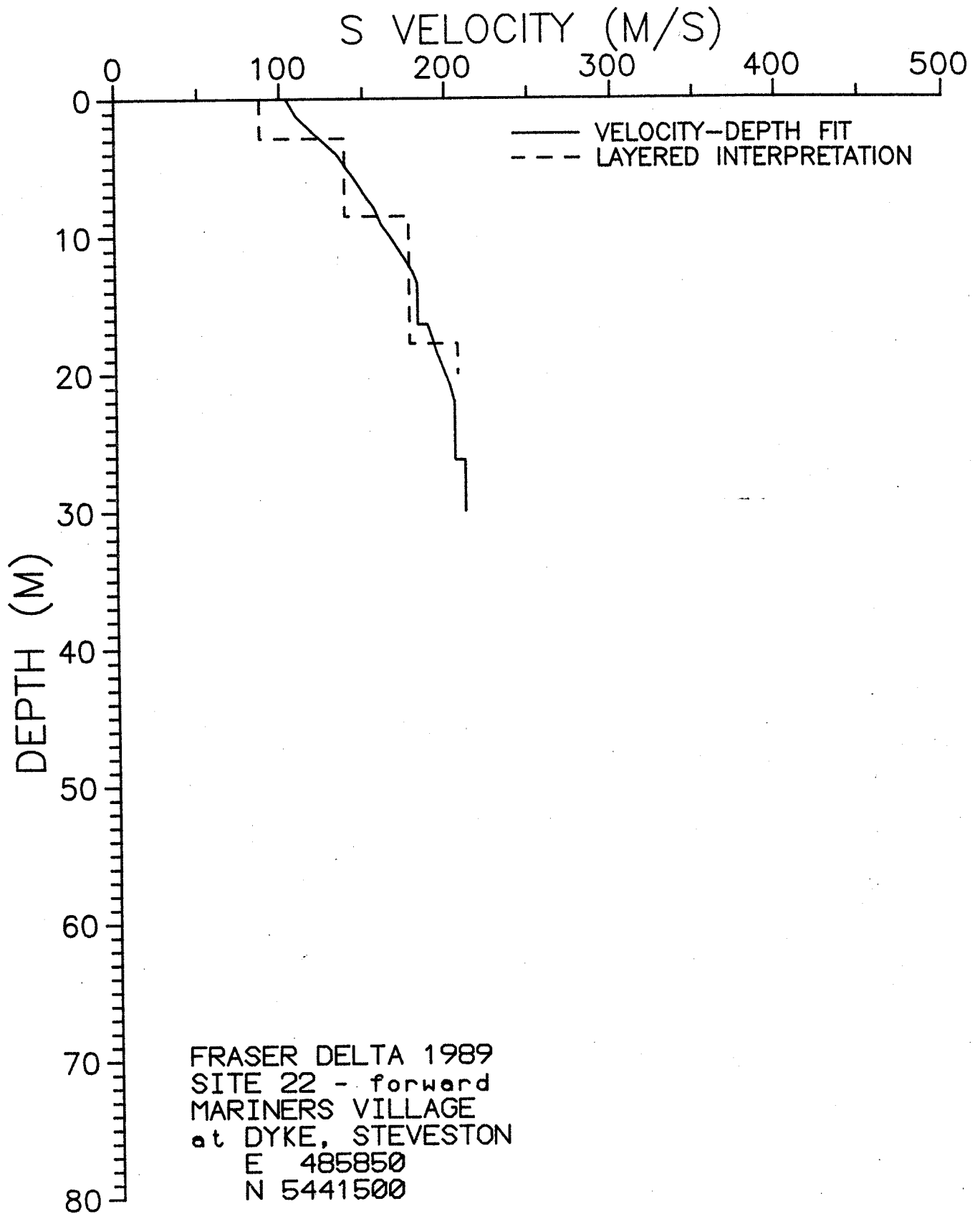


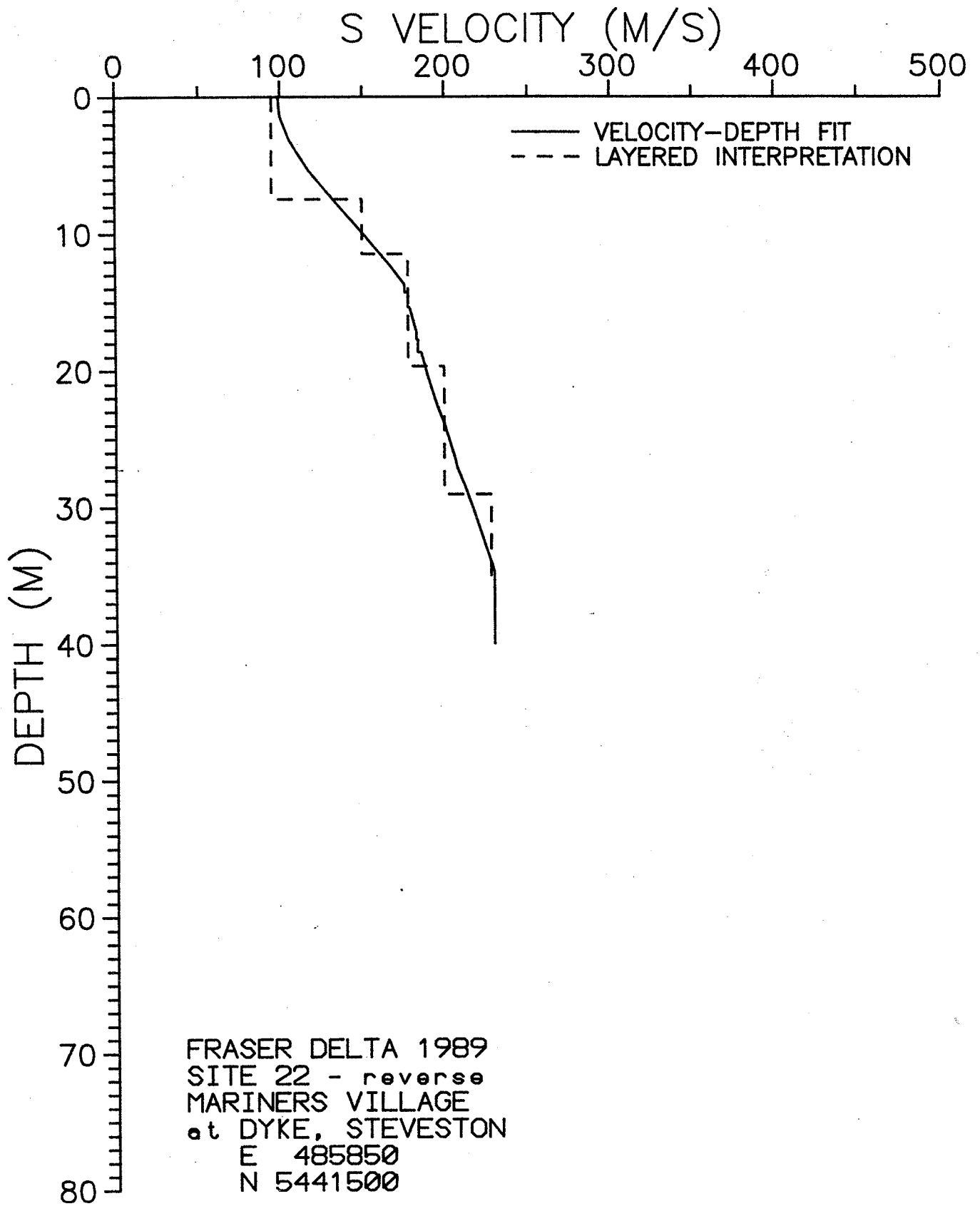


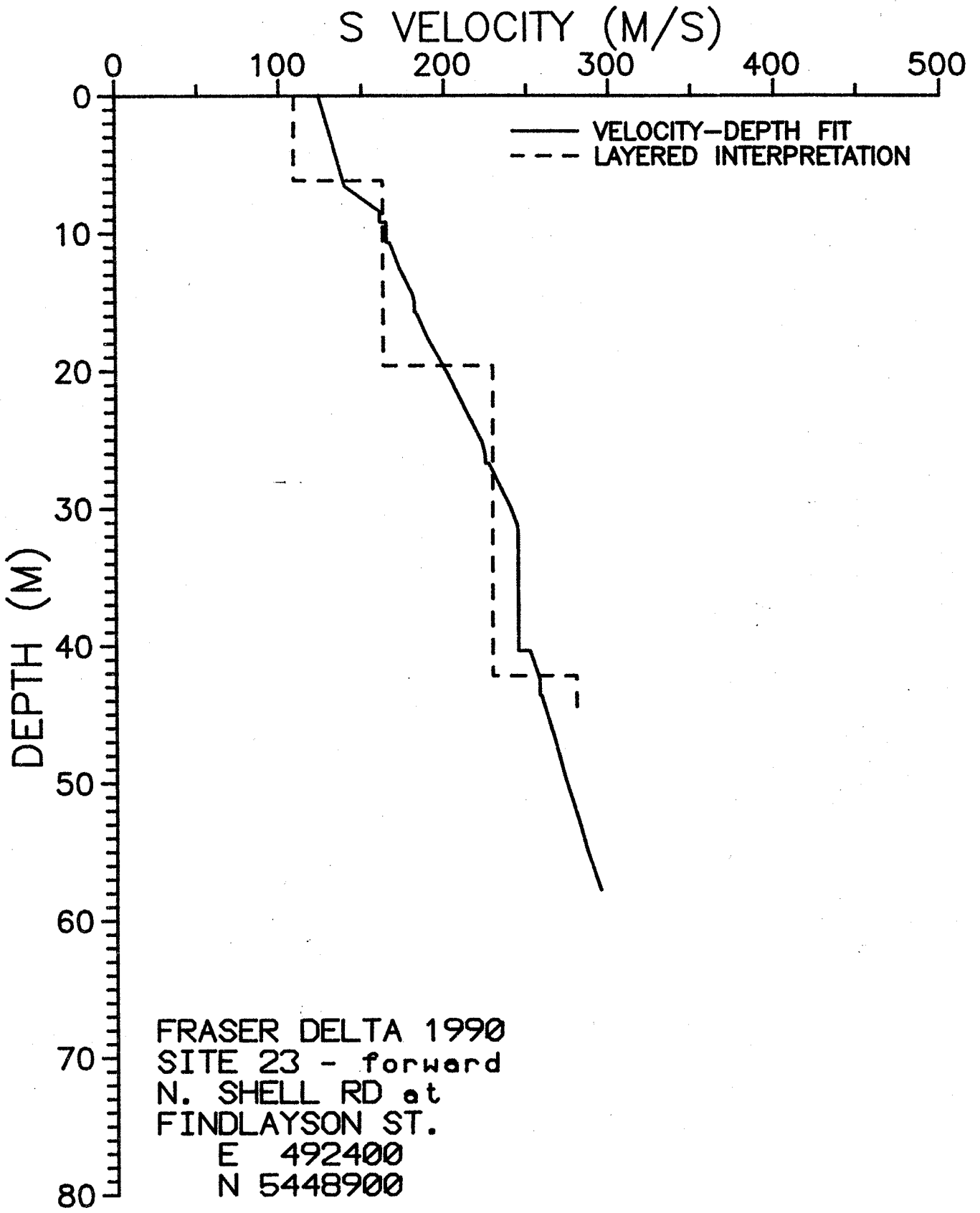


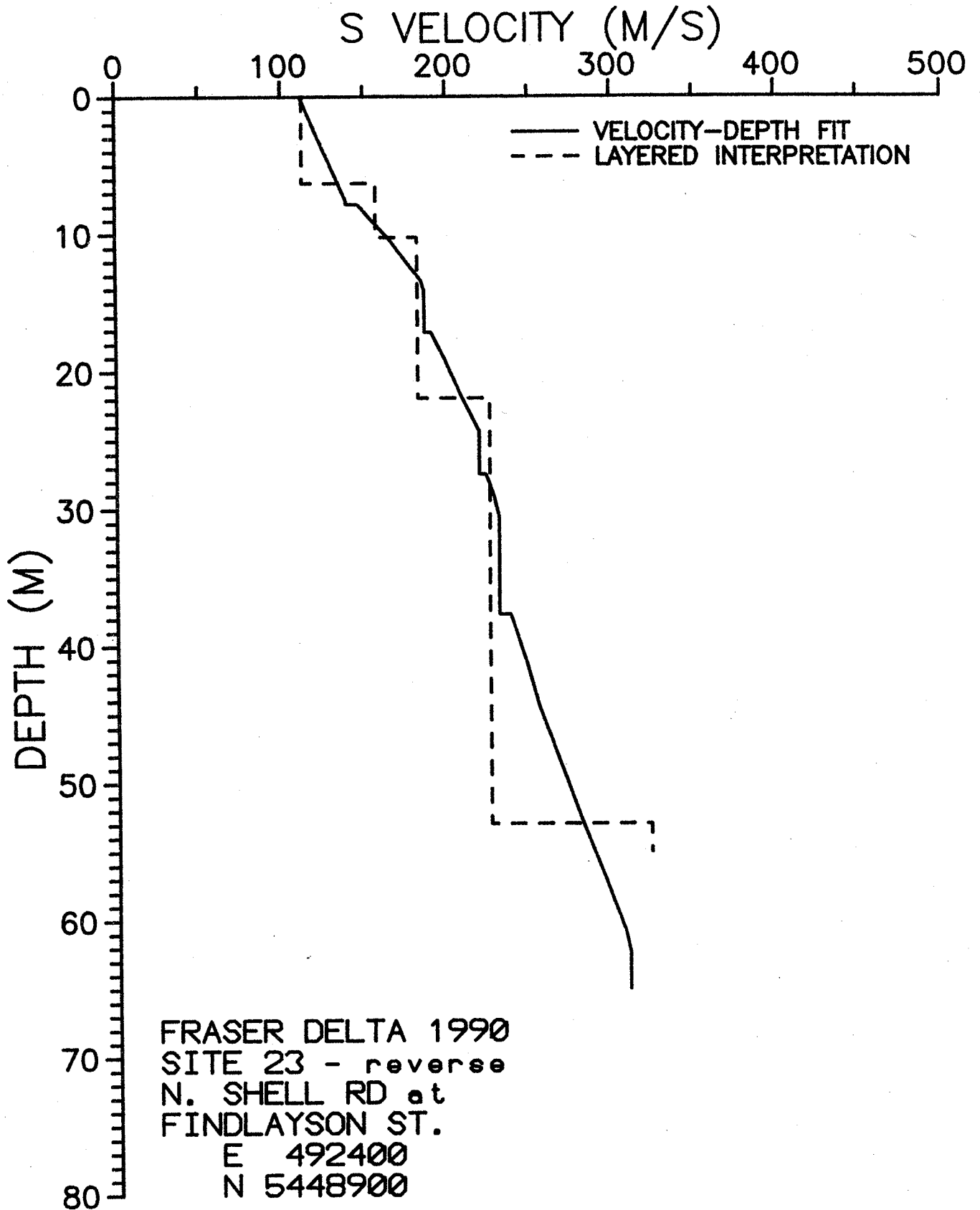


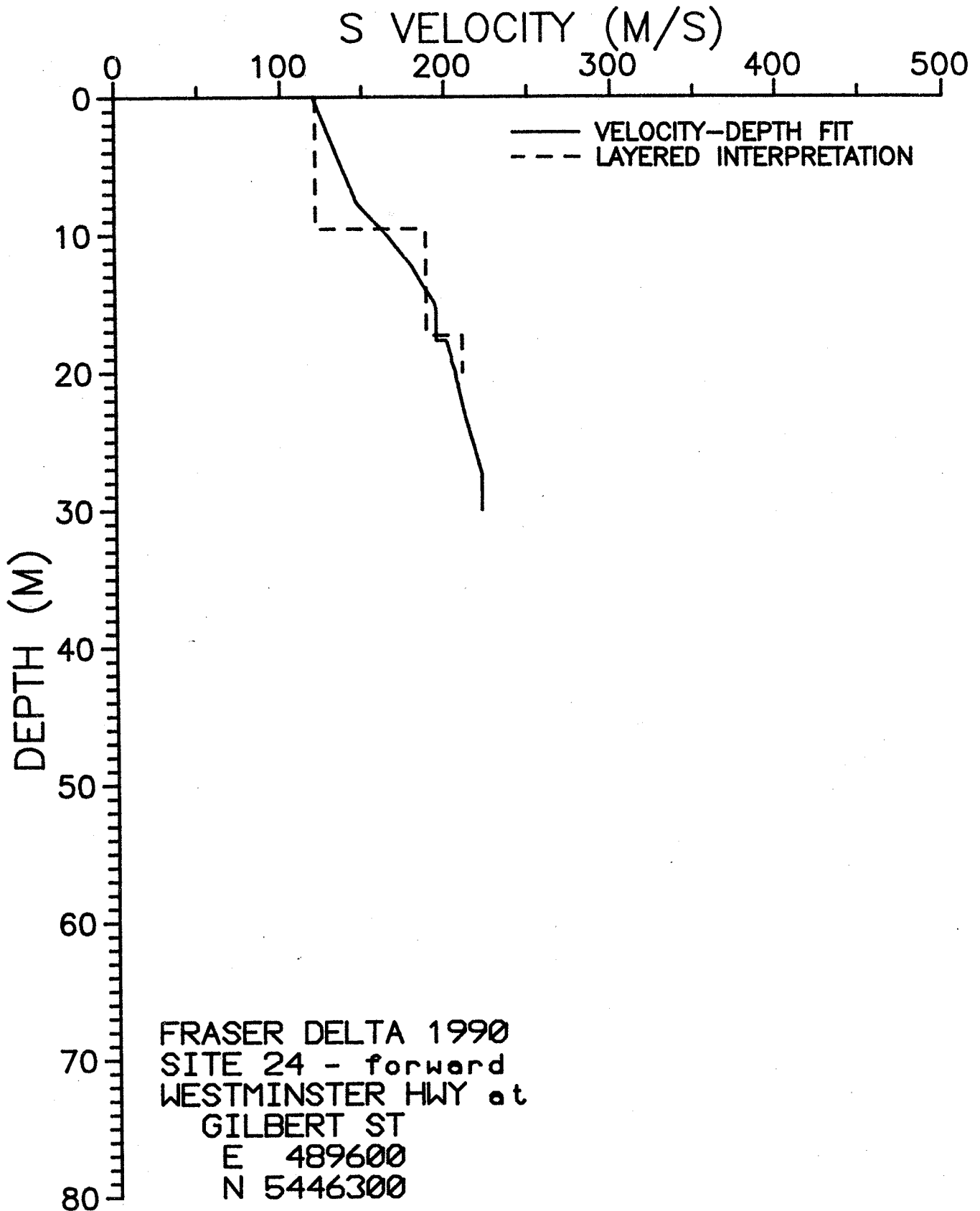


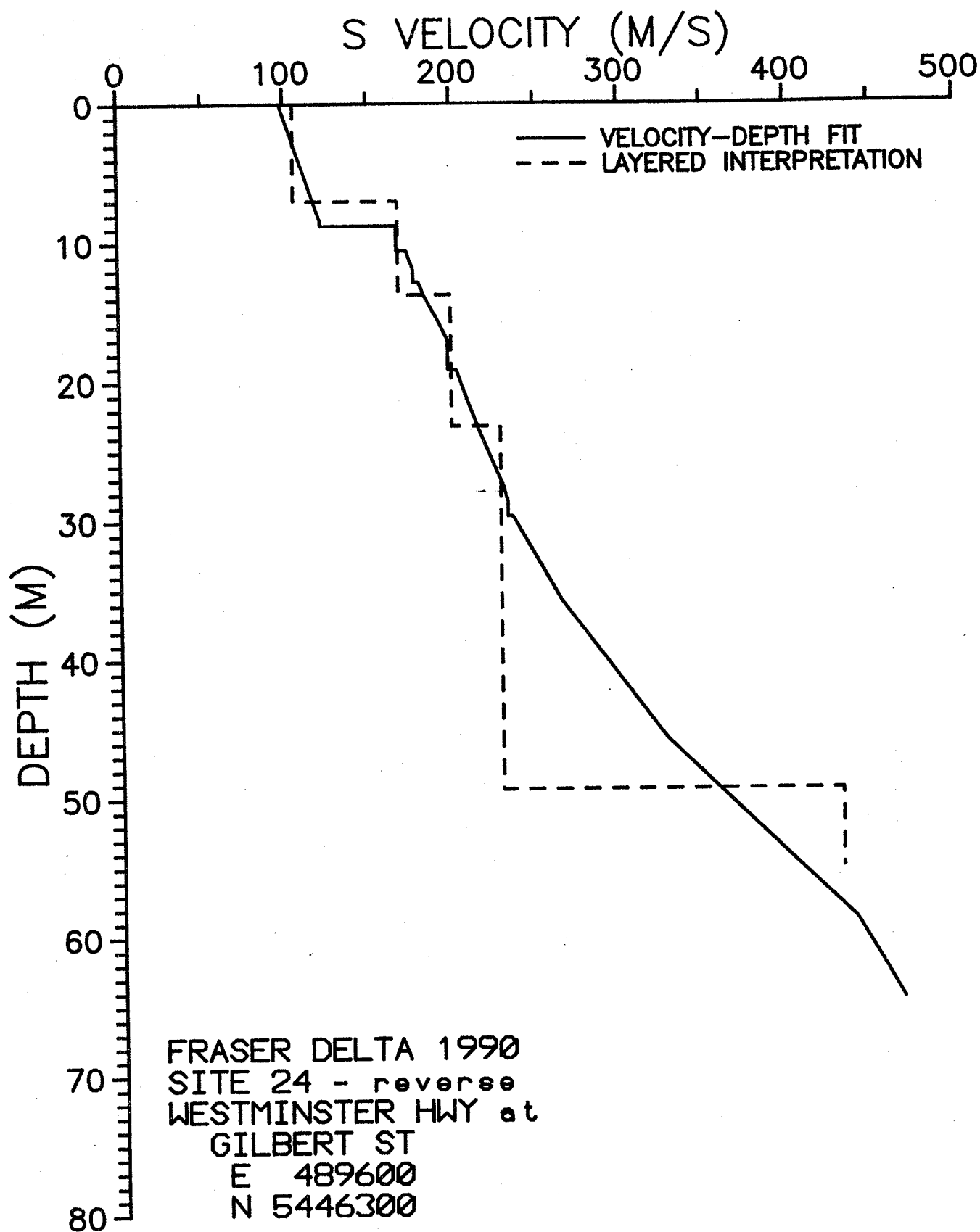


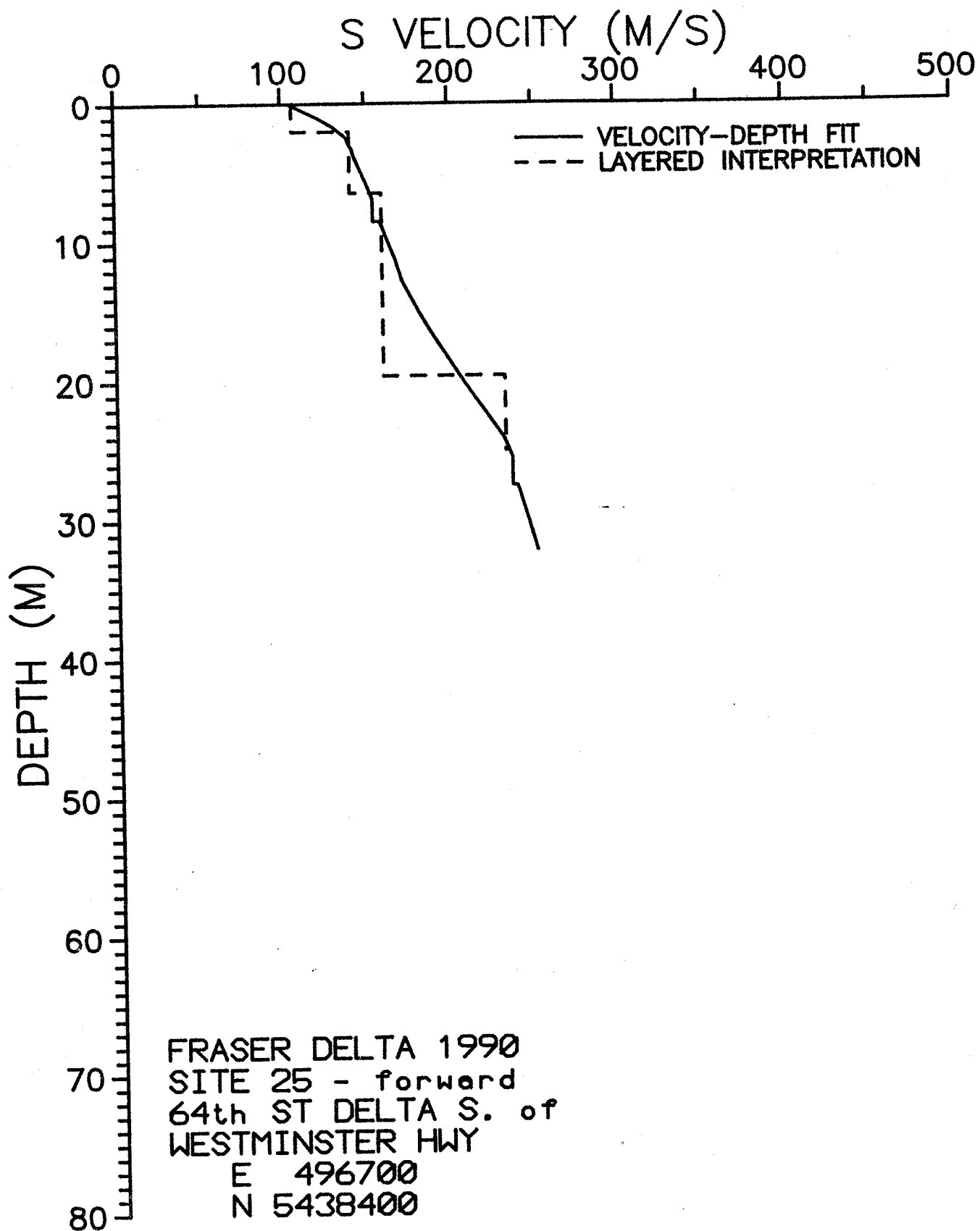


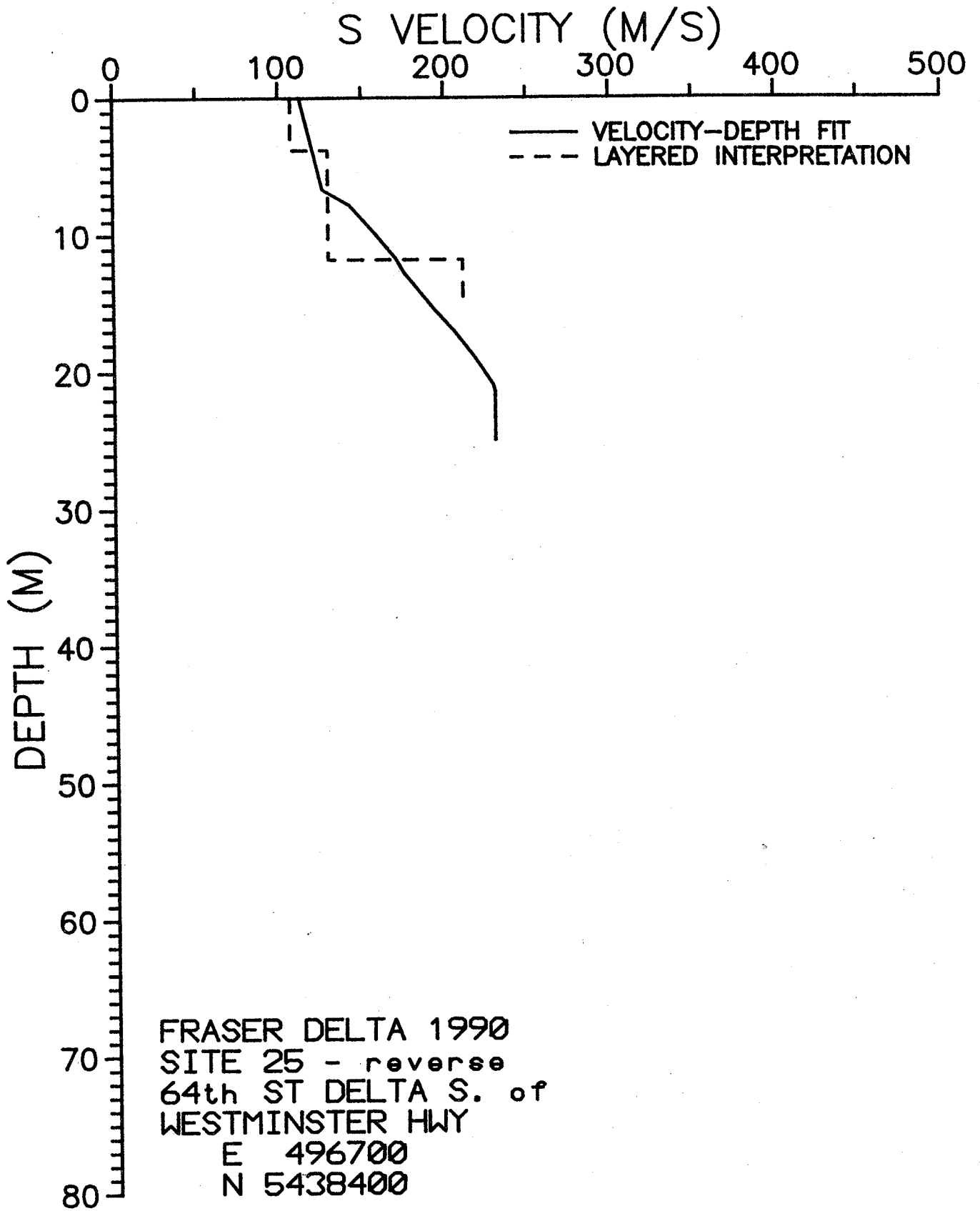


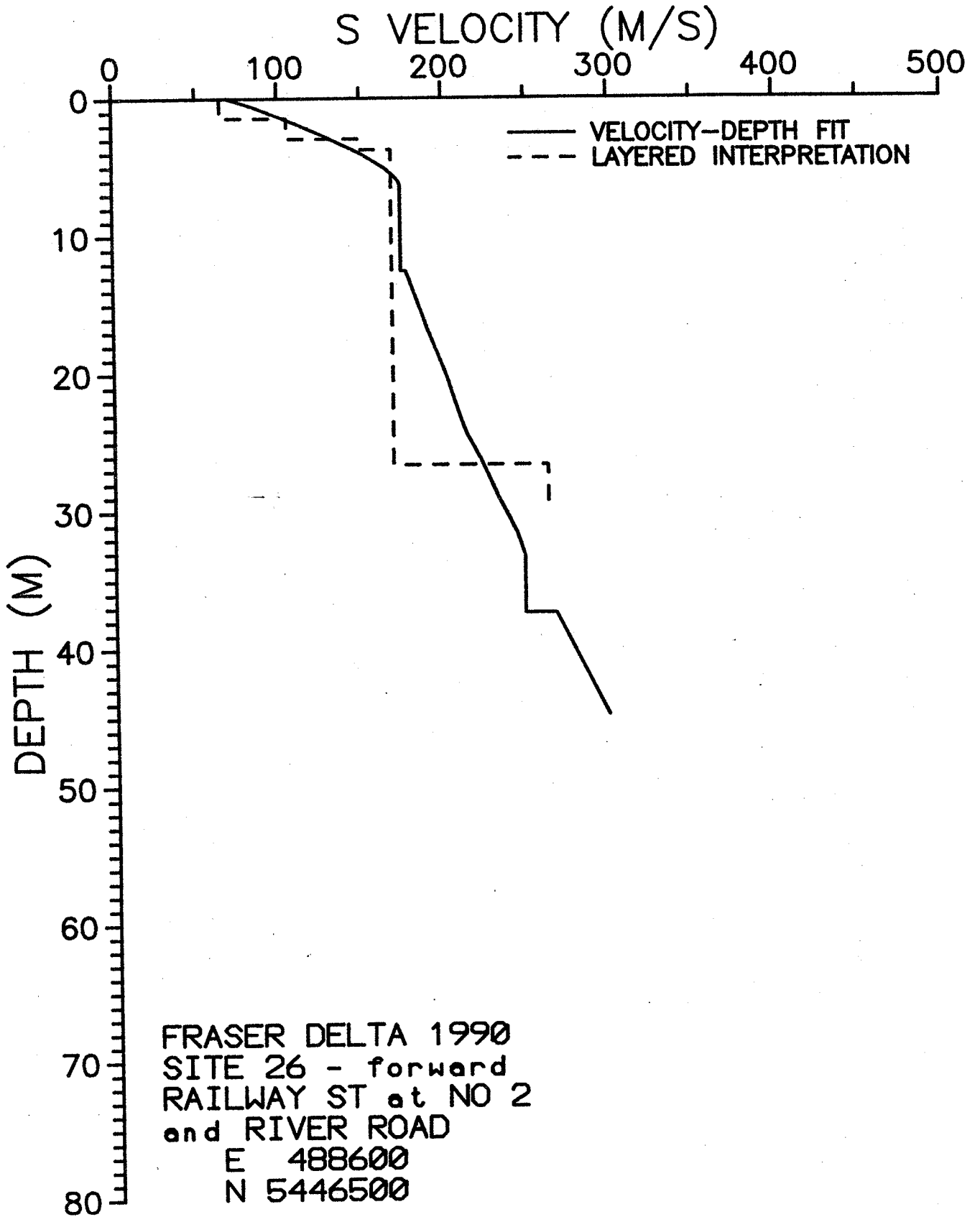


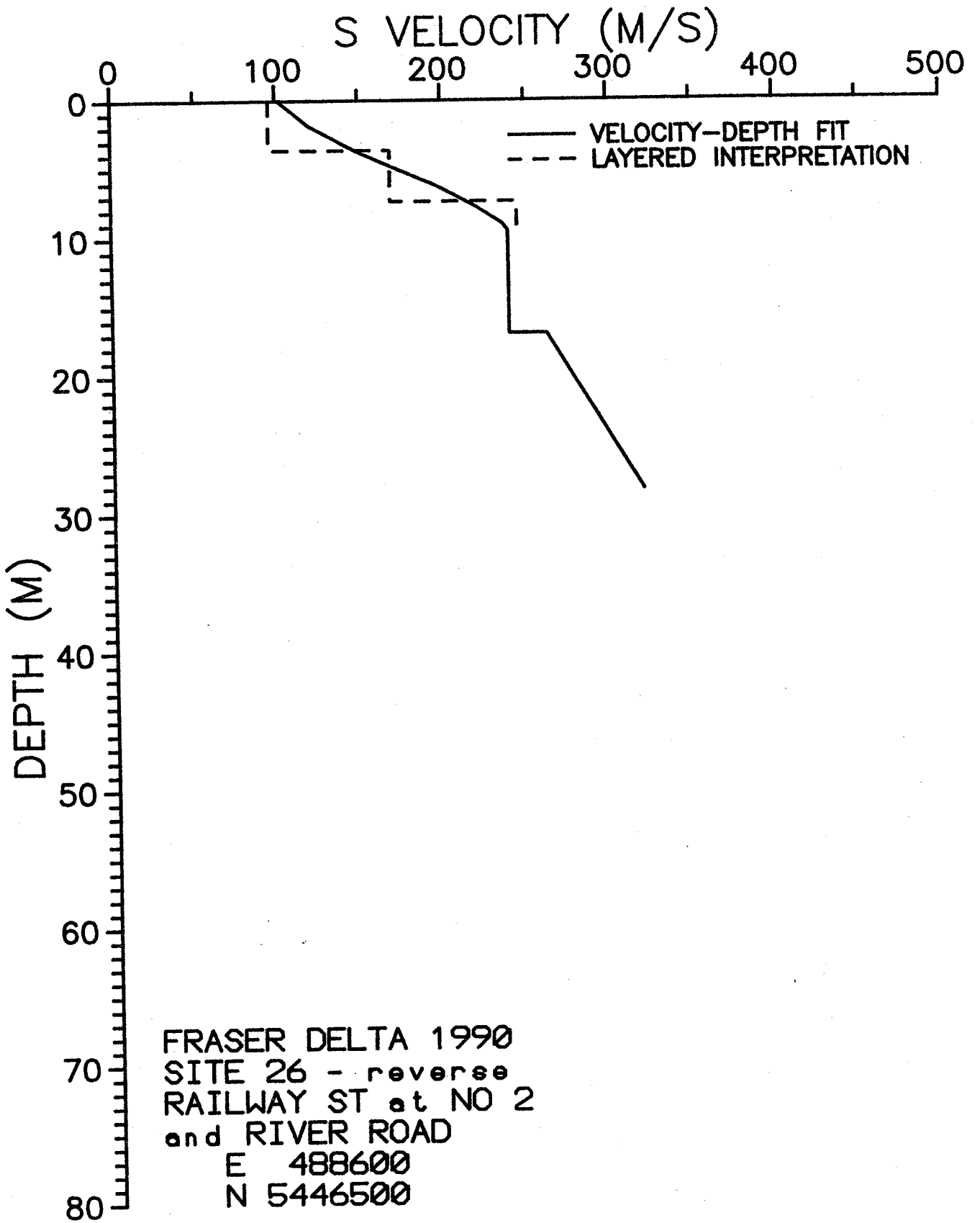


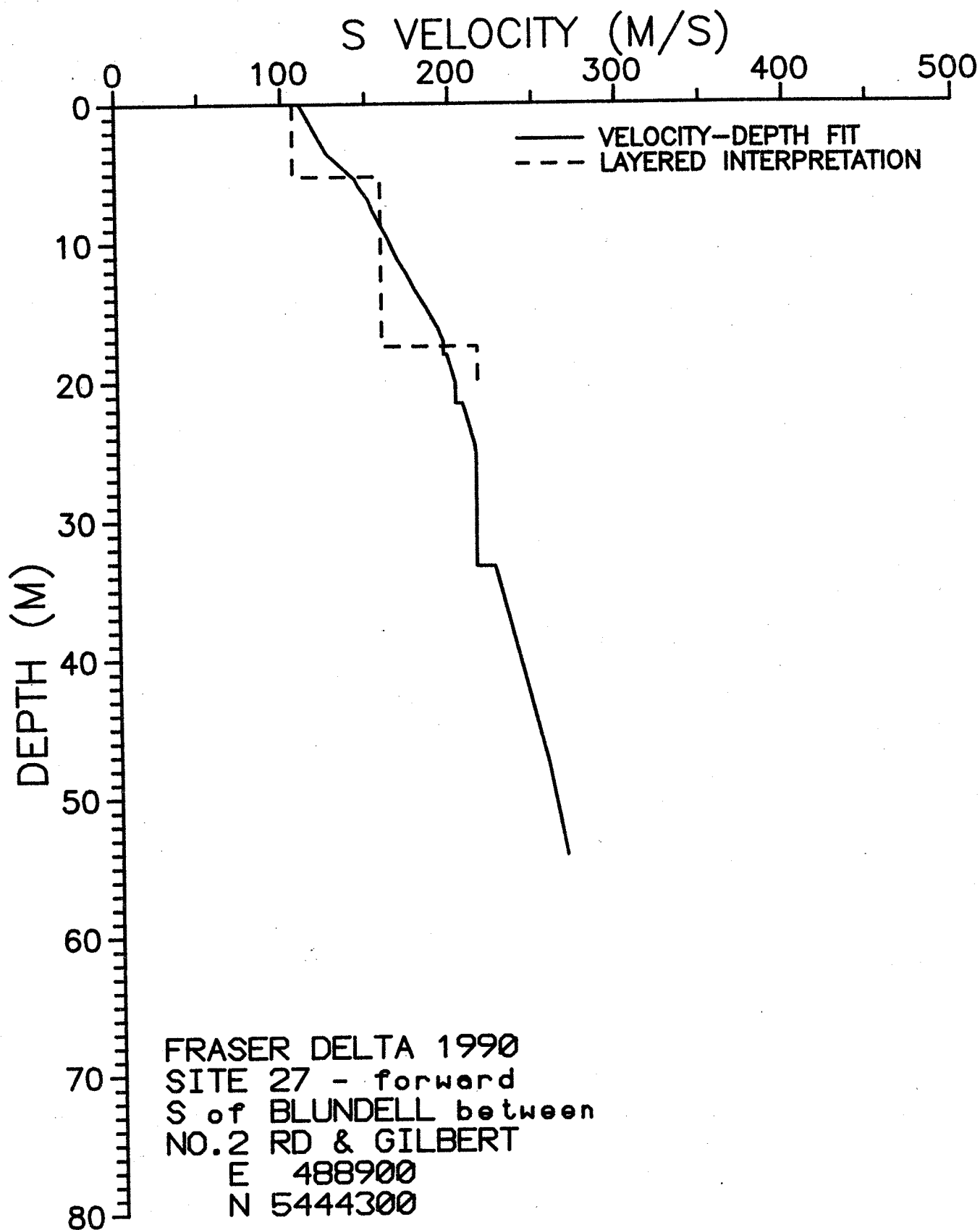


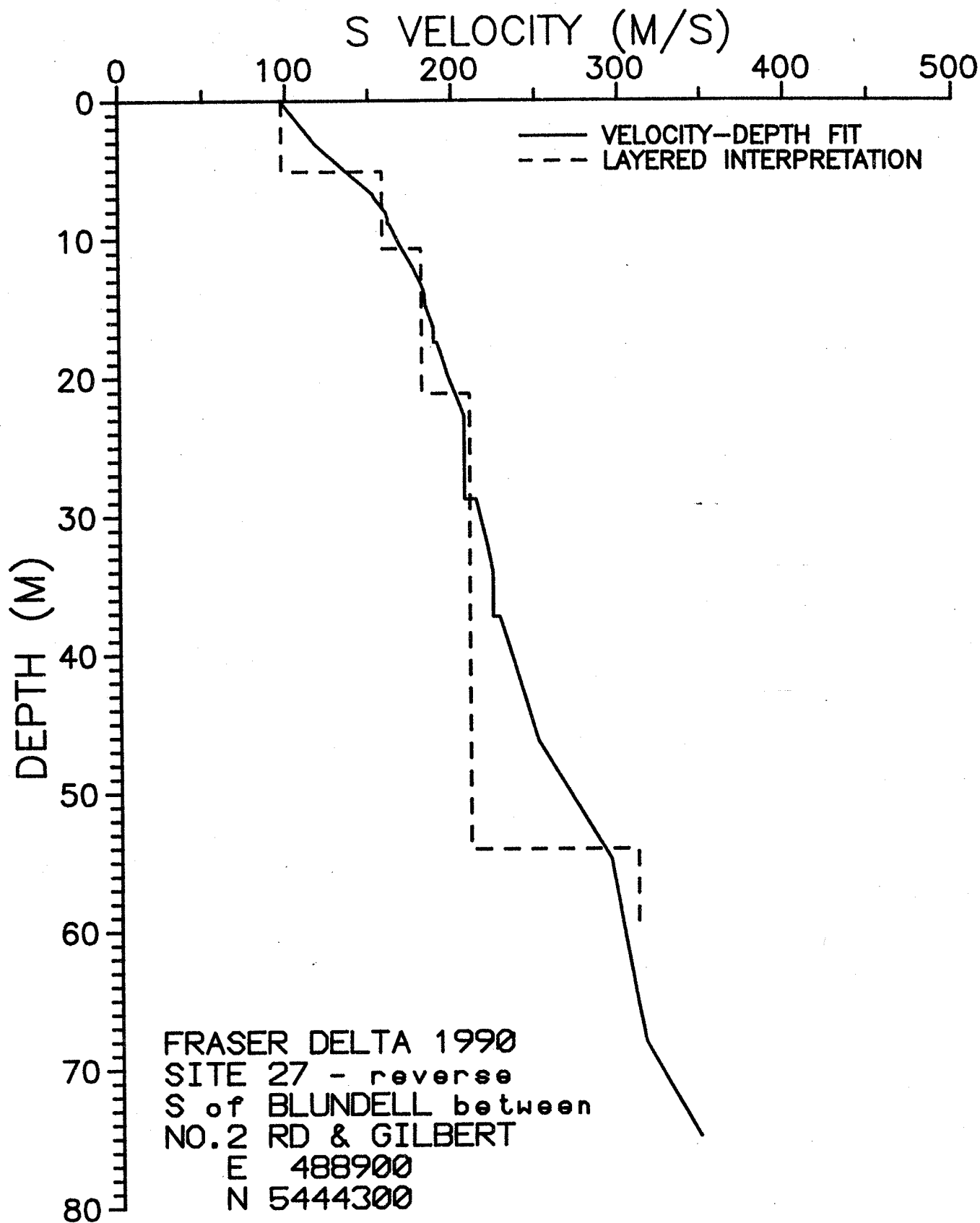


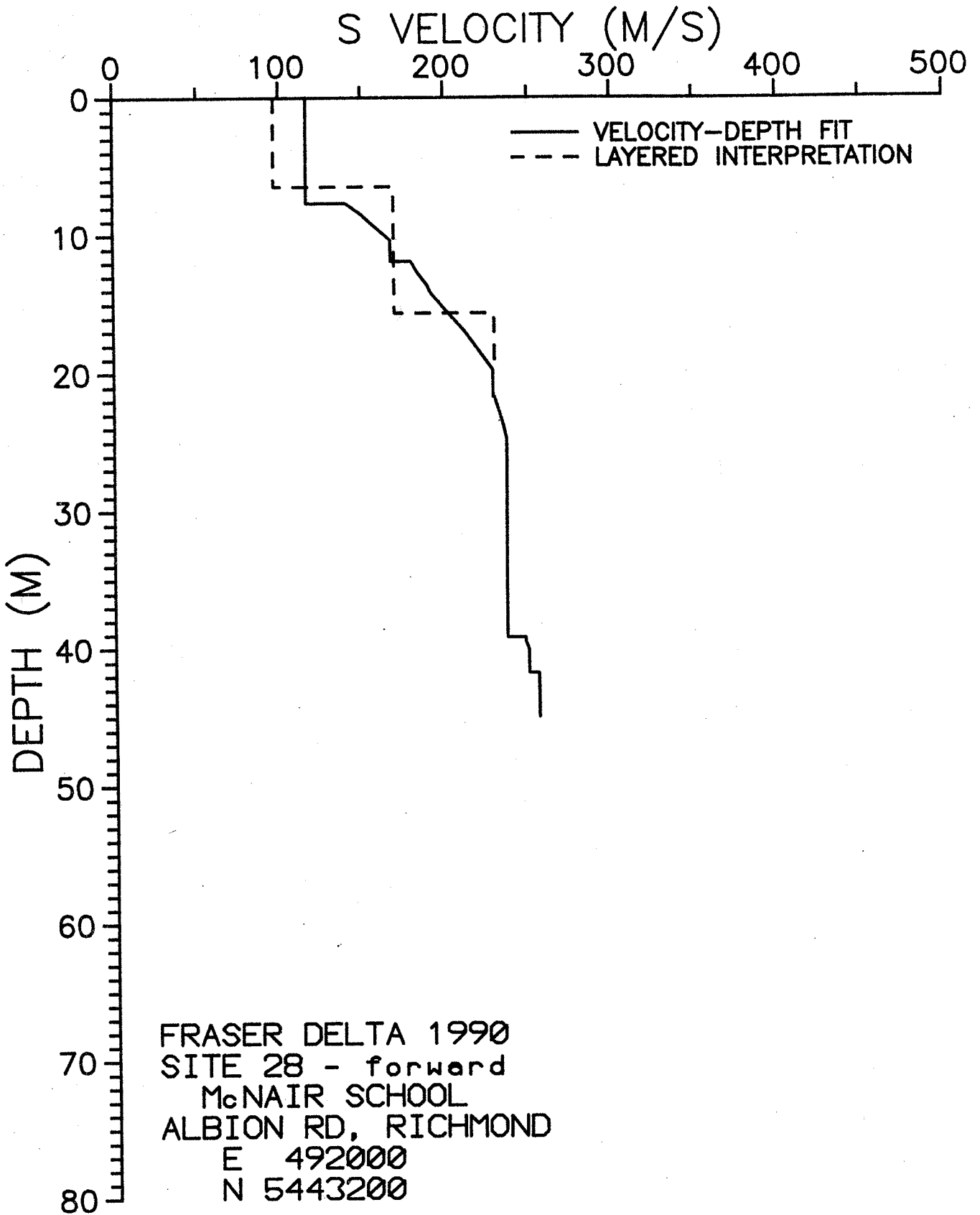


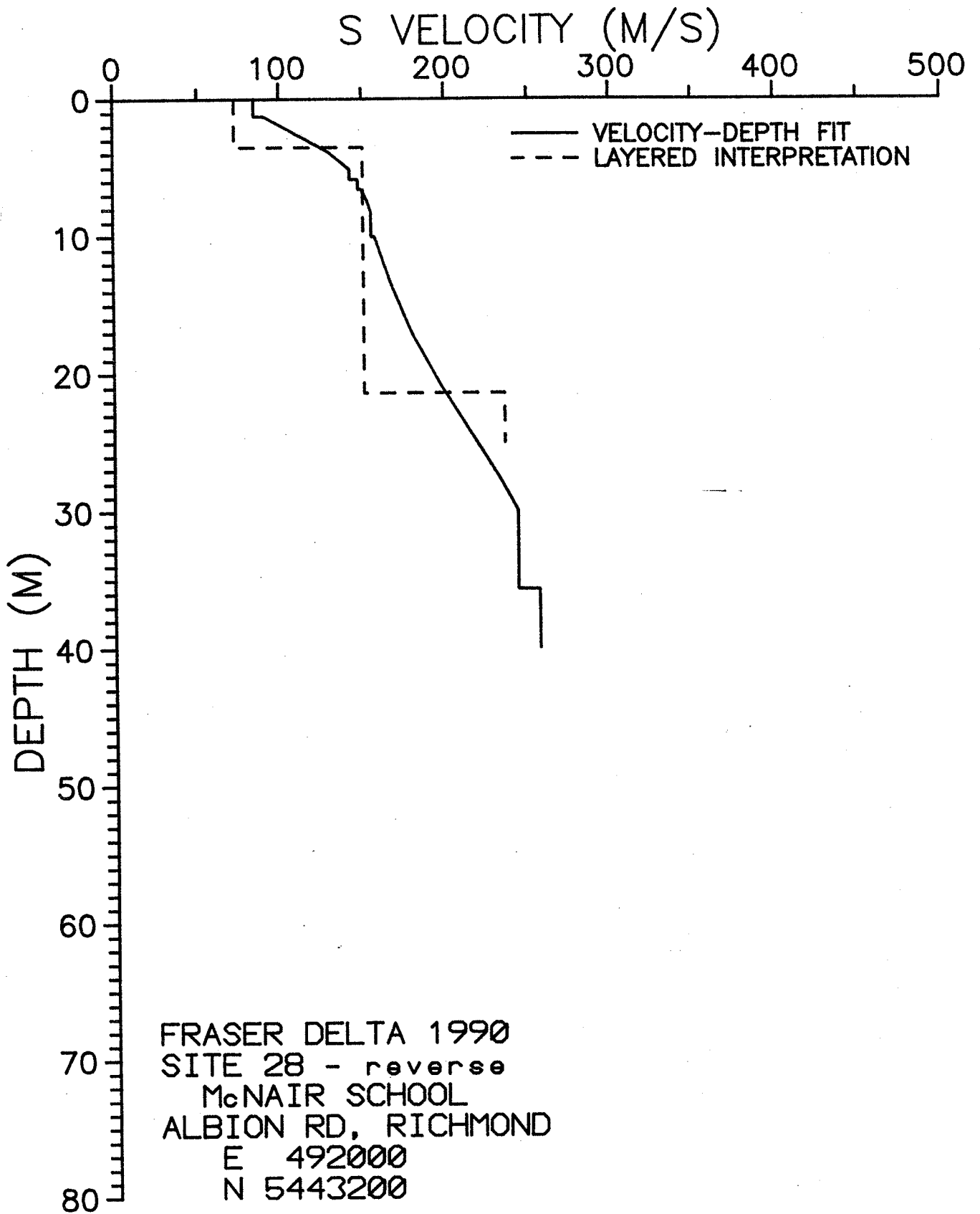


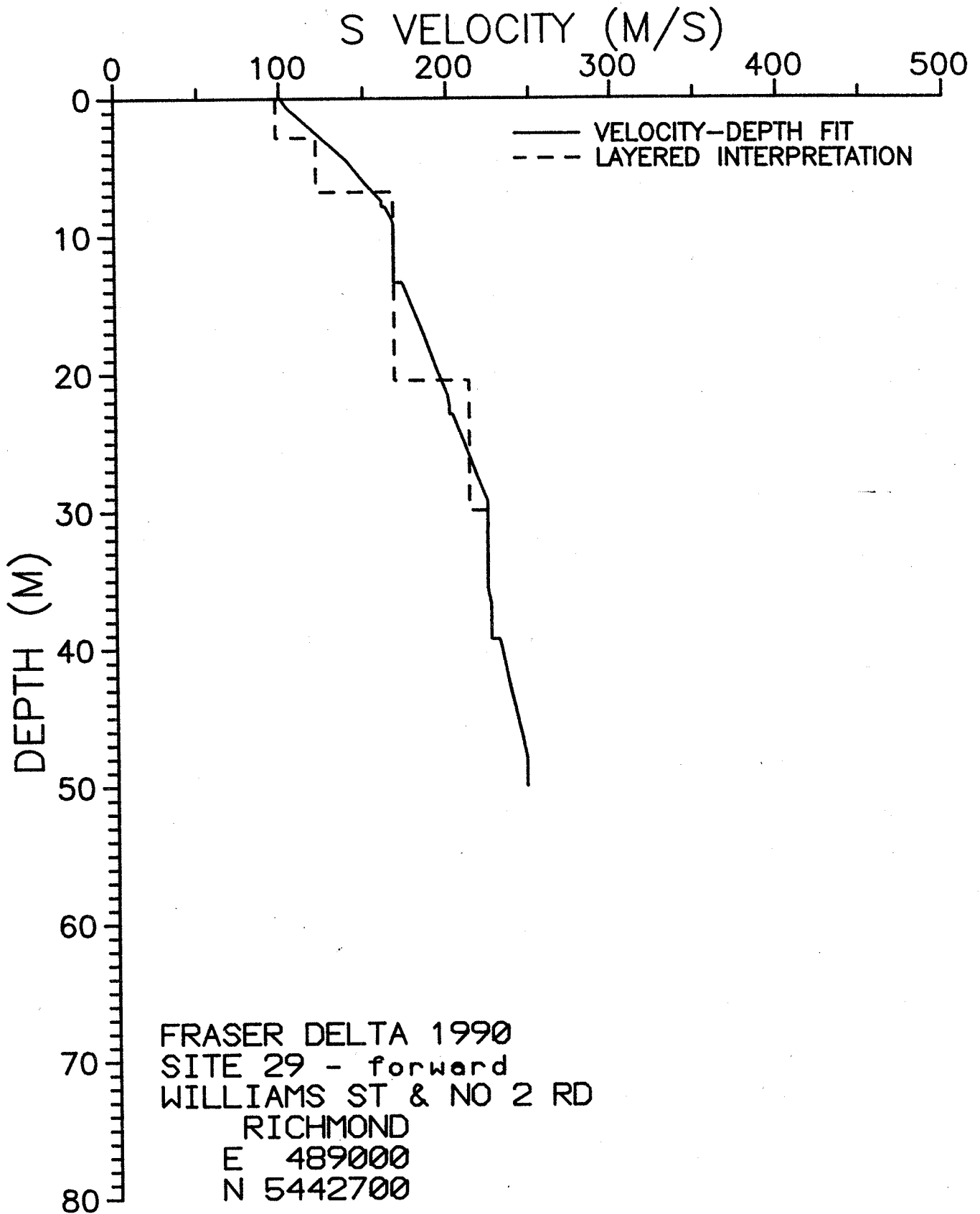


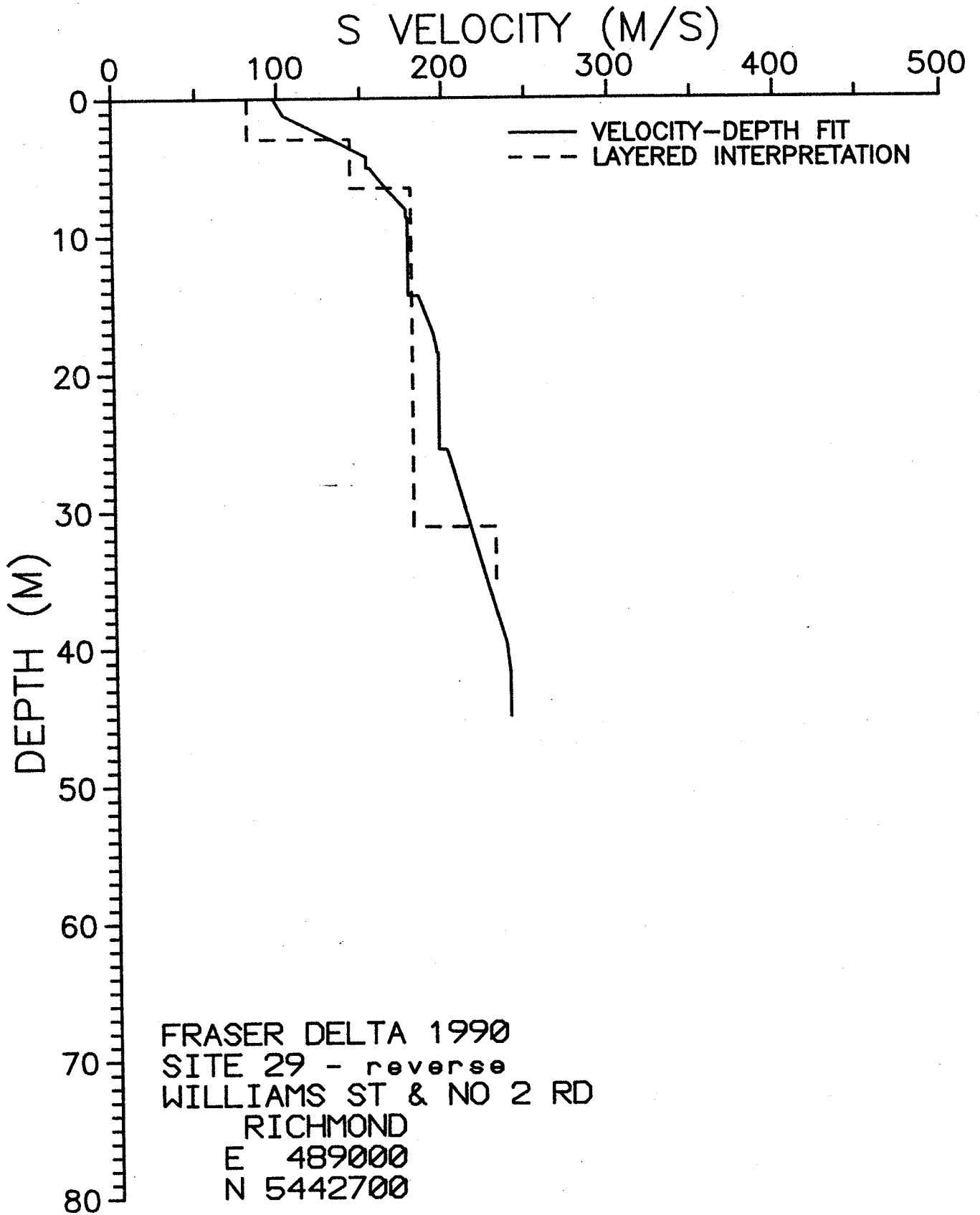


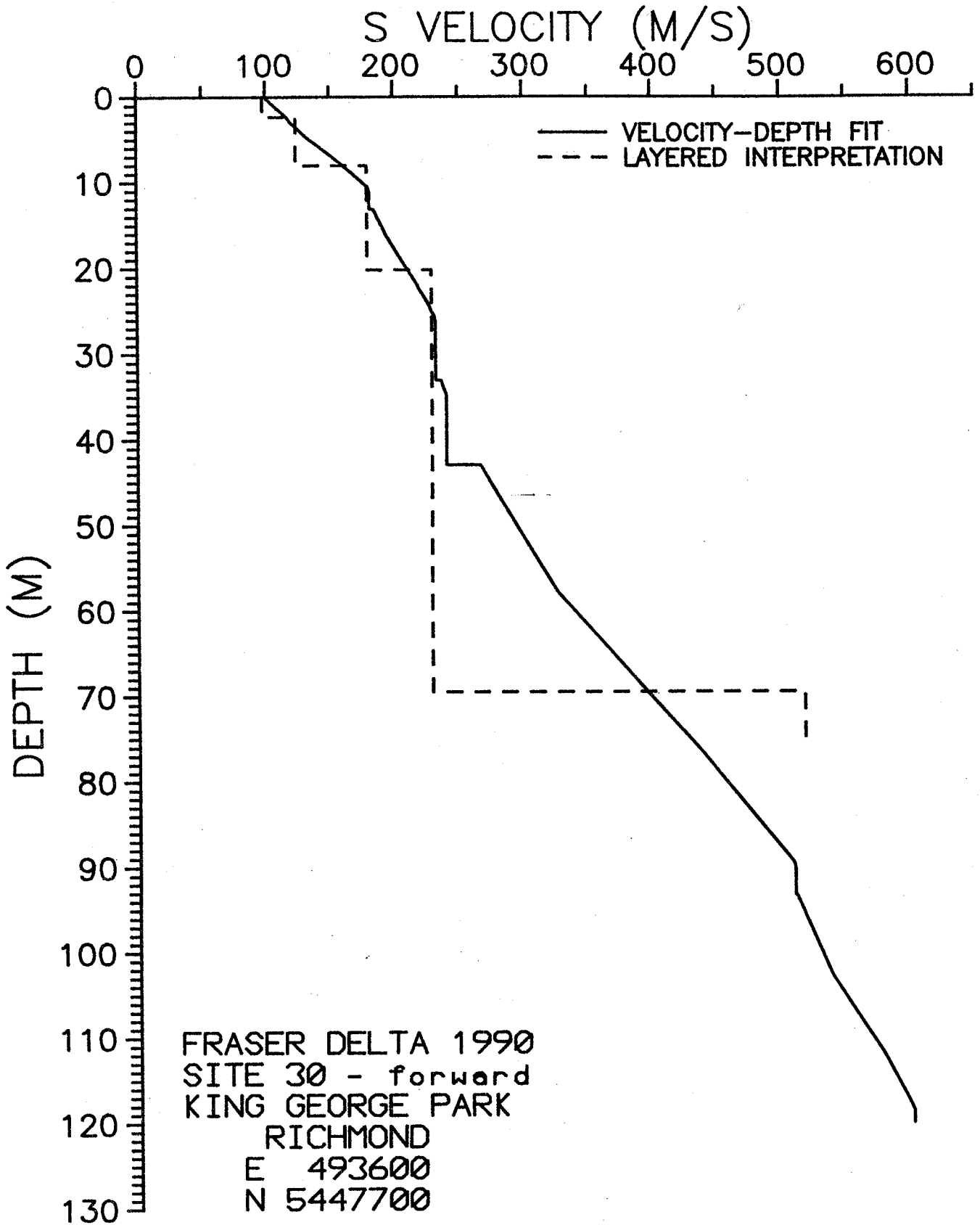


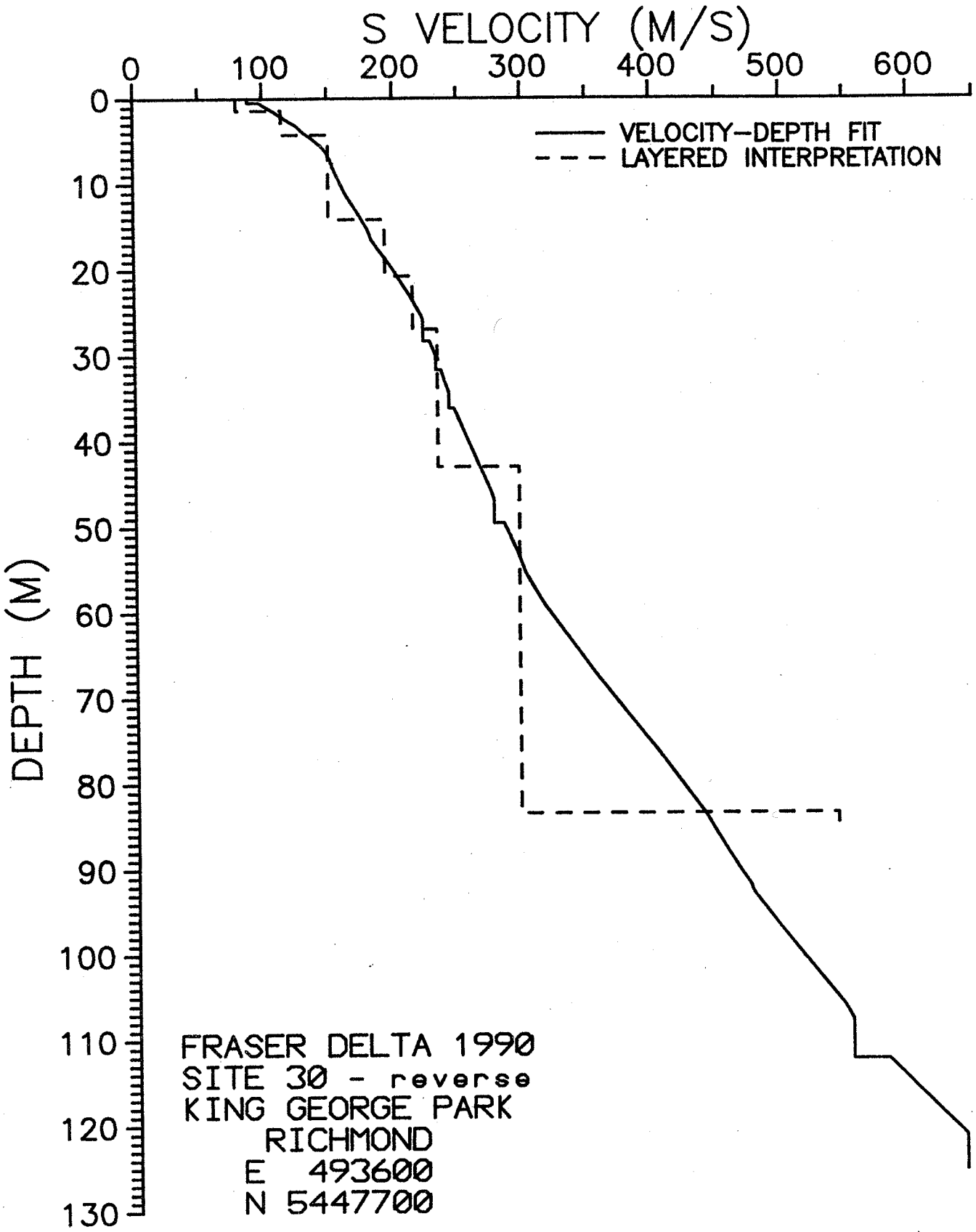


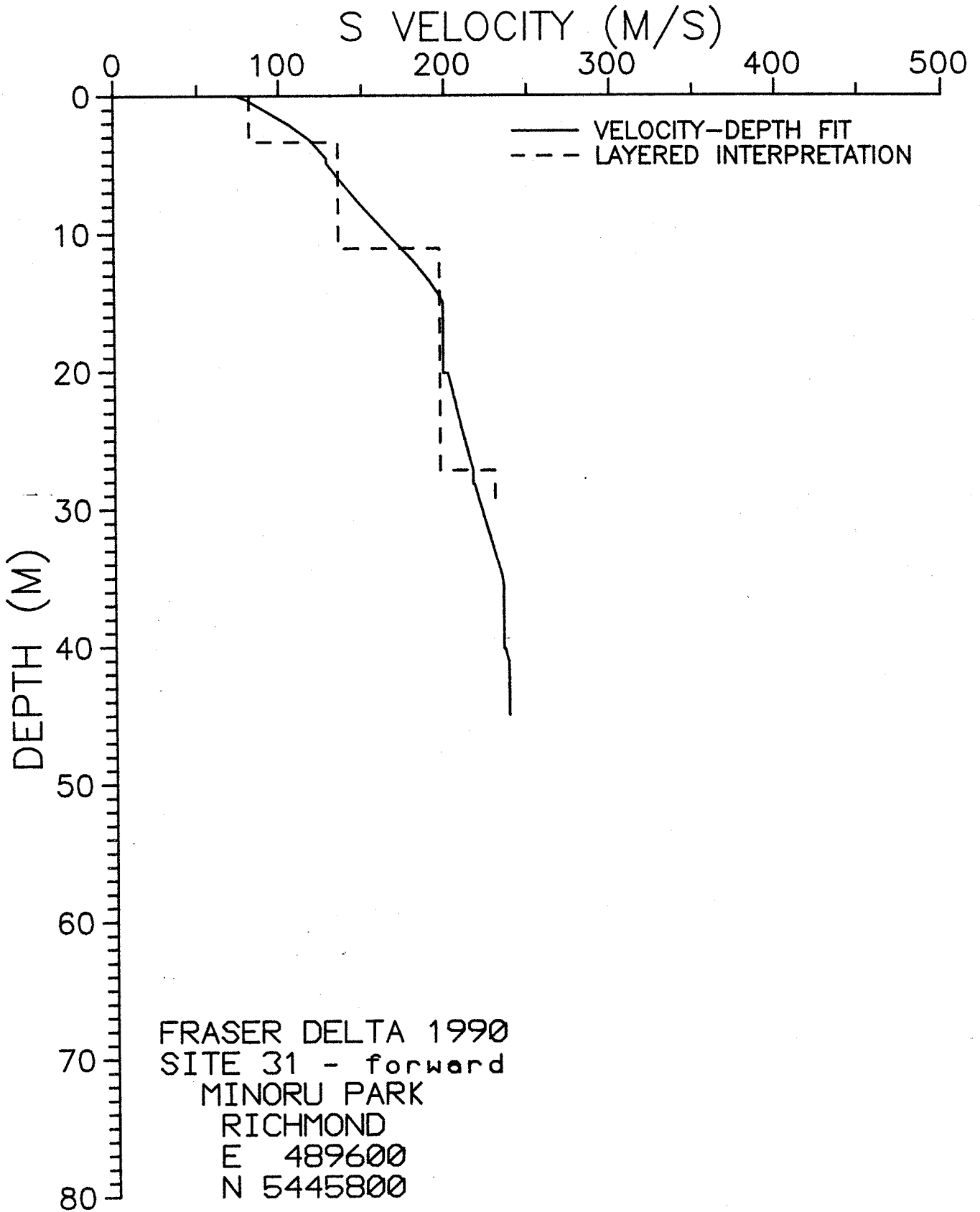


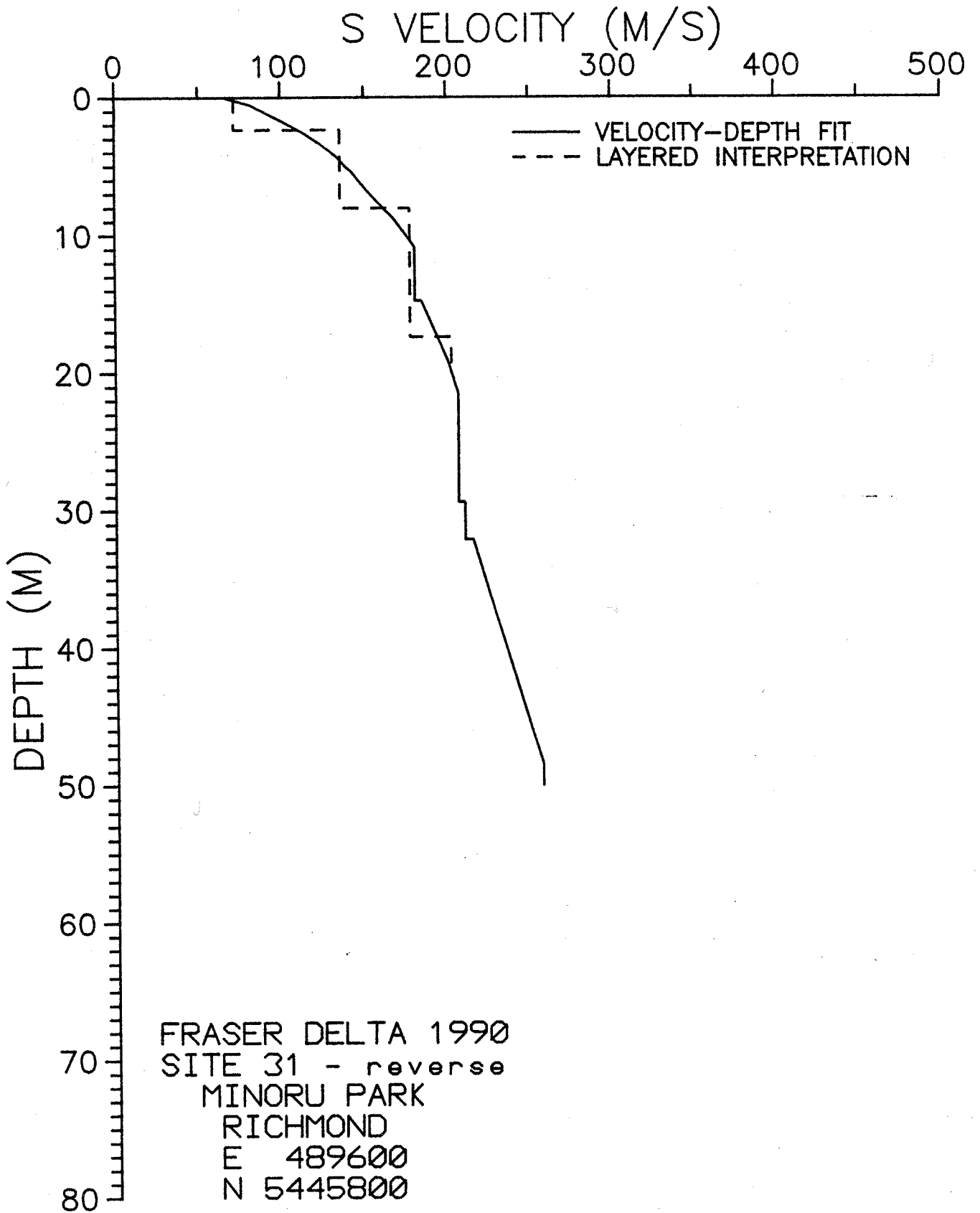


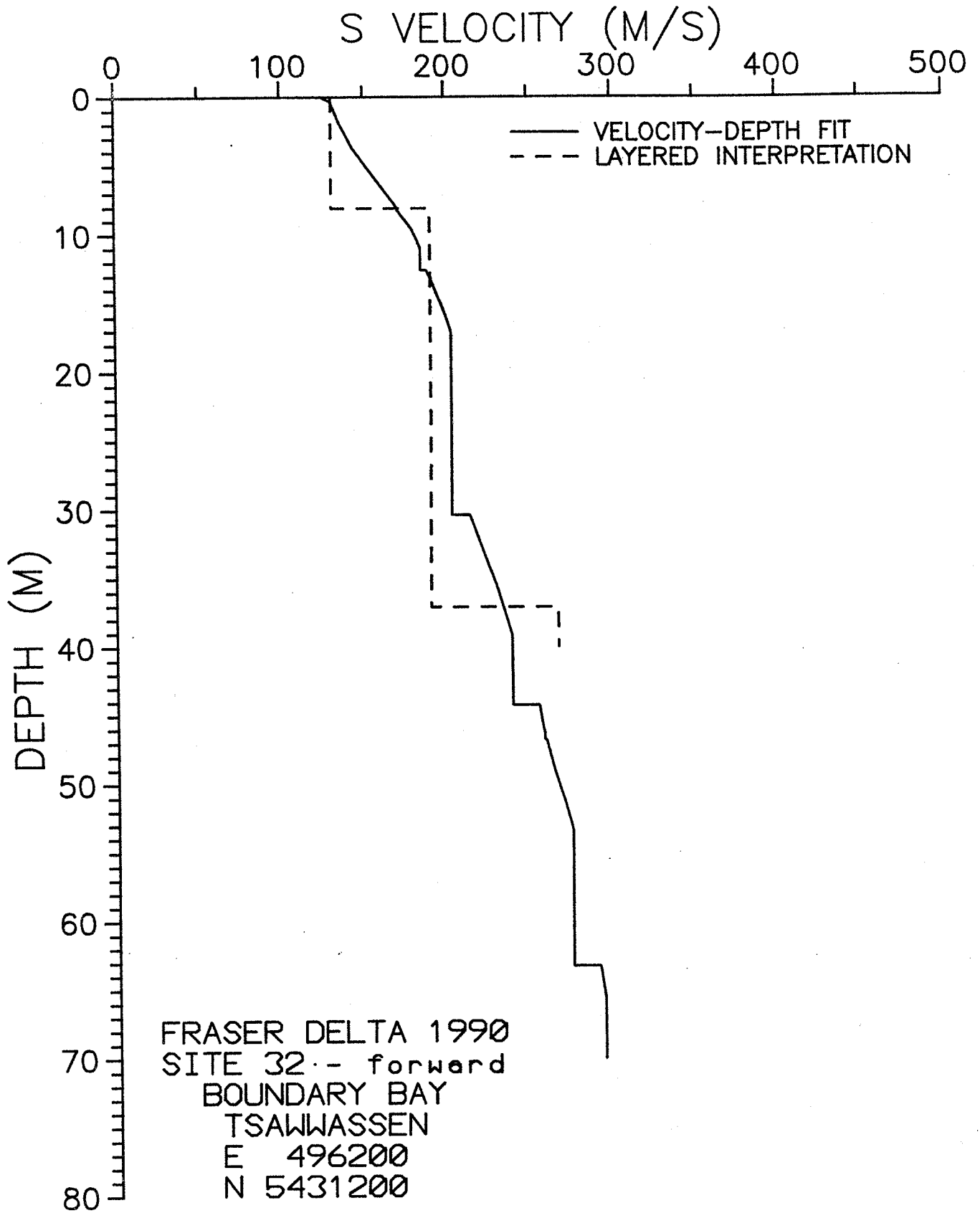


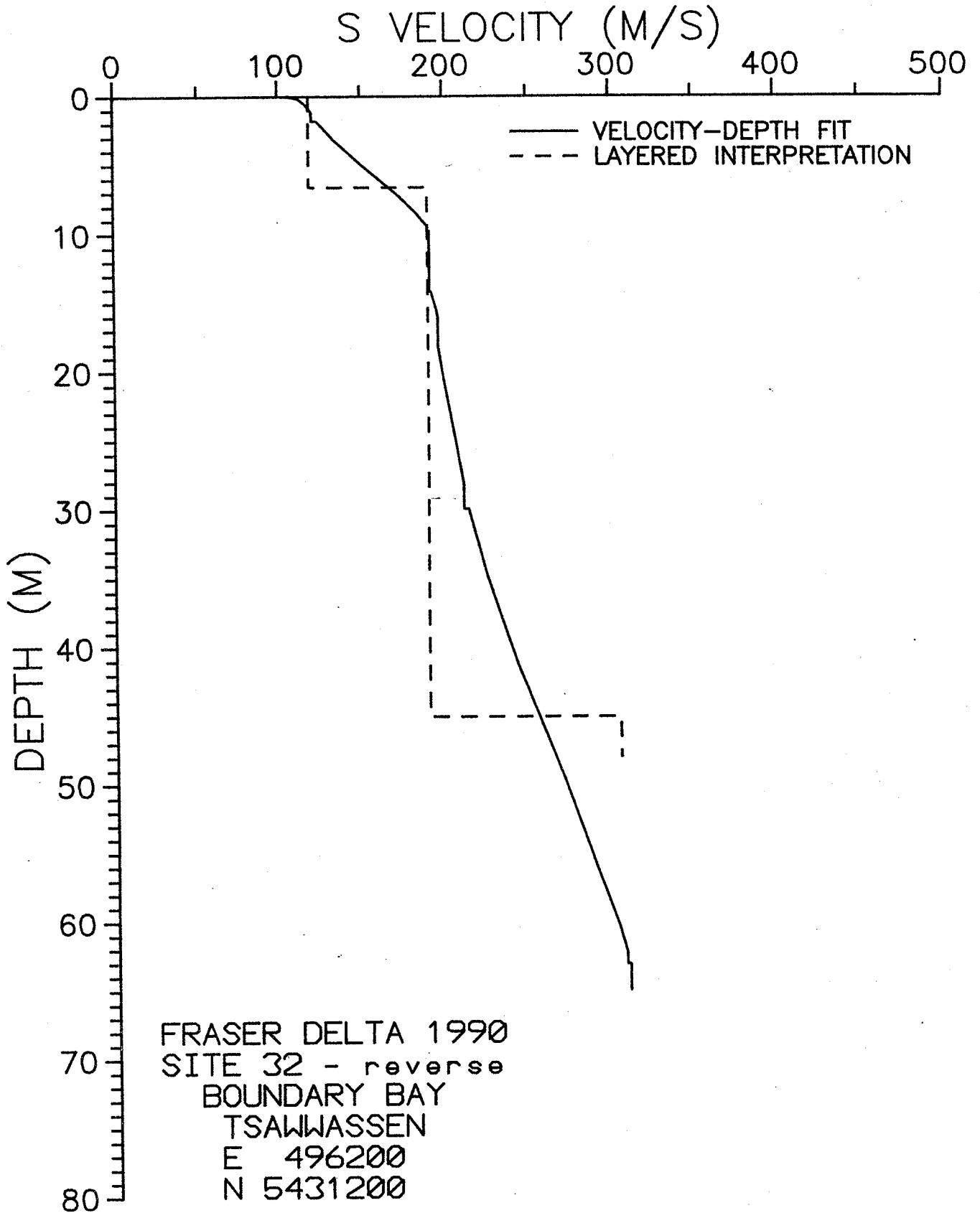




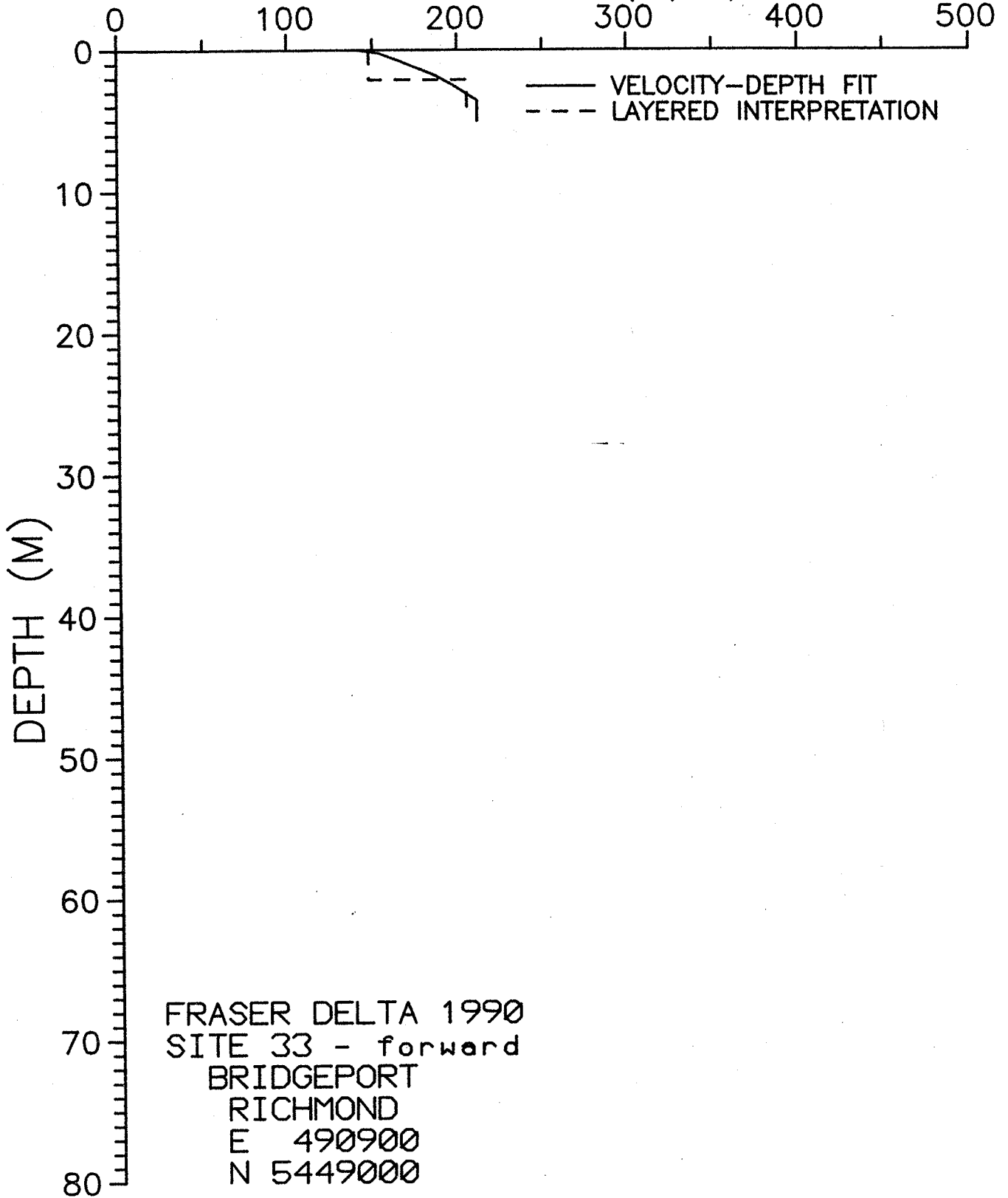


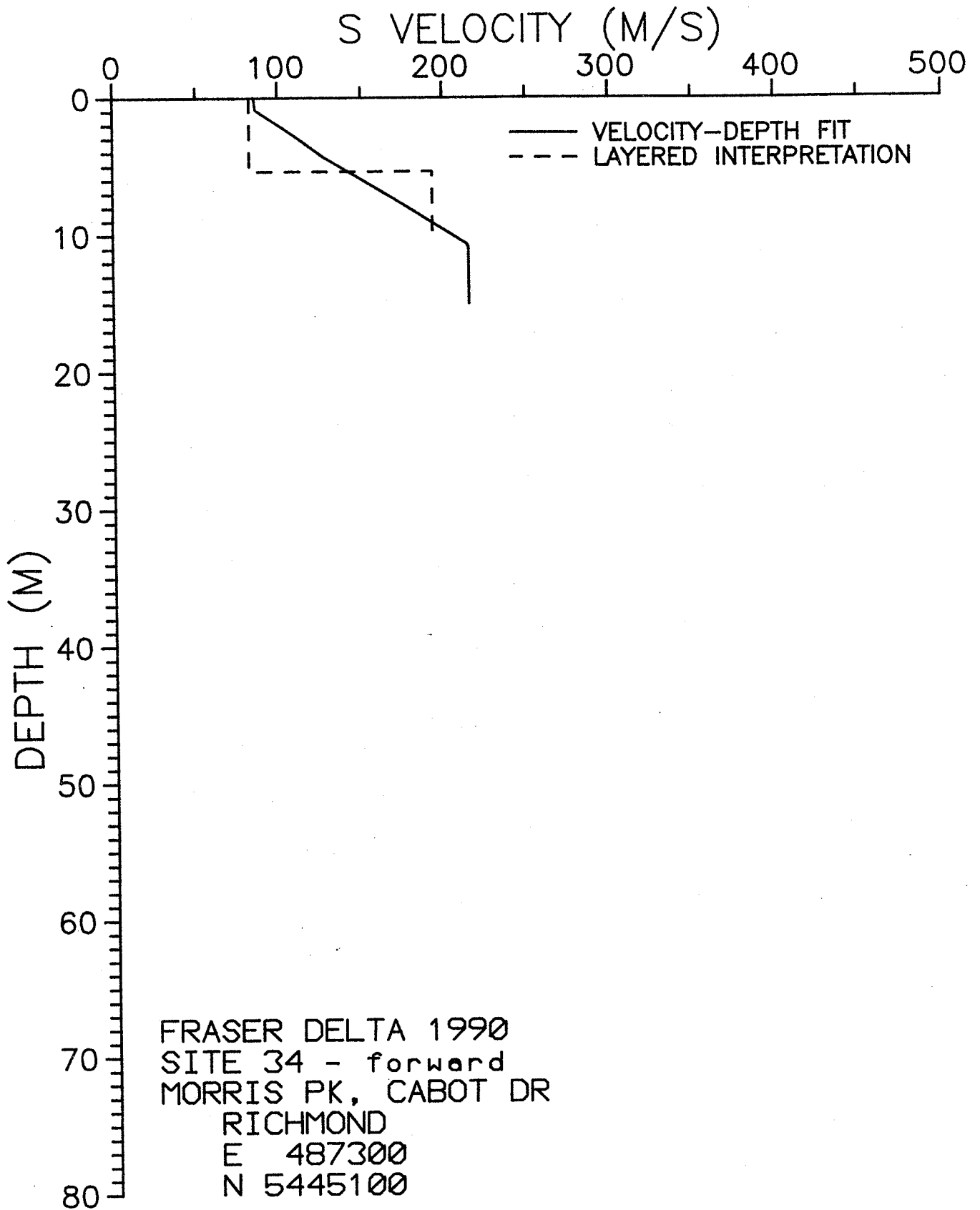


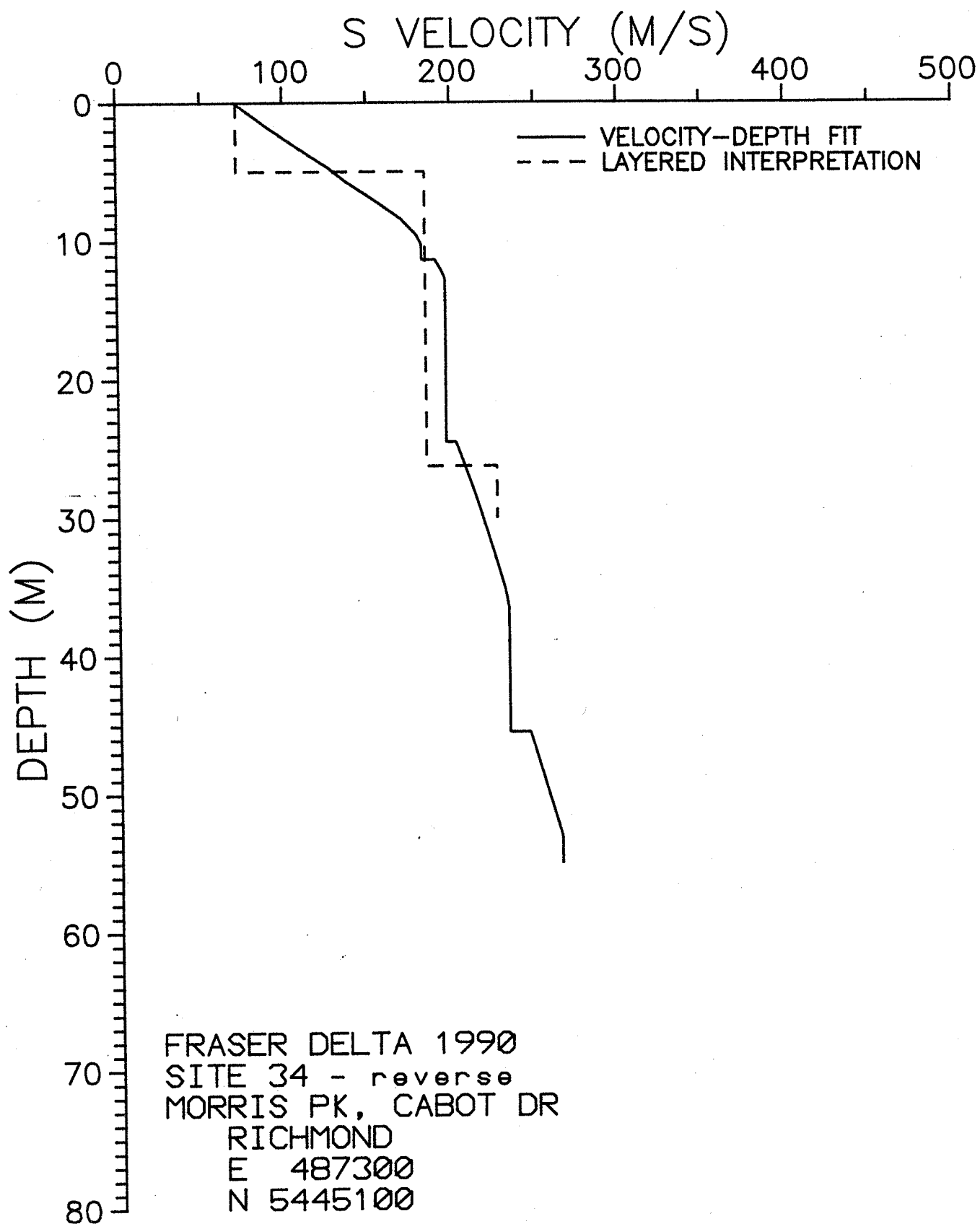


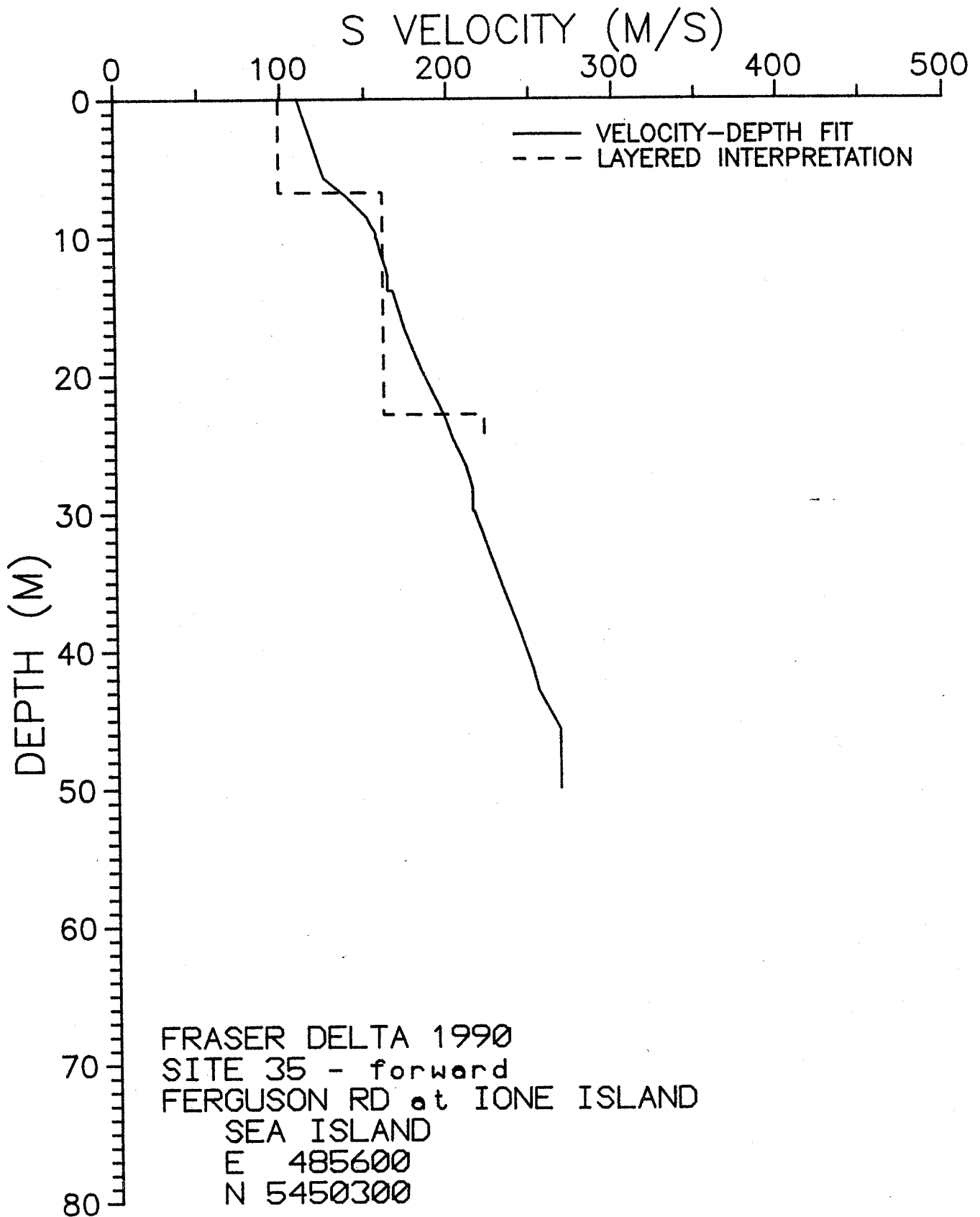


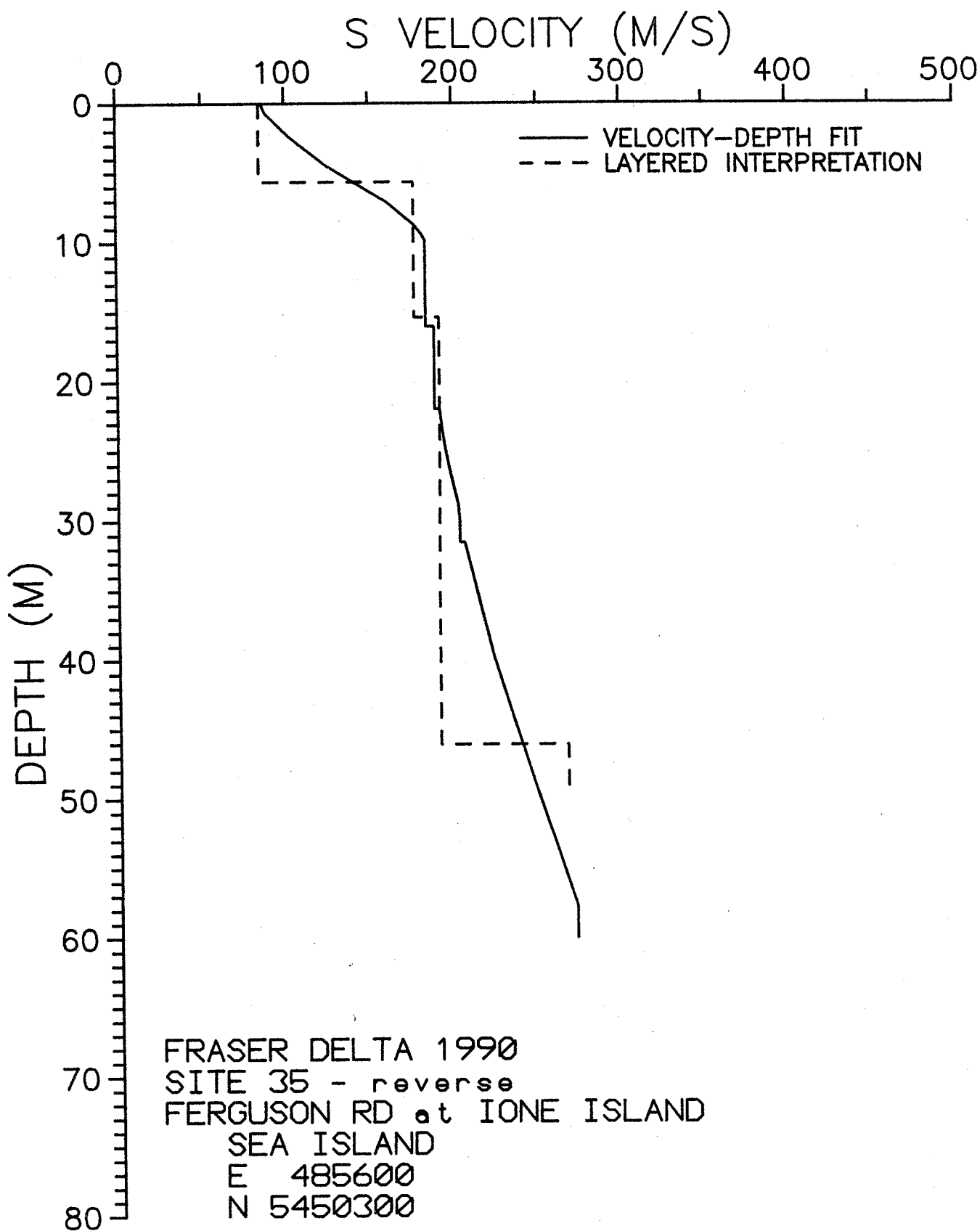
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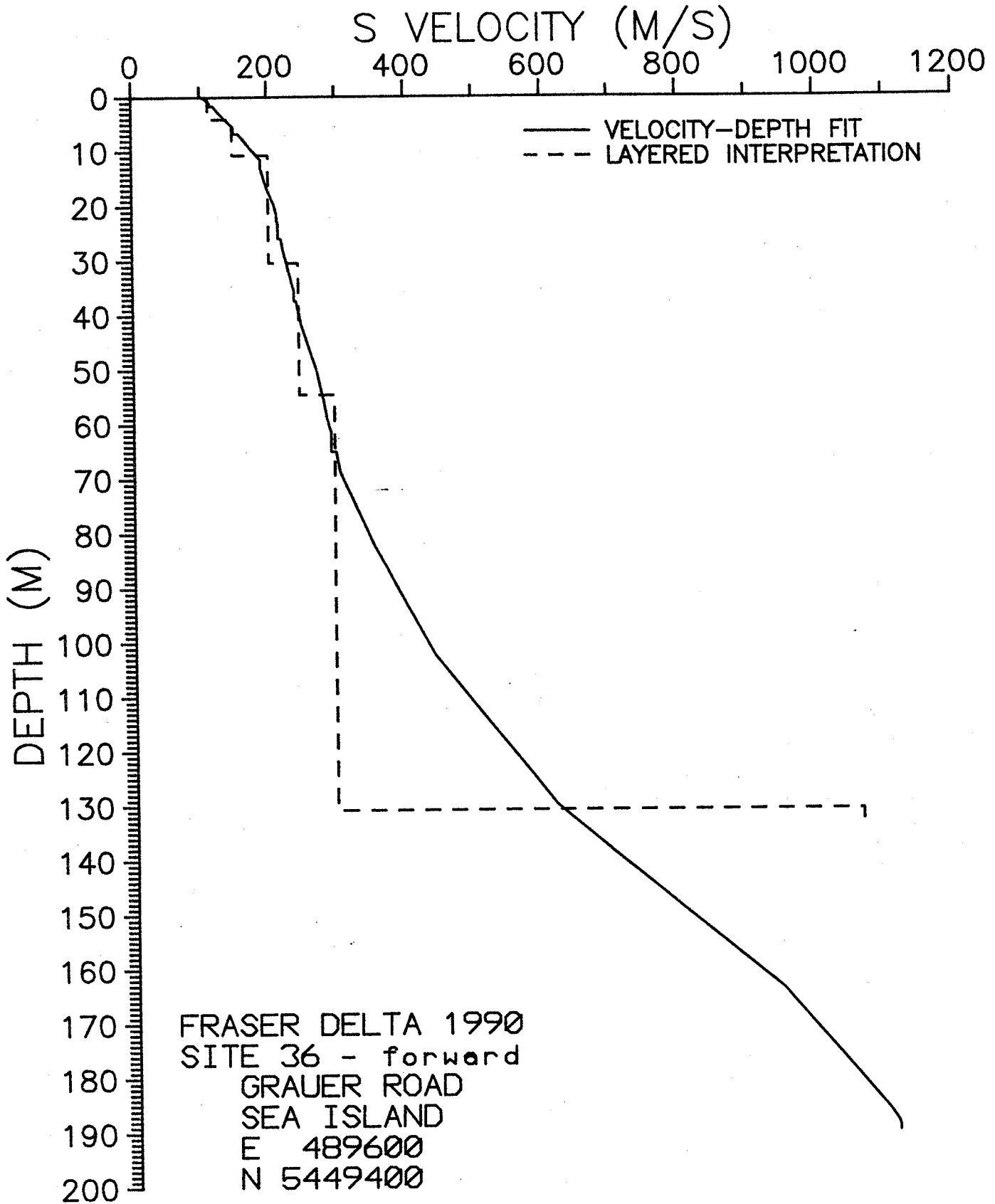


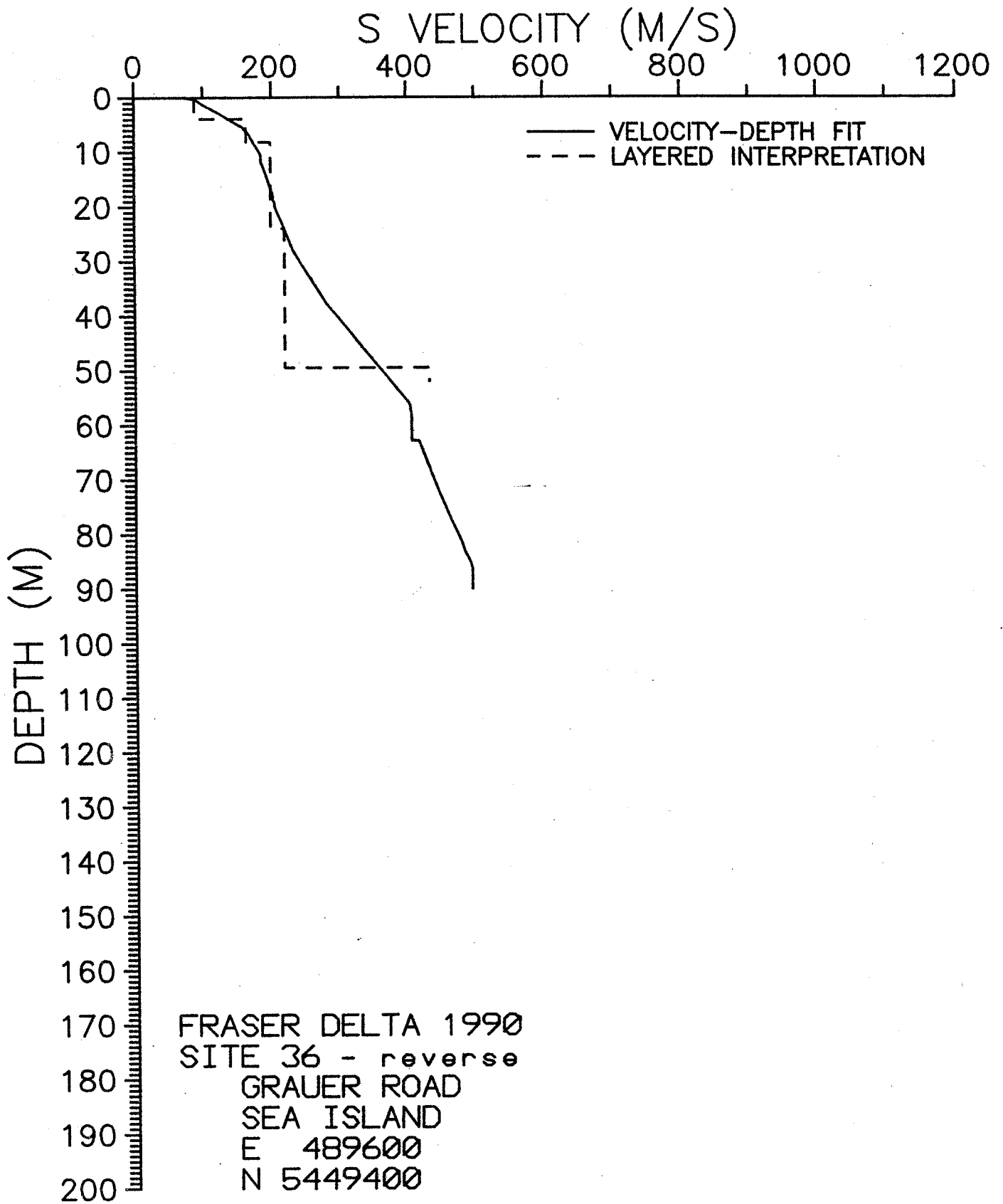


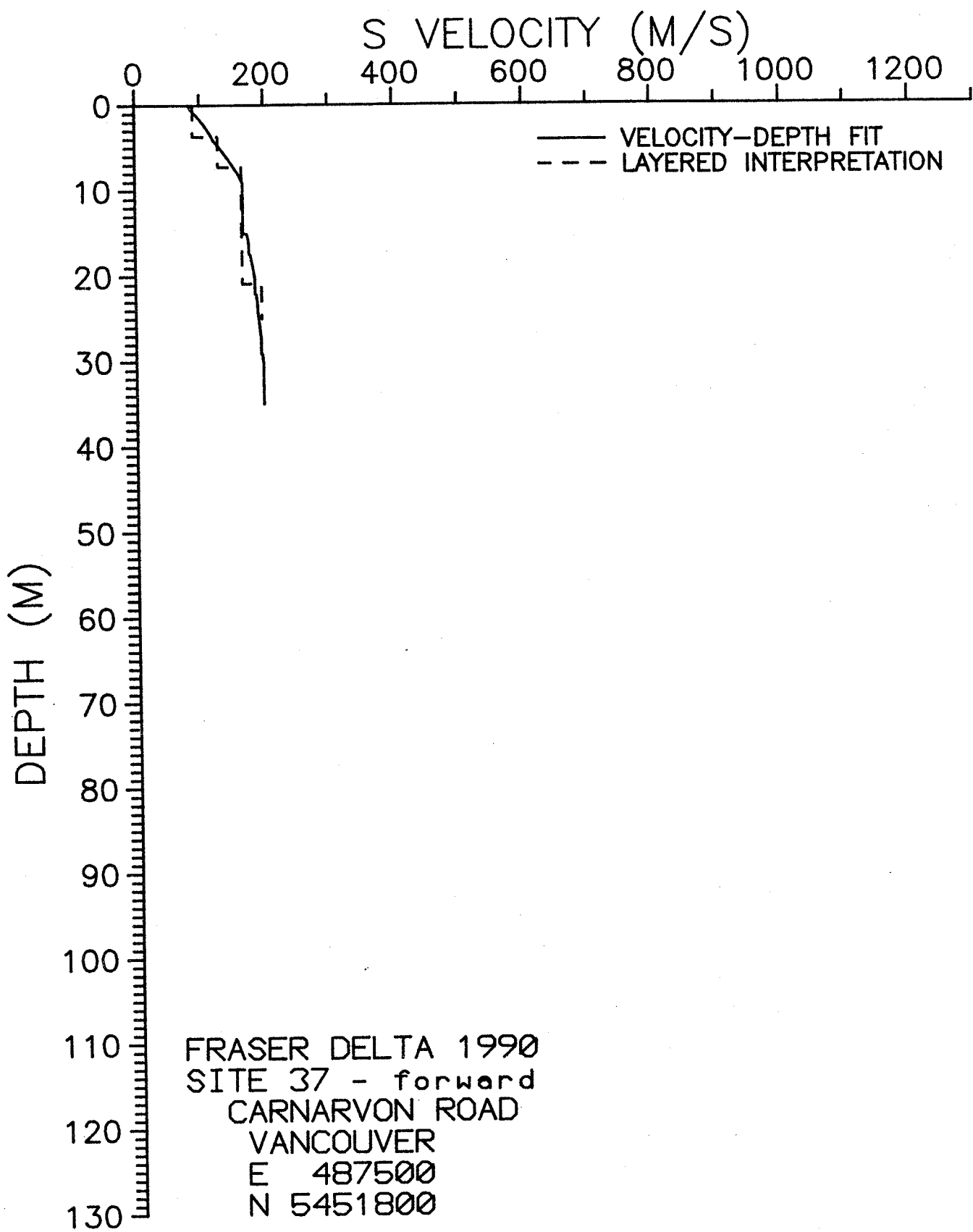












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